

# PRELIMINARY DRAINAGE STUDY



## **NEWLAND SIERRA PDS 2014 MPA-14-018 VOLUME 2 – FEBRUARY 2017**

**Prepared For:** Newland Sierra

**Prepared By:** Kenneth T. Kozlik

**Job Number:** 02660.002.02



# APPENDIX A

AES  
Rational Method Hydrology

Existing Condition

BASIN A



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003,1985,1981 HYDROLOGY MANUAL  
 (c) Copyright 1982-2004 Advanced Engineering Software (aes)  
 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC.  
 6390 GREENWICH DRIVE, SUITE 170  
 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN 1 - NO DETENTION ROUTING \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR01.DAT  
 TIME/DATE OF STUDY: 08:56 09/28/2006

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 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 101.80 IS CODE = 21

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 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 =====

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 1225.00

DOWNSTREAM ELEVATION(FEET) = 1205.00

ELEVATION DIFFERENCE(FEET) = 20.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR01.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.98  
TOTAL AREA(ACRES) = 0.32 TOTAL RUNOFF(CFS) = 0.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.80 TO NODE 101.60 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1205.00 DOWNSTREAM(FEET) = 1135.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.2333  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1744 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.98  
FLOW VELOCITY(FEET/SEC) = 2.34 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.14 Tc(MIN.) = 7.56  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 101.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.80 TO NODE 101.60 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.060  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.16 SUBAREA RUNOFF(CFS) = 5.34  
TOTAL AREA(ACRES) = 2.48 TOTAL RUNOFF(CFS) = 6.13  
TC(MIN.) = 7.56

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.60 TO NODE 101.40 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 1020.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.1917  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1558 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 6.13  
FLOW VELOCITY(FEET/SEC) = 4.04 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.47 Tc(MIN.) = 10.04  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 101.40 = 975.00 FEET.

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FLOW PROCESS FROM NODE 101.60 TO NODE 101.40 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.883  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 7.70 SUBAREA RUNOFF(CFS) = 15.85  
TOTAL AREA(ACRES) = 10.18 TOTAL RUNOFF(CFS) = 20.96  
TC(MIN.) = 10.04

MERR01.TXT

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.40 TO NODE 101.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1020.00 DOWNSTREAM(FEET) = 860.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 740.00 CHANNEL SLOPE = 0.2162
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1681 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 20.96
FLOW VELOCITY(FEET/SEC) = 6.32 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 11.99
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 101.00 = 1715.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.40 TO NODE 101.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.246
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3200
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3378
SUBAREA AREA(ACRES) = 6.99 SUBAREA RUNOFF(CFS) = 11.73
TOTAL AREA(ACRES) = 17.17 TOTAL RUNOFF(CFS) = 30.43
TC(MIN.) = 11.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.00 TO NODE 100.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 860.00 DOWNSTREAM(FEET) = 575.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1640.00 CHANNEL SLOPE = 0.1738
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1469 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 30.43
FLOW VELOCITY(FEET/SEC) = 6.69 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.08 Tc(MIN.) = 16.07
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 100.00 = 3355.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.00 TO NODE 100.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.342
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2786
SUBAREA AREA(ACRES) = 54.70 SUBAREA RUNOFF(CFS) = 61.76
TOTAL AREA(ACRES) = 71.87 TOTAL RUNOFF(CFS) = 86.94
TC(MIN.) = 16.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 1.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

MERR01.TXT

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ELEVATION DATA: UPSTREAM(FEET) = 555.40 DOWNSTREAM(FEET) = 504.80  
FLOW LENGTH(FEET) = 444.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 48.0 INCH PIPE IS 19.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.06  
GIVEN PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 86.94  
PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 16.48  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 1.00 = 3799.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 71.87 TC(MIN.) = 16.48  
PEAK FLOW RATE(CFS) = 86.94

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROGRAPH PROGRAM  
COPYRIGHT 1992, 2001 RICK ENGINEERING COMPANY

RUN DATE 9/28/2006  
HYDROGRAPH FILE NAME Text1  
TIME OF CONCENTRATION 16 MIN.  
6 H RAINFALL 3.5 INCHES  
BA AREA 71.87 ACRES  
RUNOFF COEFFICIENT 0.28  
PEAK DISCHARGE 86.94 CFS

|                  |                         |
|------------------|-------------------------|
| TIME (MIN) = 0   | DISCHARGE (CFS) = 0     |
| TIME (MIN) = 16  | DISCHARGE (CFS) = 4.2   |
| TIME (MIN) = 32  | DISCHARGE (CFS) = 4.4   |
| TIME (MIN) = 48  | DISCHARGE (CFS) = 4.6   |
| TIME (MIN) = 64  | DISCHARGE (CFS) = 4.9   |
| TIME (MIN) = 80  | DISCHARGE (CFS) = 5.1   |
| TIME (MIN) = 96  | DISCHARGE (CFS) = 5.5   |
| TIME (MIN) = 112 | DISCHARGE (CFS) = 5.8   |
| TIME (MIN) = 128 | DISCHARGE (CFS) = 6.4   |
| TIME (MIN) = 144 | DISCHARGE (CFS) = 6.8   |
| TIME (MIN) = 160 | DISCHARGE (CFS) = 7.8   |
| TIME (MIN) = 176 | DISCHARGE (CFS) = 8.5   |
| TIME (MIN) = 192 | DISCHARGE (CFS) = 10.4  |
| TIME (MIN) = 208 | DISCHARGE (CFS) = 11.8  |
| TIME (MIN) = 224 | DISCHARGE (CFS) = 17.4  |
| TIME (MIN) = 240 | DISCHARGE (CFS) = 25.1  |
| TIME (MIN) = 256 | DISCHARGE (CFS) = 86.94 |
| TIME (MIN) = 272 | DISCHARGE (CFS) = 13.9  |
| TIME (MIN) = 288 | DISCHARGE (CFS) = 9.3   |
| TIME (MIN) = 304 | DISCHARGE (CFS) = 7.3   |
| TIME (MIN) = 320 | DISCHARGE (CFS) = 6.1   |
| TIME (MIN) = 336 | DISCHARGE (CFS) = 5.3   |
| TIME (MIN) = 352 | DISCHARGE (CFS) = 4.7   |
| TIME (MIN) = 368 | DISCHARGE (CFS) = 4.3   |
| TIME (MIN) = 384 | DISCHARGE (CFS) = 0     |





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 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 2 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERRO2.DAT  
 TIME/DATE OF STUDY: 16:30 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 202.00 TO NODE 201.50 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 765.00  
 DOWNSTREAM ELEVATION(FEET) = 740.00  
 ELEVATION DIFFERENCE(FEET) = 25.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 -----

MERRO2.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
SUBAREA RUNOFF(CFS) = 0.54  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 0.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.50 TO NODE 201.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 740.00 | DOWNSTREAM(FEET) = | 600.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 300.00 | CHANNEL SLOPE =    | 0.4667 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2217 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.54  
FLOW VELOCITY(FEET/SEC) = 2.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.90 Tc(MIN.) = 8.05  
LONGEST FLOWPATH FROM NODE 202.00 TO NODE 201.00 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.50 TO NODE 201.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.784 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4900  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4754  
SUBAREA AREA(ACRES) = 4.18 SUBAREA RUNOFF(CFS) = 13.90  
TOTAL AREA(ACRES) = 4.45 TOTAL RUNOFF(CFS) = 14.35  
TC(MIN.) = 8.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 200.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 600.00 | DOWNSTREAM(FEET) = | 590.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 280.00 | CHANNEL SLOPE =    | 0.0357 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0357 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 14.35  
FLOW VELOCITY(FEET/SEC) = 2.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.82 Tc(MIN.) = 9.86  
LONGEST FLOWPATH FROM NODE 202.00 TO NODE 200.00 = 655.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 200.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.950 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3461  
SUBAREA AREA(ACRES) = 8.71 SUBAREA RUNOFF(CFS) = 14.51  
TOTAL AREA(ACRES) = 13.16 TOTAL RUNOFF(CFS) = 27.10  
TC(MIN.) = 9.86

MERRO2. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 200.00 TO NODE 2.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 574.40            | DOWNSTREAM(FEET) = | 515.40        |
| FLOW LENGTH(FEET) =              | 480.00            | MANNING'S N =      | 0.024         |
| DEPTH OF FLOW IN                 | 30.0 INCH PIPE IS | 12.6 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 13.89             |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 30.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 27.10             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.58              | Tc(MIN.) =         | 10.44         |
| LONGEST FLOWPATH FROM NODE       | 202.00 TO NODE    | 2.00 =             | 1135.00 FEET. |

=====

END OF STUDY SUMMARY:

|                     |   |       |            |       |
|---------------------|---|-------|------------|-------|
| TOTAL AREA(ACRES)   | = | 13.16 | TC(MIN.) = | 10.44 |
| PEAK FLOW RATE(CFS) | = | 27.10 |            |       |

=====

END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
 6390 GREENWICH DRIVE, SUITE 170  
 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 3 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERRO3.DAT  
 TIME/DATE OF STUDY: 11:18 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 350.20 TO NODE 350.10 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 -----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 55.00  
 UPSTREAM ELEVATION(FEET) = 1385.00  
 DOWNSTREAM ELEVATION(FEET) = 1373.00  
 ELEVATION DIFFERENCE(FEET) = 12.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.647

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERRO3. TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.16  
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 350.10 TO NODE 350.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1373.00 DOWNSTREAM(FEET) = 888.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1718.10 CHANNEL SLOPE = 0.2823  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1906 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.16  
FLOW VELOCITY(FEET/SEC) = 2.44 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 11.71 Tc(MIN.) = 16.36  
LONGEST FLOWPATH FROM NODE 350.20 TO NODE 350.00 = 1773.10 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 350.00 TO NODE 350.00 IS CODE = 81

>>>>ADDIT ION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.293  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2700  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2702  
SUBAREA AREA(ACRES) = 19.21 SUBAREA RUNOFF(CFS) = 22.27  
TOTAL AREA(ACRES) = 19.26 TOTAL RUNOFF(CFS) = 22.34  
TC(MIN.) = 16.36

\*\*\*\*\*  
FLOW PROCESS FROM NODE 350.00 TO NODE 350.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.36  
RAINFALL INTENSITY(INCH/HR) = 4.29  
TOTAL STREAM AREA(ACRES) = 19.26  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 22.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 351.40 TO NODE 351.30 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1585.00  
DOWNSTREAM ELEVATION(FEET) = 1538.00  
ELEVATION DIFFERENCE(FEET) = 47.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.778  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.401  
SUBAREA RUNOFF(CFS) = 0.24

TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*
FLOW PROCESS FROM NODE 351.30 TO NODE 351.20 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1538.00 DOWNSTREAM(FEET) = 1190.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1021.00 CHANNEL SLOPE = 0.3408
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .2036 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.24
FLOW VELOCITY(FEET/SEC) = 2.53 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 6.73 Tc(MIN.) = 12.51
LONGEST FLOWPATH FROM NODE 351.40 TO NODE 351.20 = 1106.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 351.20 TO NODE 351.20 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.104
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 8.07 SUBAREA RUNOFF(CFS) = 14.42
TOTAL AREA(ACRES) = 8.15 TOTAL RUNOFF(CFS) = 14.56
TC(MIN.) = 12.51

\*\*\*\*\*
FLOW PROCESS FROM NODE 351.20 TO NODE 351.10 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1190.00 DOWNSTREAM(FEET) = 1005.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 817.00 CHANNEL SLOPE = 0.2264
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1721 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 14.56
FLOW VELOCITY(FEET/SEC) = 5.67 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.40 Tc(MIN.) = 14.91
LONGEST FLOWPATH FROM NODE 351.40 TO NODE 351.10 = 1923.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 351.10 TO NODE 351.10 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.557
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3157
SUBAREA AREA(ACRES) = 17.76 SUBAREA RUNOFF(CFS) = 24.28
TOTAL AREA(ACRES) = 25.91 TOTAL RUNOFF(CFS) = 37.28
TC(MIN.) = 14.91

\*\*\*\*\*
FLOW PROCESS FROM NODE 351.10 TO NODE 350.00 IS CODE = 53



>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1005.00 DOWNSTREAM(FEET) = 888.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 495.00 CHANNEL SLOPE = 0.2364  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1755 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 37.28  
 FLOW VELOCITY(FEET/SEC) = 7.83 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 15.97  
 LONGEST FLOWPATH FROM NODE 351.40 TO NODE 350.00 = 2418.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 350.00 TO NODE 350.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.361  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3039  
 SUBAREA AREA(ACRES) = 5.68 SUBAREA RUNOFF(CFS) = 6.19  
 TOTAL AREA(ACRES) = 31.59 TOTAL RUNOFF(CFS) = 41.86  
 TC(MIN.) = 15.97

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 350.00 TO NODE 350.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 15.97  
 RAINFALL INTENSITY(INCH/HR) = 4.36  
 TOTAL STREAM AREA(ACRES) = 31.59  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.86

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 22.34        | 16.36     | 4.293                 | 19.26       |
| 2             | 41.86        | 15.97     | 4.361                 | 31.59       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 63.67        | 15.97     | 4.361                 |
| 2             | 63.55        | 16.36     | 4.293                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 63.67 Tc(MIN.) = 15.97  
 TOTAL AREA(ACRES) = 50.85  
 LONGEST FLOWPATH FROM NODE 351.40 TO NODE 350.00 = 2418.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 350.00 TO NODE 340.00 IS CODE = 53

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>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 888.00 | DOWNSTREAM(FEET) = | 851.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 395.00 | CHANNEL SLOPE =    | 0.0937 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0937 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 63.67  
FLOW VELOCITY(FEET/SEC) = 6.83 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.96 Tc(MIN.) = 16.93  
LONGEST FLOWPATH FROM NODE 351.40 TO NODE 340.00 = 2813.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 340.00 TO NODE 340.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.199 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2834  
SUBAREA AREA(ACRES) = 11.88 SUBAREA RUNOFF(CFS) = 12.47  
TOTAL AREA(ACRES) = 62.73 TOTAL RUNOFF(CFS) = 74.64  
TC(MIN.) = 16.93

\*\*\*\*\*  
FLOW PROCESS FROM NODE 340.00 TO NODE 330.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 851.00 | DOWNSTREAM(FEET) = | 814.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 545.00 | CHANNEL SLOPE =    | 0.0679 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0679 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 74.64  
FLOW VELOCITY(FEET/SEC) = 6.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.48 Tc(MIN.) = 18.41  
LONGEST FLOWPATH FROM NODE 351.40 TO NODE 330.00 = 3358.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 330.00 TO NODE 330.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.978 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2802  
SUBAREA AREA(ACRES) = 6.57 SUBAREA RUNOFF(CFS) = 6.53  
TOTAL AREA(ACRES) = 69.30 TOTAL RUNOFF(CFS) = 77.24  
TC(MIN.) = 18.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 330.00 TO NODE 330.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

|                           |   |
|---------------------------|---|
| TOTAL NUMBER OF STREAMS = | 3 |
|---------------------------|---|

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.41

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RAINFALL INTENSITY(INCH/HR) = 3.98  
TOTAL STREAM AREA(ACRES) = 69.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 77.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 331.20 TO NODE 331.10 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 87.00  
UPSTREAM ELEVATION(FEET) = 1622.00  
DOWNSTREAM ELEVATION(FEET) = 1585.00  
ELEVATION DIFFERENCE(FEET) = 37.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.845  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.338  
SUBAREA RUNOFF(CFS) = 0.47  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 331.10 TO NODE 330.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1585.00 DOWNSTREAM(FEET) = 814.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 2844.00 CHANNEL SLOPE = 0.2711  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1870 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.47  
FLOW VELOCITY(FEET/SEC) = 2.42 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 19.57 Tc(MIN.) = 25.42  
LONGEST FLOWPATH FROM NODE 331.20 TO NODE 330.00 = 2931.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 330.00 TO NODE 330.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.231  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3100  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3101  
SUBAREA AREA(ACRES) = 42.74 SUBAREA RUNOFF(CFS) = 42.81  
TOTAL AREA(ACRES) = 42.90 TOTAL RUNOFF(CFS) = 42.99  
TC(MIN.) = 25.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 330.00 TO NODE 330.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

-----  
TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 25.42  
RAINFALL INTENSITY(INCH/HR) = 3.23  
TOTAL STREAM AREA(ACRES) = 42.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 42.99

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 332.30 TO NODE 332.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 96.80  
UPSTREAM ELEVATION(FEET) = 1375.00  
DOWNSTREAM ELEVATION(FEET) = 1368.00  
ELEVATION DIFFERENCE(FEET) = 7.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.869  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.514  
SUBAREA RUNOFF(CFS) = 0.16  
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 332.20 TO NODE 332.10 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1368.00 DOWNSTREAM(FEET) = 980.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1273.00 CHANNEL SLOPE = 0.3048  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1962 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.16  
FLOW VELOCITY(FEET/SEC) = 2.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 8.55 Tc(MIN.) = 15.42  
LONGEST FLOWPATH FROM NODE 332.30 TO NODE 332.10 = 1369.80 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 332.10 TO NODE 332.10 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.459  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 17.65 SUBAREA RUNOFF(CFS) = 27.55  
TOTAL AREA(ACRES) = 17.71 TOTAL RUNOFF(CFS) = 27.64  
TC(MIN.) = 15.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 332.10 TO NODE 330.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 980.00 DOWNSTREAM(FEET) = 814.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1361.00 CHANNEL SLOPE = 0.1220  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1163 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 27.64  
FLOW VELOCITY(FEET/SEC) = 5.77 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.93 Tc(MIN.) = 19.35  
LONGEST FLOWPATH FROM NODE 332.30 TO NODE 330.00 = 2730.80 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 330.00 TO NODE 330.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.852  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 13.94 SUBAREA RUNOFF(CFS) = 18.79  
TOTAL AREA(ACRES) = 31.65 TOTAL RUNOFF(CFS) = 42.67  
TC(MIN.) = 19.35

\*\*\*\*\*  
FLOW PROCESS FROM NODE 330.00 TO NODE 330.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 19.35  
RAINFALL INTENSITY(INCH/HR) = 3.85  
TOTAL STREAM AREA(ACRES) = 31.65  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 42.67

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 77.24        | 18.41     | 3.978                 | 69.30       |
| 2             | 42.99        | 25.42     | 3.231                 | 42.90       |
| 3             | 42.67        | 19.35     | 3.852                 | 31.65       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 148.97       | 18.41     | 3.978                 |
| 2             | 150.20       | 19.35     | 3.852                 |
| 3             | 141.52       | 25.42     | 3.231                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 150.20 Tc(MIN.) = 19.35  
TOTAL AREA(ACRES) = 143.85  
LONGEST FLOWPATH FROM NODE 351.40 TO NODE 330.00 = 3358.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 330.00 TO NODE 320.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 814.00 DOWNSTREAM(FEET) = 600.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 871.00 CHANNEL SLOPE = 0.2457  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1786 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 150.20  
FLOW VELOCITY(FEET/SEC) = 12.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.16 Tc(MIN.) = 20.51  
LONGEST FLOWPATH FROM NODE 351.40 TO NODE 320.00 = 4229.00 FEET.

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*****
FLOW PROCESS FROM NODE      320.00 TO NODE      320.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.710
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800
S. C. S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2993
SUBAREA AREA(ACRES) =  38.87   SUBAREA RUNOFF(CFS) =  40.38
TOTAL AREA(ACRES) =  182.72   TOTAL RUNOFF(CFS) = 202.89
TC(MIN.) =  20.51
*****
FLOW PROCESS FROM NODE      320.00 TO NODE      310.00 IS CODE =  41
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  600.00  DOWNSTREAM(FEET) =  537.00
FLOW LENGTH(FEET) =  500.00  MANNING'S N =  0.015
DEPTH OF FLOW IN  84.0 INCH PIPE IS  18.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  31.75
GIVEN PIPE DIAMETER(INCH) =  84.00   NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  202.89
PIPE TRAVEL TIME(MIN.) =  0.26   Tc(MIN.) =  20.77
LONGEST FLOWPATH FROM NODE      351.40 TO NODE      310.00 =  4729.00 FEET.
*****
FLOW PROCESS FROM NODE      310.00 TO NODE      310.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.680
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600
S. C. S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2959
SUBAREA AREA(ACRES) =  16.93   SUBAREA RUNOFF(CFS) =  16.20
TOTAL AREA(ACRES) =  199.65   TOTAL RUNOFF(CFS) = 217.44
TC(MIN.) =  20.77
*****
FLOW PROCESS FROM NODE      310.00 TO NODE      3.00 IS CODE =  41
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  537.00  DOWNSTREAM(FEET) =  522.00
FLOW LENGTH(FEET) =  630.00  MANNING'S N =  0.013
DEPTH OF FLOW IN  84.0 INCH PIPE IS  27.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  19.79
GIVEN PIPE DIAMETER(INCH) =  84.00   NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  217.44
PIPE TRAVEL TIME(MIN.) =  0.53   Tc(MIN.) =  21.30
LONGEST FLOWPATH FROM NODE      351.40 TO NODE      3.00 =  5359.00 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES)      =  199.65   TC(MIN.) =  21.30
PEAK FLOW RATE(CFS)   =  217.44
=====
```

=====

END OF RATIONAL METHOD ANALYSIS

□





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003, 1985, 1981 HYDROLOGY MANUAL  
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 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 4 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERRO4.DAT  
 TIME/DATE OF STUDY: 14:22 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 402.00 TO NODE 401.80 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 110.00  
 UPSTREAM ELEVATION(FEET) = 980.00  
 DOWNSTREAM ELEVATION(FEET) = 950.00  
 ELEVATION DIFFERENCE(FEET) = 30.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

MERRO4.TXT

THE MAXIMUM OVERLAND FLOW LENGTH = 100.00  
(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.26  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.26

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.80 TO NODE 401.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 950.00 | DOWNSTREAM(FEET) = | 685.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 674.00 | CHANNEL SLOPE =    | 0.3932 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2128 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.26  
FLOW VELOCITY(FEET/SEC) = 2.58 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.35 Tc(MIN.) = 11.45  
LONGEST FLOWPATH FROM NODE 402.00 TO NODE 401.60 = 784.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.80 TO NODE 401.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.404 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 3.46 SUBAREA RUNOFF(CFS) = 4.67  
TOTAL AREA(ACRES) = 3.60 TOTAL RUNOFF(CFS) = 4.86  
TC(MIN.) = 11.45

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.60 TO NODE 401.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 685.00 | DOWNSTREAM(FEET) = | 585.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 512.00 | CHANNEL SLOPE =    | 0.1953 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1577 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.86  
FLOW VELOCITY(FEET/SEC) = 3.77 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.27 Tc(MIN.) = 13.72  
LONGEST FLOWPATH FROM NODE 402.00 TO NODE 401.00 = 1296.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.60 TO NODE 401.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.810 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 8.04 SUBAREA RUNOFF(CFS) = 9.67

MERRO4.TXT  
TOTAL AREA(ACRES) = 11.64 TOTAL RUNOFF(CFS) = 14.00  
TC(MIN.) = 13.72

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.00 TO NODE 4.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 585.00            | DOWNSTREAM(FEET) = | 515.00        |
| FLOW LENGTH(FEET) =              | 545.00            | MANNING'S N =      | 0.013         |
| DEPTH OF FLOW IN                 | 30.0 INCH PIPE IS | 6.4 INCHES         |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 18.15             |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 30.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 14.00             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.50              | Tc(MIN.) =         | 14.22         |
| LONGEST FLOWPATH FROM NODE       | 402.00 TO NODE    | 4.00 =             | 1841.00 FEET. |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 11.64 TC(MIN.) = 14.22  
PEAK FLOW RATE(CFS) = 14.00

-----  
END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

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SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 5 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR05.DAT  
TIME/DATE OF STUDY: 12:06 10/16/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 510.30 TO NODE 510.20 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 110.00  
UPSTREAM ELEVATION(FEET) = 1210.00  
DOWNSTREAM ELEVATION(FEET) = 1180.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

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THE MAXIMUM OVERLAND FLOW LENGTH = 100.00  
(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.20  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.20

\*\*\*\*\*  
FLOW PROCESS FROM NODE 510.20 TO NODE 510.10 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1180.00 DOWNSTREAM(FEET) = 860.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1145.00 CHANNEL SLOPE = 0.2795  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1898 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.20  
FLOW VELOCITY(FEET/SEC) = 2.44 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 7.82 Tc(MIN.) = 14.92  
LONGEST FLOWPATH FROM NODE 510.30 TO NODE 510.10 = 1255.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 510.20 TO NODE 510.10 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.555  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 10.24 SUBAREA RUNOFF(CFS) = 11.66  
TOTAL AREA(ACRES) = 10.35 TOTAL RUNOFF(CFS) = 11.79  
TC(MIN.) = 14.92

\*\*\*\*\*  
FLOW PROCESS FROM NODE 510.10 TO NODE 510.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 860.00 DOWNSTREAM(FEET) = 670.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 787.00 CHANNEL SLOPE = 0.2414  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1771 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 11.79  
FLOW VELOCITY(FEET/SEC) = 5.36 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.45 Tc(MIN.) = 17.37  
LONGEST FLOWPATH FROM NODE 510.30 TO NODE 510.00 = 2042.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 510.10 TO NODE 510.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.130  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 9.05 SUBAREA RUNOFF(CFS) = 9.34

TOTAL AREA(ACRES) = 19.40 TOTAL RUNOFF(CFS) = 20.03  
TC(MIN.) = 17.37

\*\*\*\*\*  
FLOW PROCESS FROM NODE 510.00 TO NODE 5.20 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 670.00 DOWNSTREAM(FEET) = 610.00  
FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 8.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.50  
GIVEN PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.03  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 17.53  
LONGEST FLOWPATH FROM NODE 510.30 TO NODE 5.20 = 2217.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.20 TO NODE 5.10 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 610.00 DOWNSTREAM(FEET) = 575.00  
FLOW LENGTH(FEET) = 225.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 9.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.71  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.03  
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 17.80  
LONGEST FLOWPATH FROM NODE 510.30 TO NODE 5.10 = 2442.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.10 TO NODE 5.10 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.80  
RAINFALL INTENSITY(INCH/HR) = 4.07  
TOTAL STREAM AREA(ACRES) = 19.40  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.03

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.50 TO NODE 5.40 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 185.00  
UPSTREAM ELEVATION(FEET) = 680.00  
DOWNSTREAM ELEVATION(FEET) = 610.00  
ELEVATION DIFFERENCE(FEET) = 70.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.935  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 100.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.467

MERR05. TXT

SUBAREA RUNOFF(CFS) = 1.09  
TOTAL AREA(ACRES) = 0.54 TOTAL RUNOFF(CFS) = 1.09

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.40 TO NODE 5.30 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 610.00 DOWNSTREAM(FEET) = 580.00  
FLOW LENGTH(FEET) = 225.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 2.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.84  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.09  
PIPE TRAVEL TIME(MIN.) = 0.42 Tc(MIN.) = 7.36  
LONGEST FLOWPATH FROM NODE 5.50 TO NODE 5.30 = 410.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.30 TO NODE 5.10 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 580.00 DOWNSTREAM(FEET) = 575.00  
FLOW LENGTH(FEET) = 520.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 3.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.51  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.09  
PIPE TRAVEL TIME(MIN.) = 2.47 Tc(MIN.) = 9.83  
LONGEST FLOWPATH FROM NODE 5.50 TO NODE 5.10 = 930.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.10 TO NODE 5.10 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.83  
RAINFALL INTENSITY(INCH/HR) = 5.96  
TOTAL STREAM AREA(ACRES) = 0.54  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.09

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.03        | 17.80     | 4.065                 | 19.40       |
| 2             | 1.09         | 9.83      | 5.964                 | 0.54        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.15        | 9.83      | 5.964                 |
| 2             | 20.77        | 17.80     | 4.065                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 20.77 Tc(MIN.) = 17.80



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TOTAL AREA(ACRES) = 19.94  
LONGEST FLOWPATH FROM NODE 510.30 TO NODE 5.10 = 2442.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.10 TO NODE 5.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPE SIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 575.00 DOWNSTREAM(FEET) = 550.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 8.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.40  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.77  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 17.90  
LONGEST FLOWPATH FROM NODE 510.30 TO NODE 5.00 = 2542.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.90  
RAINFALL INTENSITY(INCH/HR) = 4.05  
TOTAL STREAM AREA(ACRES) = 19.94  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.77

\*\*\*\*\*  
FLOW PROCESS FROM NODE 504.00 TO NODE 503.80 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1460.00  
DOWNSTREAM ELEVATION(FEET) = 1440.00  
ELEVATION DIFFERENCE(FEET) = 20.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.64  
TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 0.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 503.80 TO NODE 503.60 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVEL TIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1440.00 DOWNSTREAM(FEET) = 1380.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.2000  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1600 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.64  
FLOW VELOCITY(FEET/SEC) = 2.24 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.23 Tc(MIN.) = 7.66  
LONGEST FLOWPATH FROM NODE 504.00 TO NODE 503.60 = 375.00 FEET.

MERR05. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 503.80 TO NODE 503.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.004  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.05 SUBAREA RUNOFF(CFS) = 5.03  
TOTAL AREA(ACRES) = 2.26 TOTAL RUNOFF(CFS) = 5.54  
TC(MIN.) = 7.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 503.60 TO NODE 503.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1380.00 DOWNSTREAM(FEET) = 965.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1225.00 CHANNEL SLOPE = 0.3388  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2033 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 5.54  
FLOW VELOCITY(FEET/SEC) = 4.47 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.57 Tc(MIN.) = 12.23  
LONGEST FLOWPATH FROM NODE 504.00 TO NODE 503.00 = 1600.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 503.60 TO NODE 503.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.179  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3080  
SUBAREA AREA(ACRES) = 11.86 SUBAREA RUNOFF(CFS) = 18.43  
TOTAL AREA(ACRES) = 14.12 TOTAL RUNOFF(CFS) = 22.52  
TC(MIN.) = 12.23

\*\*\*\*\*  
FLOW PROCESS FROM NODE 503.00 TO NODE 502.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 965.00 DOWNSTREAM(FEET) = 665.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1635.00 CHANNEL SLOPE = 0.1835  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1517 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 22.52  
FLOW VELOCITY(FEET/SEC) = 6.15 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.43 Tc(MIN.) = 16.66  
LONGEST FLOWPATH FROM NODE 504.00 TO NODE 502.00 = 3235.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 503.00 TO NODE 502.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MERR05. TXT

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.243  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2686  
SUBAREA AREA(ACRES) = 29.85 SUBAREA RUNOFF(CFS) = 31.66  
TOTAL AREA(ACRES) = 43.97 TOTAL RUNOFF(CFS) = 50.12  
TC(MIN.) = 16.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 501.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 665.00 DOWNSTREAM(FEET) = 625.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 540.00 CHANNEL SLOPE = 0.0741  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0741 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 50.12  
FLOW VELOCITY(FEET/SEC) = 5.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.60 Tc(MIN.) = 18.26  
LONGEST FLOWPATH FROM NODE 504.00 TO NODE 501.00 = 3775.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 501.50 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.999  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2667  
SUBAREA AREA(ACRES) = 4.98 SUBAREA RUNOFF(CFS) = 4.98  
TOTAL AREA(ACRES) = 48.95 TOTAL RUNOFF(CFS) = 52.21  
TC(MIN.) = 18.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.50 TO NODE 501.00 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 625.00 DOWNSTREAM(FEET) = 575.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 16.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.51  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 52.21  
PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 18.67  
LONGEST FLOWPATH FROM NODE 504.00 TO NODE 501.00 = 4175.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 5.00 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 575.00 DOWNSTREAM(FEET) = 550.00  
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 42.0 INCH PIPE IS 13.1 INCHES

MERR05. TXT

PIPE-FLOW VELOCITY(FEET/SEC.) = 20.33  
GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 52.21  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 18.76  
LONGEST FLOWPATH FROM NODE 504.00 TO NODE 5.00 = 4285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
-----

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.76  
RAINFALL INTENSITY(INCH/HR) = 3.93  
TOTAL STREAM AREA(ACRES) = 48.95  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 52.21

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.77        | 17.90     | 4.050                 | 19.94       |
| 2             | 52.21        | 18.76     | 3.930                 | 48.95       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 70.61        | 17.90     | 4.050                 |
| 2             | 72.37        | 18.76     | 3.930                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 72.37 Tc(MIN.) = 18.76  
TOTAL AREA(ACRES) = 68.89  
LONGEST FLOWPATH FROM NODE 504.00 TO NODE 5.00 = 4285.00 FEET.

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 68.89 TC(MIN.) = 18.76  
PEAK FLOW RATE(CFS) = 72.37  
-----

-----  
END OF RATIONAL METHOD ANALYSIS  
-----

□



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2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
6390 GREENWICH DRIVE, SUITE 170  
SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 6 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERRO6.DAT  
TIME/DATE OF STUDY: 11:23 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 602.00 TO NODE 601.50 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 76.00  
UPSTREAM ELEVATION(FEET) = 725.00  
DOWNSTREAM ELEVATION(FEET) = 680.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.827

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERRO6.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.354  
SUBAREA RUNOFF(CFS) = 0.55  
TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 0.55

\*\*\*\*\*  
FLOW PROCESS FROM NODE 601.50 TO NODE 601.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 680.00 | DOWNSTREAM(FEET) = | 625.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 223.00 | CHANNEL SLOPE =    | 0.2466 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1789 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.55  
FLOW VELOCITY(FEET/SEC) = 2.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.57 Tc(MIN.) = 7.40  
LONGEST FLOWPATH FROM NODE 602.00 TO NODE 601.00 = 299.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 601.50 TO NODE 601.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 7.163 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3000  
SUBAREA AREA(ACRES) = 2.23 SUBAREA RUNOFF(CFS) = 4.79  
TOTAL AREA(ACRES) = 2.45 TOTAL RUNOFF(CFS) = 5.27  
TC(MIN.) = 7.40

\*\*\*\*\*  
FLOW PROCESS FROM NODE 601.00 TO NODE 6.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                    |            |                    |        |
|------------------------------------|------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =   | 625.00     | DOWNSTREAM(FEET) = | 600.00 |
| FLOW LENGTH(FEET) =                | 360.00     | MANNING'S N =      | 0.013  |
| DEPTH OF FLOW IN 24.0 INCH PIPE IS | 5.0 INCHES |                    |        |

PIPE-FLOW VELOCITY(FEET/SEC.) = 11.26  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.27  
PIPE TRAVEL TIME(MIN.) = 0.53 Tc(MIN.) = 7.93  
LONGEST FLOWPATH FROM NODE 602.00 TO NODE 6.00 = 659.00 FEET.

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 2.45 TC(MIN.) = 7.93  
PEAK FLOW RATE(CFS) = 5.27

-----  
END OF RATIONAL METHOD ANALYSIS

□











\*\*\*\*\*

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Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 7 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERRO7.DAT  
TIME/DATE OF STUDY: 11:26 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 702.00 TO NODE 701.50 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 84.00  
UPSTREAM ELEVATION(FEET) = 770.00  
DOWNSTREAM ELEVATION(FEET) = 735.00  
ELEVATION DIFFERENCE(FEET) = 35.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.126

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERRO7.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.089  
SUBAREA RUNOFF(CFS) = 0.34  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 701.50 TO NODE 701.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                   |   |        |                  |   |        |
|-----------------------------------|---|--------|------------------|---|--------|
| ELEVATION DATA: UPSTREAM(FEET)    | = | 735.00 | DOWNSTREAM(FEET) | = | 625.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) | = | 347.00 | CHANNEL SLOPE    | = | 0.3170 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1993 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.34  
FLOW VELOCITY(FEET/SEC) = 2.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.31 Tc(MIN.) = 8.44  
LONGEST FLOWPATH FROM NODE 702.00 TO NODE 701.00 = 431.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 701.50 TO NODE 701.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |   |       |
|--|---|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) | = | 6.579 |
|--|---|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2813  
SUBAREA AREA(ACRES) = 1.96 SUBAREA RUNOFF(CFS) = 3.61  
TOTAL AREA(ACRES) = 2.10 TOTAL RUNOFF(CFS) = 3.89  
TC(MIN.) = 8.44

\*\*\*\*\*  
FLOW PROCESS FROM NODE 701.00 TO NODE 7.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|  |   |              |                  |   |        |
|--|---|--------------|------------------|---|--------|
| ELEVATION DATA: UPSTREAM(FEET)                 | = | 625.00       | DOWNSTREAM(FEET) | = | 580.00 |
| FLOW LENGTH(FEET)                              | = | 375.00       | MANNING'S N      | = | 0.024  |
| DEPTH OF FLOW IN 24.0 INCH PIPE IS             |   | 5.0 INCHES   |                  |   |        |
| PIPE-FLOW VELOCITY(FEET/SEC.)                  | = | 8.11         |                  |   |        |
| GIVEN PIPE DIAMETER(INCH)                      | = | 24.00        | NUMBER OF PIPES  | = | 1      |
| PIPE-FLOW(CFS)                                 | = | 3.89         |                  |   |        |
| PIPE TRAVEL TIME(MIN.)                         | = | 0.77         | Tc(MIN.)         | = | 9.21   |
| LONGEST FLOWPATH FROM NODE 702.00 TO NODE 7.00 | = | 806.00 FEET. |                  |   |        |

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 2.10 TC(MIN.) = 9.21  
PEAK FLOW RATE(CFS) = 3.89

-----  
END OF RATIONAL METHOD ANALYSIS

□



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Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 8 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERRO8.DAT  
TIME/DATE OF STUDY: 11:27 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 804.00 TO NODE 803.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 120.00  
UPSTREAM ELEVATION(FEET) = 900.00  
DOWNSTREAM ELEVATION(FEET) = 825.00  
ELEVATION DIFFERENCE(FEET) = 75.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

MERRO8.TXT

THE MAXIMUM OVERLAND FLOW LENGTH = 100.00  
(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.51  
TOTAL AREA(ACRES) = 0.28 TOTAL RUNOFF(CFS) = 0.51

\*\*\*\*\*  
FLOW PROCESS FROM NODE 803.00 TO NODE 802.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 825.00 | DOWNSTREAM(FEET) = | 660.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 518.00 | CHANNEL SLOPE =    | 0.3185 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1996 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.51  
FLOW VELOCITY(FEET/SEC) = 2.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.45 Tc(MIN.) = 10.55  
LONGEST FLOWPATH FROM NODE 804.00 TO NODE 802.00 = 638.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 803.00 TO NODE 802.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.696 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 5.69 SUBAREA RUNOFF(CFS) = 8.10  
TOTAL AREA(ACRES) = 5.97 TOTAL RUNOFF(CFS) = 8.50  
TC(MIN.) = 10.55

\*\*\*\*\*  
FLOW PROCESS FROM NODE 802.00 TO NODE 801.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 660.00 | DOWNSTREAM(FEET) = | 590.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 395.00 | CHANNEL SLOPE =    | 0.1772 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1486 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.50  
FLOW VELOCITY(FEET/SEC) = 4.40 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.50 Tc(MIN.) = 12.05  
LONGEST FLOWPATH FROM NODE 804.00 TO NODE 801.00 = 1033.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 802.00 TO NODE 801.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.229 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2647  
SUBAREA AREA(ACRES) = 5.70 SUBAREA RUNOFF(CFS) = 8.35



MERRO8.TXT  
TOTAL AREA(ACRES) = 11.67 TOTAL RUNOFF(CFS) = 16.15  
TC(MIN.) = 12.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 801.00 TO NODE 8.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 590.00            | DOWNSTREAM(FEET) = | 560.00        |
| FLOW LENGTH(FEET) =              | 425.00            | MANNING'S N =      | 0.013         |
| DEPTH OF FLOW IN                 | 30.0 INCH PIPE IS | 8.0 INCHES         |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 15.30             |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 30.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 16.15             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.46              | Tc(MIN.) =         | 12.51         |
| LONGEST FLOWPATH FROM NODE       | 804.00 TO NODE    | 8.00 =             | 1458.00 FEET. |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 11.67 TC(MIN.) = 12.51  
PEAK FLOW RATE(CFS) = 16.15

-----  
END OF RATIONAL METHOD ANALYSIS

□









\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 9 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERRO9.DAT  
TIME/DATE OF STUDY: 12:43 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 903.00 TO NODE 902.80 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1015.00  
DOWNSTREAM ELEVATION(FEET) = 985.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERRO9.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
SUBAREA RUNOFF(CFS) = 0.30  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.80 TO NODE 902.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 985.00 | DOWNSTREAM(FEET) = | 905.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 300.00 | CHANNEL SLOPE =    | 0.2667 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1856 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.30  
FLOW VELOCITY(FEET/SEC) = 2.41 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.07 Tc(MIN.) = 8.22  
LONGEST FLOWPATH FROM NODE 903.00 TO NODE 902.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.80 TO NODE 902.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.690 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 0.58 SUBAREA RUNOFF(CFS) = 0.97  
TOTAL AREA(ACRES) = 0.73 TOTAL RUNOFF(CFS) = 1.22  
TC(MIN.) = 8.22

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.60 TO NODE 902.40 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 905.00 | DOWNSTREAM(FEET) = | 705.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 658.00 | CHANNEL SLOPE =    | 0.3040 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1960 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.22  
FLOW VELOCITY(FEET/SEC) = 2.65 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.14 Tc(MIN.) = 12.36  
LONGEST FLOWPATH FROM NODE 903.00 TO NODE 902.40 = 1033.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.60 TO NODE 902.40 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.143 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 6.61 SUBAREA RUNOFF(CFS) = 8.50  
TOTAL AREA(ACRES) = 7.34 TOTAL RUNOFF(CFS) = 9.44  
TC(MIN.) = 12.36

MERRO9.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.40 TO NODE 902.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 705.00 | DOWNSTREAM(FEET) = | 645.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 277.00 | CHANNEL SLOPE =    | 0.2166 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1683 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 9.44  
FLOW VELOCITY(FEET/SEC) = 4.85 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.95 Tc(MIN.) = 13.31  
LONGEST FLOWPATH FROM NODE 903.00 TO NODE 902.00 = 1310.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.40 TO NODE 902.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.903 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2534  
SUBAREA AREA(ACRES) = 3.86 SUBAREA RUNOFF(CFS) = 4.92  
TOTAL AREA(ACRES) = 11.20 TOTAL RUNOFF(CFS) = 13.92  
TC(MIN.) = 13.31

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.00 TO NODE 901.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 645.00 | DOWNSTREAM(FEET) = | 580.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 540.00 | CHANNEL SLOPE =    | 0.1204 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1152 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 13.92  
FLOW VELOCITY(FEET/SEC) = 4.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.97 Tc(MIN.) = 15.28  
LONGEST FLOWPATH FROM NODE 903.00 TO NODE 901.00 = 1850.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 902.00 TO NODE 901.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.485 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2700  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2628  
SUBAREA AREA(ACRES) = 14.64 SUBAREA RUNOFF(CFS) = 17.73  
TOTAL AREA(ACRES) = 25.84 TOTAL RUNOFF(CFS) = 30.46  
TC(MIN.) = 15.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 901.00 TO NODE 9.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<



MERR09. TXT

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 580.00            | DOWNSTREAM(FEET) = | 560.00        |
| FLOW LENGTH(FEET) =              | 555.00            | MANNING' S N =     | 0.024         |
| DEPTH OF FLOW IN                 | 42.0 INCH PIPE IS | 16.1 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 9.00              |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 42.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 30.46             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 1.03              | Tc(MIN.) =         | 16.31         |
| LONGEST FLOWPATH FROM NODE       | 903.00 TO NODE    | 9.00 =             | 2405.00 FEET. |

=====

END OF STUDY SUMMARY:

|                     |   |       |            |       |
|---------------------|---|-------|------------|-------|
| TOTAL AREA(ACRES)   | = | 25.84 | TC(MIN.) = | 16.31 |
| PEAK FLOW RATE(CFS) | = | 30.46 |            |       |

=====

END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - EXISTING HYDROLOGY \*
  - \* SUBBASIN 10 - NO DETENTION \*
  - \* 2660.02 - AUGUST 2016 \*
- \*\*\*\*\*

FILE NAME: E-10.DAT  
TIME/DATE OF STUDY: 17:21 08/26/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1041.00 TO NODE 1038.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1480.00  
DOWNSTREAM ELEVATION(FEET) = 1470.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 1.87  
TOTAL AREA(ACRES) = 0.61 TOTAL RUNOFF(CFS) = 1.87

\*\*\*\*\*

FLOW PROCESS FROM NODE 1038.00 TO NODE 1036.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1470.00 DOWNSTREAM(FEET) = 1455.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.0500  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.743  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.83  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.43  
AVERAGE FLOW DEPTH(FEET) = 0.30 TRAVEL TIME(MIN.) = 1.13  
Tc(MIN.) = 6.56  
SUBAREA AREA(ACRES) = 2.18 SUBAREA RUNOFF(CFS) = 5.91  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 7.56

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 FLOW VELOCITY(FEET/SEC.) = 5.10  
LONGEST FLOWPATH FROM NODE 1041.00 TO NODE 1036.00 = 375.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1036.00 TO NODE 1034.00 IS CODE = 51

E-10.TXT

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1455.00 DOWNSTREAM(FEET) = 1320.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 630.00 CHANNEL SLOPE = 0.2143  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.095

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.64  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.04  
AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 0.95  
Tc(MIN.) = 7.51  
SUBAREA AREA(ACRES) = 8.11 SUBAREA RUNOFF(CFS) = 20.14  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 10.9 PEAK FLOW RATE(CFS) = 27.07

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.53 FLOW VELOCITY(FEET/SEC.) = 12.54  
LONGEST FLOWPATH FROM NODE 1041.00 TO NODE 1034.00 = 1005.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1034.00 TO NODE 1030.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1320.00 DOWNSTREAM(FEET) = 1160.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 695.00 CHANNEL SLOPE = 0.2302  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.674

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 51.09  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.49  
AVERAGE FLOW DEPTH(FEET) = 0.74 TRAVEL TIME(MIN.) = 0.75  
Tc(MIN.) = 8.25  
SUBAREA AREA(ACRES) = 20.56 SUBAREA RUNOFF(CFS) = 48.02  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 31.5 PEAK FLOW RATE(CFS) = 73.48

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.90 FLOW VELOCITY(FEET/SEC.) = 17.13  
LONGEST FLOWPATH FROM NODE 1041.00 TO NODE 1030.00 = 1700.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 1030.00 TO NODE 1030.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.25  
RAINFALL INTENSITY(INCH/HR) = 6.67  
TOTAL STREAM AREA(ACRES) = 31.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 73.48

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1031.00 TO NODE 1030.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1620.00  
DOWNSTREAM ELEVATION(FEET) = 1590.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.24  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1030.80 TO NODE 1030.60 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1590.00 DOWNSTREAM(FEET) = 1515.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 270.00 CHANNEL SLOPE = 0.2778  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.899  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.24  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.84  
AVERAGE FLOW DEPTH(FEET) = 0.08 TRAVEL TIME(MIN.) = 0.93

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Tc(MIN.) = 6.36  
SUBAREA AREA(ACRES) = 0.72 SUBAREA RUNOFF(CFS) = 1.99  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.21

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 5.83  
LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1030.60 = 345.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1030.60 TO NODE 1030.40 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1515.00 DOWNSTREAM(FEET) = 1450.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 565.00 CHANNEL SLOPE = 0.1150  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.929

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.75  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.58  
AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 1.43  
Tc(MIN.) = 7.79  
SUBAREA AREA(ACRES) = 3.73 SUBAREA RUNOFF(CFS) = 9.05  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 10.99

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 FLOW VELOCITY(FEET/SEC.) = 7.58  
LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1030.40 = 910.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1030.40 TO NODE 1030.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1450.00 DOWNSTREAM(FEET) = 1160.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1530.00 CHANNEL SLOPE = 0.1895  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.107

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500

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S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 60.62  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.14  
 AVERAGE FLOW DEPTH(FEET) = 0.85 TRAVEL TIME(MIN.) = 1.68  
 Tc(MIN.) = 9.47  
 SUBAREA AREA(ACRES) = 46.29 SUBAREA RUNOFF(CFS) = 98.94  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
 TOTAL AREA(ACRES) = 50.8 PEAK FLOW RATE(CFS) = 108.62

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 1.15 FLOW VELOCITY(FEET/SEC.) = 17.84  
 LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1030.00 = 2440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1030.00 TO NODE 1030.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.47  
 RAINFALL INTENSITY(INCH/HR) = 6.11  
 TOTAL STREAM AREA(ACRES) = 50.82  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 108.62

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 73.48        | 8.25      | 6.674                 | 31.46       |
| 2             | 108.62       | 9.47      | 6.107                 | 50.82       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 168.14       | 8.25      | 6.674                 |
| 2             | 175.86       | 9.47      | 6.107                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 175.86 Tc(MIN.) = 9.47  
 TOTAL AREA(ACRES) = 82.3  
 LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1030.00 = 2440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1030.00 TO NODE 1023.00 IS CODE = 51



>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1175.00 DOWNSTREAM(FEET) = 950.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1130.00 CHANNEL SLOPE = 0.1991  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.772

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3400  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 215.24  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 21.75  
AVERAGE FLOW DEPTH(FEET) = 1.60 TRAVEL TIME(MIN.) = 0.87  
Tc(MIN.) = 10.34  
SUBAREA AREA(ACRES) = 40.13 SUBAREA RUNOFF(CFS) = 78.75  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.347  
TOTAL AREA(ACRES) = 122.4 PEAK FLOW RATE(CFS) = 244.97

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.70 FLOW VELOCITY(FEET/SEC.) = 22.55  
LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1023.00 = 3570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1023.00 TO NODE 1023.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.34  
RAINFALL INTENSITY(INCH/HR) = 5.77  
TOTAL STREAM AREA(ACRES) = 122.41  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 244.97

\*\*\*\*\*

FLOW PROCESS FROM NODE 1025.00 TO NODE 1024.80 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1480.00  
DOWNSTREAM ELEVATION(FEET) = 1470.00  
ELEVATION DIFFERENCE(FEET) = 10.00

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SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 5.42  
TOTAL AREA(ACRES) = 1.77 TOTAL RUNOFF(CFS) = 5.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1024.80 TO NODE 1024.40 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1470.00 DOWNSTREAM(FEET) = 1440.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1000  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.145  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.03  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.89  
AVERAGE FLOW DEPTH(FEET) = 0.45 TRAVEL TIME(MIN.) = 0.63  
Tc(MIN.) = 6.06  
SUBAREA AREA(ACRES) = 6.04 SUBAREA RUNOFF(CFS) = 17.22  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 7.8 PEAK FLOW RATE(CFS) = 22.27

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.59 FLOW VELOCITY(FEET/SEC.) = 9.02  
LONGEST FLOWPATH FROM NODE 1025.00 TO NODE 1024.40 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1024.60 TO NODE 1024.40 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1440.00 DOWNSTREAM(FEET) = 1360.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.1333  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.507  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 45.35  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 12.24

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AVERAGE FLOW DEPTH(FEET) = 0.80 TRAVEL TIME(MIN.) = 0.82  
Tc(MIN.) = 6.88  
SUBAREA AREA(ACRES) = 17.55 SUBAREA RUNOFF(CFS) = 46.11  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 25.4 PEAK FLOW RATE(CFS) = 66.64

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.98 FLOW VELOCITY(FEET/SEC.) = 13.68  
LONGEST FLOWPATH FROM NODE 1025.00 TO NODE 1024.40 = 975.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1024.40 TO NODE 1024.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1360.00 DOWNSTREAM(FEET) = 1080.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1175.00 CHANNEL SLOPE = 0.2383  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.918

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 149.36  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 21.06  
AVERAGE FLOW DEPTH(FEET) = 1.28 TRAVEL TIME(MIN.) = 0.93  
Tc(MIN.) = 7.81  
SUBAREA AREA(ACRES) = 68.27 SUBAREA RUNOFF(CFS) = 165.30  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 93.6 PEAK FLOW RATE(CFS) = 226.70

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.57 FLOW VELOCITY(FEET/SEC.) = 23.54  
LONGEST FLOWPATH FROM NODE 1025.00 TO NODE 1024.00 = 2150.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1024.00 TO NODE 1023.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1080.00 DOWNSTREAM(FEET) = 950.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 805.00 CHANNEL SLOPE = 0.1615  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1407 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 226.70  
FLOW VELOCITY(FEET/SEC) = 12.79 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 8.86  
LONGEST FLOWPATH FROM NODE 1025.00 TO NODE 1023.00 = 2955.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1023.00 TO NODE 1023.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.86  
RAINFALL INTENSITY(INCH/HR) = 6.38  
TOTAL STREAM AREA(ACRES) = 93.63  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 226.70

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 244.97       | 10.34     | 5.772                 | 122.41      |
| 2             | 226.70       | 8.86      | 6.377                 | 93.63       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 448.41       | 8.86      | 6.377                 |
| 2             | 450.14       | 10.34     | 5.772                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 450.14 Tc(MIN.) = 10.34  
TOTAL AREA(ACRES) = 216.0  
LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1023.00 = 3570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1023.00 TO NODE 1021.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 950.00 DOWNSTREAM(FEET) = 750.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 2070.00 CHANNEL SLOPE = 0.0966  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.245  
\*USER SPECIFIED(SUBAREA):

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RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .2900  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 519.93  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 20.87  
 AVERAGE FLOW DEPTH(FEET) = 2.86 TRAVEL TIME(MIN.) = 1.65  
 Tc(MIN.) = 11.99  
 SUBAREA AREA(ACRES) = 91.65 SUBAREA RUNOFF(CFS) = 139.41  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.331  
 TOTAL AREA(ACRES) = 307.7 PEAK FLOW RATE(CFS) = 533.92

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 2.89 FLOW VELOCITY(FEET/SEC.) = 20.99  
 LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1021.00 = 5640.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1021.00 TO NODE 1002.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 750.00 DOWNSTREAM(FEET) = 675.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 625.00 CHANNEL SLOPE = 0.1200  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1150 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 533.92  
 FLOW VELOCITY(FEET/SEC) = 15.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 0.68 Tc(MIN.) = 12.67  
 LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1002.00 = 6265.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1002.00 TO NODE 1002.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.67  
 RAINFALL INTENSITY(INCH/HR) = 5.06  
 TOTAL STREAM AREA(ACRES) = 307.69  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 533.92

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1004.00 TO NODE 1003.80 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500

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S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 1450.00  
 DOWNSTREAM ELEVATION(FEET) = 1435.00  
 ELEVATION DIFFERENCE(FEET) = 15.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
 SUBAREA RUNOFF(CFS) = 0.83  
 TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 1003.80 TO NODE 1003.60 IS CODE = 51

-----  
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1435.00 DOWNSTREAM(FEET) = 1410.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.0833  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.867

\*USER SPECIFIED(SUBAREA):  
 RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.77  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.16  
 AVERAGE FLOW DEPTH(FEET) = 0.26 TRAVEL TIME(MIN.) = 0.97  
 Tc(MIN.) = 6.40  
 SUBAREA AREA(ACRES) = 2.85 SUBAREA RUNOFF(CFS) = 7.85  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
 TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 8.59

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.36 FLOW VELOCITY(FEET/SEC.) = 6.34  
 LONGEST FLOWPATH FROM NODE 1004.00 TO NODE 1003.60 = 375.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1003.60 TO NODE 1003.40 IS CODE = 51

-----  
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1410.00 DOWNSTREAM(FEET) = 1135.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 818.00 CHANNEL SLOPE = 0.3362  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.162

E-10.TXT

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 22.11  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.61  
AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 1.00  
Tc(MIN.) = 7.40  
SUBAREA AREA(ACRES) = 13.89 SUBAREA RUNOFF(CFS) = 26.86  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.285  
TOTAL AREA(ACRES) = 17.0 PEAK FLOW RATE(CFS) = 34.68

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.54 FLOW VELOCITY(FEET/SEC.) = 15.79  
LONGEST FLOWPATH FROM NODE 1004.00 TO NODE 1003.40 = 1193.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1003.40 TO NODE 1003.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 965.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1370.00 CHANNEL SLOPE = 0.1241  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.310

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .2800  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 84.09  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 14.21  
AVERAGE FLOW DEPTH(FEET) = 1.13 TRAVEL TIME(MIN.) = 1.61  
Tc(MIN.) = 9.00  
SUBAREA AREA(ACRES) = 55.80 SUBAREA RUNOFF(CFS) = 98.58  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.281  
TOTAL AREA(ACRES) = 72.8 PEAK FLOW RATE(CFS) = 129.14

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.40 FLOW VELOCITY(FEET/SEC.) = 15.92  
LONGEST FLOWPATH FROM NODE 1004.00 TO NODE 1003.00 = 2563.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1003.00 TO NODE 1002.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 975.00 DOWNSTREAM(FEET) = 700.00

E-10.TXT

CHANNEL LENGTH THRU SUBAREA(FEET) = 1941.00 CHANNEL SLOPE = 0.1417  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.646  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 210.33  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 19.09  
AVERAGE FLOW DEPTH(FEET) = 1.71 TRAVEL TIME(MIN.) = 1.69  
Tc(MIN.) = 10.70  
SUBAREA AREA(ACRES) = 106.38 SUBAREA RUNOFF(CFS) = 162.16  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.275  
TOTAL AREA(ACRES) = 179.2 PEAK FLOW RATE(CFS) = 277.71

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.96 FLOW VELOCITY(FEET/SEC.) = 20.51  
LONGEST FLOWPATH FROM NODE 1004.00 TO NODE 1002.00 = 4504.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1002.00 TO NODE 1002.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.70  
RAINFALL INTENSITY(INCH/HR) = 5.65  
TOTAL STREAM AREA(ACRES) = 179.19  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 277.71

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 533.92       | 12.67     | 5.063                 | 307.69      |
| 2             | 277.71       | 10.70     | 5.646                 | 179.19      |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 756.47       | 10.70     | 5.646                 |
| 2             | 782.94       | 12.67     | 5.063                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:



E-10.TXT  
PEAK FLOW RATE(CFS) = 782.94 Tc(MIN.) = 12.67  
TOTAL AREA(ACRES) = 486.9  
LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1002.00 = 6265.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1002.00 TO NODE 1001.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 700.00 DOWNSTREAM(FEET) = 675.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1175.00 CHANNEL SLOPE = 0.0213  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0213 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 782.94  
FLOW VELOCITY(FEET/SEC) = 7.51 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.61 Tc(MIN.) = 15.28  
LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1001.00 = 7440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1001.00 TO NODE 10.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 675.00 DOWNSTREAM(FEET) = 550.00  
FLOW LENGTH(FEET) = 755.00 MANNING'S N = 0.015  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 38.58  
(PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
AT DEPTH = 0.94 \* DIAMETER)  
GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 782.94  
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 15.60  
LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 10.00 = 8195.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 486.9 TC(MIN.) = 15.60  
PEAK FLOW RATE(CFS) = 782.94

-----  
END OF RATIONAL METHOD ANALYSIS

↑



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 19.0 Release Date: 06/01/2012 License ID 1355

Analysis prepared by:

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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* EXISTING HYDROLOGY \*  
\* BASIN 11 \*  
\* JANUARY 2015 \*  
\*\*\*\*\*

FILE NAME: E-11.DAT  
TIME/DATE OF STUDY: 10:09 01/15/2015

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS  
\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-CROWN TO STREET-CROSSFALL: |                   | IN- / OUT-/PARK-<br>SIDE / SIDE/ WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES: |             |              | MANNING<br>HIKE FACTOR<br>(n) |
|-----|---------------------------------|-------------------|--------------------------------------|------------------------|--------------------|-------------|--------------|-------------------------------|
|     | WIDTH<br>(FT)                   | CROSSFALL<br>(FT) |                                      |                        | WIDTH<br>(FT)      | LIP<br>(FT) | HIKE<br>(FT) |                               |
| 1   | 30.0                            | 20.0              | 0.018/0.018/0.020                    | 0.67                   | 2.00               | 0.0312      | 0.167        | 0.0150                        |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1121.00 TO NODE 1120.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1325.00  
DOWNSTREAM ELEVATION(FEET) = 1280.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

E-11.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1120.00 TO NODE 1119.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1280.00 DOWNSTREAM(FEET) = 850.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 800.00 CHANNEL SLOPE = 0.5375  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.967

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.46  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.16  
AVERAGE FLOW DEPTH(FEET) = 0.15 TRAVEL TIME(MIN.) = 1.46  
Tc(MIN.) = 7.72  
SUBAREA AREA(ACRES) = 3.75 SUBAREA RUNOFF(CFS) = 7.84  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.302  
TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 8.28

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.21 FLOW VELOCITY(FEET/SEC.) = 11.60  
LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 1119.00 = 900.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1119.00 TO NODE 1103.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 850.00 DOWNSTREAM(FEET) = 750.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 535.00 CHANNEL SLOPE = 0.1869  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.504

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.66  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.26  
AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 0.87  
Tc(MIN.) = 8.59  
SUBAREA AREA(ACRES) = 8.59 SUBAREA RUNOFF(CFS) = 16.76  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.301  
TOTAL AREA(ACRES) = 12.5 PEAK FLOW RATE(CFS) = 24.49

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.52 FLOW VELOCITY(FEET/SEC.) = 11.56  
LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 1103.00 = 1435.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1103.00 TO NODE 1103.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

E-11. TXT  
TIME OF CONCENTRATION(MIN.) = 8.59  
RAINFALL INTENSITY(INCH/HR) = 6.50  
TOTAL STREAM AREA(ACRES) = 12.52  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 24.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1124.00 TO NODE 1123.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 1165.00  
DOWNSTREAM ELEVATION(FEET) = 1145.00  
ELEVATION DIFFERENCE(FEET) = 20.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.243  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.944  
SUBAREA RUNOFF(CFS) = 0.19  
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1123.00 TO NODE 1122.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1145.00 DOWNSTREAM(FEET) = 765.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 690.00 CHANNEL SLOPE = 0.5507  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.074  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .2900  
S. C. S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.01  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 12.76  
AVERAGE FLOW DEPTH(FEET) = 0.25 TRAVEL TIME(MIN.) = 0.90  
Tc(MIN.) = 6.14  
SUBAREA AREA(ACRES) = 9.16 SUBAREA RUNOFF(CFS) = 21.45  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.290  
TOTAL AREA(ACRES) = 9.2 PEAK FLOW RATE(CFS) = 21.62

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 FLOW VELOCITY(FEET/SEC.) = 16.06  
LONGEST FLOWPATH FROM NODE 1124.00 TO NODE 1122.00 = 760.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1122.00 TO NODE 1103.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 759.00 DOWNSTREAM(FEET) = 744.00  
FLOW LENGTH(FEET) = 365.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.75  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 21.62  
PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 6.59  
LONGEST FLOWPATH FROM NODE 1124.00 TO NODE 1103.00 = 1125.00 FEET.

E-11. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1103.00 TO NODE 1103.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<  
-----

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.59  
RAINFALL INTENSITY(INCH/HR) = 7.72  
TOTAL STREAM AREA(ACRES) = 9.22  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.62

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 24.49        | 8.59      | 6.504                 | 12.52       |
| 2             | 21.62        | 6.59      | 7.720                 | 9.22        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 40.39        | 6.59      | 7.720                 |
| 2             | 42.70        | 8.59      | 6.504                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 42.70 Tc(MIN.) = 8.59  
TOTAL AREA(ACRES) = 21.7  
LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 1103.00 = 1435.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1103.00 TO NODE 11.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<<  
-----

ELEVATION DATA: UPSTREAM(FEET) = 744.00 DOWNSTREAM(FEET) = 625.00  
FLOW LENGTH(FEET) = 615.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.27  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 42.70  
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 8.95  
LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 11.00 = 2050.00 FEET.

-----  
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 21.7 TC(MIN.) = 8.95  
PEAK FLOW RATE(CFS) = 42.70

-----  
END OF RATIONAL METHOD ANALYSIS

♀



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 12 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR12.DAT  
TIME/DATE OF STUDY: 12:47 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1203.00 TO NODE 1202.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1160.00  
DOWNSTREAM ELEVATION(FEET) = 1110.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!



MERR12.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 2.11  
TOTAL AREA(ACRES) = 0.69 TOTAL RUNOFF(CFS) = 2.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1202.80 TO NODE 1202.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1110.00 | DOWNSTREAM(FEET) = | 1055.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 300.00  | CHANNEL SLOPE =    | 0.1833  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1517 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.11  
FLOW VELOCITY(FEET/SEC) = 2.80 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.79 Tc(MIN.) = 7.21  
LONGEST FLOWPATH FROM NODE 1203.00 TO NODE 1202.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1202.80 TO NODE 1202.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 7.280 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.56 SUBAREA RUNOFF(CFS) = 3.97  
TOTAL AREA(ACRES) = 2.25 TOTAL RUNOFF(CFS) = 5.73  
TC(MIN.) = 7.21

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1202.60 TO NODE 1202.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1055.00 | DOWNSTREAM(FEET) = | 1040.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 137.00  | CHANNEL SLOPE =    | 0.1095  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1071 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 5.73  
FLOW VELOCITY(FEET/SEC) = 3.28 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.70 Tc(MIN.) = 7.91  
LONGEST FLOWPATH FROM NODE 1203.00 TO NODE 1202.00 = 512.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1202.60 TO NODE 1202.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.859 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.08 SUBAREA RUNOFF(CFS) = 2.59  
TOTAL AREA(ACRES) = 3.33 TOTAL RUNOFF(CFS) = 7.99  
TC(MIN.) = 7.91

\*\*\*\*\*

MERR12.TXT

FLOW PROCESS FROM NODE 1202.00 TO NODE 1201.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1040.00 DOWNSTREAM(FEET) = 775.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 910.00 CHANNEL SLOPE = 0.2912  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1928 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.99  
FLOW VELOCITY(FEET/SEC) = 4.91 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.09 Tc(MIN.) = 11.00  
LONGEST FLOWPATH FROM NODE 1203.00 TO NODE 1201.00 = 1422.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1202.00 TO NODE 1201.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.546  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2964  
SUBAREA AREA(ACRES) = 10.88 SUBAREA RUNOFF(CFS) = 16.90  
TOTAL AREA(ACRES) = 14.21 TOTAL RUNOFF(CFS) = 23.36  
TC(MIN.) = 11.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 1201.00 TO NODE 12.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 775.00 DOWNSTREAM(FEET) = 650.00  
FLOW LENGTH(FEET) = 545.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 9.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.45  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 23.36  
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 11.55  
LONGEST FLOWPATH FROM NODE 1203.00 TO NODE 12.00 = 1967.00 FEET.

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 14.21 TC(MIN.) = 11.55  
PEAK FLOW RATE(CFS) = 23.36

END OF RATIONAL METHOD ANALYSIS

□

## APPENDIX B

### Existing Detention Storage Analysis

#### SUB-BASIN 13



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003,1985,1981 HYDROLOGY MANUAL  
 (c) Copyright 1982-2004 Advanced Engineering Software (aes)  
 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTIANS - EXISTING HYDROLOGY \*  
 \* SUBBASIN 13 - NO DETENTION ROUTING \*  
 \* 2469.01A - MARCH 2007 \*  
 \*\*\*\*\*

FILE NAME: MERR13.DAT  
 TIME/DATE OF STUDY: 09:59 03/15/2007

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-CROWN TO STREET-CROSSFALL: |                | STREET-CROSSFALL: |                   | CURB HEIGHT (FT) | GUTTER-GEOMETRIES: |          |           | MANNING FACTOR (n) |
|-----|---------------------------------|----------------|-------------------|-------------------|------------------|--------------------|----------|-----------|--------------------|
|     | WIDTH (FT)                      | CROSSFALL (FT) | IN-SIDE /         | OUT-SIDE/PARK-WAY |                  | WIDTH (FT)         | LIP (FT) | HIKE (FT) |                    |
| 1   | 30.0                            | 20.0           | 0.018/0.018/0.020 |                   | 0.67             | 2.00               | 0.0313   | 0.167     | 0.0150             |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1305.00 TO NODE 1304.80 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 -----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 1350.00

DOWNSTREAM ELEVATION(FEET) = 1315.00

ELEVATION DIFFERENCE(FEET) = 35.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR13.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 1.10  
TOTAL AREA(ACRES) = 0.36 TOTAL RUNOFF(CFS) = 1.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1304.80 TO NODE 1306.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1315.00 | DOWNSTREAM(FEET) = | 1270.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 300.00  | CHANNEL SLOPE =    | 0.1500  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1350 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.10  
FLOW VELOCITY(FEET/SEC) = 2.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.35 Tc(MIN.) = 7.78  
LONGEST FLOWPATH FROM NODE 1305.00 TO NODE 1306.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1304.80 TO NODE 1304.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.934 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.77 SUBAREA RUNOFF(CFS) = 6.72  
TOTAL AREA(ACRES) = 3.13 TOTAL RUNOFF(CFS) = 7.60  
TC(MIN.) = 7.78

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1304.60 TO NODE 1304.40 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1270.00 | DOWNSTREAM(FEET) = | 1195.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 600.00  | CHANNEL SLOPE =    | 0.1250  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1183 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.60  
FLOW VELOCITY(FEET/SEC) = 3.78 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.64 Tc(MIN.) = 10.42  
LONGEST FLOWPATH FROM NODE 1305.00 TO NODE 1304.40 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1304.60 TO NODE 1304.40 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.742 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 9.59 SUBAREA RUNOFF(CFS) = 19.27  
TOTAL AREA(ACRES) = 12.72 TOTAL RUNOFF(CFS) = 25.56  
TC(MIN.) = 10.42

\*\*\*\*\*  
Page 2

FLOW PROCESS FROM NODE 1304.40 TO NODE 1304.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1195.00 DOWNSTREAM(FEET) = 1150.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 315.00 CHANNEL SLOPE = 0.1429
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1302 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 25.56
FLOW VELOCITY(FEET/SEC) = 5.95 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.88 Tc(MIN.) = 11.31
LONGEST FLOWPATH FROM NODE 1305.00 TO NODE 1304.00 = 1290.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1304.40 TO NODE 1304.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.449
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 5.42 SUBAREA RUNOFF(CFS) = 10.34
TOTAL AREA(ACRES) = 18.14 TOTAL RUNOFF(CFS) = 34.59
TC(MIN.) = 11.31

\*\*\*\*\*
FLOW PROCESS FROM NODE 1304.00 TO NODE 1303.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1150.00 DOWNSTREAM(FEET) = 835.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1044.00 CHANNEL SLOPE = 0.3017
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1954 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 34.59
FLOW VELOCITY(FEET/SEC) = 8.06 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.16 Tc(MIN.) = 13.46
LONGEST FLOWPATH FROM NODE 1305.00 TO NODE 1303.00 = 2334.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1304.00 TO NODE 1303.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.868
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 58.45 SUBAREA RUNOFF(CFS) = 99.58
TOTAL AREA(ACRES) = 76.59 TOTAL RUNOFF(CFS) = 130.48
TC(MIN.) = 13.46

\*\*\*\*\*
FLOW PROCESS FROM NODE 1303.00 TO NODE 1301.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

MERR13.TXT

ELEVATION DATA: UPSTREAM(FEET) = 835.00 DOWNSTREAM(FEET) = 795.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 875.00 CHANNEL SLOPE = 0.0457  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0457 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 130.48  
FLOW VELOCITY(FEET/SEC) = 6.06 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.41 Tc(MIN.) = 15.87  
LONGEST FLOWPATH FROM NODE 1305.00 TO NODE 1301.00 = 3209.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1302.00 TO NODE 1301.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.378  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 53.44 SUBAREA RUNOFF(CFS) = 81.88  
TOTAL AREA(ACRES) = 130.03 TOTAL RUNOFF(CFS) = 199.24  
TC(MIN.) = 15.87

\*\*\*\*\*

FLOW PROCESS FROM NODE 1301.00 TO NODE 13.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 795.00 DOWNSTREAM(FEET) = 700.00  
FLOW LENGTH(FEET) = 645.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 24.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 38.26  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 199.24  
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 16.15  
LONGEST FLOWPATH FROM NODE 1305.00 TO NODE 13.00 = 3854.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 130.03 TC(MIN.) = 16.15  
PEAK FLOW RATE(CFS) = 199.24

-----  
END OF RATIONAL METHOD ANALYSIS

□





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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
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 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
 6390 GREENWICH DRIVE, SUITE 170  
 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS -EXISTING HYDROLOGY \*  
 \* SUBBASIN # 141 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR141.DAT  
 TIME/DATE OF STUDY: 12:53 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1412.00 TO NODE 1411.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 -----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 99.00  
 UPSTREAM ELEVATION(FEET) = 1175.00  
 DOWNSTREAM ELEVATION(FEET) = 1125.00  
 ELEVATION DIFFERENCE(FEET) = 50.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.067

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR141.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.377  
SUBAREA RUNOFF(CFS) = 0.37  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1411.00 TO NODE 1410.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1125.00 DOWNSTREAM(FEET) = 900.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 358.00 CHANNEL SLOPE = 0.6285  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2300 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.37  
FLOW VELOCITY(FEET/SEC) = 2.69 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.22 Tc(MIN.) = 9.29  
LONGEST FLOWPATH FROM NODE 1412.00 TO NODE 1410.00 = 457.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1411.00 TO NODE 1410.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.185  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 4.24 SUBAREA RUNOFF(CFS) = 6.56  
TOTAL AREA(ACRES) = 4.44 TOTAL RUNOFF(CFS) = 6.87  
TC(MIN.) = 9.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1410.00 TO NODE 14.10 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 900.00 DOWNSTREAM(FEET) = 750.00  
FLOW LENGTH(FEET) = 630.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 5.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.21  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.87  
PIPE TRAVEL TIME(MIN.) = 0.86 Tc(MIN.) = 10.15  
LONGEST FLOWPATH FROM NODE 1412.00 TO NODE 14.10 = 1087.00 FEET.

-----

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 4.44 TC(MIN.) = 10.15  
PEAK FLOW RATE(CFS) = 6.87

-----

END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 14 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR14.DAT  
TIME/DATE OF STUDY: 12:49 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1403.00 TO NODE 1402.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1075.00  
DOWNSTREAM ELEVATION(FEET) = 1030.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.548

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR14. TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.749  
SUBAREA RUNOFF(CFS) = 0.27  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1402.00 TO NODE 1401.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|   |         |  |                        |
|---|---------|--|------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =                                | 1030.00 | DOWNSTREAM(FEET) =                     | 835.00                 |
| CHANNEL LENGTH THRU SUBAREA(FEET) =                             | 340.00  | CHANNEL SLOPE =                        | 0.5735                 |
| SLOPE ADJUSTMENT CURVE USED:                                    |         |  |                        |
| EFFECTIVE SLOPE =   | .2287   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION |         |  |                        |
| CHANNEL FLOW THRU SUBAREA(CFS) =                                | 0.27    |  |                        |
| FLOW VELOCITY(FEET/SEC) =                                       | 2.68    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| TRAVEL TIME(MIN.) =   | 2.12    | Tc(MIN.) =                             | 8.66                   |
| LONGEST FLOWPATH FROM NODE                                      | 1403.00 | TO NODE                                | 1401.00 = 425.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1402.00 TO NODE 1401.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|   |        |                       |      |
|---|--------|-----------------------|------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =        | 6.469  |                       |      |
| *USER SPECIFIED(SUBAREA):                       |        |                       |      |
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = | .2500  |                       |      |
| S. C. S. CURVE NUMBER (AMC II) =                | 0      |                       |      |
| AREA-AVERAGE RUNOFF COEFFICIENT =               | 0.2500 |                       |      |
| SUBAREA AREA(ACRES) =                           | 3.79   | SUBAREA RUNOFF(CFS) = | 6.13 |
| TOTAL AREA(ACRES) =                             | 3.93   | TOTAL RUNOFF(CFS) =   | 6.36 |
| TC(MIN.) =                                      | 8.66   |                       |      |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1401.00 TO NODE 14.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                    |            |                    |                       |
|------------------------------------|------------|--------------------|-----------------------|
| ELEVATION DATA: UPSTREAM(FEET) =   | 835.00     | DOWNSTREAM(FEET) = | 720.00                |
| FLOW LENGTH(FEET) =                | 615.00     | MANNING'S N =      | 0.024                 |
| DEPTH OF FLOW IN 24.0 INCH PIPE IS | 5.8 INCHES |                    |                       |
| PIPE-FLOW VELOCITY(FEET/SEC.) =    | 10.95      |                    |                       |
| GIVEN PIPE DIAMETER(INCH) =        | 24.00      | NUMBER OF PIPES =  | 1                     |
| PIPE-FLOW(CFS) =                   | 6.36       |                    |                       |
| PIPE TRAVEL TIME(MIN.) =           | 0.94       | Tc(MIN.) =         | 9.60                  |
| LONGEST FLOWPATH FROM NODE         | 1403.00    | TO NODE            | 14.00 = 1040.00 FEET. |

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 3.93 TC(MIN.) = 9.60  
PEAK FLOW RATE(CFS) = 6.36

-----  
END OF RATIONAL METHOD ANALYSIS

□











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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003, 1985, 1981 HYDROLOGY MANUAL

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 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 151 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR151.DAT  
 TIME/DATE OF STUDY: 12:55 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1512.00 TO NODE 1511.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1245.00  
 DOWNSTREAM ELEVATION(FEET) = 1230.00  
 ELEVATION DIFFERENCE(FEET) = 15.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR151.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.26  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.26

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1511.00 TO NODE 1510.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|   |         |  |                         |
|---|---------|--|-------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =                                | 1230.00 | DOWNSTREAM(FEET) =                     | 908.00                  |
| CHANNEL LENGTH THRU SUBAREA(FEET) =                             | 920.00  | CHANNEL SLOPE =                        | 0.3500                  |
| SLOPE ADJUSTMENT CURVE USED:                                    |         |  |                         |
| EFFECTIVE SLOPE =   | .2052   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                         |
| NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION |         |  |                         |
| CHANNEL FLOW THRU SUBAREA(CFS) =                                | 0.26    |  |                         |
| FLOW VELOCITY(FEET/SEC) =                                       | 2.54    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                         |
| TRAVEL TIME(MIN.) =   | 6.04    | Tc(MIN.) =                             | 13.15                   |
| LONGEST FLOWPATH FROM NODE                                      | 1512.00 | TO NODE                                | 1510.00 = 1020.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1511.00 TO NODE 1510.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|   |        |                       |      |
|---|--------|-----------------------|------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =        | 4.943  |                       |      |
| *USER SPECIFIED(SUBAREA):                       |        |                       |      |
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = | .2500  |                       |      |
| S. C. S. CURVE NUMBER (AMC II) =                | 0      |                       |      |
| AREA-AVERAGE RUNOFF COEFFICIENT =               | 0.2500 |                       |      |
| SUBAREA AREA(ACRES) =                           | 6.70   | SUBAREA RUNOFF(CFS) = | 8.28 |
| TOTAL AREA(ACRES) =                             | 6.84   | TOTAL RUNOFF(CFS) =   | 8.45 |
| TC(MIN.) =                                      | 13.15  |                       |      |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1510.00 TO NODE 15.10 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                    |         |                    |                       |
|------------------------------------|---------|--------------------|-----------------------|
| ELEVATION DATA: UPSTREAM(FEET) =   | 908.00  | DOWNSTREAM(FEET) = | 834.00                |
| FLOW LENGTH(FEET) =                | 360.00  | MANNING'S N =      | 0.015                 |
| DEPTH OF FLOW IN 24.0 INCH PIPE IS | 5.1     | INCHES             |                       |
| PIPE-FLOW VELOCITY(FEET/SEC.) =    | 17.18   |                    |                       |
| GIVEN PIPE DIAMETER(INCH) =        | 24.00   | NUMBER OF PIPES =  | 1                     |
| PIPE-FLOW(CFS) =                   | 8.45    |                    |                       |
| PIPE TRAVEL TIME(MIN.) =           | 0.35    | Tc(MIN.) =         | 13.50                 |
| LONGEST FLOWPATH FROM NODE         | 1512.00 | TO NODE            | 15.10 = 1380.00 FEET. |

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 6.84 TC(MIN.) = 13.50  
PEAK FLOW RATE(CFS) = 8.45

-----  
END OF RATIONAL METHOD ANALYSIS

□











\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 15 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR15.DAT  
TIME/DATE OF STUDY: 12:51 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1509.00 TO NODE 1508.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1535.00  
DOWNSTREAM ELEVATION(FEET) = 1500.00  
ELEVATION DIFFERENCE(FEET) = 35.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR15. TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
SUBAREA RUNOFF(CFS) = 0.42  
TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1508.00 TO NODE 1507.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1500.00 | DOWNSTREAM(FEET) = | 1335.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 500.00  | CHANNEL SLOPE =    | 0.3300  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2018 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.42  
FLOW VELOCITY(FEET/SEC) = 2.52 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.31 Tc(MIN.) = 9.46  
LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 1507.00 = 575.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1508.00 TO NODE 1507.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.111 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 1.77 SUBAREA RUNOFF(CFS) = 2.70  
TOTAL AREA(ACRES) = 1.98 TOTAL RUNOFF(CFS) = 3.02  
TC(MIN.) = 9.46

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1507.00 TO NODE 1506.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1335.00 | DOWNSTREAM(FEET) = | 1135.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 400.00  | CHANNEL SLOPE =    | 0.5000  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2250 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.02  
FLOW VELOCITY(FEET/SEC) = 3.84 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.74 Tc(MIN.) = 11.20  
LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 1506.00 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1507.00 TO NODE 1506.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.482 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 8.61 SUBAREA RUNOFF(CFS) = 11.80  
TOTAL AREA(ACRES) = 10.59 TOTAL RUNOFF(CFS) = 14.51  
TC(MIN.) = 11.20

MERR15. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1506.00 TO NODE 1505.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 904.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 960.00 CHANNEL SLOPE = 0.2406  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1769 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 14.51  
FLOW VELOCITY(FEET/SEC) = 5.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.79 Tc(MIN.) = 13.99  
LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 1505.00 = 1935.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1506.00 TO NODE 1505.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.749  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 19.77 SUBAREA RUNOFF(CFS) = 23.47  
TOTAL AREA(ACRES) = 30.36 TOTAL RUNOFF(CFS) = 36.05  
Tc(MIN.) = 13.99

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1505.00 TO NODE 1504.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 904.00 DOWNSTREAM(FEET) = 857.00  
FLOW LENGTH(FEET) = 220.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 11.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.15  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 36.05  
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 14.19  
LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 1504.00 = 2155.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1504.00 TO NODE 1504.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.19  
RAINFALL INTENSITY(INCH/HR) = 4.71  
TOTAL STREAM AREA(ACRES) = 30.36  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1504.30 TO NODE 1504.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500

MERR15. TXT

S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1225.00  
 DOWNSTREAM ELEVATION(FEET) = 1195.00  
 ELEVATION DIFFERENCE(FEET) = 30.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
 SUBAREA RUNOFF(CFS) = 0.28  
 TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1504.20 TO NODE 1504.10 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1195.00 DOWNSTREAM(FEET) = 891.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1070.00 CHANNEL SLOPE = 0.2841  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1910 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
 CHANNEL FLOW THRU SUBAREA(CFS) = 0.28  
 FLOW VELOCITY(FEET/SEC) = 2.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 7.29 Tc(MIN.) = 14.39  
 LONGEST FLOWPATH FROM NODE 1504.30 TO NODE 1504.10 = 1170.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1504.20 TO NODE 1504.10 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.664  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
 SUBAREA AREA(ACRES) = 5.31 SUBAREA RUNOFF(CFS) = 6.19  
 TOTAL AREA(ACRES) = 5.46 TOTAL RUNOFF(CFS) = 6.37  
 TC(MIN.) = 14.39

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1504.10 TO NODE 1504.00 IS CODE = 41

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 891.00 DOWNSTREAM(FEET) = 857.00  
 FLOW LENGTH(FEET) = 574.00 MANNING'S N = 0.015  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 6.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.18  
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 6.37  
 PIPE TRAVEL TIME(MIN.) = 0.94 Tc(MIN.) = 15.33  
 LONGEST FLOWPATH FROM NODE 1504.30 TO NODE 1504.00 = 1744.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1504.00 TO NODE 1504.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

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CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.33  
RAINFALL INTENSITY(INCH/HR) = 4.48  
TOTAL STREAM AREA(ACRES) = 5.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.37

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 36.05        | 14.19     | 4.706                 | 30.36       |
| 2             | 6.37         | 15.33     | 4.477                 | 5.46        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 41.94        | 14.19     | 4.706                 |
| 2             | 40.66        | 15.33     | 4.477                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 41.94 Tc(MIN.) = 14.19  
TOTAL AREA(ACRES) = 35.82  
LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 1504.00 = 2155.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1504.00 TO NODE 1500.00 IS CODE = 41

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 857.00 DOWNSTREAM(FEET) = 846.00  
FLOW LENGTH(FEET) = 234.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 42.0 INCH PIPE IS 17.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.81  
GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 41.94  
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 14.55  
LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 1500.00 = 2389.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1500.00 TO NODE 1500.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.55  
RAINFALL INTENSITY(INCH/HR) = 4.63  
TOTAL STREAM AREA(ACRES) = 35.82  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.94

\*\*\*\*\*

FLOW PROCESS FROM NODE 1503.00 TO NODE 1502.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1310.00

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DOWNSTREAM ELEVATION(FEET) = 1280.00
ELEVATION DIFFERENCE(FEET) = 30.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353
SUBAREA RUNOFF(CFS) = 0.31
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.31

\*\*\*\*\*
FLOW PROCESS FROM NODE 1502.00 TO NODE 1501.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1280.00 DOWNSTREAM(FEET) = 902.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 890.00 CHANNEL SLOPE = 0.4247
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .2170 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.31
FLOW VELOCITY(FEET/SEC) = 2.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 5.69 Tc(MIN.) = 12.79
LONGEST FLOWPATH FROM NODE 1503.00 TO NODE 1501.00 = 990.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1502.00 TO NODE 1501.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.032
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500
SUBAREA AREA(ACRES) = 7.31 SUBAREA RUNOFF(CFS) = 9.20
TOTAL AREA(ACRES) = 7.48 TOTAL RUNOFF(CFS) = 9.41
TC(MIN.) = 12.79

\*\*\*\*\*
FLOW PROCESS FROM NODE 1501.00 TO NODE 1500.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 902.00 DOWNSTREAM(FEET) = 846.00
FLOW LENGTH(FEET) = 344.00 MANNING'S N = 0.015
DEPTH OF FLOW IN 24.0 INCH PIPE IS 5.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.31
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.41
PIPE TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 13.14
LONGEST FLOWPATH FROM NODE 1503.00 TO NODE 1500.00 = 1334.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1500.00 TO NODE 1500.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 13.14
RAINFALL INTENSITY(INCH/HR) = 4.94

MERR15. TXT  
 TOTAL STREAM AREA(ACRES) = 7.48  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.41

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 41.94        | 14.55     | 4.630                 | 35.82       |
| 2             | 9.41         | 13.14     | 4.945                 | 7.48        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 48.68        | 13.14     | 4.945                 |
| 2             | 50.75        | 14.55     | 4.630                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 50.75 Tc(MIN.) = 14.55  
 TOTAL AREA(ACRES) = 43.30  
 LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 1500.00 = 2389.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1500.00 TO NODE 15.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 846.00 DOWNSTREAM(FEET) = 791.00  
 FLOW LENGTH(FEET) = 162.00 MANNING'S N = 0.024  
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 11.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 22.97  
 GIVEN PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 50.75  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 14.67  
 LONGEST FLOWPATH FROM NODE 1509.00 TO NODE 15.00 = 2551.00 FEET.

=====

END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 43.30 TC(MIN.) = 14.67  
 PEAK FLOW RATE(CFS) = 50.75

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

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SAN DIEGO, CALIFORNIA 92122
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*
\* SUBBASIN #16 - NO DETENTION ROUTING \*
\* 2469.01A - OCTOBER 2006 \*
\*\*\*\*\*

FILE NAME: MERR16.DAT
TIME/DATE OF STUDY: 14:17 09/28/2006

-----
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

Table with 10 columns: NO., WIDTH (FT), CROSSFALL (FT), STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY, CURB HEIGHT (FT), GUTTER WIDTH (FT), LIP (FT), GEOMETRIES (FT), HIKE (FT), MANNING FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0313, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*
FLOW PROCESS FROM NODE 1603.00 TO NODE 1602.80 IS CODE = 21
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00
UPSTREAM ELEVATION(FEET) = 1580.00
DOWNSTREAM ELEVATION(FEET) = 1565.00
ELEVATION DIFFERENCE(FEET) = 15.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN TC CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 1.35  
TOTAL AREA(ACRES) = 0.44 TOTAL RUNOFF(CFS) = 1.35

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1602.80 TO NODE 1602.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1565.00 DOWNSTREAM(FEET) = 1325.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 515.00 CHANNEL SLOPE = 0.4660  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2216 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.35  
FLOW VELOCITY(FEET/SEC) = 2.91 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.95 Tc(MIN.) = 8.38  
LONGEST FLOWPATH FROM NODE 1603.00 TO NODE 1602.60 = 590.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1602.80 TO NODE 1602.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.611  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3044  
SUBAREA AREA(ACRES) = 4.58 SUBAREA RUNOFF(CFS) = 9.08  
TOTAL AREA(ACRES) = 5.02 TOTAL RUNOFF(CFS) = 10.10  
TC(MIN.) = 8.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1602.60 TO NODE 1602.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1325.00 DOWNSTREAM(FEET) = 1210.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 605.00 CHANNEL SLOPE = 0.1901  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1550 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 10.10  
FLOW VELOCITY(FEET/SEC) = 4.76 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.12 Tc(MIN.) = 10.49  
LONGEST FLOWPATH FROM NODE 1603.00 TO NODE 1602.00 = 1195.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1602.60 TO NODE 1602.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.717  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2796  
SUBAREA AREA(ACRES) = 12.87 SUBAREA RUNOFF(CFS) = 19.87  
TOTAL AREA(ACRES) = 17.89 TOTAL RUNOFF(CFS) = 28.60  
TC(MIN.) = 10.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 1602.00 TO NODE 1601.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1210.00 DOWNSTREAM(FEET) = 950.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 850.00 CHANNEL SLOPE = 0.3059
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1965 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 28.60
FLOW VELOCITY(FEET/SEC) = 7.58 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 12.36
LONGEST FLOWPATH FROM NODE 1603.00 TO NODE 1601.00 = 2045.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1602.00 TO NODE 1601.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.144
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2719
SUBAREA AREA(ACRES) = 11.70 SUBAREA RUNOFF(CFS) = 15.65
TOTAL AREA(ACRES) = 29.59 TOTAL RUNOFF(CFS) = 41.38
TC(MIN.) = 12.36

\*\*\*\*\*
FLOW PROCESS FROM NODE 1601.00 TO NODE 16.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 950.00 DOWNSTREAM(FEET) = 850.00
FLOW LENGTH(FEET) = 605.00 MANNING'S N = 0.015
DEPTH OF FLOW IN 42.0 INCH PIPE IS 9.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.74
GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 41.38
PIPE TRAVEL TIME(MIN.) = 0.42 Tc(MIN.) = 12.79
LONGEST FLOWPATH FROM NODE 1603.00 TO NODE 16.00 = 2650.00 FEET.

END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 29.59 TC(MIN.) = 12.79
PEAK FLOW RATE(CFS) = 41.38

END OF RATIONAL METHOD ANALYSIS

□

RATIONAL METHOD HYDROGRAPH PROGRAM  
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RUN DATE 9/28/2006  
HYDROGRAPH FILE NAME Text1  
TIME OF CONCENTRATION 13 MIN.  
61 RAINFALL 3.5 INCHES  
BA AREA 29.59 ACRES  
RUNOFF COEFFICIENT 0.2719  
PEAK DISCHARGE 41.38 CFS

|                  |                         |
|------------------|-------------------------|
| TIME (MIN) = 0   | DISCHARGE (CFS) = 0     |
| TIME (MIN) = 13  | DISCHARGE (CFS) = 0     |
| TIME (MIN) = 26  | DISCHARGE (CFS) = 1.7   |
| TIME (MIN) = 39  | DISCHARGE (CFS) = 1.8   |
| TIME (MIN) = 52  | DISCHARGE (CFS) = 1.9   |
| TIME (MIN) = 65  | DISCHARGE (CFS) = 1.9   |
| TIME (MIN) = 78  | DISCHARGE (CFS) = 2     |
| TIME (MIN) = 91  | DISCHARGE (CFS) = 2.1   |
| TIME (MIN) = 104 | DISCHARGE (CFS) = 2.2   |
| TIME (MIN) = 117 | DISCHARGE (CFS) = 2.3   |
| TIME (MIN) = 130 | DISCHARGE (CFS) = 2.5   |
| TIME (MIN) = 143 | DISCHARGE (CFS) = 2.7   |
| TIME (MIN) = 156 | DISCHARGE (CFS) = 2.9   |
| TIME (MIN) = 169 | DISCHARGE (CFS) = 3.1   |
| TIME (MIN) = 182 | DISCHARGE (CFS) = 3.6   |
| TIME (MIN) = 195 | DISCHARGE (CFS) = 3.9   |
| TIME (MIN) = 208 | DISCHARGE (CFS) = 4.7   |
| TIME (MIN) = 221 | DISCHARGE (CFS) = 5.4   |
| TIME (MIN) = 234 | DISCHARGE (CFS) = 7.9   |
| TIME (MIN) = 247 | DISCHARGE (CFS) = 9.9   |
| TIME (MIN) = 260 | DISCHARGE (CFS) = 41.38 |
| TIME (MIN) = 273 | DISCHARGE (CFS) = 6.4   |
| TIME (MIN) = 286 | DISCHARGE (CFS) = 4.3   |
| TIME (MIN) = 299 | DISCHARGE (CFS) = 3.3   |
| TIME (MIN) = 312 | DISCHARGE (CFS) = 2.8   |
| TIME (MIN) = 325 | DISCHARGE (CFS) = 2.4   |
| TIME (MIN) = 338 | DISCHARGE (CFS) = 2.2   |
| TIME (MIN) = 351 | DISCHARGE (CFS) = 2     |
| TIME (MIN) = 364 | DISCHARGE (CFS) = 1.8   |
| TIME (MIN) = 377 | DISCHARGE (CFS) = 0     |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 17 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR17.DAT  
TIME/DATE OF STUDY: 12:58 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1702.00 TO NODE 1701.80 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1355.00  
DOWNSTREAM ELEVATION(FEET) = 1320.00  
ELEVATION DIFFERENCE(FEET) = 35.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR17.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.34  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1701.80 TO NODE 1701.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1320.00 | DOWNSTREAM(FEET) = | 1120.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 325.00  | CHANNEL SLOPE =    | 0.6154  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2300 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.34  
FLOW VELOCITY(FEET/SEC) = 2.69 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 7.44  
LONGEST FLOWPATH FROM NODE 1702.00 TO NODE 1701.60 = 400.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1701.80 TO NODE 1701.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 7.134 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2780  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2822  
SUBAREA AREA(ACRES) = 1.78 SUBAREA RUNOFF(CFS) = 3.53  
TOTAL AREA(ACRES) = 1.89 TOTAL RUNOFF(CFS) = 3.80  
TC(MIN.) = 7.44

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1701.60 TO NODE 1701.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1120.00 | DOWNSTREAM(FEET) = | 950.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 760.00  | CHANNEL SLOPE =    | 0.2237 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1712 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.80  
FLOW VELOCITY(FEET/SEC) = 3.62 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.50 Tc(MIN.) = 10.95  
LONGEST FLOWPATH FROM NODE 1702.00 TO NODE 1701.00 = 1160.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1701.60 TO NODE 1701.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.563 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2629  
SUBAREA AREA(ACRES) = 12.38 SUBAREA RUNOFF(CFS) = 17.91  
TOTAL AREA(ACRES) = 14.27 TOTAL RUNOFF(CFS) = 20.87  
TC(MIN.) = 10.95

MERR17. TXT

\*\*\*\*\*

FLOW PROCESS FROM NODE 1701.00 TO NODE 17.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 950.00            | DOWNSTREAM(FEET) = | 900.00        |
| FLOW LENGTH(FEET) =              | 440.00            | MANNING'S N =      | 0.024         |
| DEPTH OF FLOW IN                 | 30.0 INCH PIPE IS | 11.1 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 12.58             |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 30.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 20.87             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.58              | Tc(MIN.) =         | 11.53         |
| LONGEST FLOWPATH FROM NODE       | 1702.00 TO NODE   | 17.00 =            | 1600.00 FEET. |

=====

END OF STUDY SUMMARY:

|                     |   |       |            |       |
|---------------------|---|-------|------------|-------|
| TOTAL AREA(ACRES)   | = | 14.27 | TC(MIN.) = | 11.53 |
| PEAK FLOW RATE(CFS) | = | 20.87 |            |       |

=====

END OF RATIONAL METHOD ANALYSIS

□











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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
6390 GREENWICH DRIVE, SUITE 170  
SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 18 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR18.DAT  
TIME/DATE OF STUDY: 13:00 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1802.00 TO NODE 1801.50 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 88.00  
UPSTREAM ELEVATION(FEET) = 1370.00  
DOWNSTREAM ELEVATION(FEET) = 1365.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.097  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.357

MERR18.TXT

SUBAREA RUNOFF(CFS) = 0.39  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.39

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1801.50 TO NODE 1801.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1365.00 DOWNSTREAM(FEET) = 950.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 970.00 CHANNEL SLOPE = 0.4278  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2173 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.39  
FLOW VELOCITY(FEET/SEC) = 2.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 6.19 Tc(MIN.) = 13.29  
LONGEST FLOWPATH FROM NODE 1802.00 TO NODE 1801.00 = 1058.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1801.50 TO NODE 1801.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.909  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2621  
SUBAREA AREA(ACRES) = 6.35 SUBAREA RUNOFF(CFS) = 8.10  
TOTAL AREA(ACRES) = 6.50 TOTAL RUNOFF(CFS) = 8.36  
TC(MIN.) = 13.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1801.00 TO NODE 18.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 950.00 DOWNSTREAM(FEET) = 925.00  
FLOW LENGTH(FEET) = 440.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 6.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.99  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.36  
PIPE TRAVEL TIME(MIN.) = 0.61 Tc(MIN.) = 13.90  
LONGEST FLOWPATH FROM NODE 1802.00 TO NODE 18.00 = 1498.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 6.50 TC(MIN.) = 13.90  
PEAK FLOW RATE(CFS) = 8.36

=====

END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC.  
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 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN #19 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR19.DAT  
 TIME/DATE OF STUDY: 15:06 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-CROWN TO STREET-CROSSFALL: |                | STREET-CROSSFALL: |               | CURB HEIGHT (FT) | GUTTER-GEOMETRIES: |          |           | MANNING FACTOR (n) |
|-----|---------------------------------|----------------|-------------------|---------------|------------------|--------------------|----------|-----------|--------------------|
|     | WIDTH (FT)                      | CROSSFALL (FT) | IN-SIDE /         | OUT-/PARK-WAY |                  | WIDTH (FT)         | LIP (FT) | HIKE (FT) |                    |
| 1   | 30.0                            | 20.0           | 0.018/0.018/0.020 |               | 0.67             | 2.00               | 0.0313   | 0.167     | 0.0150             |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1903.00 TO NODE 1902.80 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 1595.00  
 DOWNSTREAM ELEVATION(FEET) = 1530.00  
 ELEVATION DIFFERENCE(FEET) = 65.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 -----



MERR19.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.43  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.43

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1902.80 TO NODE 1902.60 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1530.00 DOWNSTREAM(FEET) = 1420.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.3667  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2082 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.43  
FLOW VELOCITY(FEET/SEC) = 2.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.96 Tc(MIN.) = 7.38  
LONGEST FLOWPATH FROM NODE 1903.00 TO NODE 1902.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1902.80 TO NODE 1902.60 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.171  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.04 SUBAREA RUNOFF(CFS) = 2.61  
TOTAL AREA(ACRES) = 1.18 TOTAL RUNOFF(CFS) = 2.96  
TC(MIN.) = 7.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1902.60 TO NODE 1902.40 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1420.00 DOWNSTREAM(FEET) = 1245.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.2917  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1929 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.96  
FLOW VELOCITY(FEET/SEC) = 3.53 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.83 Tc(MIN.) = 10.22  
LONGEST FLOWPATH FROM NODE 1903.00 TO NODE 1902.40 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1902.60 TO NODE 1902.40 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.816  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 9.05 SUBAREA RUNOFF(CFS) = 18.42  
TOTAL AREA(ACRES) = 10.23 TOTAL RUNOFF(CFS) = 20.83  
TC(MIN.) = 10.22

MERR19.TXT

\*\*\*\*\*

FLOW PROCESS FROM NODE 1902.40 TO NODE 1902.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1245.00 DOWNSTREAM(FEET) = 1090.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1145.00 CHANNEL SLOPE = 0.1354
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1252 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 20.83
FLOW VELOCITY(FEET/SEC) = 5.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.50 Tc(MIN.) = 13.72
LONGEST FLOWPATH FROM NODE 1903.00 TO NODE 1902.00 = 2120.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1902.40 TO NODE 1902.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.809
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3150
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3242
SUBAREA AREA(ACRES) = 28.68 SUBAREA RUNOFF(CFS) = 43.45
TOTAL AREA(ACRES) = 38.91 TOTAL RUNOFF(CFS) = 60.66
TC(MIN.) = 13.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 1902.00 TO NODE 1901.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1090.00 DOWNSTREAM(FEET) = 950.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1950.00 CHANNEL SLOPE = 0.0718
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .0718 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 60.66
FLOW VELOCITY(FEET/SEC) = 5.89 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 5.52 Tc(MIN.) = 19.24
LONGEST FLOWPATH FROM NODE 1903.00 TO NODE 1901.00 = 4070.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1902.00 TO NODE 1901.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.867
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2670
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2944
SUBAREA AREA(ACRES) = 42.31 SUBAREA RUNOFF(CFS) = 43.68
TOTAL AREA(ACRES) = 81.22 TOTAL RUNOFF(CFS) = 92.46
TC(MIN.) = 19.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 1901.00 TO NODE 19.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

MERR19.TXT

=====

ELEVATION DATA: UPSTREAM(FEET) = 950.00 DOWNSTREAM(FEET) = 930.00  
FLOW LENGTH(FEET) = 441.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 60.0 INCH PIPE IS 17.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.13  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 92.46  
PIPE TRAVEL TIME(MIN.) = 0.37 Tc(MIN.) = 19.60  
LONGEST FLOWPATH FROM NODE 1903.00 TO NODE 19.00 = 4511.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 81.22 TC(MIN.) = 19.60  
PEAK FLOW RATE(CFS) = 92.46

=====

END OF RATIONAL METHOD ANALYSIS

□

RUN DATE 9/29/2006  
HYDROGRAPH FILE NAME Text1  
TIME OF CONCENTRATION 20 MIN.  
6 HOUR RAINFALL 3.5 INCHES  
BASIN AREA 81.22 ACRES  
RUNOFF COEFFICIENT 0.2944  
PEAK DISCHARGE 92.46 CFS

|                  |                         |
|------------------|-------------------------|
| TIME (MIN) = 0   | DISCHARGE (CFS) = 0     |
| TIME (MIN) = 20  | DISCHARGE (CFS) = 5.1   |
| TIME (MIN) = 40  | DISCHARGE (CFS) = 5.2   |
| TIME (MIN) = 60  | DISCHARGE (CFS) = 5.7   |
| TIME (MIN) = 80  | DISCHARGE (CFS) = 6     |
| TIME (MIN) = 100 | DISCHARGE (CFS) = 6.6   |
| TIME (MIN) = 120 | DISCHARGE (CFS) = 7     |
| TIME (MIN) = 140 | DISCHARGE (CFS) = 8.1   |
| TIME (MIN) = 160 | DISCHARGE (CFS) = 8.7   |
| TIME (MIN) = 180 | DISCHARGE (CFS) = 10.7  |
| TIME (MIN) = 200 | DISCHARGE (CFS) = 12.2  |
| TIME (MIN) = 220 | DISCHARGE (CFS) = 17.9  |
| TIME (MIN) = 240 | DISCHARGE (CFS) = 22.9  |
| TIME (MIN) = 260 | DISCHARGE (CFS) = 92.46 |
| TIME (MIN) = 280 | DISCHARGE (CFS) = 14.3  |
| TIME (MIN) = 300 | DISCHARGE (CFS) = 9.6   |
| TIME (MIN) = 320 | DISCHARGE (CFS) = 7.5   |
| TIME (MIN) = 340 | DISCHARGE (CFS) = 6.3   |
| TIME (MIN) = 360 | DISCHARGE (CFS) = 5.5   |
| TIME (MIN) = 380 | DISCHARGE (CFS) = 0     |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 19.0 Release Date: 06/01/2012 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Dr.  
Suite 170  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* EXISTING HYDROLOGY \*  
\* SUBBASIN #20 \*  
\* SEPTEMBER 2014 \*  
\*\*\*\*\*

FILE NAME: E-20. DAT  
TIME/DATE OF STUDY: 10:33 09/24/2014

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-CROWN TO |                | STREET-CROSSFALL: |                 | CURB HEIGHT (FT) | GUTTER-GEOMETRIES: |          |           | MANNING FACTOR (n) |
|-----|---------------|----------------|-------------------|-----------------|------------------|--------------------|----------|-----------|--------------------|
|     | WIDTH (FT)    | CROSSFALL (FT) | IN-SIDE /         | OUT-PARK-SIDE / |                  | WIDTH (FT)         | LIP (FT) | HIKE (FT) |                    |
| 1   | 30.0          | 20.0           | 0.018/0.018/0.020 |                 | 0.67             | 2.00               | 0.0312   | 0.167     | 0.0150             |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2001.00 TO NODE 2000.80 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1065.00  
DOWNSTREAM ELEVATION(FEET) = 1055.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
-----

E-20. TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
SUBAREA RUNOFF(CFS) = 0.71  
TOTAL AREA(ACRES) = 0.35 TOTAL RUNOFF(CFS) = 0.71

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.80 TO NODE 2000.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1055.00 | DOWNSTREAM(FEET) = | 1025.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 300.00  | CHANNEL SLOPE =    | 0.1000  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1000 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.71  
FLOW VELOCITY(FEET/SEC) = 1.77 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.82 Tc(MIN.) = 8.97  
LONGEST FLOWPATH FROM NODE 2001.00 TO NODE 2000.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.80 TO NODE 2000.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.324 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2964  
SUBAREA AREA(ACRES) = 4.54 SUBAREA RUNOFF(CFS) = 8.61  
TOTAL AREA(ACRES) = 4.9 TOTAL RUNOFF(CFS) = 9.17  
TC(MIN.) = 8.97

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.60 TO NODE 2000.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1025.00 | DOWNSTREAM(FEET) = | 985.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 475.00  | CHANNEL SLOPE =    | 0.0842 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0842 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 9.17  
FLOW VELOCITY(FEET/SEC) = 3.40 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.33 Tc(MIN.) = 11.30  
LONGEST FLOWPATH FROM NODE 2001.00 TO NODE 2000.00 = 850.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.60 TO NODE 2000.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.449 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3286  
SUBAREA AREA(ACRES) = 7.37 SUBAREA RUNOFF(CFS) = 14.06  
TOTAL AREA(ACRES) = 12.3 TOTAL RUNOFF(CFS) = 21.95  
TC(MIN.) = 11.30

E-20. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.00 TO NODE 20.20 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 986.50            | DOWNSTREAM(FEET) = | 969.10        |
| FLOW LENGTH(FEET) =              | 300.00            | MANNING'S N =      | 0.024         |
| DEPTH OF FLOW IN                 | 30.0 INCH PIPE IS | 13.8 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 9.97              |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 30.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 21.95             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.50              | Tc(MIN.) =         | 11.81         |
| LONGEST FLOWPATH FROM NODE       | 2001.00 TO NODE   | 20.20 =            | 1150.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 20.20 TO NODE 20.10 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 968.60            | DOWNSTREAM(FEET) = | 958.00        |
| FLOW LENGTH(FEET) =              | 532.00            | MANNING'S N =      | 0.024         |
| DEPTH OF FLOW IN                 | 42.0 INCH PIPE IS | 15.8 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 6.64              |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 42.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 21.95             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 1.34              | Tc(MIN.) =         | 13.14         |
| LONGEST FLOWPATH FROM NODE       | 2001.00 TO NODE   | 20.10 =            | 1682.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 20.10 TO NODE 20.10 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

|  |       |
|--|-------|
| TOTAL NUMBER OF STREAMS =                            | 2     |
| CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE: |       |
| TIME OF CONCENTRATION(MIN.) =                        | 13.14 |
| RAINFALL INTENSITY(INCH/HR) =                        | 4.94  |
| TOTAL STREAM AREA(ACRES) =                           | 12.26 |
| PEAK FLOW RATE(CFS) AT CONFLUENCE =                  | 21.95 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2004.00 TO NODE 2003.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

|   |         |
|---|---------|
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = | .3500   |
| S. C. S. CURVE NUMBER (AMC II) =                | 0       |
| INITIAL SUBAREA FLOW-LENGTH(FEET) =             | 75.00   |
| UPSTREAM ELEVATION(FEET) =                      | 1050.00 |
| DOWNSTREAM ELEVATION(FEET) =                    | 1045.00 |
| ELEVATION DIFFERENCE(FEET) =                    | 5.00    |
| SUBAREA OVERLAND TIME OF FLOW(MIN.) =           | 6.212   |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =        | 8.017   |
| SUBAREA RUNOFF(CFS) =                           | 0.28    |
| TOTAL AREA(ACRES) =                             | 0.10    |
| TOTAL RUNOFF(CFS) =                             | 0.28    |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2003.00 TO NODE 2002.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<



>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1045.00 DOWNSTREAM(FEET) = 973.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 450.00 CHANNEL SLOPE = 0.1600
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1400 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.28
FLOW VELOCITY(FEET/SEC) = 2.10 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.58 Tc(MIN.) = 9.79
LONGEST FLOWPATH FROM NODE 2004.00 TO NODE 2002.00 = 525.00 FEET.
    
```

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2003.00 TO NODE 2002.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.978
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 1.92 SUBAREA RUNOFF(CFS) = 4.02
TOTAL AREA(ACRES) = 2.0 TOTAL RUNOFF(CFS) = 4.23
TC(MIN.) = 9.79
    
```

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2002.00 TO NODE 20.10 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 966.90 DOWNSTREAM(FEET) = 958.80
FLOW LENGTH(FEET) = 198.00 MANNING'S N = 0.024
DEPTH OF FLOW IN 24.0 INCH PIPE IS 6.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.67
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.23
PIPE TRAVEL TIME(MIN.) = 0.58 Tc(MIN.) = 10.37
LONGEST FLOWPATH FROM NODE 2004.00 TO NODE 20.10 = 723.00 FEET.
    
```

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 20.10 TO NODE 20.10 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.37
RAINFALL INTENSITY(INCH/HR) = 5.76
TOTAL STREAM AREA(ACRES) = 2.02
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.23
    
```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 21.95        | 13.14     | 4.944                 | 12.26       |
| 2             | 4.23         | 10.37     | 5.759                 | 2.02        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

E-20. TXT

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 21.56        | 10.37     | 5.759                 |
| 2             | 25.58        | 13.14     | 4.944                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 25.58 Tc(MIN.) = 13.14  
 TOTAL AREA(ACRES) = 14.3  
 LONGEST FLOWPATH FROM NODE 2001.00 TO NODE 20.10 = 1682.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 20.10 TO NODE 20.00 IS CODE = 41

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 957.00 DOWNSTREAM(FEET) = 944.80  
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.024  
 DEPTH OF FLOW IN 42.0 INCH PIPE IS 12.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.37  
 GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 25.58  
 PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 13.46  
 LONGEST FLOWPATH FROM NODE 2001.00 TO NODE 20.00 = 1882.00 FEET.

=====

END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 14.3 TC(MIN.) = 13.46  
 PEAK FLOW RATE(CFS) = 25.58

=====

END OF RATIONAL METHOD ANALYSIS

□

# APPENDIX A

AES  
Rational Method Hydrology

Existing Condition

BASIN B



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

(c) Copyright 1982-2012 Advanced Engineering Software (aes)  
Ver. 19.0 Release Date: 06/01/2012 License ID 1355

Analysis prepared by:

Fuscoe Engineering  
6390 Greenwich Dr.  
Suite 170  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* EXISTING HYDROLOGY \*  
\* SUBBASIN 21 \*  
\* \*  
\*\*\*\*\*

FILE NAME: E-21. DAT  
TIME/DATE OF STUDY: 16:36 09/24/2014

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2101.00 TO NODE 2100.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1235.00  
DOWNSTREAM ELEVATION(FEET) = 1215.00  
ELEVATION DIFFERENCE(FEET) = 20.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.789

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

E-21. TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.390  
SUBAREA RUNOFF(CFS) = 0.28  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2100.80 TO NODE 2100.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1215.00 | DOWNSTREAM(FEET) = | 1105.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 300.00  | CHANNEL SLOPE =    | 0.3667  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2082 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.28  
FLOW VELOCITY(FEET/SEC) = 2.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.96 Tc(MIN.) = 7.75  
LONGEST FLOWPATH FROM NODE 2101.00 TO NODE 2100.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2100.80 TO NODE 2100.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.953 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2627  
SUBAREA AREA(ACRES) = 1.52 SUBAREA RUNOFF(CFS) = 2.75  
TOTAL AREA(ACRES) = 1.6 TOTAL RUNOFF(CFS) = 2.98  
TC(MIN.) = 7.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2100.60 TO NODE 2100.40 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1105.00 | DOWNSTREAM(FEET) = | 1045.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 600.00  | CHANNEL SLOPE =    | 0.1000  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1000 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.98  
FLOW VELOCITY(FEET/SEC) = 2.55 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.93 Tc(MIN.) = 11.67  
LONGEST FLOWPATH FROM NODE 2101.00 TO NODE 2100.40 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2100.60 TO NODE 2100.40 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.337 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2758  
SUBAREA AREA(ACRES) = 5.09 SUBAREA RUNOFF(CFS) = 7.61  
TOTAL AREA(ACRES) = 6.7 TOTAL RUNOFF(CFS) = 9.89  
TC(MIN.) = 11.67

E-21. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2100.40 TO NODE 21.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |  |                       |
|-------------------------------------|---------|--|-----------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1045.00 | DOWNSTREAM(FEET) =                     | 1000.00               |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1175.00 | CHANNEL SLOPE =                        | 0.0383                |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 9.89    |  |                       |
| FLOW VELOCITY(FEET/SEC) =           | 2.35    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                       |
| TRAVEL TIME(MIN.) =                 | 8.33    | Tc(MIN.) =                             | 20.00                 |
| LONGEST FLOWPATH FROM NODE          | 2101.00 | TO NODE                                | 21.00 = 2150.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2100.40 TO NODE 21.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |        |                       |       |
|--|--------|-----------------------|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.771  |                       |       |
| *USER SPECIFIED(SUBAREA):                |        |                       |       |
| USER-SPECIFIED RUNOFF COEFFICIENT =      | .3200  |                       |       |
| S. C. S. CURVE NUMBER (AMC II) =         | 0      |                       |       |
| AREA-AVERAGE RUNOFF COEFFICIENT =        | 0.3117 |                       |       |
| SUBAREA AREA(ACRES) =                    | 29.11  | SUBAREA RUNOFF(CFS) = | 35.13 |
| TOTAL AREA(ACRES) =                      | 35.8   | TOTAL RUNOFF(CFS) =   | 42.11 |
| TC(MIN.) =                               | 20.00  |                       |       |

=====

|                       |       |            |       |
|-----------------------|-------|------------|-------|
| END OF STUDY SUMMARY: |       |            |       |
| TOTAL AREA(ACRES) =   | 35.8  | TC(MIN.) = | 20.00 |
| PEAK FLOW RATE(CFS) = | 42.11 |            |       |

-----  
END OF RATIONAL METHOD ANALYSIS

□





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
6390 GREENWICH DRIVE, SUITE 170  
SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 221 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR221.DAT  
TIME/DATE OF STUDY: 13:05 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2213.00 TO NODE 2212.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1260.00  
DOWNSTREAM ELEVATION(FEET) = 1230.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR221.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 1.31  
TOTAL AREA(ACRES) = 0.47 TOTAL RUNOFF(CFS) = 1.31

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2212.00 TO NODE 2211.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1230.00 | DOWNSTREAM(FEET) = | 1095.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 647.90  | CHANNEL SLOPE =    | 0.2084  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1642 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.31  
FLOW VELOCITY(FEET/SEC) = 2.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.35 Tc(MIN.) = 10.61  
LONGEST FLOWPATH FROM NODE 2213.00 TO NODE 2211.00 = 747.90 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2212.00 TO NODE 2211.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.675 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4452  
SUBAREA AREA(ACRES) = 3.03 SUBAREA RUNOFF(CFS) = 7.91  
TOTAL AREA(ACRES) = 3.50 TOTAL RUNOFF(CFS) = 8.84  
TC(MIN.) = 10.61

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2211.00 TO NODE 2210.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1095.00 | DOWNSTREAM(FEET) = | 843.40 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 880.30  | CHANNEL SLOPE =    | 0.2858 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1915 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.84  
FLOW VELOCITY(FEET/SEC) = 5.06 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.90 Tc(MIN.) = 13.51  
LONGEST FLOWPATH FROM NODE 2213.00 TO NODE 2210.00 = 1628.20 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2211.00 TO NODE 2210.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.856 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4430  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4436  
SUBAREA AREA(ACRES) = 8.57 SUBAREA RUNOFF(CFS) = 18.44  
TOTAL AREA(ACRES) = 12.07 TOTAL RUNOFF(CFS) = 26.01  
TC(MIN.) = 13.51

\*\*\*\*\*

MERR221.TXT

FLOW PROCESS FROM NODE 2210.00 TO NODE 22.10 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<  
-----

-----  
ELEVATION DATA: UPSTREAM(FEET) = 831.00 DOWNSTREAM(FEET) = 827.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.60  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.01  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 13.58  
LONGEST FLOWPATH FROM NODE 2213.00 TO NODE 22.10 = 1678.20 FEET.  
-----

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 12.07 TC(MIN.) = 13.58  
PEAK FLOW RATE(CFS) = 26.01  
-----

-----  
END OF RATIONAL METHOD ANALYSIS  
-----

□



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003, 1985, 1981 HYDROLOGY MANUAL

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 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
 6390 GREENWICH DRIVE, SUITE 170  
 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 222 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR222.DAT  
 TIME/DATE OF STUDY: 13:06 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 5.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2223.00 TO NODE 2222.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):  
 RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 92.10  
 UPSTREAM ELEVATION(FEET) = 1260.00  
 DOWNSTREAM ELEVATION(FEET) = 1210.00  
 ELEVATION DIFFERENCE(FEET) = 50.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.014  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 -----

MERR222.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.186  
SUBAREA RUNOFF(CFS) = 0.66  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 0.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2222.00 TO NODE 2221.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1210.00 | DOWNSTREAM(FEET) = | 1115.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 382.10  | CHANNEL SLOPE =    | 0.2486  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1795 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.66  
FLOW VELOCITY(FEET/SEC) = 2.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.68 Tc(MIN.) = 8.70  
LONGEST FLOWPATH FROM NODE 2223.00 TO NODE 2221.00 = 474.20 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2222.00 TO NODE 2221.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.452 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4540  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4502  
SUBAREA AREA(ACRES) = 5.99 SUBAREA RUNOFF(CFS) = 17.55  
TOTAL AREA(ACRES) = 6.22 TOTAL RUNOFF(CFS) = 18.07  
TC(MIN.) = 8.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2221.00 TO NODE 2220.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1115.00 | DOWNSTREAM(FEET) = | 885.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 797.90  | CHANNEL SLOPE =    | 0.2883 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1921 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 18.07  
FLOW VELOCITY(FEET/SEC) = 6.43 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.07 Tc(MIN.) = 10.76  
LONGEST FLOWPATH FROM NODE 2223.00 TO NODE 2220.00 = 1272.10 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2221.00 TO NODE 2220.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.623 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4490  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4495  
SUBAREA AREA(ACRES) = 7.16 SUBAREA RUNOFF(CFS) = 18.08  
TOTAL AREA(ACRES) = 13.38 TOTAL RUNOFF(CFS) = 33.82  
TC(MIN.) = 10.76

MERR222.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2220.00 TO NODE 22.20 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 885.00            | DOWNSTREAM(FEET) = | 845.00        |
| FLOW LENGTH(FEET) =              | 235.00            | MANNING'S N =      | 0.024         |
| DEPTH OF FLOW IN                 | 24.0 INCH PIPE IS | 14.9 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 16.55             |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 24.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 33.82             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.24              | Tc(MIN.) =         | 11.00         |
| LONGEST FLOWPATH FROM NODE       | 2223.00 TO NODE   | 22.20 =            | 1507.10 FEET. |

=====

END OF STUDY SUMMARY:

|                     |   |       |            |       |
|---------------------|---|-------|------------|-------|
| TOTAL AREA(ACRES)   | = | 13.38 | TC(MIN.) = | 11.00 |
| PEAK FLOW RATE(CFS) | = | 33.82 |            |       |

=====

END OF RATIONAL METHOD ANALYSIS

□





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
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 2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

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 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 223 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR223.DAT  
 TIME/DATE OF STUDY: 13:07 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2232.00 TO NODE 2231.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):  
 RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1240.00  
 DOWNSTREAM ELEVATION(FEET) = 1195.00  
 ELEVATION DIFFERENCE(FEET) = 45.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 -----

MERR223.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.73  
TOTAL AREA(ACRES) = 0.26 TOTAL RUNOFF(CFS) = 0.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2231.00 TO NODE 2230.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|   |              |  |        |
|---|--------------|--|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                                | 1195.00      | DOWNSTREAM(FEET) =                     | 895.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) =                             | 628.00       | CHANNEL SLOPE =                        | 0.4777 |
| SLOPE ADJUSTMENT CURVE USED:                                    |              |  |        |
| EFFECTIVE SLOPE =   | .2228        | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |        |
| NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION |              |  |        |
| CHANNEL FLOW THRU SUBAREA(CFS) =                                | 0.73         |  |        |
| FLOW VELOCITY(FEET/SEC) =                                       | 2.64         | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |        |
| TRAVEL TIME(MIN.) =   | 3.96         | Tc(MIN.) =                             | 10.23  |
| LONGEST FLOWPATH FROM NODE 2232.00 TO NODE 2230.00 =            | 728.00 FEET. |  |        |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2231.00 TO NODE 2230.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|   |        |                       |       |
|---|--------|-----------------------|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =            | 5.813  |                       |       |
| *USER SPECIFIED(SUBAREA):                           |        |                       |       |
| RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = | .4490  |                       |       |
| S. C. S. CURVE NUMBER (AMC II) =                    | 0      |                       |       |
| AREA-AVERAGE RUNOFF COEFFICIENT =                   | 0.4438 |                       |       |
| SUBAREA AREA(ACRES) =                               | 4.67   | SUBAREA RUNOFF(CFS) = | 12.19 |
| TOTAL AREA(ACRES) =                                 | 4.93   | TOTAL RUNOFF(CFS) =   | 12.72 |
| TC(MIN.) =  | 10.23  |                       |       |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2230.00 TO NODE 22.30 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|  |              |                    |        |
|--|--------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 895.00       | DOWNSTREAM(FEET) = | 888.90 |
| FLOW LENGTH(FEET) =                                | 40.00        | MANNING'S N =      | 0.024  |
| DEPTH OF FLOW IN 24.0 INCH PIPE IS                 | 8.7 INCHES   |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 12.40        |                    |        |
| GIVEN PIPE DIAMETER(INCH) =                        | 24.00        | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 12.72        |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.05         | Tc(MIN.) =         | 10.28  |
| LONGEST FLOWPATH FROM NODE 2232.00 TO NODE 22.30 = | 768.00 FEET. |                    |        |

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 4.93 TC(MIN.) = 10.28  
PEAK FLOW RATE(CFS) = 12.72

-----  
END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
6390 GREENWICH DRIVE, SUITE 170  
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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 224 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR224.DAT  
TIME/DATE OF STUDY: 13:09 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2242.00 TO NODE 2241.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1205.00  
DOWNSTREAM ELEVATION(FEET) = 1135.00  
ELEVATION DIFFERENCE(FEET) = 70.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR224.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.42  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2241.00 TO NODE 2240.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 920.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 874.50 CHANNEL SLOPE = 0.2459  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1786 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.42  
FLOW VELOCITY(FEET/SEC) = 2.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 6.16 Tc(MIN.) = 12.42  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2240.00 = 974.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2241.00 TO NODE 2240.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.127  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3330  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3335  
SUBAREA AREA(ACRES) = 5.17 SUBAREA RUNOFF(CFS) = 8.83  
TOTAL AREA(ACRES) = 5.32 TOTAL RUNOFF(CFS) = 9.10  
TC(MIN.) = 12.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2240.00 TO NODE 22.40 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 920.00 DOWNSTREAM(FEET) = 915.00  
FLOW LENGTH(FEET) = 57.50 MANNING'S N = 0.024  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.31  
GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.10  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 12.53  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 22.40 = 1032.00 FEET.

-----

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 5.32 TC(MIN.) = 12.53  
PEAK FLOW RATE(CFS) = 9.10

-----  
END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
 6390 GREENWICH DRIVE, SUITE 170  
 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 22 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR22.DAT  
 TIME/DATE OF STUDY: 13:03 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2203.00 TO NODE 2202.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):  
 RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
 UPSTREAM ELEVATION(FEET) = 1445.00  
 DOWNSTREAM ELEVATION(FEET) = 1405.00  
 ELEVATION DIFFERENCE(FEET) = 40.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.108  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 -----

MERR22.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.105  
SUBAREA RUNOFF(CFS) = 0.57  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2202.00 TO NODE 2201.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1405.00 DOWNSTREAM(FEET) = 890.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1382.20 CHANNEL SLOPE = 0.3726  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2092 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.57  
FLOW VELOCITY(FEET/SEC) = 2.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 8.99 Tc(MIN.) = 15.10  
LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2201.00 = 1477.20 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2202.00 TO NODE 2201.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.520  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4520  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4497  
SUBAREA AREA(ACRES) = 8.69 SUBAREA RUNOFF(CFS) = 17.76  
TOTAL AREA(ACRES) = 8.89 TOTAL RUNOFF(CFS) = 18.07  
TC(MIN.) = 15.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2204.00 TO NODE 2201.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.520  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4570  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4537  
SUBAREA AREA(ACRES) = 10.77 SUBAREA RUNOFF(CFS) = 22.25  
TOTAL AREA(ACRES) = 19.66 TOTAL RUNOFF(CFS) = 40.32  
TC(MIN.) = 15.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2201.00 TO NODE 2200.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 890.00 DOWNSTREAM(FEET) = 830.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 471.50 CHANNEL SLOPE = 0.1273  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1198 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 40.32  
FLOW VELOCITY(FEET/SEC) = 6.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.18 Tc(MIN.) = 16.29  
LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2200.00 = 1948.70 FEET.



MERR22. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2201.00 TO NODE 2200.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.306  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4280  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4510  
SUBAREA AREA(ACRES) = 2.31 SUBAREA RUNOFF(CFS) = 4.26  
TOTAL AREA(ACRES) = 21.97 TOTAL RUNOFF(CFS) = 42.66  
TC(MIN.) = 16.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2200.00 TO NODE 2200.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

-----  
TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.29  
RAINFALL INTENSITY(INCH/HR) = 4.31  
TOTAL STREAM AREA(ACRES) = 21.97  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 42.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2207.00 TO NODE 2206.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 76.30  
UPSTREAM ELEVATION(FEET) = 1290.00  
DOWNSTREAM ELEVATION(FEET) = 1265.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.474  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.698  
SUBAREA RUNOFF(CFS) = 0.64  
TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 0.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2206.00 TO NODE 2205.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1265.00 DOWNSTREAM(FEET) = 1065.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 461.70 CHANNEL SLOPE = 0.4332  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2180 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.64  
FLOW VELOCITY(FEET/SEC) = 2.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.94 Tc(MIN.) = 8.42  
LONGEST FLOWPATH FROM NODE 2207.00 TO NODE 2205.00 = 538.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2206.00 TO NODE 2205.00 IS CODE = 81

MERR22.TXT

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.590
*USER SPECIFIED(SUBAREA):
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4553
SUBAREA AREA(ACRES) = 4.73 SUBAREA RUNOFF(CFS) = 14.34
TOTAL AREA(ACRES) = 4.94 TOTAL RUNOFF(CFS) = 14.82
TC(MIN.) = 8.42

```

```

*****
FLOW PROCESS FROM NODE 2205.00 TO NODE 2200.00 IS CODE = 53
-----

```

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1065.00 DOWNSTREAM(FEET) = 830.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1125.00 CHANNEL SLOPE = 0.2089
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1644 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 14.82
FLOW VELOCITY(FEET/SEC) = 5.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.36 Tc(MIN.) = 11.78
LONGEST FLOWPATH FROM NODE 2207.00 TO NODE 2200.00 = 1663.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 2205.00 TO NODE 2200.00 IS CODE = 81
-----

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.305
*USER SPECIFIED(SUBAREA):
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4516
SUBAREA AREA(ACRES) = 11.51 SUBAREA RUNOFF(CFS) = 27.48
TOTAL AREA(ACRES) = 16.45 TOTAL RUNOFF(CFS) = 39.41
TC(MIN.) = 11.78

```

```

*****
FLOW PROCESS FROM NODE 2200.00 TO NODE 2200.00 IS CODE = 1
-----

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 11.78
RAINFALL INTENSITY(INCH/HR) = 5.31
TOTAL STREAM AREA(ACRES) = 16.45
PEAK FLOW RATE(CFS) AT CONFLUENCE = 39.41

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 42.66        | 16.29     | 4.306                 | 21.97       |
| 2             | 39.41        | 11.78     | 5.305                 | 16.45       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| MERR22. TXT   |              |           |                       |
|---------------|--------------|-----------|-----------------------|
| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
| 1             | 70.28        | 11.78     | 5.305                 |
| 2             | 74.65        | 16.29     | 4.306                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 74.65 Tc(MIN.) = 16.29  
 TOTAL AREA(ACRES) = 38.42  
 LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2200.00 = 1948.70 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2200.00 TO NODE 22.00 IS CODE = 41

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

-----  
 ELEVATION DATA: UPSTREAM(FEET) = 817.00 DOWNSTREAM(FEET) = 815.00  
 FLOW LENGTH(FEET) = 46.00 MANNING'S N = 0.024  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.51  
 (PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
 AT DEPTH = 0.94 \* DIAMETER)  
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 74.65  
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 16.38  
 LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 22.00 = 1994.70 FEET.

-----  
 END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 38.42 TC(MIN.) = 16.38  
 PEAK FLOW RATE(CFS) = 74.65  
 -----

-----  
 END OF RATIONAL METHOD ANALYSIS  
 -----

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 231 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR231.DAT  
TIME/DATE OF STUDY: 13:11 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2312.00 TO NODE 2311.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1150.00  
DOWNSTREAM ELEVATION(FEET) = 1080.00  
ELEVATION DIFFERENCE(FEET) = 70.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.348

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR231.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.830  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2311.00 TO NODE 2310.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1080.00 | DOWNSTREAM(FEET) = | 815.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 930.00  | CHANNEL SLOPE =    | 0.2849 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1912 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.53  
FLOW VELOCITY(FEET/SEC) = 2.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 6.33 Tc(MIN.) = 11.68  
LONGEST FLOWPATH FROM NODE 2312.00 TO NODE 2310.00 = 1030.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2311.00 TO NODE 2310.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.336 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4280  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4289  
SUBAREA AREA(ACRES) = 4.32 SUBAREA RUNOFF(CFS) = 9.87  
TOTAL AREA(ACRES) = 4.45 TOTAL RUNOFF(CFS) = 10.19  
TC(MIN.) = 11.68

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2310.00 TO NODE 23.10 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|  |             |                    |               |
|--|-------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) =           | 815.00      | DOWNSTREAM(FEET) = | 813.00        |
| FLOW LENGTH(FEET) =                        | 46.00       | MANNING'S N =      | 0.024         |
| DEPTH OF FLOW IN 24.0 INCH PIPE IS         | 10.9 INCHES |                    |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =            | 7.38        |                    |               |
| GIVEN PIPE DIAMETER(INCH) =                | 24.00       | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                           | 10.19       |                    |               |
| PIPE TRAVEL TIME(MIN.) =                   | 0.10        | Tc(MIN.) =         | 11.78         |
| LONGEST FLOWPATH FROM NODE 2312.00 TO NODE | 23.10       | =                  | 1076.00 FEET. |

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 4.45 TC(MIN.) = 11.78  
PEAK FLOW RATE(CFS) = 10.19

-----  
END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

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2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 232 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR232.DAT  
TIME/DATE OF STUDY: 13:13 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2323.00 TO NODE 2322.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1350.00  
DOWNSTREAM ELEVATION(FEET) = 1300.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.348

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!



MERR232.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.830  
SUBAREA RUNOFF(CFS) = 1.18  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 1.18

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2322.00 TO NODE 2321.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |  |                        |
|-------------------------------------|---------|--|------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1300.00 | DOWNSTREAM(FEET) =                     | 950.00                 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 715.00  | CHANNEL SLOPE =                        | 0.4895                 |
| SLOPE ADJUSTMENT CURVE USED:        |         |  |                        |
| EFFECTIVE SLOPE =                   | .2240   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 1.18    |  |                        |
| FLOW VELOCITY(FEET/SEC) =           | 2.80    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| TRAVEL TIME(MIN.) =                 | 4.26    | Tc(MIN.) =                             | 9.61                   |
| LONGEST FLOWPATH FROM NODE          | 2323.00 | TO NODE                                | 2321.00 = 815.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2322.00 TO NODE 2321.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|   |        |                       |      |
|---|--------|-----------------------|------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =            | 6.052  |                       |      |
| *USER SPECIFIED(SUBAREA):                           |        |                       |      |
| RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = | .4600  |                       |      |
| S. C. S. CURVE NUMBER (AMC II) =                    | 0      |                       |      |
| AREA-AVERAGE RUNOFF COEFFICIENT =                   | 0.4600 |                       |      |
| SUBAREA AREA(ACRES) =                               | 2.78   | SUBAREA RUNOFF(CFS) = | 7.74 |
| TOTAL AREA(ACRES) =                                 | 3.07   | TOTAL RUNOFF(CFS) =   | 8.55 |
| TC(MIN.) =  | 9.61   |                       |      |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2321.00 TO NODE 2320.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |  |                         |
|-------------------------------------|---------|--|-------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 950.00  | DOWNSTREAM(FEET) =                     | 810.00                  |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 715.00  | CHANNEL SLOPE =                        | 0.1958                  |
| SLOPE ADJUSTMENT CURVE USED:        |         |  |                         |
| EFFECTIVE SLOPE =                   | .1579   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                         |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 8.55    |  |                         |
| FLOW VELOCITY(FEET/SEC) =           | 4.55    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                         |
| TRAVEL TIME(MIN.) =                 | 2.62    | Tc(MIN.) =                             | 12.23                   |
| LONGEST FLOWPATH FROM NODE          | 2323.00 | TO NODE                                | 2320.00 = 1530.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2321.00 TO NODE 2320.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|   |        |                       |       |
|---|--------|-----------------------|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =            | 5.180  |                       |       |
| *USER SPECIFIED(SUBAREA):                           |        |                       |       |
| RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = | .4200  |                       |       |
| S. C. S. CURVE NUMBER (AMC II) =                    | 0      |                       |       |
| AREA-AVERAGE RUNOFF COEFFICIENT =                   | 0.4355 |                       |       |
| SUBAREA AREA(ACRES) =                               | 4.83   | SUBAREA RUNOFF(CFS) = | 10.51 |
| TOTAL AREA(ACRES) =                                 | 7.90   | TOTAL RUNOFF(CFS) =   | 17.82 |
| TC(MIN.) =  | 12.23  |                       |       |

\*\*\*\*\*

FLOW PROCESS FROM NODE 2320.00 TO NODE 23.20 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<  
-----

-----  
ELEVATION DATA: UPSTREAM(FEET) = 810.00 DOWNSTREAM(FEET) = 808.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.16  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 17.82  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 12.33  
LONGEST FLOWPATH FROM NODE 2323.00 TO NODE 23.20 = 1580.00 FEET.  
-----

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 7.90 TC(MIN.) = 12.33  
PEAK FLOW RATE(CFS) = 17.82  
-----

-----  
END OF RATIONAL METHOD ANALYSIS  
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\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003, 1985, 1981 HYDROLOGY MANUAL  
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 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
 6390 GREENWICH DRIVE, SUITE 170  
 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 233 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR233.DAT  
 TIME/DATE OF STUDY: 13:15 09/28/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2333.00 TO NODE 2332.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 -----

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1270.00  
 DOWNSTREAM ELEVATION(FEET) = 1195.00  
 ELEVATION DIFFERENCE(FEET) = 75.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.348

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR233.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.830  
SUBAREA RUNOFF(CFS) = 1.30  
TOTAL AREA(ACRES) = 0.32 TOTAL RUNOFF(CFS) = 1.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2332.00 TO NODE 2331.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1195.00 | DOWNSTREAM(FEET) = | 925.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 515.00  | CHANNEL SLOPE =    | 0.5243 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2262 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.30  
FLOW VELOCITY(FEET/SEC) = 2.91 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.95 Tc(MIN.) = 8.30  
LONGEST FLOWPATH FROM NODE 2333.00 TO NODE 2331.00 = 615.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2332.00 TO NODE 2331.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.650 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4600  
SUBAREA AREA(ACRES) = 2.23 SUBAREA RUNOFF(CFS) = 6.82  
TOTAL AREA(ACRES) = 2.55 TOTAL RUNOFF(CFS) = 7.80  
TC(MIN.) = 8.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2331.00 TO NODE 2330.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 925.00 | DOWNSTREAM(FEET) = | 810.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 700.00 | CHANNEL SLOPE =    | 0.1643 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1421 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.80  
FLOW VELOCITY(FEET/SEC) = 4.18 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.79 Tc(MIN.) = 11.09  
LONGEST FLOWPATH FROM NODE 2333.00 TO NODE 2330.00 = 1315.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2331.00 TO NODE 2330.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.517 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4320  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4415  
SUBAREA AREA(ACRES) = 4.94 SUBAREA RUNOFF(CFS) = 11.77  
TOTAL AREA(ACRES) = 7.49 TOTAL RUNOFF(CFS) = 18.24  
TC(MIN.) = 11.09

\*\*\*\*\*

FLOW PROCESS FROM NODE 2330.00 TO NODE 23.30 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<  
-----

-----  
ELEVATION DATA: UPSTREAM(FEET) = 810.00 DOWNSTREAM(FEET) = 808.00  
FLOW LENGTH(FEET) = 54.00 MANNING'S N = 0.024  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.48  
(PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
AT DEPTH = 0.94 \* DIAMETER)  
GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 18.24  
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 11.23  
LONGEST FLOWPATH FROM NODE 2333.00 TO NODE 23.30 = 1369.00 FEET.  
-----

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 7.49 TC(MIN.) = 11.23  
PEAK FLOW RATE(CFS) = 18.24  
-----

-----  
END OF RATIONAL METHOD ANALYSIS  
-----

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 234 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR234.DAT  
TIME/DATE OF STUDY: 13:16 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2343.00 TO NODE 2342.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3410  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1360.00  
DOWNSTREAM ELEVATION(FEET) = 1305.00  
ELEVATION DIFFERENCE(FEET) = 55.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.342

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!



MERR234.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.911  
SUBAREA RUNOFF(CFS) = 0.33  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.33

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2342.00 TO NODE 2341.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1305.00 | DOWNSTREAM(FEET) = | 890.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1720.00 | CHANNEL SLOPE =    | 0.2413 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1771 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.33  
FLOW VELOCITY(FEET/SEC) = 2.36 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 12.16 Tc(MIN.) = 18.51  
LONGEST FLOWPATH FROM NODE 2343.00 TO NODE 2341.00 = 1820.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2342.00 TO NODE 2341.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.965 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4510  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4472  
SUBAREA AREA(ACRES) = 3.46 SUBAREA RUNOFF(CFS) = 6.19  
TOTAL AREA(ACRES) = 3.58 TOTAL RUNOFF(CFS) = 6.35  
TC(MIN.) = 18.51

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2341.00 TO NODE 2340.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 890.00 | DOWNSTREAM(FEET) = | 810.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 631.00 | CHANNEL SLOPE =    | 0.1268 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1195 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 6.35  
FLOW VELOCITY(FEET/SEC) = 3.58 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.93 Tc(MIN.) = 21.44  
LONGEST FLOWPATH FROM NODE 2343.00 TO NODE 2340.00 = 2451.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2341.00 TO NODE 2340.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.606 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4294  
SUBAREA AREA(ACRES) = 6.83 SUBAREA RUNOFF(CFS) = 10.34  
TOTAL AREA(ACRES) = 10.41 TOTAL RUNOFF(CFS) = 16.12  
TC(MIN.) = 21.44

MERR234.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2340.00 TO NODE 23.40 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 810.00            | DOWNSTREAM(FEET) = | 808.00        |
| FLOW LENGTH(FEET) =              | 64.00             | MANNING'S N =      | 0.024         |
| DEPTH OF FLOW IN                 | 24.0 INCH PIPE IS | 16.0 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 7.24              |                    |               |
| GIVEN PIPE DIAMETER(INCH) =      | 24.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 16.12             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.15              | Tc(MIN.) =         | 21.59         |
| LONGEST FLOWPATH FROM NODE       | 2343.00 TO NODE   | 23.40 =            | 2515.00 FEET. |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 10.41 TC(MIN.) = 21.59  
PEAK FLOW RATE(CFS) = 16.12

-----  
END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 23 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR23.DAT  
TIME/DATE OF STUDY: 13:10 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2304.00 TO NODE 2303.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1325.00  
DOWNSTREAM ELEVATION(FEET) = 1268.00  
ELEVATION DIFFERENCE(FEET) = 57.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR23.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 2.90  
TOTAL AREA(ACRES) = 1.04 TOTAL RUNOFF(CFS) = 2.90

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2303.00 TO NODE 2301.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1268.00 | DOWNSTREAM(FEET) = | 863.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1070.00 | CHANNEL SLOPE =    | 0.3785 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2102 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.90  
FLOW VELOCITY(FEET/SEC) = 3.66 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.87 Tc(MIN.) = 11.14  
LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 2301.00 = 1170.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2303.00 TO NODE 2301.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.501 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3450  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3456  
SUBAREA AREA(ACRES) = 7.47 SUBAREA RUNOFF(CFS) = 14.18  
TOTAL AREA(ACRES) = 8.51 TOTAL RUNOFF(CFS) = 16.18  
TC(MIN.) = 11.14

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2301.00 TO NODE 2300.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 863.00 | DOWNSTREAM(FEET) = | 808.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 510.00 | CHANNEL SLOPE =    | 0.1078 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1059 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 16.18  
FLOW VELOCITY(FEET/SEC) = 4.60 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.85 Tc(MIN.) = 12.98  
LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 2300.00 = 1680.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2301.00 TO NODE 2300.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.983 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4460  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4113  
SUBAREA AREA(ACRES) = 16.11 SUBAREA RUNOFF(CFS) = 35.81  
TOTAL AREA(ACRES) = 24.62 TOTAL RUNOFF(CFS) = 50.47  
TC(MIN.) = 12.98

\*\*\*\*\*

MERR23.TXT

FLOW PROCESS FROM NODE 2300.00 TO NODE 23.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<  
-----

-----  
ELEVATION DATA: UPSTREAM(FEET) = 808.00 DOWNSTREAM(FEET) = 801.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 19.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.17  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 50.47  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 13.11  
LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 23.00 = 1780.00 FEET.  
-----

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 24.62 TC(MIN.) = 13.11  
PEAK FLOW RATE(CFS) = 50.47  
-----

-----  
END OF RATIONAL METHOD ANALYSIS  
-----

□



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

Fuscoe Engineering, San Diego  
6390 Greenwich Dr. Suite 170  
San Diego, CA 92122  
858-554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 24.1 \*  
\* 2469.01A - MARCH 2007 \*  
\*\*\*\*\*

FILE NAME: MERR241.DAT  
TIME/DATE OF STUDY: 09:55 02/19/2007

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2412.00 TO NODE 2411.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 91.00  
UPSTREAM ELEVATION(FEET) = 987.00  
DOWNSTREAM ELEVATION(FEET) = 953.00  
ELEVATION DIFFERENCE(FEET) = 34.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.420

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!



MERR241.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.754  
SUBAREA RUNOFF(CFS) = 0.29  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2411.00 TO NODE 2410.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 953.00  | DOWNSTREAM(FEET) = | 805.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1161.00 | CHANNEL SLOPE =    | 0.1275 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1200 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.29  
FLOW VELOCITY(FEET/SEC) = 1.94 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 9.98 Tc(MIN.) = 15.40  
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 2410.00 = 1252.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2410.00 TO NODE 24.10 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.465 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 10.58 SUBAREA RUNOFF(CFS) = 19.84  
TOTAL AREA(ACRES) = 10.66 TOTAL RUNOFF(CFS) = 19.99  
TC(MIN.) = 15.40

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 10.66 TC(MIN.) = 15.40  
PEAK FLOW RATE(CFS) = 19.99

-----  
END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 242 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR242.DAT  
TIME/DATE OF STUDY: 13:21 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2422.00 TO NODE 2421.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1075.00  
DOWNSTREAM ELEVATION(FEET) = 1015.00  
ELEVATION DIFFERENCE(FEET) = 60.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.682  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR242.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.492  
SUBAREA RUNOFF(CFS) = 1.18  
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 1.18

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2421.00 TO NODE 2420.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |  |                         |
|-------------------------------------|---------|--|-------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1015.00 | DOWNSTREAM(FEET) =                     | 815.00                  |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1080.00 | CHANNEL SLOPE =                        | 0.1852                  |
| SLOPE ADJUSTMENT CURVE USED:        |         |  |                         |
| EFFECTIVE SLOPE =                   | .1526   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                         |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 1.18    |  |                         |
| FLOW VELOCITY(FEET/SEC) =           | 2.31    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                         |
| TRAVEL TIME(MIN.) =                 | 7.79    | Tc(MIN.) =                             | 13.48                   |
| LONGEST FLOWPATH FROM NODE          | 2422.00 | TO NODE                                | 2420.00 = 1180.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2421.00 TO NODE 2420.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|   |        |                       |       |
|---|--------|-----------------------|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =        | 4.865  |                       |       |
| *USER SPECIFIED(SUBAREA):                       |        |                       |       |
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = | .4290  |                       |       |
| S. C. S. CURVE NUMBER (AMC II) =                | 0      |                       |       |
| AREA-AVERAGE RUNOFF COEFFICIENT =               | 0.4287 |                       |       |
| SUBAREA AREA(ACRES) =                           | 8.69   | SUBAREA RUNOFF(CFS) = | 18.14 |
| TOTAL AREA(ACRES) =                             | 9.02   | TOTAL RUNOFF(CFS) =   | 18.81 |
| TC(MIN.) =                                      | 13.48  |                       |       |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2420.00 TO NODE 24.20 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

|   |         |                    |                       |
|---|---------|--------------------|-----------------------|
| ELEVATION DATA: UPSTREAM(FEET) =  | 806.00  | DOWNSTREAM(FEET) = | 802.00                |
| FLOW LENGTH(FEET) =   | 36.00   | MANNING'S N =      | 0.024                 |
| ASSUME FULL-FLOWING PIPELINE  |         |                    |                       |
| PIPE-FLOW VELOCITY(FEET/SEC.) =   | 11.22   |                    |                       |
| (PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW<br>AT DEPTH = 0.94 * DIAMETER) |         |                    |                       |
| GIVEN PIPE DIAMETER(INCH) =   | 18.00   | NUMBER OF PIPES =  | 1                     |
| PIPE-FLOW(CFS) =  | 18.81   |                    |                       |
| PIPE TRAVEL TIME(MIN.) =  | 0.05    | Tc(MIN.) =         | 13.53                 |
| LONGEST FLOWPATH FROM NODE  | 2422.00 | TO NODE            | 24.20 = 1216.00 FEET. |

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 9.02 TC(MIN.) = 13.53  
PEAK FLOW RATE(CFS) = 18.81

-----  
END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
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Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 24 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR24.DAT  
TIME/DATE OF STUDY: 13:19 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2403.00 TO NODE 2402.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1360.00  
DOWNSTREAM ELEVATION(FEET) = 1310.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.212

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

MERR24.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.978  
SUBAREA RUNOFF(CFS) = 1.36  
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 1.36

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2402.00 TO NODE 2401.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1310.00 | DOWNSTREAM(FEET) = | 1130.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 305.00  | CHANNEL SLOPE =    | 0.5902  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2295 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.36  
FLOW VELOCITY(FEET/SEC) = 2.97 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.71 Tc(MIN.) = 6.92  
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 2401.00 = 400.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2402.00 TO NODE 2401.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 7.477 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4600  
SUBAREA AREA(ACRES) = 1.82 SUBAREA RUNOFF(CFS) = 6.26  
TOTAL AREA(ACRES) = 2.15 TOTAL RUNOFF(CFS) = 7.39  
TC(MIN.) = 6.92

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2401.00 TO NODE 2400.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1130.00 | DOWNSTREAM(FEET) = | 805.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1330.00 | CHANNEL SLOPE =    | 0.2444 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1781 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.39  
FLOW VELOCITY(FEET/SEC) = 4.60 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.82 Tc(MIN.) = 11.74  
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 2400.00 = 1730.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2401.00 TO NODE 2400.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.318 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4430  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4441  
SUBAREA AREA(ACRES) = 31.33 SUBAREA RUNOFF(CFS) = 73.81  
TOTAL AREA(ACRES) = 33.48 TOTAL RUNOFF(CFS) = 79.07  
TC(MIN.) = 11.74

\*\*\*\*\*

MERR24.TXT

FLOW PROCESS FROM NODE 2400.00 TO NODE 24.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<  
-----

-----  
ELEVATION DATA: UPSTREAM(FEET) = 805.00 DOWNSTREAM(FEET) = 803.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.024  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.69  
(PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
AT DEPTH = 0.94 \* DIAMETER)  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 79.07  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 11.82  
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 24.00 = 1780.00 FEET.  
-----

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 33.48 TC(MIN.) = 11.82  
PEAK FLOW RATE(CFS) = 79.07  
-----

-----  
END OF RATIONAL METHOD ANALYSIS  
-----

□





Job Name:  
Merriam Mountains - Existing Hydrology

Date:  
October 2006

Job #:  
2469.01A

Run Name:  
MERR25  
Page 1

| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | Runoff<br>Coeff. | Area<br>(ac.) | Comments        |
|--------------|--------|------|------------------|------------------|------------------|------------------|---------------|-----------------|
| 2532         | 2531.8 | 2    | 1,315.0          | 1,300.0          | 75.0             | 0.25             | 0.36          |                 |
| 2531.8       | 2531.6 | 5    | 1,295.0          | 1,250.0          | 300.0            |                  |               |                 |
| 2531.8       | 2531.6 | 8    |                  |                  |                  | 0.25             | 2.59          |                 |
| 2531.6       | 2531.4 | 5    | 1,250.0          | 1,195.0          | 600.0            |                  |               |                 |
| 2531.6       | 2531.4 | 8    |                  |                  |                  | 0.25             | 6.81          |                 |
| 2531.4       | 2531   | 5    | 1,195.0          | 1,170.0          | 525.0            |                  |               |                 |
| 2531.4       | 2531   | 8    |                  |                  |                  | 0.25             | 19.66         |                 |
| 2531         | 2530   | 5    | 1,170.0          | 915.0            | 1,765.0          |                  |               |                 |
| 2531         | 2530   | 8    |                  |                  |                  | 0.27             | 74.78         |                 |
| 2530         | 2502   | 5    | 915.0            | 835.0            | 1,820.0          |                  |               | L=1820*ADD      |
| 2502         | 2502   | 10   |                  |                  |                  |                  |               | Memory Bank     |
| 2506         | 2505.8 | 2    | 1,330.0          | 1,315.0          | 75.0             | 0.25             | 0.67          |                 |
| 2505.8       | 2505.6 | 5    | 1,315.0          | 1,285.0          | 300.0            |                  |               |                 |
| 2505.8       | 2505.6 | 8    |                  |                  |                  | 0.29             | 1.87          |                 |
| 2505.6       | 2505.4 | 5    | 1,285.0          | 1,220.0          | 600.0            |                  |               |                 |
| 2505.6       | 2505.4 | 8    |                  |                  |                  | 0.26             | 8.11          |                 |
| 2505.4       | 2505   | 5    | 1,220.0          | 1,105.0          | 815.0            |                  |               |                 |
| 2505.4       | 2505   | 8    |                  |                  |                  | 0.31             | 54.68         |                 |
| 2505         | 2504   | 5    | 1,105.0          | 885.0            | 1,775.0          |                  |               |                 |
| 2505         | 2504   | 8    |                  |                  |                  | 0.42             | 88.48         |                 |
| 2504         | 2504   | 1    |                  |                  |                  |                  |               | 1 of 2          |
| 2521         | 2520.8 | 2    | 1,400.0          | 1,375.0          | 75.0             | 0.35             | 0.26          |                 |
| 2520.8       | 2520.6 | 5    | 1,375.0          | 1,290.0          | 300.0            |                  |               |                 |
| 2520.8       | 2520.6 | 8    |                  |                  |                  | 0.33             | 3.33          |                 |
| 2520.6       | 2520.4 | 5    | 1,290.0          | 1,120.0          | 680.0            |                  |               | L= 680          |
| 2520.6       | 2520.4 | 8    |                  |                  |                  | 0.34             | 17.84         |                 |
| 2520.4       | 2520   | 5    | 1,120.0          | 935.0            | 1,225.0          |                  |               | L=1225          |
| 2520.4       | 2520   | 8    |                  |                  |                  | 0.43             | 53.58         |                 |
| 2520         | 2504   | 5    | 935.0            | 885.0            | 590.0            |                  |               |                 |
| 2504         | 2504   | 1    |                  |                  |                  |                  |               | 2 of 2          |
| 2504         | 2502   | 5    | 885.0            | 835.0            | 1,655.0          |                  |               | L= 1655         |
| 2502         | 2502   | 11   |                  |                  |                  |                  |               | Add Memory Bank |
| 2502         | 2501   | 5    | 835.0            | 825.0            | 475.0            |                  |               |                 |
| 2501         | 2501   | 1    |                  |                  |                  |                  |               | 1 of 2          |
| 2511         | 2510.8 | 2    | 1,180.0          | 1,155.0          | 75.0             | 0.38             | 0.14          |                 |
| 2510.8       | 2510.6 | 5    | 1,155.0          | 1,070.0          | 300.0            |                  |               |                 |
| 2510.8       | 2510.6 | 8    |                  |                  |                  | 0.38             | 1.86          |                 |
| 2510.6       | 2510.4 | 5    | 1,070.0          | 955.0            | 600.0            |                  |               |                 |
| 2510.6       | 2510.4 | 8    |                  |                  |                  | 0.38             | 10.41         |                 |
| 2510.4       | 2510   | 5    | 955.0            | 885.0            | 440.0            |                  |               |                 |
| 2510.4       | 2510   | 8    |                  |                  |                  | 0.38             | 16.1          |                 |
| 2510         | 2501   | 5    | 885.0            | 825.0            | 1,010.0          |                  |               |                 |
| 2501         | 2501   | 1    |                  |                  |                  |                  |               | 2 of 2          |
| 2501         | 25.2   | 5    | 825.0            | 815.0            | 660.0            |                  |               |                 |







\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 25 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR25.DAT  
TIME/DATE OF STUDY: 13:39 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2532.00 TO NODE 2531.80 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1315.00  
DOWNSTREAM ELEVATION(FEET) = 1300.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
SUBAREA RUNOFF(CFS) = 0.73  
TOTAL AREA(ACRES) = 0.36 TOTAL RUNOFF(CFS) = 0.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.80 TO NODE 2531.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1295.00 DOWNSTREAM(FEET) = 1250.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1500  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1350 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.73  
FLOW VELOCITY(FEET/SEC) = 2.06 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.43 Tc(MIN.) = 8.58  
LONGEST FLOWPATH FROM NODE 2532.00 TO NODE 2531.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.80 TO NODE 2531.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.509  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 2.59 SUBAREA RUNOFF(CFS) = 4.21  
TOTAL AREA(ACRES) = 2.95 TOTAL RUNOFF(CFS) = 4.80  
TC(MIN.) = 8.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.60 TO NODE 2531.40 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1250.00 DOWNSTREAM(FEET) = 1195.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.0917  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0917 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.80  
FLOW VELOCITY(FEET/SEC) = 2.86 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.50 Tc(MIN.) = 12.08  
LONGEST FLOWPATH FROM NODE 2532.00 TO NODE 2531.40 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.60 TO NODE 2531.40 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.221  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 6.81 SUBAREA RUNOFF(CFS) = 8.89  
TOTAL AREA(ACRES) = 9.76 TOTAL RUNOFF(CFS) = 12.74  
TC(MIN.) = 12.08

MERR25. TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.40 TO NODE 2531.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1195.00 | DOWNSTREAM(FEET) = | 1170.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 525.00  | CHANNEL SLOPE =    | 0.0476  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0476 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 12.74  
FLOW VELOCITY(FEET/SEC) = 2.85 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.07 Tc(MIN.) = 15.15  
LONGEST FLOWPATH FROM NODE 2532.00 TO NODE 2531.00 = 1500.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.40 TO NODE 2531.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.512 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 19.66 SUBAREA RUNOFF(CFS) = 22.17  
TOTAL AREA(ACRES) = 29.42 TOTAL RUNOFF(CFS) = 33.18  
TC(MIN.) = 15.15

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.00 TO NODE 2530.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1170.00 | DOWNSTREAM(FEET) = | 915.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1765.00 | CHANNEL SLOPE =    | 0.1445 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1313 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 33.18  
FLOW VELOCITY(FEET/SEC) = 6.51 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.52 Tc(MIN.) = 19.66  
LONGEST FLOWPATH FROM NODE 2532.00 TO NODE 2530.00 = 3265.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2531.00 TO NODE 2530.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.813 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2700  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2644  
SUBAREA AREA(ACRES) = 74.78 SUBAREA RUNOFF(CFS) = 76.98  
TOTAL AREA(ACRES) = 104.20 TOTAL RUNOFF(CFS) = 105.02  
TC(MIN.) = 19.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2530.00 TO NODE 2502.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

MERR25. TXT

=====

ELEVATION DATA: UPSTREAM(FEET) = 915.00 DOWNSTREAM(FEET) = 835.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1820.00 CHANNEL SLOPE = 0.0440  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0440 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 105.02  
FLOW VELOCITY(FEET/SEC) = 5.53 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.48 Tc(MIN.) = 25.15  
LONGEST FLOWPATH FROM NODE 2532.00 TO NODE 2502.00 = 5085.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2502.00 TO NODE 2502.00 IS CODE = 10

-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2506.00 TO NODE 2505.80 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1330.00  
DOWNSTREAM ELEVATION(FEET) = 1315.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
SUBAREA RUNOFF(CFS) = 1.35  
TOTAL AREA(ACRES) = 0.67 TOTAL RUNOFF(CFS) = 1.35

\*\*\*\*\*

FLOW PROCESS FROM NODE 2505.80 TO NODE 2505.60 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1315.00 DOWNSTREAM(FEET) = 1285.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1000  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1000 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.35  
FLOW VELOCITY(FEET/SEC) = 1.96 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 8.70  
LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 2505.60 = 375.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2505.80 TO NODE 2505.60 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.449  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2900  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2794  
SUBAREA AREA(ACRES) = 1.87 SUBAREA RUNOFF(CFS) = 3.50  
TOTAL AREA(ACRES) = 2.54 TOTAL RUNOFF(CFS) = 4.58  
Tc(MIN.) = 8.70



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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2505.60 TO NODE 2505.40 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1285.00 | DOWNSTREAM(FEET) = | 1220.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 600.00  | CHANNEL SLOPE =    | 0.1083  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1063 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.58  
FLOW VELOCITY(FEET/SEC) = 3.03 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.30 Tc(MIN.) = 12.01  
LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 2505.40 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2505.60 TO NODE 2505.40 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.241 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2646  
SUBAREA AREA(ACRES) = 8.11 SUBAREA RUNOFF(CFS) = 11.05  
TOTAL AREA(ACRES) = 10.65 TOTAL RUNOFF(CFS) = 14.77  
TC(MIN.) = 12.01

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2505.40 TO NODE 2505.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1220.00 | DOWNSTREAM(FEET) = | 1105.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 815.00  | CHANNEL SLOPE =    | 0.1411  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1291 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 14.77  
FLOW VELOCITY(FEET/SEC) = 4.93 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.75 Tc(MIN.) = 14.76  
LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 2505.00 = 1790.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2505.40 TO NODE 2505.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.588 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3100  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3026  
SUBAREA AREA(ACRES) = 54.68 SUBAREA RUNOFF(CFS) = 77.76  
TOTAL AREA(ACRES) = 65.33 TOTAL RUNOFF(CFS) = 90.69  
TC(MIN.) = 14.76

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2505.00 TO NODE 2504.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

MERR25. TXT

=====

ELEVATION DATA: UPSTREAM(FEET) = 1105.00 DOWNSTREAM(FEET) = 885.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1775.00 CHANNEL SLOPE = 0.1239  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1176 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 90.69  
FLOW VELOCITY(FEET/SEC) = 8.62 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.43 Tc(MIN.) = 18.19  
LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 2504.00 = 3565.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2505.00 TO NODE 2504.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.009  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3701  
SUBAREA AREA(ACRES) = 88.48 SUBAREA RUNOFF(CFS) = 148.97  
TOTAL AREA(ACRES) = 153.81 TOTAL RUNOFF(CFS) = 228.22  
TC(MIN.) = 18.19

\*\*\*\*\*

FLOW PROCESS FROM NODE 2504.00 TO NODE 2504.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.19  
RAINFALL INTENSITY(INCH/HR) = 4.01  
TOTAL STREAM AREA(ACRES) = 153.81  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 228.22

\*\*\*\*\*

FLOW PROCESS FROM NODE 2521.00 TO NODE 2520.80 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1400.00  
DOWNSTREAM ELEVATION(FEET) = 1375.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.80  
TOTAL AREA(ACRES) = 0.26 TOTAL RUNOFF(CFS) = 0.80

\*\*\*\*\*

FLOW PROCESS FROM NODE 2520.80 TO NODE 2520.60 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1375.00 DOWNSTREAM(FEET) = 1290.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.2833  
SLOPE ADJUSTMENT CURVE USED:

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EFFECTIVE SLOPE = .1908 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.80  
FLOW VELOCITY(FEET/SEC) = 2.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 7.47  
LONGEST FLOWPATH FROM NODE 2521.00 TO NODE 2520.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2520.80 TO NODE 2520.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.117  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3300  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3314  
SUBAREA AREA(ACRES) = 3.33 SUBAREA RUNOFF(CFS) = 7.82  
TOTAL AREA(ACRES) = 3.59 TOTAL RUNOFF(CFS) = 8.47  
TC(MIN.) = 7.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2520.60 TO NODE 2520.40 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1290.00 DOWNSTREAM(FEET) = 1120.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 680.00 CHANNEL SLOPE = 0.2500  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1800 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.47  
FLOW VELOCITY(FEET/SEC) = 4.84 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.34 Tc(MIN.) = 9.81  
LONGEST FLOWPATH FROM NODE 2521.00 TO NODE 2520.40 = 1055.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2520.60 TO NODE 2520.40 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.969  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3400  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3386  
SUBAREA AREA(ACRES) = 17.84 SUBAREA RUNOFF(CFS) = 36.21  
TOTAL AREA(ACRES) = 21.43 TOTAL RUNOFF(CFS) = 43.31  
TC(MIN.) = 9.81

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2520.40 TO NODE 2520.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1120.00 DOWNSTREAM(FEET) = 935.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1225.00 CHANNEL SLOPE = 0.1510  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1355 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 43.31  
FLOW VELOCITY(FEET/SEC) = 7.23 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.82 Tc(MIN.) = 12.64

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LONGEST FLOWPATH FROM NODE 2521.00 TO NODE 2520.00 = 2280.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2520.40 TO NODE 2520.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.071
\*USER SPECIFIED(SUBAREA):
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4039
SUBAREA AREA(ACRES) = 53.58 SUBAREA RUNOFF(CFS) = 116.83
TOTAL AREA(ACRES) = 75.01 TOTAL RUNOFF(CFS) = 153.62
TC(MIN.) = 12.64

\*\*\*\*\*
FLOW PROCESS FROM NODE 2520.00 TO NODE 2504.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 935.00 DOWNSTREAM(FEET) = 885.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 590.00 CHANNEL SLOPE = 0.0847
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .0847 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 153.62
FLOW VELOCITY(FEET/SEC) = 8.72 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.13 Tc(MIN.) = 13.76
LONGEST FLOWPATH FROM NODE 2521.00 TO NODE 2504.00 = 2870.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2504.00 TO NODE 2504.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 13.76
RAINFALL INTENSITY(INCH/HR) = 4.80
TOTAL STREAM AREA(ACRES) = 75.01
PEAK FLOW RATE(CFS) AT CONFLUENCE = 153.62

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 356.54 Tc(MIN.) = 18.19
TOTAL AREA(ACRES) = 228.82
LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 2504.00 = 3565.00 FEET.

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\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2504.00 TO NODE 2502.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |  |                    |                         |
|-------------------------------------|--|--------------------|-------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 885.00                                       | DOWNSTREAM(FEET) = | 835.00                  |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1655.00                                      | CHANNEL SLOPE =    | 0.0302                  |
| SLOPE ADJUSTMENT CURVE USED:        |  |                    |                         |
| EFFECTIVE SLOPE =                   | .0302 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                    |                         |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 356.54                                       |                    |                         |
| FLOW VELOCITY(FEET/SEC) =           | 6.89 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  |                    |                         |
| TRAVEL TIME(MIN.) =                 | 4.00   | Tc(MIN.) =         | 22.20                   |
| LONGEST FLOWPATH FROM NODE          | 2506.00                                      | TO NODE            | 2502.00 = 5220.00 FEET. |

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2502.00 TO NODE 2502.00 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
 \*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER  | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|--|--------------|-----------|-----------------------|-------------|
| 1  | 356.54       | 22.20     | 3.526                 | 228.82      |
| LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 2502.00 = 5220.00 FEET. |              |           |                       |             |

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER  | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|--|--------------|-----------|-----------------------|-------------|
| 1  | 105.02       | 25.15     | 3.253                 | 104.20      |
| LONGEST FLOWPATH FROM NODE 2532.00 TO NODE 2502.00 = 5085.00 FEET. |              |           |                       |             |

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 449.24       | 22.20     | 3.526                 |
| 2             | 433.99       | 25.15     | 3.253                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 449.24 Tc(MIN.) = 22.20  
 TOTAL AREA(ACRES) = 333.02

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2502.00 TO NODE 2501.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |  |                    |                         |
|-------------------------------------|--|--------------------|-------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 835.00                                       | DOWNSTREAM(FEET) = | 825.00                  |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 475.00                                       | CHANNEL SLOPE =    | 0.0211                  |
| SLOPE ADJUSTMENT CURVE USED:        |  |                    |                         |
| EFFECTIVE SLOPE =                   | .0211 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                    |                         |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 449.24                                       |                    |                         |
| FLOW VELOCITY(FEET/SEC) =           | 6.21 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  |                    |                         |
| TRAVEL TIME(MIN.) =                 | 1.27   | Tc(MIN.) =         | 23.47                   |
| LONGEST FLOWPATH FROM NODE          | 2506.00                                      | TO NODE            | 2501.00 = 5695.00 FEET. |

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2501.00 TO NODE 2501.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 23.47  
RAINFALL INTENSITY(INCH/HR) = 3.40  
TOTAL STREAM AREA(ACRES) = 333.02  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 449.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2511.00 TO NODE 2510.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3800  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1180.00  
DOWNSTREAM ELEVATION(FEET) = 1155.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.210  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.980  
SUBAREA RUNOFF(CFS) = 0.48  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.48

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.80 TO NODE 2510.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1155.00 DOWNSTREAM(FEET) = 1070.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.2833  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1908 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.48  
FLOW VELOCITY(FEET/SEC) = 2.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 7.25  
LONGEST FLOWPATH FROM NODE 2511.00 TO NODE 2510.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.80 TO NODE 2510.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.254  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3800  
SUBAREA AREA(ACRES) = 1.86 SUBAREA RUNOFF(CFS) = 5.13  
TOTAL AREA(ACRES) = 2.00 TOTAL RUNOFF(CFS) = 5.51  
TC(MIN.) = 7.25

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.60 TO NODE 2510.40 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1070.00 DOWNSTREAM(FEET) = 955.00

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CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.1917  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1558 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 5.51  
FLOW VELOCITY(FEET/SEC) = 3.90 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.56 Tc(MIN.) = 9.82  
LONGEST FLOWPATH FROM NODE 2511.00 TO NODE 2510.40 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.60 TO NODE 2510.40 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.968  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3800  
SUBAREA AREA(ACRES) = 10.41 SUBAREA RUNOFF(CFS) = 23.61  
TOTAL AREA(ACRES) = 12.41 TOTAL RUNOFF(CFS) = 28.14  
TC(MIN.) = 9.82

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.40 TO NODE 2510.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 955.00 DOWNSTREAM(FEET) = 885.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 440.00 CHANNEL SLOPE = 0.1591  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1395 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 28.14  
FLOW VELOCITY(FEET/SEC) = 6.36 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.15 Tc(MIN.) = 10.97  
LONGEST FLOWPATH FROM NODE 2511.00 TO NODE 2510.00 = 1415.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.40 TO NODE 2510.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3800  
SUBAREA AREA(ACRES) = 16.10 SUBAREA RUNOFF(CFS) = 33.99  
TOTAL AREA(ACRES) = 28.51 TOTAL RUNOFF(CFS) = 60.19  
TC(MIN.) = 10.97

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.00 TO NODE 2501.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 885.00 DOWNSTREAM(FEET) = 825.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1010.00 CHANNEL SLOPE = 0.0594  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0594 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 60.19  
FLOW VELOCITY(FEET/SEC) = 5.34 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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 TRAVEL TIME(MIN.) = 3.15 Tc(MIN.) = 14.12  
 LONGEST FLOWPATH FROM NODE 2511.00 TO NODE 2501.00 = 2425.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2501.00 TO NODE 2501.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 14.12  
 RAINFALL INTENSITY(INCH/HR) = 4.72  
 TOTAL STREAM AREA(ACRES) = 28.51  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 60.19

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 449.24       | 23.47     | 3.401                 | 333.02      |
| 2             | 60.19        | 14.12     | 4.720                 | 28.51       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 330.45       | 14.12     | 4.720                 |
| 2             | 492.61       | 23.47     | 3.401                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 492.61 Tc(MIN.) = 23.47  
 TOTAL AREA(ACRES) = 361.53  
 LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 2501.00 = 5695.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2501.00 TO NODE 25.20 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 825.00 DOWNSTREAM(FEET) = 815.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 660.00 CHANNEL SLOPE = 0.0152  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .0152 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 492.61  
 FLOW VELOCITY(FEET/SEC) = 5.43 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 25.50  
 LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 25.20 = 6355.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2530.00 TO NODE 25.20 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.224  
 \*USER SPECIFIED(SUBAREA):  
 RESIDENTIAL (2.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .4700  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3801  
 SUBAREA AREA(ACRES) = 131.22 SUBAREA RUNOFF(CFS) = 198.86  
 TOTAL AREA(ACRES) = 492.75 TOTAL RUNOFF(CFS) = 603.87



TC(MIN. ) = 25.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.20 TO NODE 25.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 815.00 DOWNSTREAM(FEET) = 793.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 949.00 CHANNEL SLOPE = 0.0232  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0232 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 603.87  
FLOW VELOCITY(FEET/SEC) = 7.19 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN. ) = 2.20 Tc(MIN. ) = 27.70  
LONGEST FLOWPATH FROM NODE 2506.00 TO NODE 25.00 = 7304.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.00 TO NODE 25.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.07 TO NODE 25.06 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 84.00  
UPSTREAM ELEVATION(FEET) = 1184.00  
DOWNSTREAM ELEVATION(FEET) = 1162.00  
ELEVATION DIFFERENCE(FEET) = 22.00  
SUBAREA OVERLAND TIME OF FLOW(MIN. ) = 5.207  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.983  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.06 TO NODE 25.05 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1162.00 DOWNSTREAM(FEET) = 1155.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 500.00 CHANNEL SLOPE = 0.0140  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0140 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.53  
FLOW VELOCITY(FEET/SEC) = 0.66 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN. ) = 12.58 Tc(MIN. ) = 17.78  
LONGEST FLOWPATH FROM NODE 25.07 TO NODE 25.05 = 584.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.05 TO NODE 25.05 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.068

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\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 6.15 SUBAREA RUNOFF(CFS) = 10.51  
TOTAL AREA(ACRES) = 6.29 TOTAL RUNOFF(CFS) = 10.75  
TC(MIN.) = 17.78

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.05 TO NODE 25.01 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1155.00 DOWNSTREAM(FEET) = 817.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1196.00 CHANNEL SLOPE = 0.2826  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1907 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 10.75  
FLOW VELOCITY(FEET/SEC) = 5.39 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.70 Tc(MIN.) = 21.48  
LONGEST FLOWPATH FROM NODE 25.07 TO NODE 25.01 = 1780.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.01 TO NODE 25.01 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.601  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .5200  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4988  
SUBAREA AREA(ACRES) = 23.41 SUBAREA RUNOFF(CFS) = 43.84  
TOTAL AREA(ACRES) = 29.70 TOTAL RUNOFF(CFS) = 53.35  
TC(MIN.) = 21.48

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.01 TO NODE 25.01 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 21.48  
RAINFALL INTENSITY(INCH/HR) = 3.60  
TOTAL STREAM AREA(ACRES) = 29.70  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 53.35

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.04 TO NODE 25.03 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 96.00  
UPSTREAM ELEVATION(FEET) = 1300.00  
DOWNSTREAM ELEVATION(FEET) = 1272.00  
ELEVATION DIFFERENCE(FEET) = 28.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.239  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.947  
SUBAREA RUNOFF(CFS) = 0.37  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.03 TO NODE 25.02 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1272.00 DOWNSTREAM(FEET) = 1050.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 582.00 CHANNEL SLOPE = 0.3814  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2108 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.37  
FLOW VELOCITY(FEET/SEC) = 2.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.77 Tc(MIN.) = 9.01  
LONGEST FLOWPATH FROM NODE 25.04 TO NODE 25.02 = 678.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.02 TO NODE 25.02 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.306  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4207  
SUBAREA AREA(ACRES) = 5.10 SUBAREA RUNOFF(CFS) = 13.51  
TOTAL AREA(ACRES) = 5.19 TOTAL RUNOFF(CFS) = 13.77  
TC(MIN.) = 9.01

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.02 TO NODE 25.01 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1050.00 DOWNSTREAM(FEET) = 817.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1482.00 CHANNEL SLOPE = 0.1572  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1386 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 13.77  
FLOW VELOCITY(FEET/SEC) = 4.99 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.95 Tc(MIN.) = 13.96  
LONGEST FLOWPATH FROM NODE 25.04 TO NODE 25.01 = 2160.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.01 TO NODE 25.01 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.755  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4200  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4202  
SUBAREA AREA(ACRES) = 13.52 SUBAREA RUNOFF(CFS) = 27.00  
TOTAL AREA(ACRES) = 18.71 TOTAL RUNOFF(CFS) = 37.39  
TC(MIN.) = 13.96

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\*\*\*\*\*  
 FLOW PROCESS FROM NODE 25.01 TO NODE 25.01 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 13.96  
 RAINFALL INTENSITY(INCH/HR) = 4.76  
 TOTAL STREAM AREA(ACRES) = 18.71  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 37.39

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 53.35        | 21.48     | 3.601                 | 29.70       |
| 2             | 37.39        | 13.96     | 4.755                 | 18.71       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 72.06        | 13.96     | 4.755                 |
| 2             | 81.67        | 21.48     | 3.601                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 81.67 Tc(MIN.) = 21.48  
 TOTAL AREA(ACRES) = 48.41  
 LONGEST FLOWPATH FROM NODE 25.04 TO NODE 25.01 = 2160.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 25.01 TO NODE 25.00 IS CODE = 53  
 -----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 817.00 DOWNSTREAM(FEET) = 793.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 553.00 CHANNEL SLOPE = 0.0434  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .0434 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 81.67  
 FLOW VELOCITY(FEET/SEC) = 5.05 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 1.82 Tc(MIN.) = 23.30  
 LONGEST FLOWPATH FROM NODE 25.04 TO NODE 25.00 = 2713.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 25.00 TO NODE 25.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 81.67        | 23.30     | 3.417                 | 48.41       |

LONGEST FLOWPATH FROM NODE 25.04 TO NODE 25.00 = 2713.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

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1      603.87      27.70      3.057      492.75  
 LONGEST FLOWPATH FROM NODE      2506.00 TO NODE      25.00 = 7304.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 589.78       | 23.30     | 3.417                 |
| 2             | 676.93       | 27.70     | 3.057                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 676.93      Tc(MIN.) = 27.70  
 TOTAL AREA(ACRES) = 541.16

=====

END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 541.16      TC(MIN.) = 27.70  
 PEAK FLOW RATE(CFS) = 676.93

=====

=====

END OF RATIONAL METHOD ANALYSIS

=====

□

APPENDIX A

AES  
Rational Method Hydrology

Existing Condition

BASIN C



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

(c) Copyright 1982-2004 Advanced Engineering Software (aes)  
Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC  
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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 26 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR26.DAT  
TIME/DATE OF STUDY: 13:32 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2604.00 TO NODE 2603.80 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4210  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1410.00  
DOWNSTREAM ELEVATION(FEET) = 1395.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.913

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!



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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 4.58  
TOTAL AREA(ACRES) = 1.18 TOTAL RUNOFF(CFS) = 4.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.80 TO NODE 2603.60 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1395.00 DOWNSTREAM(FEET) = 1365.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1000  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1000 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.58  
FLOW VELOCITY(FEET/SEC) = 2.94 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.70 Tc(MIN.) = 6.61  
LONGEST FLOWPATH FROM NODE 2604.00 TO NODE 2603.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.80 TO NODE 2603.60 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.699  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4470  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4398  
SUBAREA AREA(ACRES) = 3.09 SUBAREA RUNOFF(CFS) = 10.63  
TOTAL AREA(ACRES) = 4.27 TOTAL RUNOFF(CFS) = 14.46  
TC(MIN.) = 6.61

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.60 TO NODE 2603.40 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1365.00 DOWNSTREAM(FEET) = 1325.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.0667  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0667 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 14.46  
FLOW VELOCITY(FEET/SEC) = 3.52 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.84 Tc(MIN.) = 9.46  
LONGEST FLOWPATH FROM NODE 2604.00 TO NODE 2603.40 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.60 TO NODE 2603.40 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.114  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3230  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3493  
SUBAREA AREA(ACRES) = 14.67 SUBAREA RUNOFF(CFS) = 28.97  
TOTAL AREA(ACRES) = 18.94 TOTAL RUNOFF(CFS) = 40.45  
TC(MIN.) = 9.46

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.40 TO NODE 2603.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1325.00 | DOWNSTREAM(FEET) = | 1230.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 794.00  | CHANNEL SLOPE =    | 0.1196  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1147 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 40.45  
FLOW VELOCITY(FEET/SEC) = 6.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.03 Tc(MIN.) = 11.49  
LONGEST FLOWPATH FROM NODE 2604.00 TO NODE 2603.00 = 1769.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.40 TO NODE 2603.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.392 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3290  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3350  
SUBAREA AREA(ACRES) = 44.85 SUBAREA RUNOFF(CFS) = 79.56  
TOTAL AREA(ACRES) = 63.79 TOTAL RUNOFF(CFS) = 115.23  
TC(MIN.) = 11.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.00 TO NODE 2602.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1230.00 | DOWNSTREAM(FEET) = | 1175.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1365.00 | CHANNEL SLOPE =    | 0.0403  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0403 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 115.23  
FLOW VELOCITY(FEET/SEC) = 5.46 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.17 Tc(MIN.) = 15.66  
LONGEST FLOWPATH FROM NODE 2604.00 TO NODE 2602.00 = 3134.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2603.00 TO NODE 2602.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.416 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2550  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3034  
SUBAREA AREA(ACRES) = 41.75 SUBAREA RUNOFF(CFS) = 47.02  
TOTAL AREA(ACRES) = 105.54 TOTAL RUNOFF(CFS) = 141.41  
TC(MIN.) = 15.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2602.00 TO NODE 2601.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

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=====

ELEVATION DATA: UPSTREAM(FEET) = 1175.00 DOWNSTREAM(FEET) = 1135.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1135.00 CHANNEL SLOPE = 0.0352  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0352 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 141.41  
FLOW VELOCITY(FEET/SEC) = 5.47 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.46 Tc(MIN.) = 19.12  
LONGEST FLOWPATH FROM NODE 2604.00 TO NODE 2601.00 = 4269.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2602.00 TO NODE 2601.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.883  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2896  
SUBAREA AREA(ACRES) = 36.58 SUBAREA RUNOFF(CFS) = 35.51  
TOTAL AREA(ACRES) = 142.12 TOTAL RUNOFF(CFS) = 159.83  
TC(MIN.) = 19.12

\*\*\*\*\*

FLOW PROCESS FROM NODE 2601.00 TO NODE 26.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 970.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1405.00 CHANNEL SLOPE = 0.1174  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1131 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 159.83  
FLOW VELOCITY(FEET/SEC) = 10.20 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.30 Tc(MIN.) = 21.41  
LONGEST FLOWPATH FROM NODE 2604.00 TO NODE 26.00 = 5674.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2601.00 TO NODE 26.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.609  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .3800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3063  
SUBAREA AREA(ACRES) = 32.13 SUBAREA RUNOFF(CFS) = 44.06  
TOTAL AREA(ACRES) = 174.25 TOTAL RUNOFF(CFS) = 192.62  
TC(MIN.) = 21.41

-----

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 174.25 TC(MIN.) = 21.41  
PEAK FLOW RATE(CFS) = 192.62

-----

END OF RATIONAL METHOD ANALYSIS

□



Job Name:  
Merriam Mountains - Existing Hydrology

Date:  
October 2006

Job #:  
2469.01A

Run Name:  
MERR27  
Page 1

| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | Runoff<br>Coeff. | Area<br>(ac.) | Comments |
|--------------|------|------|------------------|------------------|------------------|------------------|---------------|----------|
| 2775         | 2774 | 2    | 1,540.0          | 1,520.0          | 75.0             | 0.35             | 0.55          |          |
| 2774         | 2773 | 5    | 1,520.0          | 1,480.0          | 300.0            |                  |               |          |
| 2774         | 2773 | 8    |                  |                  |                  | 0.35             | 2.97          |          |
| 2773         | 2772 | 5    | 1,480.0          | 1,415.0          | 600.0            |                  |               |          |
| 2773         | 2772 | 8    |                  |                  |                  | 0.35             | 10.84         |          |
| 2772         | 2771 | 5    | 1,415.0          | 1,300.0          | 587.0            |                  |               |          |
| 2772         | 2771 | 8    |                  |                  |                  | 0.34             | 11.52         |          |
| 2771         | 2771 | 1    |                  |                  |                  |                  |               | 1 of 3   |
| 2782         | 2781 | 2    | 1,595.0          | 1,565.0          | 75.0             | 0.35             | 0.22          |          |
| 2781         | 2780 | 5    | 1,565.0          | 1,375.0          | 783.7            |                  |               |          |
| 2781         | 2780 | 8    |                  |                  |                  | 0.34             | 4.37          |          |
| 2780         | 2771 | 5    | 1,375.0          | 1,300.0          | 515.9            |                  |               |          |
| 2780         | 2771 | 8    |                  |                  |                  | 0.28             | 2.61          |          |
| 2771         | 2771 | 1    |                  |                  |                  |                  |               | 2 of 3   |
| 2792         | 2791 | 2    | 1,405.0          | 1,400.0          | 75.0             | 0.35             | 0.52          |          |
| 2791         | 2790 | 5    | 1,400.0          | 1,350.0          | 300.0            |                  |               |          |
| 2791         | 2790 | 8    |                  |                  |                  | 0.28             | 2.06          |          |
| 2790         | 2771 | 5    | 1,350.0          | 1,300.0          | 425.0            |                  |               |          |
| 2790         | 2771 | 8    |                  |                  |                  | 0.25             | 3.49          |          |
| 2771         | 2771 | 1    |                  |                  |                  |                  |               | 3 of 3   |
| 2771         | 2770 | 5    | 1,300.0          | 1,135.0          | 1,408.4          |                  |               |          |
| 2771         | 2770 | 8    |                  |                  |                  | 0.30             | 28.14         |          |
| 2770         | 2761 | 5    | 1,135.0          | 1,040.0          | 670.0            |                  |               |          |
| 2770         | 2761 | 8    |                  |                  |                  | 0.25             | 8.96          |          |
| 2761         | 2761 | 1    |                  |                  |                  |                  |               | 1 of 2   |
| 2765         | 2764 | 2    | 1,445.0          | 1,435.0          | 75.0             | 0.25             | 0.14          |          |
| 2764         | 2763 | 5    | 1,435.0          | 1,395.0          | 300.0            |                  |               |          |
| 2764         | 2763 | 8    |                  |                  |                  | 0.25             | 1.76          |          |
| 2763         | 2762 | 5    | 1,395.0          | 1,305.0          | 585.0            |                  |               |          |
| 2763         | 2762 | 8    |                  |                  |                  | 0.25             | 5.55          |          |
| 2762         | 2761 | 5    | 1,305.0          | 1,040.0          | 1,335.0          |                  |               |          |
| 2762         | 2761 | 8    |                  |                  |                  | 0.25             | 16.86         |          |
| 2761         | 2761 | 1    |                  |                  |                  |                  |               | 2 of 2   |
| 2761         | 2760 | 5    | 1,040.0          | 970.0            | 1,200.0          |                  |               |          |
| 2761         | 2760 | 8    |                  |                  |                  | 0.28             | 21.22         |          |
| 2760         | 2740 | 5    | 970.0            | 930.0            | 930.0            |                  |               |          |
| 2760         | 2740 | 8    |                  |                  |                  | 0.29             | 16.81         |          |
| 2740         | 2740 | 1    |                  |                  |                  |                  |               | 1 of 2   |
| 2752         | 2751 | 2    | 1,155.0          | 1,140.0          | 75.0             | 0.25             | 0.16          |          |
| 2751         | 2750 | 5    | 1,140.0          | 1,035.0          | 440.0            |                  |               |          |
| 2751         | 2750 | 8    |                  |                  |                  | 0.25             | 14.39         |          |
| 2750         | 2740 | 5    | 1,035.0          | 930.0            | 990.0            |                  |               |          |
| 2750         | 2740 | 8    |                  |                  |                  | 0.26             | 14.22         |          |
| 2740         | 2740 | 1    |                  |                  |                  |                  |               | 2 of 2   |





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC.  
6390 GREENWICH DRIVE, SUITE 170  
SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 27 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR27.DAT  
TIME/DATE OF STUDY: 16:30 10/02/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2775.00 TO NODE 2774.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1540.00  
DOWNSTREAM ELEVATION(FEET) = 1520.00  
ELEVATION DIFFERENCE(FEET) = 20.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 1.68  
TOTAL AREA(ACRES) = 0.55 TOTAL RUNOFF(CFS) = 1.68

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2774.00 TO NODE 2773.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |  |                        |
|-------------------------------------|---------|--|------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1520.00 | DOWNSTREAM(FEET) =                     | 1480.00                |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 300.00  | CHANNEL SLOPE =                        | 0.1333                 |
| SLOPE ADJUSTMENT CURVE USED:        |         |  |                        |
| EFFECTIVE SLOPE =                   | .1239   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 1.68    |  |                        |
| FLOW VELOCITY(FEET/SEC) =           | 2.34    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| TRAVEL TIME(MIN.) =                 | 2.13    | Tc(MIN.) =                             | 7.56                   |
| LONGEST FLOWPATH FROM NODE          | 2775.00 | TO NODE                                | 2773.00 = 375.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2774.00 TO NODE 2773.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|   |        |                       |      |
|---|--------|-----------------------|------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =        | 7.063  |                       |      |
| *USER SPECIFIED(SUBAREA):                       |        |                       |      |
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = | .3500  |                       |      |
| S. C. S. CURVE NUMBER (AMC II) =                | 0      |                       |      |
| AREA-AVERAGE RUNOFF COEFFICIENT =               | 0.3500 |                       |      |
| SUBAREA AREA(ACRES) =                           | 2.97   | SUBAREA RUNOFF(CFS) = | 7.34 |
| TOTAL AREA(ACRES) =                             | 3.52   | TOTAL RUNOFF(CFS) =   | 8.70 |
| TC(MIN.) =                                      | 7.56   |                       |      |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2773.00 TO NODE 2772.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |  |                        |
|-------------------------------------|---------|--|------------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1480.00 | DOWNSTREAM(FEET) =                     | 1415.00                |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 600.00  | CHANNEL SLOPE =                        | 0.1083                 |
| SLOPE ADJUSTMENT CURVE USED:        |         |  |                        |
| EFFECTIVE SLOPE =                   | .1063   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 8.70    |  |                        |
| FLOW VELOCITY(FEET/SEC) =           | 3.75    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                        |
| TRAVEL TIME(MIN.) =                 | 2.67    | Tc(MIN.) =                             | 10.23                  |
| LONGEST FLOWPATH FROM NODE          | 2775.00 | TO NODE                                | 2772.00 = 975.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2773.00 TO NODE 2772.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|   |        |                       |       |
|---|--------|-----------------------|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =        | 5.813  |                       |       |
| *USER SPECIFIED(SUBAREA):                       |        |                       |       |
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = | .3500  |                       |       |
| S. C. S. CURVE NUMBER (AMC II) =                | 0      |                       |       |
| AREA-AVERAGE RUNOFF COEFFICIENT =               | 0.3500 |                       |       |
| SUBAREA AREA(ACRES) =                           | 10.84  | SUBAREA RUNOFF(CFS) = | 22.05 |
| TOTAL AREA(ACRES) =                             | 14.36  | TOTAL RUNOFF(CFS) =   | 29.22 |
| TC(MIN.) =                                      | 10.23  |                       |       |

\*\*\*\*\*



FLOW PROCESS FROM NODE 2772.00 TO NODE 2771.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1415.00 DOWNSTREAM(FEET) = 1300.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 587.00 CHANNEL SLOPE = 0.1959
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1580 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 29.22
FLOW VELOCITY(FEET/SEC) = 6.85 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.43 Tc(MIN.) = 11.65
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2771.00 = 1562.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2772.00 TO NODE 2771.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.343
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3400
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3455
SUBAREA AREA(ACRES) = 11.52 SUBAREA RUNOFF(CFS) = 20.93
TOTAL AREA(ACRES) = 25.88 TOTAL RUNOFF(CFS) = 47.78
TC(MIN.) = 11.65

\*\*\*\*\*

FLOW PROCESS FROM NODE 2771.00 TO NODE 2771.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.65
RAINFALL INTENSITY(INCH/HR) = 5.34
TOTAL STREAM AREA(ACRES) = 25.88
PEAK FLOW RATE(CFS) AT CONFLUENCE = 47.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 2782.00 TO NODE 2781.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S. C. S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00
UPSTREAM ELEVATION(FEET) = 1595.00
DOWNSTREAM ELEVATION(FEET) = 1565.00
ELEVATION DIFFERENCE(FEET) = 30.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747
SUBAREA RUNOFF(CFS) = 0.67
TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 0.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 2781.00 TO NODE 2780.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

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=====

ELEVATION DATA: UPSTREAM(FEET) = 1565.00 DOWNSTREAM(FEET) = 1375.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 783.70 CHANNEL SLOPE = 0.2424  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1775 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.67  
FLOW VELOCITY(FEET/SEC) = 2.36 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.54 Tc(MIN.) = 10.96  
LONGEST FLOWPATH FROM NODE 2782.00 TO NODE 2780.00 = 858.70 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2781.00 TO NODE 2780.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.557  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3400  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3405  
SUBAREA AREA(ACRES) = 4.37 SUBAREA RUNOFF(CFS) = 8.26  
TOTAL AREA(ACRES) = 4.59 TOTAL RUNOFF(CFS) = 8.69  
TC(MIN.) = 10.96

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2780.00 TO NODE 2771.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1375.00 DOWNSTREAM(FEET) = 1300.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 515.90 CHANNEL SLOPE = 0.1454  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1319 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.69  
FLOW VELOCITY(FEET/SEC) = 4.18 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 13.02  
LONGEST FLOWPATH FROM NODE 2782.00 TO NODE 2771.00 = 1374.60 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2780.00 TO NODE 2771.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.974  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3186  
SUBAREA AREA(ACRES) = 2.61 SUBAREA RUNOFF(CFS) = 3.63  
TOTAL AREA(ACRES) = 7.20 TOTAL RUNOFF(CFS) = 11.41  
TC(MIN.) = 13.02

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2771.00 TO NODE 2771.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.02  
RAINFALL INTENSITY(INCH/HR) = 4.97

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TOTAL STREAM AREA(ACRES) = 7.20  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2792.00 TO NODE 2791.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1405.00  
DOWNSTREAM ELEVATION(FEET) = 1400.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.212  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.017  
SUBAREA RUNOFF(CFS) = 1.46  
TOTAL AREA(ACRES) = 0.52 TOTAL RUNOFF(CFS) = 1.46

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2791.00 TO NODE 2790.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1400.00 DOWNSTREAM(FEET) = 1350.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1667  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1433 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.46  
FLOW VELOCITY(FEET/SEC) = 2.40 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.08 Tc(MIN.) = 8.29  
LONGEST FLOWPATH FROM NODE 2792.00 TO NODE 2790.00 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2791.00 TO NODE 2790.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.654  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2941  
SUBAREA AREA(ACRES) = 2.06 SUBAREA RUNOFF(CFS) = 3.84  
TOTAL AREA(ACRES) = 2.58 TOTAL RUNOFF(CFS) = 5.05  
TC(MIN.) = 8.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2790.00 TO NODE 2771.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1350.00 DOWNSTREAM(FEET) = 1300.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 425.00 CHANNEL SLOPE = 0.1176  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1132 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 5.05  
FLOW VELOCITY(FEET/SEC) = 3.23 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.19 Tc(MIN.) = 10.48  
LONGEST FLOWPATH FROM NODE 2792.00 TO NODE 2771.00 = 800.00 FEET.

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\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2790.00 TO NODE 2771.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.720  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.2687  
 SUBAREA AREA(ACRES) = 3.49 SUBAREA RUNOFF(CFS) = 4.99  
 TOTAL AREA(ACRES) = 6.07 TOTAL RUNOFF(CFS) = 9.33  
 TC(MIN.) = 10.48

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2771.00 TO NODE 2771.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.48  
 RAINFALL INTENSITY(INCH/HR) = 5.72  
 TOTAL STREAM AREA(ACRES) = 6.07  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.33

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 47.78        | 11.65     | 5.343                 | 25.88       |
| 2             | 11.41        | 13.02     | 4.974                 | 7.20        |
| 3             | 9.33         | 10.48     | 5.720                 | 6.07        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 61.50        | 10.48     | 5.720                 |
| 2             | 66.70        | 11.65     | 5.343                 |
| 3             | 64.00        | 13.02     | 4.974                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 66.70 Tc(MIN.) = 11.65  
 TOTAL AREA(ACRES) = 39.15  
 LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2771.00 = 1562.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2771.00 TO NODE 2770.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1300.00 DOWNSTREAM(FEET) = 1135.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1408.40 CHANNEL SLOPE = 0.1172  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1129 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 66.70  
 FLOW VELOCITY(FEET/SEC) = 7.62 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 3.08 Tc(MIN.) = 14.73

```

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LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2770.00 = 2970.40 FEET.
*****
FLOW PROCESS FROM NODE 2771.00 TO NODE 2770.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.593
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3167
SUBAREA AREA(ACRES) = 28.14 SUBAREA RUNOFF(CFS) = 38.77
TOTAL AREA(ACRES) = 67.29 TOTAL RUNOFF(CFS) = 97.87
TC(MIN.) = 14.73
*****
FLOW PROCESS FROM NODE 2770.00 TO NODE 2761.00 IS CODE = 53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 1040.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 670.00 CHANNEL SLOPE = 0.1418
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1295 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 97.87
FLOW VELOCITY(FEET/SEC) = 9.27 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.20 Tc(MIN.) = 15.94
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2761.00 = 3640.40 FEET.
*****
FLOW PROCESS FROM NODE 2770.00 TO NODE 2761.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.366
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3088
SUBAREA AREA(ACRES) = 8.96 SUBAREA RUNOFF(CFS) = 9.78
TOTAL AREA(ACRES) = 76.25 TOTAL RUNOFF(CFS) = 102.81
TC(MIN.) = 15.94
*****
FLOW PROCESS FROM NODE 2761.00 TO NODE 2761.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 15.94
RAINFALL INTENSITY(INCH/HR) = 4.37
TOTAL STREAM AREA(ACRES) = 76.25
PEAK FLOW RATE(CFS) AT CONFLUENCE = 102.81
*****
FLOW PROCESS FROM NODE 2765.00 TO NODE 2764.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):

```

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NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 1445.00  
 DOWNSTREAM ELEVATION(FEET) = 1435.00  
 ELEVATION DIFFERENCE(FEET) = 10.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
 SUBAREA RUNOFF(CFS) = 0.28  
 TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2764.00 TO NODE 2763.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1435.00 DOWNSTREAM(FEET) = 1395.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1333  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1239 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
 CHANNEL FLOW THRU SUBAREA(CFS) = 0.28  
 FLOW VELOCITY(FEET/SEC) = 1.97 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 2.54 Tc(MIN.) = 8.69  
 LONGEST FLOWPATH FROM NODE 2765.00 TO NODE 2763.00 = 375.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2764.00 TO NODE 2763.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.457  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
 SUBAREA AREA(ACRES) = 1.76 SUBAREA RUNOFF(CFS) = 2.84  
 TOTAL AREA(ACRES) = 1.90 TOTAL RUNOFF(CFS) = 3.07  
 TC(MIN.) = 8.69

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2763.00 TO NODE 2762.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1395.00 DOWNSTREAM(FEET) = 1305.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 585.00 CHANNEL SLOPE = 0.1538  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1369 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 3.07  
 FLOW VELOCITY(FEET/SEC) = 3.01 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 3.24 Tc(MIN.) = 11.93  
 LONGEST FLOWPATH FROM NODE 2765.00 TO NODE 2762.00 = 960.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2763.00 TO NODE 2762.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.264

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\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500
SUBAREA AREA(ACRES) = 5.55 SUBAREA RUNOFF(CFS) = 7.30
TOTAL AREA(ACRES) = 7.45 TOTAL RUNOFF(CFS) = 9.80
TC(MIN.) = 11.93

\*\*\*\*\*
FLOW PROCESS FROM NODE 2762.00 TO NODE 2761.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1305.00 DOWNSTREAM(FEET) = 1040.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1335.00 CHANNEL SLOPE = 0.1985
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1593 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 9.80
FLOW VELOCITY(FEET/SEC) = 4.78 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.66 Tc(MIN.) = 16.58
LONGEST FLOWPATH FROM NODE 2765.00 TO NODE 2761.00 = 2295.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2762.00 TO NODE 2761.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.256
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500
SUBAREA AREA(ACRES) = 16.86 SUBAREA RUNOFF(CFS) = 17.94
TOTAL AREA(ACRES) = 24.31 TOTAL RUNOFF(CFS) = 25.86
TC(MIN.) = 16.58

\*\*\*\*\*
FLOW PROCESS FROM NODE 2761.00 TO NODE 2761.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 16.58
RAINFALL INTENSITY(INCH/HR) = 4.26
TOTAL STREAM AREA(ACRES) = 24.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 25.86

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Row for stream 1.

2 126.08 16.58 MERR27.TXT  
4.256

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 127.67 Tc(MIN.) = 15.94  
TOTAL AREA(ACRES) = 100.56  
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2761.00 = 3640.40 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2761.00 TO NODE 5760.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1040.00 | DOWNSTREAM(FEET) = | 970.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1200.00 | CHANNEL SLOPE =    | 0.0583 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0583 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 127.67  
FLOW VELOCITY(FEET/SEC) = 6.80 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.94 Tc(MIN.) = 18.88  
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 5760.00 = 4840.40 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2761.00 TO NODE 2760.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.914 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2921  
SUBAREA AREA(ACRES) = 21.22 SUBAREA RUNOFF(CFS) = 23.26  
TOTAL AREA(ACRES) = 121.78 TOTAL RUNOFF(CFS) = 139.22  
TC(MIN.) = 18.88

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2760.00 TO NODE 2740.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 970.00 | DOWNSTREAM(FEET) = | 930.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 930.00 | CHANNEL SLOPE =    | 0.0430 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0430 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 139.22  
FLOW VELOCITY(FEET/SEC) = 6.01 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.58 Tc(MIN.) = 21.46  
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2740.00 = 5770.40 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2760.00 TO NODE 2740.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.604 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2900  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2918  
SUBAREA AREA(ACRES) = 16.81 SUBAREA RUNOFF(CFS) = 17.57  
TOTAL AREA(ACRES) = 138.59 TOTAL RUNOFF(CFS) = 145.75



TC(MIN.) = 21.46

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2740.00 TO NODE 2740.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 21.46  
RAINFALL INTENSITY(INCH/HR) = 3.60  
TOTAL STREAM AREA(ACRES) = 138.59  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 145.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2752.00 TO NODE 2751.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1155.00  
DOWNSTREAM ELEVATION(FEET) = 1140.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068  
SUBAREA RUNOFF(CFS) = 0.32  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.32

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2751.00 TO NODE 2750.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1140.00 DOWNSTREAM(FEET) = 1035.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 440.00 CHANNEL SLOPE = 0.2386  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1762 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.32  
FLOW VELOCITY(FEET/SEC) = 2.35 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 9.27  
LONGEST FLOWPATH FROM NODE 2752.00 TO NODE 2750.00 = 515.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2751.00 TO NODE 2750.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.193  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 14.39 SUBAREA RUNOFF(CFS) = 22.28  
TOTAL AREA(ACRES) = 14.55 TOTAL RUNOFF(CFS) = 22.53  
TC(MIN.) = 9.27

\*\*\*\*\*

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FLOW PROCESS FROM NODE 2750.00 TO NODE 2740.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1035.00 DOWNSTREAM(FEET) = 930.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 990.00 CHANNEL SLOPE = 0.1061
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1045 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 22.53
FLOW VELOCITY(FEET/SEC) = 5.11 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.23 Tc(MIN.) = 12.50
LONGEST FLOWPATH FROM NODE 2752.00 TO NODE 2740.00 = 1505.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2750.00 TO NODE 2740.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.107
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2549
SUBAREA AREA(ACRES) = 14.22 SUBAREA RUNOFF(CFS) = 18.88
TOTAL AREA(ACRES) = 28.77 TOTAL RUNOFF(CFS) = 37.46
TC(MIN.) = 12.50

\*\*\*\*\*
FLOW PROCESS FROM NODE 2740.00 TO NODE 2740.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.50
RAINFALL INTENSITY(INCH/HR) = 5.11
TOTAL STREAM AREA(ACRES) = 28.77
PEAK FLOW RATE(CFS) AT CONFLUENCE = 37.46

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 172.18 Tc(MIN.) = 21.46
TOTAL AREA(ACRES) = 167.36
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2740.00 = 5770.40 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2740.00 TO NODE 27.00 IS CODE = 53

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-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 930.00 | DOWNSTREAM(FEET) = | 920.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 385.00 | CHANNEL SLOPE =    | 0.0260 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0260 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 172.18  
FLOW VELOCITY(FEET/SEC) = 5.01 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.28 Tc(MIN.) = 22.74  
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 27.00 = 6155.40 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2740.00 TO NODE 27.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.471 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3300  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2864  
SUBAREA AREA(ACRES) = 3.57 SUBAREA RUNOFF(CFS) = 4.09  
TOTAL AREA(ACRES) = 170.93 TOTAL RUNOFF(CFS) = 172.18  
TC(MIN.) = 22.74  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*  
FLOW PROCESS FROM NODE 27.00 TO NODE 27.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2722.00 TO NODE 2721.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1300.00  
DOWNSTREAM ELEVATION(FEET) = 1295.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.041  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.395  
SUBAREA RUNOFF(CFS) = 0.57  
TOTAL AREA(ACRES) = 0.31 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2721.00 TO NODE 2720.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1295.00 | DOWNSTREAM(FEET) = | 1230.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 430.00  | CHANNEL SLOPE =    | 0.1512  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1356 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.57

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FLOW VELOCITY(FEET/SEC) = 2.06 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.48 Tc(MIN.) = 10.52  
LONGEST FLOWPATH FROM NODE 2722.00 TO NODE 2720.00 = 505.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2721.00 TO NODE 2720.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|   |   |        |
|---|---|--------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR)        | = | 5.709  |
| *USER SPECIFIED(SUBAREA):                     |   |        |
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT | = | .2500  |
| S. C. S. CURVE NUMBER (AMC II)                | = | 0      |
| AREA-AVERAGE RUNOFF COEFFICIENT               | = | 0.2500 |
| SUBAREA AREA(ACRES)                           | = | 6.42   |
| SUBAREA RUNOFF(CFS)                           | = | 9.16   |
| TOTAL AREA(ACRES)                             | = | 6.73   |
| TOTAL RUNOFF(CFS)                             | = | 9.60   |
| TC(MIN.)                                      | = | 10.52  |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2720.00 TO NODE 2710.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|  |   |               |  |   |         |
|--|---|---------------|--|---|---------|
| ELEVATION DATA: UPSTREAM(FEET)                     | = | 1230.00       | DOWNSTREAM(FEET)                       | = | 1170.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET)                  | = | 650.00        | CHANNEL SLOPE                          | = | 0.0923  |
| SLOPE ADJUSTMENT CURVE USED:                       |   |               |  |   |         |
| EFFECTIVE SLOPE                                    | = | .0923         | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |   |         |
| CHANNEL FLOW THRU SUBAREA(CFS)                     | = | 9.60          |  |   |         |
| FLOW VELOCITY(FEET/SEC)                            | = | 3.61          | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |   |         |
| TRAVEL TIME(MIN.)                                  | = | 3.00          | Tc(MIN.)                               | = | 13.51   |
| LONGEST FLOWPATH FROM NODE 2722.00 TO NODE 2710.00 | = | 1155.00 FEET. |  |   |         |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2720.00 TO NODE 2710.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|   |   |        |
|---|---|--------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR)        | = | 4.856  |
| *USER SPECIFIED(SUBAREA):                     |   |        |
| NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT | = | .2500  |
| S. C. S. CURVE NUMBER (AMC II)                | = | 0      |
| AREA-AVERAGE RUNOFF COEFFICIENT               | = | 0.2500 |
| SUBAREA AREA(ACRES)                           | = | 18.32  |
| SUBAREA RUNOFF(CFS)                           | = | 22.24  |
| TOTAL AREA(ACRES)                             | = | 25.05  |
| TOTAL RUNOFF(CFS)                             | = | 30.41  |
| TC(MIN.)                                      | = | 13.51  |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2710.00 TO NODE 2710.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

|  |   |       |
|--|---|-------|
| TOTAL NUMBER OF STREAMS                              | = | 2     |
| CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE: |   |       |
| TIME OF CONCENTRATION(MIN.)                          | = | 13.51 |
| RAINFALL INTENSITY(INCH/HR)                          | = | 4.86  |
| TOTAL STREAM AREA(ACRES)                             | = | 25.05 |
| PEAK FLOW RATE(CFS) AT CONFLUENCE                    | = | 30.41 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2732.00 TO NODE 2731.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1450.00  
DOWNSTREAM ELEVATION(FEET) = 1445.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.196  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.705  
SUBAREA RUNOFF(CFS) = 0.59  
TOTAL AREA(ACRES) = 0.35 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2731.00 TO NODE 2730.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1445.00 DOWNSTREAM(FEET) = 1390.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 305.00 CHANNEL SLOPE = 0.1803  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1502 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.59  
FLOW VELOCITY(FEET/SEC) = 2.17 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.34 Tc(MIN.) = 10.54  
LONGEST FLOWPATH FROM NODE 2732.00 TO NODE 2730.00 = 395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2731.00 TO NODE 2730.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.701  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 1.97 SUBAREA RUNOFF(CFS) = 2.81  
TOTAL AREA(ACRES) = 2.32 TOTAL RUNOFF(CFS) = 3.31  
TC(MIN.) = 10.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2730.00 TO NODE 2710.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1390.00 DOWNSTREAM(FEET) = 1170.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 820.00 CHANNEL SLOPE = 0.2683  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1861 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.31  
FLOW VELOCITY(FEET/SEC) = 3.60 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.80 Tc(MIN.) = 14.34  
LONGEST FLOWPATH FROM NODE 2732.00 TO NODE 2710.00 = 1215.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2730.00 TO NODE 2710.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.674
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500
SUBAREA AREA(ACRES) = 8.79 SUBAREA RUNOFF(CFS) = 10.27
TOTAL AREA(ACRES) = 11.11 TOTAL RUNOFF(CFS) = 12.98
TC(MIN.) = 14.34

\*\*\*\*\*
FLOW PROCESS FROM NODE 2710.00 TO NODE 2710.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 14.34
RAINFALL INTENSITY(INCH/HR) = 4.67
TOTAL STREAM AREA(ACRES) = 11.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.98

\*\* CONFLUENCE DATA \*\*
Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*
Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 42.65 Tc(MIN.) = 13.51
TOTAL AREA(ACRES) = 36.16
LONGEST FLOWPATH FROM NODE 2732.00 TO NODE 2710.00 = 1215.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2710.00 TO NODE 2710.50 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1170.00 DOWNSTREAM(FEET) = 1105.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.1083
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1063 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 42.65
FLOW VELOCITY(FEET/SEC) = 6.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.57 Tc(MIN.) = 15.08
LONGEST FLOWPATH FROM NODE 2732.00 TO NODE 2710.50 = 1815.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2710.00 TO NODE 2710.50 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.524

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\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
 SUBAREA AREA(ACRES) = 10.99 SUBAREA RUNOFF(CFS) = 12.43  
 TOTAL AREA(ACRES) = 47.15 TOTAL RUNOFF(CFS) = 53.32  
 TC(MIN.) = 15.08

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2710.50 TO NODE 27.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1105.00 DOWNSTREAM(FEET) = 920.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1420.00 CHANNEL SLOPE = 0.1303  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1219 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 53.32  
 FLOW VELOCITY(FEET/SEC) = 7.35 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 3.22 Tc(MIN.) = 18.30  
 LONGEST FLOWPATH FROM NODE 2732.00 TO NODE 27.00 = 3235.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2710.50 TO NODE 27.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.993  
 \*USER SPECIFIED(SUBAREA):  
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2600  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.2528  
 SUBAREA AREA(ACRES) = 18.20 SUBAREA RUNOFF(CFS) = 18.89  
 TOTAL AREA(ACRES) = 65.35 TOTAL RUNOFF(CFS) = 65.96  
 TC(MIN.) = 18.30

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 27.00 TO NODE 27.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 65.96        | 18.30     | 3.993                 | 65.35       |

LONGEST FLOWPATH FROM NODE 2732.00 TO NODE 27.00 = 3235.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 172.18       | 22.74     | 3.471                 | 170.93      |

LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 27.00 = 6155.40 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 204.56       | 18.30     | 3.993                 |
| 2             | 229.53       | 22.74     | 3.471                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 229.53 Tc(MIN.) = 22.74

TOTAL AREA(ACRES) = 236.28

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 236.28 TC(MIN.) = 22.74

PEAK FLOW RATE(CFS) = 229.53

=====

=====

END OF RATIONAL METHOD ANALYSIS

□



# APPENDIX A

AES  
Rational Method Hydrology

Existing Condition

BASIN D



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - EXISTING HYDROLOGY \*
  - \* SUBBASIN # 28 \*
  - \* JANUARY 2017 \*
- \*\*\*\*\*

FILE NAME: MERR28.DAT  
TIME/DATE OF STUDY: 09:07 01/30/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2823.00 TO NODE 2822.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1702.00  
DOWNSTREAM ELEVATION(FEET) = 1695.00  
ELEVATION DIFFERENCE(FEET) = 7.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.058  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.383  
SUBAREA RUNOFF(CFS) = 0.85  
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 0.85

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2822.00 TO NODE 2821.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1695.00 DOWNSTREAM(FEET) = 1430.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 517.00 CHANNEL SLOPE = 0.5126  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2256 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.85  
FLOW VELOCITY(FEET/SEC) = 2.66 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.24 Tc(MIN.) = 10.30  
LONGEST FLOWPATH FROM NODE 2823.00 TO NODE 2821.00 = 617.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2822.00 TO NODE 2821.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.787  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 3.06 SUBAREA RUNOFF(CFS) = 6.20  
TOTAL AREA(ACRES) = 3.4 TOTAL RUNOFF(CFS) = 6.87  
TC(MIN.) = 10.30

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2821.00 TO NODE 2820.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1430.00 DOWNSTREAM(FEET) = 1265.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 669.00 CHANNEL SLOPE = 0.2466  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1789 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 6.87  
FLOW VELOCITY(FEET/SEC) = 4.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.48 Tc(MIN.) = 12.78  
LONGEST FLOWPATH FROM NODE 2823.00 TO NODE 2820.00 = 1286.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2821.00 TO NODE 2820.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.035  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3268  
SUBAREA AREA(ACRES) = 11.46 SUBAREA RUNOFF(CFS) = 18.47  
TOTAL AREA(ACRES) = 14.9 TOTAL RUNOFF(CFS) = 24.44  
TC(MIN.) = 12.78

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2820.00 TO NODE 2811.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1265.00 DOWNSTREAM(FEET) = 1145.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 650.00 CHANNEL SLOPE = 0.1846  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1523 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 24.44  
FLOW VELOCITY(FEET/SEC) = 6.34 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.71 Tc(MIN.) = 14.49  
LONGEST FLOWPATH FROM NODE 2823.00 TO NODE 2811.00 = 1936.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2820.00 TO NODE 2811.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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```
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.643
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2800
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3101
SUBAREA AREA(ACRES) = 8.25 SUBAREA RUNOFF(CFS) = 10.73
TOTAL AREA(ACRES) = 23.1 TOTAL RUNOFF(CFS) = 33.26
TC(MIN.) = 14.49
```

```
*****
FLOW PROCESS FROM NODE 2812.00 TO NODE 2811.00 IS CODE = 81
```

```
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
```

```
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.643
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3072
SUBAREA AREA(ACRES) = 9.50 SUBAREA RUNOFF(CFS) = 13.23
TOTAL AREA(ACRES) = 32.6 TOTAL RUNOFF(CFS) = 46.50
TC(MIN.) = 14.49
```

```
*****
FLOW PROCESS FROM NODE 2811.00 TO NODE 2810.00 IS CODE = 53
```

```
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1145.00 DOWNSTREAM(FEET) = 1045.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 611.00 CHANNEL SLOPE = 0.1637
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1418 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 46.50
FLOW VELOCITY(FEET/SEC) = 7.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.34 Tc(MIN.) = 15.83
LONGEST FLOWPATH FROM NODE 2823.00 TO NODE 2810.00 = 2547.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 2811.00 TO NODE 2810.00 IS CODE = 81
```

```
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
```

```
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.385
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
```

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.2945  
SUBAREA AREA(ACRES) = 9.27 SUBAREA RUNOFF(CFS) = 10.16  
TOTAL AREA(ACRES) = 41.9 TOTAL RUNOFF(CFS) = 54.07  
TC(MIN.) = 15.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2810.00 TO NODE 28.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1045.00 DOWNSTREAM(FEET) = 975.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 671.00 CHANNEL SLOPE = 0.1043  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1032 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 54.07  
FLOW VELOCITY(FEET/SEC) = 6.80 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.65 Tc(MIN.) = 17.48  
LONGEST FLOWPATH FROM NODE 2823.00 TO NODE 28.00 = 3218.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2810.00 TO NODE 28.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.114  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2890  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2933  
SUBAREA AREA(ACRES) = 11.80 SUBAREA RUNOFF(CFS) = 14.03  
TOTAL AREA(ACRES) = 53.7 TOTAL RUNOFF(CFS) = 64.76  
TC(MIN.) = 17.48

\*\*\*\*\*  
FLOW PROCESS FROM NODE 28.00 TO NODE 28.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.48  
RAINFALL INTENSITY(INCH/HR) = 4.11  
TOTAL STREAM AREA(ACRES) = 53.67  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 64.76

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2807.00 TO NODE 2806.00 IS CODE = 21

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-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 106.00

UPSTREAM ELEVATION(FEET) = 1738.00

DOWNSTREAM ELEVATION(FEET) = 1705.00

ELEVATION DIFFERENCE(FEET) = 33.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 100.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972

SUBAREA RUNOFF(CFS) = 0.78

TOTAL AREA(ACRES) = 0.28 TOTAL RUNOFF(CFS) = 0.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 2806.00 TO NODE 2805.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1705.00 DOWNSTREAM(FEET) = 1500.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 455.00 CHANNEL SLOPE = 0.4505

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .2201 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION

CHANNEL FLOW THRU SUBAREA(CFS) = 0.78

FLOW VELOCITY(FEET/SEC) = 2.63 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 2.89 Tc(MIN.) = 9.15

LONGEST FLOWPATH FROM NODE 2807.00 TO NODE 2805.00 = 561.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2806.00 TO NODE 2805.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.243

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500

SUBAREA AREA(ACRES) = 3.49 SUBAREA RUNOFF(CFS) = 7.63

TOTAL AREA(ACRES) = 3.8 TOTAL RUNOFF(CFS) = 8.24

TC(MIN.) = 9.15



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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2805.00 TO NODE 2804.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1500.00 | DOWNSTREAM(FEET) = | 1200.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1117.00 | CHANNEL SLOPE =    | 0.2686  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1862 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.24  
FLOW VELOCITY(FEET/SEC) = 4.88 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.82 Tc(MIN.) = 12.97  
LONGEST FLOWPATH FROM NODE 2807.00 TO NODE 2804.00 = 1678.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2805.00 TO NODE 2804.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.986 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3091  
SUBAREA AREA(ACRES) = 16.91 SUBAREA RUNOFF(CFS) = 25.30  
TOTAL AREA(ACRES) = 20.7 TOTAL RUNOFF(CFS) = 31.88  
TC(MIN.) = 12.97

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2804.00 TO NODE 2803.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1200.00 | DOWNSTREAM(FEET) = | 1073.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 885.00  | CHANNEL SLOPE =    | 0.1435  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1307 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 31.88  
FLOW VELOCITY(FEET/SEC) = 6.41 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.30 Tc(MIN.) = 15.27  
LONGEST FLOWPATH FROM NODE 2807.00 TO NODE 2803.00 = 2563.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2804.00 TO NODE 2803.00 IS CODE = 81  
-----

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.488  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2883  
SUBAREA AREA(ACRES) = 11.28 SUBAREA RUNOFF(CFS) = 12.66  
TOTAL AREA(ACRES) = 32.0 TOTAL RUNOFF(CFS) = 41.34  
TC(MIN.) = 15.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 28.03 TO NODE 2801.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1073.00 DOWNSTREAM(FEET) = 985.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 558.00 CHANNEL SLOPE = 0.1577  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1389 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 41.34  
FLOW VELOCITY(FEET/SEC) = 7.21 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.29 Tc(MIN.) = 16.56  
LONGEST FLOWPATH FROM NODE 2807.00 TO NODE 2801.00 = 3121.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2803.00 TO NODE 2801.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.259  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2900  
SUBAREA AREA(ACRES) = 5.72 SUBAREA RUNOFF(CFS) = 7.31  
TOTAL AREA(ACRES) = 37.7 TOTAL RUNOFF(CFS) = 46.55  
TC(MIN.) = 16.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 2802.00 TO NODE 2801.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.259  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2860

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S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2888
SUBAREA AREA(ACRES) = 16.01 SUBAREA RUNOFF(CFS) = 19.50
TOTAL AREA(ACRES) = 53.7 TOTAL RUNOFF(CFS) = 66.05
TC(MIN.) = 16.56

\*\*\*\*\*
FLOW PROCESS FROM NODE 2801.00 TO NODE 28.00 IS CODE = 52
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 985.00 DOWNSTREAM(FEET) = 975.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 360.00 CHANNEL SLOPE = 0.0278
CHANNEL FLOW THRU SUBAREA(CFS) = 66.05
FLOW VELOCITY(FEET/SEC) = 6.99 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.86 Tc(MIN.) = 17.42
LONGEST FLOWPATH FROM NODE 2807.00 TO NODE 28.00 = 3481.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 28.00 TO NODE 28.00 IS CODE = 1
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 17.42
RAINFALL INTENSITY(INCH/HR) = 4.12
TOTAL STREAM AREA(ACRES) = 53.69
PEAK FLOW RATE(CFS) AT CONFLUENCE = 66.05

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

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PEAK FLOW RATE(CFS) = 130.67 Tc(MIN.) = 17.48  
TOTAL AREA(ACRES) = 107.4  
LONGEST FLOWPATH FROM NODE 2807.00 TO NODE 28.00 = 3481.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 107.4 TC(MIN.) = 17.48  
PEAK FLOW RATE(CFS) = 130.67

=====

END OF RATIONAL METHOD ANALYSIS





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC.  
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SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 29 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR29.DAT  
TIME/DATE OF STUDY: 13:20 10/10/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2927.00 TO NODE 2926.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1603.00  
DOWNSTREAM ELEVATION(FEET) = 1570.00  
ELEVATION DIFFERENCE(FEET) = 33.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2926.00 TO NODE 2925.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1570.00 | DOWNSTREAM(FEET) = | 1470.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 307.00  | CHANNEL SLOPE =    | 0.3257  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2010 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.53  
FLOW VELOCITY(FEET/SEC) = 2.51 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 8.30  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2925.00 = 407.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2926.00 TO NODE 2925.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.648 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.15 SUBAREA RUNOFF(CFS) = 2.68  
TOTAL AREA(ACRES) = 1.34 TOTAL RUNOFF(CFS) = 3.12  
TC(MIN.) = 8.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2925.00 TO NODE 2924.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1470.00 | DOWNSTREAM(FEET) = | 1390.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 520.00  | CHANNEL SLOPE =    | 0.1538  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1369 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.12  
FLOW VELOCITY(FEET/SEC) = 3.03 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.86 Tc(MIN.) = 11.17  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2924.00 = 927.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2925.00 TO NODE 2924.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.491 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 6.88 SUBAREA RUNOFF(CFS) = 13.22  
TOTAL AREA(ACRES) = 8.22 TOTAL RUNOFF(CFS) = 15.80  
TC(MIN.) = 11.17

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2924.00 TO NODE 2922.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1390.00 | DOWNSTREAM(FEET) = | 1370.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 361.00  | CHANNEL SLOPE =    | 0.0554  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0554 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 15.80  
FLOW VELOCITY(FEET/SEC) = 3.30 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.82 Tc(MIN.) = 12.99  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2922.00 = 1288.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2923.00 TO NODE 2922.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.982 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3480  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3489  
SUBAREA AREA(ACRES) = 9.30 SUBAREA RUNOFF(CFS) = 16.12  
TOTAL AREA(ACRES) = 17.52 TOTAL RUNOFF(CFS) = 30.46  
TC(MIN.) = 12.99

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2922.00 TO NODE 2921.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1370.00 | DOWNSTREAM(FEET) = | 1300.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1235.00 | CHANNEL SLOPE =    | 0.0567  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0567 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 30.46  
FLOW VELOCITY(FEET/SEC) = 4.16 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.95 Tc(MIN.) = 17.94  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2921.00 = 2523.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2922.00 TO NODE 2921.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.045 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4290  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3992  
SUBAREA AREA(ACRES) = 29.57 SUBAREA RUNOFF(CFS) = 51.32  
TOTAL AREA(ACRES) = 47.09 TOTAL RUNOFF(CFS) = 76.05  
TC(MIN.) = 17.94

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2921.00 TO NODE 2920.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<



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=====

ELEVATION DATA: UPSTREAM(FEET) = 1300.00 DOWNSTREAM(FEET) = 893.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1300.00 CHANNEL SLOPE = 0.3131  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1983 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 76.05  
FLOW VELOCITY(FEET/SEC) = 10.55 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.05 Tc(MIN.) = 19.99  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2920.00 = 3823.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2921.00 TO NODE 2920.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.772  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4400  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4091  
SUBAREA AREA(ACRES) = 15.07 SUBAREA RUNOFF(CFS) = 25.01  
TOTAL AREA(ACRES) = 62.16 TOTAL RUNOFF(CFS) = 95.92  
TC(MIN.) = 19.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 2920.00 TO NODE 29.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 893.00 DOWNSTREAM(FEET) = 800.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 335.00 CHANNEL SLOPE = 0.2776  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1892 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 95.92  
FLOW VELOCITY(FEET/SEC) = 11.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 20.49  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 29.00 = 4158.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2920.00 TO NODE 29.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.712  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4245  
SUBAREA AREA(ACRES) = 27.04 SUBAREA RUNOFF(CFS) = 46.17  
TOTAL AREA(ACRES) = 89.20 TOTAL RUNOFF(CFS) = 140.58  
TC(MIN.) = 20.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 29.00 TO NODE 29.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 20.49  
RAINFALL INTENSITY(INCH/HR) = 3.71  
TOTAL STREAM AREA(ACRES) = 89.20

PEAK FLOW RATE(CFS) AT CONFLUENCE = 140.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2915.00 TO NODE 2914.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1550.00  
DOWNSTREAM ELEVATION(FEET) = 1460.00  
ELEVATION DIFFERENCE(FEET) = 90.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.945  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.247  
SUBAREA RUNOFF(CFS) = 3.98  
TOTAL AREA(ACRES) = 1.38 TOTAL RUNOFF(CFS) = 3.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2914.00 TO NODE 2913.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1460.00 DOWNSTREAM(FEET) = 1400.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.1500  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1350 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.98  
FLOW VELOCITY(FEET/SEC) = 3.26 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 7.99  
LONGEST FLOWPATH FROM NODE 2915.00 TO NODE 2913.00 = 490.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2914.00 TO NODE 2913.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.816  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 5.20 SUBAREA RUNOFF(CFS) = 12.40  
TOTAL AREA(ACRES) = 6.58 TOTAL RUNOFF(CFS) = 15.70  
TC(MIN.) = 7.99

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2913.00 TO NODE 2912.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1400.00 DOWNSTREAM(FEET) = 1290.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.1833  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1517 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 15.70  
FLOW VELOCITY(FEET/SEC) = 5.46 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.83 Tc(MIN.) = 9.82  
LONGEST FLOWPATH FROM NODE 2915.00 TO NODE 2912.00 = 1090.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2913.00 TO NODE 2912.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.965  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 5.12 SUBAREA RUNOFF(CFS) = 10.69  
TOTAL AREA(ACRES) = 11.70 TOTAL RUNOFF(CFS) = 24.43  
TC(MIN.) = 9.82

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2912.00 TO NODE 2911.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1290.00 DOWNSTREAM(FEET) = 1025.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1175.00 CHANNEL SLOPE = 0.2255  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1718 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 24.43  
FLOW VELOCITY(FEET/SEC) = 6.73 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.91 Tc(MIN.) = 12.73  
LONGEST FLOWPATH FROM NODE 2915.00 TO NODE 2911.00 = 2265.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2912.00 TO NODE 2911.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.046  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4330  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4015  
SUBAREA AREA(ACRES) = 19.17 SUBAREA RUNOFF(CFS) = 41.89  
TOTAL AREA(ACRES) = 30.87 TOTAL RUNOFF(CFS) = 62.55  
TC(MIN.) = 12.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2911.00 TO NODE 2910.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1025.00 DOWNSTREAM(FEET) = 835.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 830.00 CHANNEL SLOPE = 0.2289  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1730 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 62.55  
FLOW VELOCITY(FEET/SEC) = 9.23 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.50 Tc(MIN.) = 14.23  
LONGEST FLOWPATH FROM NODE 2915.00 TO NODE 2910.00 = 3095.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2911.00 TO NODE 2910.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.697
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4250
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4118
SUBAREA AREA(ACRES) = 23.79 SUBAREA RUNOFF(CFS) = 47.49
TOTAL AREA(ACRES) = 54.66 TOTAL RUNOFF(CFS) = 105.70
TC(MIN.) = 14.23

```

```

*****
FLOW PROCESS FROM NODE 2910.00 TO NODE 29.00 IS CODE = 52
-----

```

```

>>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
-----

```

```

ELEVATION DATA: UPSTREAM(FEET) = 835.00 DOWNSTREAM(FEET) = 800.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 455.00 CHANNEL SLOPE = 0.0769
CHANNEL FLOW THRU SUBAREA(CFS) = 105.70
FLOW VELOCITY(FEET/SEC) = 13.39 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.57 Tc(MIN.) = 14.80
LONGEST FLOWPATH FROM NODE 2915.00 TO NODE 29.00 = 3550.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 29.00 TO NODE 29.00 IS CODE = 1
-----

```

```

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
-----

```

```

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 14.80
RAINFALL INTENSITY(INCH/HR) = 4.58
TOTAL STREAM AREA(ACRES) = 54.66
PEAK FLOW RATE(CFS) AT CONFLUENCE = 105.70

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 140.58       | 20.49     | 3.712                 | 89.20       |
| 2             | 105.70       | 14.80     | 4.580                 | 54.66       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 207.21       | 14.80     | 4.580                 |
| 2             | 226.26       | 20.49     | 3.712                 |

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 226.26 Tc(MIN.) = 20.49
TOTAL AREA(ACRES) = 143.86
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 29.00 = 4158.00 FEET.

```

```

=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 143.86 TC(MIN.) = 20.49
PEAK FLOW RATE(CFS) = 226.26
=====

```

=====

END OF RATIONAL METHOD ANALYSIS

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0



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003, 1985, 1981 HYDROLOGY MANUAL  
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 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC.  
 6390 GREENWICH DRIVE, SUITE 170  
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 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
 \* SUBBASIN # 30 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR30.DAT  
 TIME/DATE OF STUDY: 10:33 10/06/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3006.00 TO NODE 3005.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 -----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 76.06  
 UPSTREAM ELEVATION(FEET) = 1615.00  
 DOWNSTREAM ELEVATION(FEET) = 1580.00  
 ELEVATION DIFFERENCE(FEET) = 35.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.465

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.707  
SUBAREA RUNOFF(CFS) = 0.52  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.52

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3005.00 TO NODE 3004.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1580.00 | DOWNSTREAM(FEET) = | 1360.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 465.90  | CHANNEL SLOPE =    | 0.4722  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2222 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.52  
FLOW VELOCITY(FEET/SEC) = 2.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.94 Tc(MIN.) = 8.41  
LONGEST FLOWPATH FROM NODE 3006.00 TO NODE 3004.00 = 541.96 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3005.00 TO NODE 3004.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.596 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.06 SUBAREA RUNOFF(CFS) = 4.76  
TOTAL AREA(ACRES) = 2.23 TOTAL RUNOFF(CFS) = 5.15  
TC(MIN.) = 8.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3004.00 TO NODE 3003.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1360.00 | DOWNSTREAM(FEET) = | 1210.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 558.50  | CHANNEL SLOPE =    | 0.2686  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1862 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 5.15  
FLOW VELOCITY(FEET/SEC) = 4.17 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.23 Tc(MIN.) = 10.64  
LONGEST FLOWPATH FROM NODE 3006.00 TO NODE 3003.00 = 1100.46 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3004.00 TO NODE 3003.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.666 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4000  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3901  
SUBAREA AREA(ACRES) = 9.02 SUBAREA RUNOFF(CFS) = 20.44  
TOTAL AREA(ACRES) = 11.25 TOTAL RUNOFF(CFS) = 24.87  
TC(MIN.) = 10.64



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\*\*\*\*\*  
FLOW PROCESS FROM NODE 3003.00 TO NODE 3002.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1210.00 | DOWNSTREAM(FEET) = | 1080.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 596.60  | CHANNEL SLOPE =    | 0.2179  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1690 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 24.87  
FLOW VELOCITY(FEET/SEC) = 6.71 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.48 Tc(MIN.) = 12.12  
LONGEST FLOWPATH FROM NODE 3006.00 TO NODE 3002.00 = 1697.06 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3003.00 TO NODE 3002.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.209 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4000  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3965  
SUBAREA AREA(ACRES) = 21.04 SUBAREA RUNOFF(CFS) = 43.84  
TOTAL AREA(ACRES) = 32.29 TOTAL RUNOFF(CFS) = 66.70  
TC(MIN.) = 12.12

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3002.00 TO NODE 2001.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1080.00 | DOWNSTREAM(FEET) = | 870.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 870.80  | CHANNEL SLOPE =    | 0.2412 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1771 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 66.70  
FLOW VELOCITY(FEET/SEC) = 9.54 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.52 Tc(MIN.) = 13.64  
LONGEST FLOWPATH FROM NODE 3006.00 TO NODE 2001.00 = 2567.86 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3002.00 TO NODE 3001.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.827 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4000  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3979  
SUBAREA AREA(ACRES) = 21.39 SUBAREA RUNOFF(CFS) = 41.30  
TOTAL AREA(ACRES) = 53.68 TOTAL RUNOFF(CFS) = 103.10  
TC(MIN.) = 13.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3001.00 TO NODE 30.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

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=====

ELEVATION DATA: UPSTREAM(FEET) = 870.00 DOWNSTREAM(FEET) = 665.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1720.80 CHANNEL SLOPE = 0.1191  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1143 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 103.10  
FLOW VELOCITY(FEET/SEC) = 8.87 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.23 Tc(MIN.) = 16.88  
LONGEST FLOWPATH FROM NODE 3006.00 TO NODE 30.00 = 4288.66 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3001.00 TO NODE 30.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.208  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4000  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3990  
SUBAREA AREA(ACRES) = 54.15 SUBAREA RUNOFF(CFS) = 91.14  
TOTAL AREA(ACRES) = 107.83 TOTAL RUNOFF(CFS) = 181.02  
TC(MIN.) = 16.88

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 107.83 TC(MIN.) = 16.88  
PEAK FLOW RATE(CFS) = 181.02

=====

END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

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SAN DIEGO, CALIFORNIA 92122  
(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 31 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR31.DAT  
TIME/DATE OF STUDY: 13:56 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3103.00 TO NODE 3102.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 82.00  
UPSTREAM ELEVATION(FEET) = 1335.00  
DOWNSTREAM ELEVATION(FEET) = 1300.00  
ELEVATION DIFFERENCE(FEET) = 35.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.675

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.499  
SUBAREA RUNOFF(CFS) = 1.40  
TOTAL AREA(ACRES) = 0.47 TOTAL RUNOFF(CFS) = 1.40

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3102.00 TO NODE 3101.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1300.00 | DOWNSTREAM(FEET) = | 1035.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 594.00  | CHANNEL SLOPE =    | 0.4461  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2195 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.40  
FLOW VELOCITY(FEET/SEC) = 2.93 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.37 Tc(MIN.) = 9.05  
LONGEST FLOWPATH FROM NODE 3103.00 TO NODE 3101.00 = 676.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3102.00 TO NODE 3101.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.290 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4514  
SUBAREA AREA(ACRES) = 5.56 SUBAREA RUNOFF(CFS) = 16.09  
TOTAL AREA(ACRES) = 6.03 TOTAL RUNOFF(CFS) = 17.12  
TC(MIN.) = 9.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3101.00 TO NODE 31.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1035.00 | DOWNSTREAM(FEET) = | 650.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1825.00 | CHANNEL SLOPE =    | 0.2110 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1655 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 17.12  
FLOW VELOCITY(FEET/SEC) = 5.87 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.19 Tc(MIN.) = 14.23  
LONGEST FLOWPATH FROM NODE 3103.00 TO NODE 31.00 = 2501.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3101.00 TO NODE 31.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.696 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4586  
SUBAREA AREA(ACRES) = 31.91 SUBAREA RUNOFF(CFS) = 68.93  
TOTAL AREA(ACRES) = 37.94 TOTAL RUNOFF(CFS) = 81.71  
TC(MIN.) = 14.23

-----  
END OF STUDY SUMMARY:

MERR31.TXT  
TOTAL AREA(ACRES) = 37.94 TC(MI N.) = 14.23  
PEAK FLOW RATE(CFS) = 81.71

=====  
=====  
END OF RATIONAL METHOD ANALYSIS

□

# APPENDIX A

AES  
Rational Method Hydrology

Existing Condition

BASIN E





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

(c) Copyright 1982-2012 Advanced Engineering Software (aes)  
Ver. 19.0 Release Date: 06/01/2012 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Dr.  
Suite 170  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* NEWLAND SIERRA - EXISTING HYDROLOGY \*  
\* SUBBASIN # 32 \*  
\* JANUARY 2015 \*  
\*\*\*\*\*

FILE NAME: MERR32.DAT  
TIME/DATE OF STUDY: 16:27 01/14/2015

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS  
\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-CROWN TO STREET-CROSSFALL: |                   | IN- / OUT-/PARK-<br>SIDE / SIDE/ WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES: |             |              | MANNING<br>HIKE FACTOR<br>(n) |
|-----|---------------------------------|-------------------|--------------------------------------|------------------------|--------------------|-------------|--------------|-------------------------------|
|     | WIDTH<br>(FT)                   | CROSSFALL<br>(FT) |                                      |                        | WIDTH<br>(FT)      | LIP<br>(FT) | HIKE<br>(FT) |                               |
| 1   | 30.0                            | 20.0              | 0.018/0.018/0.020                    | 0.67                   | 2.00               | 0.0313      | 0.167        | 0.0150                        |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3215.00 TO NODE 3214.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1450.00  
DOWNSTREAM ELEVATION(FEET) = 1445.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.212  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.017

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SUBAREA RUNOFF(CFS) = 0.70  
TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 0.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3214.00 TO NODE 3213.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1445.00 DOWNSTREAM(FEET) = 1415.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1000  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1000 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.70  
FLOW VELOCITY(FEET/SEC) = 1.77 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.82 Tc(MIN.) = 9.04  
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 3213.00 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3214.00 TO NODE 3213.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.296  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 15.25 SUBAREA RUNOFF(CFS) = 33.60  
TOTAL AREA(ACRES) = 15.5 TOTAL RUNOFF(CFS) = 34.15  
TC(MIN.) = 9.04

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3213.00 TO NODE 3212.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1415.00 DOWNSTREAM(FEET) = 1360.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.0917  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0917 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 34.15  
FLOW VELOCITY(FEET/SEC) = 5.49 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.82 Tc(MIN.) = 10.86  
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 3212.00 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3213.00 TO NODE 3212.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.593  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 12.04 SUBAREA RUNOFF(CFS) = 23.57  
TOTAL AREA(ACRES) = 27.5 TOTAL RUNOFF(CFS) = 53.91  
TC(MIN.) = 10.86

\*\*\*\*\*  
Page 2

FLOW PROCESS FROM NODE 3212.00 TO NODE 3209.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1343.00 DOWNSTREAM(FEET) = 1237.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 606.50 CHANNEL SLOPE = 0.1748
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1474 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 53.91
FLOW VELOCITY(FEET/SEC) = 8.11 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.25 Tc(MIN.) = 12.10
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 3209.00 = 1581.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3212.00 TO NODE 3209.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.214
\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 11.05 SUBAREA RUNOFF(CFS) = 20.17
TOTAL AREA(ACRES) = 38.6 TOTAL RUNOFF(CFS) = 70.43
TC(MIN.) = 12.10

\*\*\*\*\*

FLOW PROCESS FROM NODE 3209.00 TO NODE 3209.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.10
RAINFALL INTENSITY(INCH/HR) = 5.21
TOTAL STREAM AREA(ACRES) = 38.59
PEAK FLOW RATE(CFS) AT CONFLUENCE = 70.43

\*\*\*\*\*

FLOW PROCESS FROM NODE 3211.00 TO NODE 3210.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S. C. S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 136.80
UPSTREAM ELEVATION(FEET) = 1612.00
DOWNSTREAM ELEVATION(FEET) = 1580.00
ELEVATION DIFFERENCE(FEET) = 32.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 100.00
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972
SUBAREA RUNOFF(CFS) = 0.56
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 3210.00 TO NODE 3209.00 IS CODE = 53

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>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1580.00 DOWNSTREAM(FEET) = 1237.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1282.00 CHANNEL SLOPE = 0.2676  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1859 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.56  
FLOW VELOCITY(FEET/SEC) = 2.41 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 8.85 Tc(MIN.) = 15.12  
LONGEST FLOWPATH FROM NODE 3211.00 TO NODE 3209.00 = 1418.80 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3210.00 TO NODE 3209.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.517  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 9.72 SUBAREA RUNOFF(CFS) = 15.37  
TOTAL AREA(ACRES) = 9.9 TOTAL RUNOFF(CFS) = 15.68  
Tc(MIN.) = 15.12

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3209.00 TO NODE 3209.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.12  
RAINFALL INTENSITY(INCH/HR) = 4.52  
TOTAL STREAM AREA(ACRES) = 9.92  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.68

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 70.43        | 12.10     | 5.214                 | 38.59       |
| 2             | 15.68        | 15.12     | 4.517                 | 9.92        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 82.98        | 12.10     | 5.214                 |
| 2             | 76.70        | 15.12     | 4.517                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 82.98 Tc(MIN.) = 12.10  
TOTAL AREA(ACRES) = 48.5  
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 3209.00 = 1581.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3209.00 TO NODE 2508.00 IS CODE = 53

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>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1237.00 DOWNSTREAM(FEET) = 1020.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 807.70 CHANNEL SLOPE = 0.2687  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1862 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 82.98  
FLOW VELOCITY(FEET/SEC) = 10.53 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.28 Tc(MIN.) = 13.38  
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 2508.00 = 2389.20 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3209.00 TO NODE 3208.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.887  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 12.33 SUBAREA RUNOFF(CFS) = 21.09  
TOTAL AREA(ACRES) = 60.8 TOTAL RUNOFF(CFS) = 104.07  
TC(MIN.) = 13.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3208.00 TO NODE 3204.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1020.00 DOWNSTREAM(FEET) = 831.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1048.90 CHANNEL SLOPE = 0.1802  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1501 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 104.07  
FLOW VELOCITY(FEET/SEC) = 10.19 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.72 Tc(MIN.) = 15.10  
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 3204.00 = 3438.10 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3208.00 TO NODE 3204.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.521  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3701  
SUBAREA AREA(ACRES) = 13.59 SUBAREA RUNOFF(CFS) = 28.26  
TOTAL AREA(ACRES) = 74.4 TOTAL RUNOFF(CFS) = 124.54  
TC(MIN.) = 15.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3204.00 TO NODE 3204.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

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TIME OF CONCENTRATION(MIN.) = 15.10  
RAINFALL INTENSITY(INCH/HR) = 4.52  
TOTAL STREAM AREA(ACRES) = 74.43  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 124.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3207.00 TO NODE 3206.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 93.00  
UPSTREAM ELEVATION(FEET) = 1347.00  
DOWNSTREAM ELEVATION(FEET) = 1335.00  
ELEVATION DIFFERENCE(FEET) = 12.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.043  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.161  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3206.00 TO NODE 3205.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1335.00 DOWNSTREAM(FEET) = 1063.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1106.80 CHANNEL SLOPE = 0.2458  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1786 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.83  
FLOW VELOCITY(FEET/SEC) = 2.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 7.79 Tc(MIN.) = 13.84  
LONGEST FLOWPATH FROM NODE 3207.00 TO NODE 3205.00 = 1199.80 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3206.00 TO NODE 3205.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.782  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 15.11 SUBAREA RUNOFF(CFS) = 25.29  
TOTAL AREA(ACRES) = 15.4 TOTAL RUNOFF(CFS) = 25.78  
TC(MIN.) = 13.84

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3205.00 TO NODE 3204.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1063.00 DOWNSTREAM(FEET) = 831.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 830.90 CHANNEL SLOPE = 0.2792  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1897 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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CHANNEL FLOW THRU SUBAREA(CFS) = 25.78  
 FLOW VELOCITY(FEET/SEC) = 7.20 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 1.92 Tc(MIN.) = 15.76  
 LONGEST FLOWPATH FROM NODE 3207.00 TO NODE 3204.00 = 2030.70 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3205.00 TO NODE 3204.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.397  
 \*USER SPECIFIED(SUBAREA):  
 RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
 S. C. S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3999  
 SUBAREA AREA(ACRES) = 12.79 SUBAREA RUNOFF(CFS) = 25.87  
 TOTAL AREA(ACRES) = 28.2 TOTAL RUNOFF(CFS) = 49.57  
 TC(MIN.) = 15.76

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3204.00 TO NODE 3204.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 15.76  
 RAINFALL INTENSITY(INCH/HR) = 4.40  
 TOTAL STREAM AREA(ACRES) = 28.19  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 49.57

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 124.54       | 15.10     | 4.521                 | 74.43       |
| 2             | 49.57        | 15.76     | 4.397                 | 28.19       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 172.02       | 15.10     | 4.521                 |
| 2             | 170.70       | 15.76     | 4.397                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 172.02 Tc(MIN.) = 15.10  
 TOTAL AREA(ACRES) = 102.6  
 LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 3204.00 = 3438.10 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3204.00 TO NODE 3203.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 831.00 DOWNSTREAM(FEET) = 759.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 426.80 CHANNEL SLOPE = 0.1687  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1443 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 172.02

MERR32.TXT

FLOW VELOCITY(FEET/SEC) = 11.81 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.60 Tc(MIN.) = 15.70
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 3203.00 = 3864.90 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3204.00 TO NODE 3203.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.409
\*USER SPECIFIED(SUBAREA):
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3823
SUBAREA AREA(ACRES) = 5.34 SUBAREA RUNOFF(CFS) = 10.83
TOTAL AREA(ACRES) = 108.0 TOTAL RUNOFF(CFS) = 181.97
TC(MIN.) = 15.70

\*\*\*\*\*

FLOW PROCESS FROM NODE 3203.00 TO NODE 32.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 759.00 DOWNSTREAM(FEET) = 724.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 430.00 CHANNEL SLOPE = 0.0814
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .0814 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 181.97
FLOW VELOCITY(FEET/SEC) = 9.04 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.79 Tc(MIN.) = 16.49
LONGEST FLOWPATH FROM NODE 3215.00 TO NODE 32.00 = 4294.90 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3203.00 TO NODE 32.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.271
\*USER SPECIFIED(SUBAREA):
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
S. C. S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3913
SUBAREA AREA(ACRES) = 14.09 SUBAREA RUNOFF(CFS) = 27.68
TOTAL AREA(ACRES) = 122.1 TOTAL RUNOFF(CFS) = 203.95
TC(MIN.) = 16.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 32.00 TO NODE 32.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.49
RAINFALL INTENSITY(INCH/HR) = 4.27
TOTAL STREAM AREA(ACRES) = 122.05
PEAK FLOW RATE(CFS) AT CONFLUENCE = 203.95

\*\*\*\*\*

FLOW PROCESS FROM NODE 3202.00 TO NODE 3201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<



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=====

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4600

S. C. S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 113.00

UPSTREAM ELEVATION(FEET) = 993.00

DOWNSTREAM ELEVATION(FEET) = 968.00

ELEVATION DIFFERENCE(FEET) = 25.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.348

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 100.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.830

SUBAREA RUNOFF(CFS) = 1.10

TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 1.10

\*\*\*\*\*

FLOW PROCESS FROM NODE 3201.00 TO NODE 32.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

-----

ELEVATION DATA: UPSTREAM(FEET) = 968.00 DOWNSTREAM(FEET) = 724.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1301.84 CHANNEL SLOPE = 0.1874

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1537 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 1.10

FLOW VELOCITY(FEET/SEC) = 2.26 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 9.58 Tc(MIN.) = 14.93

LONGEST FLOWPATH FROM NODE 3202.00 TO NODE 32.00 = 1414.84 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3201.00 TO NODE 32.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.554

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .4600

S. C. S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.4600

SUBAREA AREA(ACRES) = 13.92 SUBAREA RUNOFF(CFS) = 29.16

TOTAL AREA(ACRES) = 14.2 TOTAL RUNOFF(CFS) = 29.72

TC(MIN.) = 14.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 32.00 TO NODE 32.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 14.93

RAINFALL INTENSITY(INCH/HR) = 4.55

TOTAL STREAM AREA(ACRES) = 14.19

PEAK FLOW RATE(CFS) AT CONFLUENCE = 29.72

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 203.95       | 16.49     | 4.271                 | 122.05      |





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\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 33 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR33.DAT  
TIME/DATE OF STUDY: 14:00 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3302.00 TO NODE 3301.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1155.00  
DOWNSTREAM ELEVATION(FEET) = 1065.00  
ELEVATION DIFFERENCE(FEET) = 90.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 1.65  
TOTAL AREA(ACRES) = 0.54 TOTAL RUNOFF(CFS) = 1.65

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3301.80 TO NODE 3301.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1065.00 | DOWNSTREAM(FEET) = | 945.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 375.00  | CHANNEL SLOPE =    | 0.3200 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2000 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.65  
FLOW VELOCITY(FEET/SEC) = 2.96 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.11 Tc(MIN.) = 7.54  
LONGEST FLOWPATH FROM NODE 3302.00 TO NODE 3301.60 = 450.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3301.80 TO NODE 3301.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 7.076 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.73 SUBAREA RUNOFF(CFS) = 6.76  
TOTAL AREA(ACRES) = 3.27 TOTAL RUNOFF(CFS) = 8.10  
TC(MIN.) = 7.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3301.60 TO NODE 3301.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 945.00 | DOWNSTREAM(FEET) = | 810.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 415.00 | CHANNEL SLOPE =    | 0.3253 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2009 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.10  
FLOW VELOCITY(FEET/SEC) = 5.04 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.37 Tc(MIN.) = 8.91  
LONGEST FLOWPATH FROM NODE 3302.00 TO NODE 3301.00 = 865.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3301.60 TO NODE 3301.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.352 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4211  
SUBAREA AREA(ACRES) = 5.97 SUBAREA RUNOFF(CFS) = 17.44  
TOTAL AREA(ACRES) = 9.24 TOTAL RUNOFF(CFS) = 24.72  
TC(MIN.) = 8.91

\*\*\*\*\*

MERR33.TXT

FLOW PROCESS FROM NODE 3301.00 TO NODE 33.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 810.00 DOWNSTREAM(FEET) = 725.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 925.00 CHANNEL SLOPE = 0.0919  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0919 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 24.72  
FLOW VELOCITY(FEET/SEC) = 4.94 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 12.03  
LONGEST FLOWPATH FROM NODE 3302.00 TO NODE 33.00 = 1790.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3301.00 TO NODE 33.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.234  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4499  
SUBAREA AREA(ACRES) = 26.36 SUBAREA RUNOFF(CFS) = 63.46  
TOTAL AREA(ACRES) = 35.60 TOTAL RUNOFF(CFS) = 83.83  
TC(MIN.) = 12.03

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 35.60 TC(MIN.) = 12.03  
PEAK FLOW RATE(CFS) = 83.83

END OF RATIONAL METHOD ANALYSIS

□





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Analysis prepared by:

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(858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MERRIAM MOUNTAINS - EXISTING HYDROLOGY \*  
\* SUBBASIN # 34 \*  
\* 2469.01A - OCTOBER 2006 \*  
\*\*\*\*\*

FILE NAME: MERR34.DAT  
TIME/DATE OF STUDY: 14:01 09/28/2006

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3403.00 TO NODE 3402.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

\*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1575.00  
DOWNSTREAM ELEVATION(FEET) = 1520.00  
ELEVATION DIFFERENCE(FEET) = 55.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.89  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.89

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3402.80 TO NODE 3402.60 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1520.00 | DOWNSTREAM(FEET) = | 1440.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 250.00  | CHANNEL SLOPE =    | 0.3200  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2000 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.89  
FLOW VELOCITY(FEET/SEC) = 2.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.66 Tc(MIN.) = 7.09  
LONGEST FLOWPATH FROM NODE 3403.00 TO NODE 3402.60 = 325.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3402.80 TO NODE 3402.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 7.361 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 3.35  
TOTAL AREA(ACRES) = 1.59 TOTAL RUNOFF(CFS) = 4.10  
TC(MIN.) = 7.09

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3402.60 TO NODE 3402.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1440.00 | DOWNSTREAM(FEET) = | 1330.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 655.00  | CHANNEL SLOPE =    | 0.1679  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1440 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.10  
FLOW VELOCITY(FEET/SEC) = 3.40 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.21 Tc(MIN.) = 10.30  
LONGEST FLOWPATH FROM NODE 3403.00 TO NODE 3402.00 = 980.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3402.60 TO NODE 3402.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.785 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 14.27 SUBAREA RUNOFF(CFS) = 28.89  
TOTAL AREA(ACRES) = 15.86 TOTAL RUNOFF(CFS) = 32.11  
TC(MIN.) = 10.30

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 3402.00 TO NODE 3401.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1330.00 | DOWNSTREAM(FEET) = | 890.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1965.00 | CHANNEL SLOPE =    | 0.2239 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1713 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 32.11  
FLOW VELOCITY(FEET/SEC) = 7.36 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.45 Tc(MIN.) = 14.75  
LONGEST FLOWPATH FROM NODE 3403.00 TO NODE 3401.00 = 2945.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3402.00 TO NODE 3401.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.589 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 71.31 SUBAREA RUNOFF(CFS) = 114.53  
TOTAL AREA(ACRES) = 87.17 TOTAL RUNOFF(CFS) = 140.00  
TC(MIN.) = 14.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3401.00 TO NODE 34.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 890.00 | DOWNSTREAM(FEET) = | 805.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 525.00 | CHANNEL SLOPE =    | 0.1619 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1410 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 140.00  
FLOW VELOCITY(FEET/SEC) = 10.90 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.80 Tc(MIN.) = 15.56  
LONGEST FLOWPATH FROM NODE 3403.00 TO NODE 34.00 = 3470.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3401.00 TO NODE 34.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.435 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3617  
SUBAREA AREA(ACRES) = 10.38 SUBAREA RUNOFF(CFS) = 21.17  
TOTAL AREA(ACRES) = 97.55 TOTAL RUNOFF(CFS) = 156.47  
TC(MIN.) = 15.56

-----  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 97.55 TC(MIN.) = 15.56  
PEAK FLOW RATE(CFS) = 156.47

=====

END OF RATIONAL METHOD ANALYSIS

MERR34.TXT

0



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
 2003,1985,1981 HYDROLOGY MANUAL  
 (c) Copyright 1982-2004 Advanced Engineering Software (aes)  
 Ver. 2.0 Release Date: 01/01/2004 License ID 1355

Analysis prepared by:

FUSCOE ENGINEERING - SAN DIEGO, INC.  
 6390 GREENWICH DRIVE, SUITE 170  
 SAN DIEGO, CALIFORNIA 92122  
 (858) 554-1500

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* MERRIAM MOUNTAINS - PROPOSED HYDROLOGY \*  
 \* SUBBASIN # 35 \*  
 \* 2469.01A - OCTOBER 2006 \*  
 \*\*\*\*\*

FILE NAME: MERR35-P.DAT  
 TIME/DATE OF STUDY: 11:46 10/06/2006

-----  
 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
 -----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
 NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/PARK-<br>SIDE / SIDE/ WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020   | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3502.00 TO NODE 3501.80 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 1150.00  
 DOWNSTREAM ELEVATION(FEET) = 1085.00  
 ELEVATION DIFFERENCE(FEET) = 65.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 1.32  
TOTAL AREA(ACRES) = 0.43 TOTAL RUNOFF(CFS) = 1.32

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3501.80 TO NODE 3501.60 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1085.00 DOWNSTREAM(FEET) = 1035.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1667  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1433 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.32  
FLOW VELOCITY(FEET/SEC) = 2.32 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 7.58  
LONGEST FLOWPATH FROM NODE 3502.00 TO NODE 3501.60 = 375.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3501.80 TO NODE 3501.60 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.052  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.65 SUBAREA RUNOFF(CFS) = 6.54  
TOTAL AREA(ACRES) = 3.08 TOTAL RUNOFF(CFS) = 7.60  
TC(MIN.) = 7.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3501.60 TO NODE 3501.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1035.00 DOWNSTREAM(FEET) = 905.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 540.00 CHANNEL SLOPE = 0.2407  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1769 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.60  
FLOW VELOCITY(FEET/SEC) = 4.63 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.94 Tc(MIN.) = 9.52  
LONGEST FLOWPATH FROM NODE 3502.00 TO NODE 3501.00 = 915.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3501.60 TO NODE 3501.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.086  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4251  
SUBAREA AREA(ACRES) = 6.62 SUBAREA RUNOFF(CFS) = 18.53  
TOTAL AREA(ACRES) = 9.70 TOTAL RUNOFF(CFS) = 25.09  
TC(MIN.) = 9.52

FLOW PROCESS FROM NODE 3501.00 TO NODE 35.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 905.00 DOWNSTREAM(FEET) = 810.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1300.00 CHANNEL SLOPE = 0.0731
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .0731 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 25.09
FLOW VELOCITY(FEET/SEC) = 4.43 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.89 TC(MIN.) = 14.42
LONGEST FLOWPATH FROM NODE 3502.00 TO NODE 35.00 = 2215.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3501.00 TO NODE 35.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.657
\*USER SPECIFIED(SUBAREA):
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4400
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4369
SUBAREA AREA(ACRES) = 37.33 SUBAREA RUNOFF(CFS) = 76.50
TOTAL AREA(ACRES) = 47.03 TOTAL RUNOFF(CFS) = 95.70
TC(MIN.) = 14.42

END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 47.03 TC(MIN.) = 14.42
PEAK FLOW RATE(CFS) = 95.70

END OF RATIONAL METHOD ANALYSIS

□



# APPENDIX A

AES  
Rational Method Hydrology

Proposed Condition

BASIN A

THE FOLLOWING SUBBASINS OF MAJOR BASIN A  
HAVE NO GRADING, THUS THERE IS NO CHANGE IN HYDROLOGY FOR  
THE PROPOSED CONDITION.

1

2

3

4

5

6

7

8

9

12

14

14.1

15.1

17

18



Job Name: Newland Sierra

Date: 1/20/16

Job #:

Run Name:  
P-1000.DAT  
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| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1010         | 1009 | 2    | 1480             | 1470             | 100              | 0.35        | 0.61          |                |      |   |   |
| 1009         | 1008 | 5    | 1470             | 1455             | 300              | 0.35        | 2.18          |                |      |   |   |
| 1008         | 1007 | 5    | 1455             | 1320             | 630              | 0.35        | 8.11          |                |      |   |   |
| 1007         | 1006 | 5    | 1320             | 1160             | 695              | 0.35        | 20.56         |                |      |   |   |
| 1006         | 1006 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1014         | 1013 | 2    | 1620             | 1590             | 75               | 0.35        | 0.07          |                |      |   |   |
| 1013         | 1012 | 5    | 1590             | 1515             | 270              | 0.35        | 0.72          |                |      |   |   |
| 1012         | 1011 | 5    | 1515             | 1450             | 565              | 0.35        | 3.73          |                |      |   |   |
| 1011         | 1006 | 5    | 1450             | 1160             | 1530             | 0.35        | 46.29         |                |      |   |   |
| 1006         | 1006 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1006         | 1005 | 5    | 1160             | 945              | 1180             | 0.35        | 40.13         |                |      |   |   |
| 1005         | 1005 | 10   |                  |                  |                  |             |               | Save to Bank 1 |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1027         | 1026 | 2    | 1680             | 1640             | 100              | 0.35        | 0.10          |                |      |   |   |
| 1026         | 1025 | 5    | 1640             | 1495             | 460              | 0.35        | 1.59          |                |      |   |   |
| 1025         | 1024 | 3    | 1495             | 1485             | 100              |             |               |                |      |   |   |
| 1024         | 1024 | 10   |                  |                  |                  |             |               | Save to Bank 2 |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1035         | 1034 | 2    | 1531.8           | 1531.2           | 60               | 0.9         | 0.07          |                |      |   |   |
| 1034         | 1033 | 6    | 1531.2           | 1511             | 455              | 0.9         | 0.60          | 2 sides        |      |   |   |
| 1033         | 1031 | 3    | 1510             | 1500             | 515              |             |               |                |      |   |   |
| 1031         | 1031 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1033         | 1032 | 2    | 1510             | 1508             | 65               | 0.9         | 0.10          |                |      |   |   |
| 1032         | 1031 | 6    | 1508             | 1500             | 460              | 0.9         | 0.45          | 2 sides        |      |   |   |
| 1031         | 1031 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1031         | 1029 | 3    | 1500             | 1485             | 430              |             |               |                |      |   |   |
| 1029         | 1029 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1031         | 1030 | 2    | 1500             | 1498             | 65               | 0.9         | 0.06          |                |      |   |   |
| 1030         | 1029 | 6    | 1498             | 1485             | 365              | 0.9         | 0.35          | 2 sides        |      |   |   |
| 1029         | 1029 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1029         | 1024 | 3    | 1485             | 1480             | 60               |             |               |                |      |   |   |
| 1024         | 1024 | 11   |                  |                  |                  |             |               | Add Bank 2     |      |   |   |
| 1024         | 1024 | 12   |                  |                  |                  |             |               | Clear Bank 2   |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1024         | 1021 | 3    | 1480             | 1475             | 50               |             |               |                |      |   |   |
| 1021         | 1021 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 1023         | 1022 | 2    | 1485             | 1484             | 65               | 0.9         | 0.32          |                |      |   |   |



Job #:

Run Name:  
P-1000.DAT  
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| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1022         | 1021 | 3    | 1479             | 1475             | 60               |             |               |                |      |   |   |
| 1021         | 1021 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1021         | 1020 | 5    | 1475             | 1440             | 300              | 0.35        | 4.30          |                |      |   |   |
| 1020         | 1019 | 5    | 1440             | 1430             | 140              | 0.35        | 1.40          |                |      |   |   |
| 1019         | 1019 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1039         | 1038 | 2    | 1690             | 1665             | 80               | 0.35        | 0.34          |                |      |   |   |
| 1038         | 1037 | 5    | 1665             | 1520             | 285              | 0.35        | 2.57          |                |      |   |   |
| 1037         | 1036 | 3    | 1514             | 1490             | 85               |             |               |                |      |   |   |
| 1036         | 1019 | 5    | 1490             | 1430             | 335              | 0.35        | 1.38          |                |      |   |   |
| 1019         | 1019 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1019         | 1018 | 5    | 1430             | 1420             | 100              | 0.35        | 0.37          |                |      |   |   |
| 1018         | 1018 | 10   |                  |                  |                  |             |               | Save to bank 2 |      |   |   |
| 1044         | 1043 | 2    | 1733             | 1720             | 100              | 0.35        | 0.28          |                |      |   |   |
| 1043         | 1042 | 5    | 1720             | 1510             | 520              | 0.35        | 3.01          |                |      |   |   |
| 1042         | 1041 | 3    | 1504             | 1500             | 50               |             |               |                |      |   |   |
| 1041         | 1040 | 5    | 1500             | 1450             | 160              | 0.35        | 0.31          |                |      |   |   |
| 1040         | 1040 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1048         | 1047 | 2    | 1715             | 1675             | 100              | 0.35        | 0.20          |                |      |   |   |
| 1047         | 1046 | 5    | 1675             | 1515             | 465              | 0.35        | 2.26          |                |      |   |   |
| 1046         | 1045 | 3    | 1509             | 1500             | 65               |             |               |                |      |   |   |
| 1045         | 1040 | 5    | 1500             | 1450             | 195              | 0.35        | 0.40          |                |      |   |   |
| 1040         | 1040 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1040         | 1018 | 5    | 1450             | 1420             | 195              | 0.35        | 0.46          |                |      |   |   |
| 1018         | 1018 | 11   |                  |                  |                  |             |               | Add bank 2     |      |   |   |
| 1018         | 1018 | 12   |                  |                  |                  |             |               | Clear bank 2   |      |   |   |
| 1018         | 1017 | 5    | 1420             | 1355             | 370              | 0.35        | 4.79          |                |      |   |   |
| 1017         | 1016 | 5    | 1355             | 1340             | 195              | 0.35        | 2.10          |                |      |   |   |
| 1016         | 1016 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1052         | 1051 | 2    | 1615             | 1605             | 100              | 0.35        | 0.17          |                |      |   |   |
| 1051         | 1050 | 5    | 1605             | 1535             | 250              | 0.35        | 1.32          |                |      |   |   |
| 1050         | 1049 | 3    | 1524             | 1475             | 130              |             |               |                |      |   |   |
| 1049         | 1016 | 5    | 1475             | 1340             | 395              | 0.35        | 3.17          |                |      |   |   |
| 1016         | 1016 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1016         | 1015 | 5    | 1340             | 1080             | 1015             | 0.35        | 12.60         |                |      |   |   |
| 1015         | 1015 | 10   |                  |                  |                  |             |               | Save to bank 2 |      |   |   |



Job #:

Run Name:  
P-1000.DAT  
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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1058         | 1057   | 2    | 1735             | 1712             | 100              | 0.35        | 0.29          |                |      |   |   |
| 1057         | 1056   | 5    | 1712             | 1585             | 435              | 0.35        | 2.26          |                |      |   |   |
| 1056         | 1055   | 3    | 1579             | 1560             | 110              |             |               |                |      |   |   |
| 1055         | 1054   | 5    | 1560             | 1510             | 190              | 0.35        | 2.45          |                |      |   |   |
| 1054         | 1054   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1061         | 1060   | 2    | 1750             | 1730             | 80               | 0.35        | 0.11          |                |      |   |   |
| 1060         | 1059.4 | 5    | 1730             | 1545             | 600              | 0.35        | 4.11          |                |      |   |   |
| 1059.4       | 1059.2 | 3    | 1539             | 1535             | 45               |             |               |                |      |   |   |
| 1059.2       | 1054   | 5    | 1535             | 1510             | 130              |             |               | brow ditch     |      |   |   |
| 1054         | 1054   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1054         | 1053.2 | 3    | 1504             | 1485             | 100              |             |               |                |      |   |   |
| 1053.2       | 1053   | 5    | 1485             | 1448             | 175              |             |               | valley flow    |      |   |   |
| 1053         | 1053   | 10   |                  |                  |                  |             |               | Save to bank 3 |      |   |   |
| 1128         | 1126   | 2    | 1530             | 1526             | 70               | 0.9         | 0.07          |                |      |   |   |
| 1126         | 1063   | 6    | 1526             | 1465             | 720              | 0.9         | 1.18          | 2 sides        |      |   |   |
| 1063         | 1062   | 3    | 1464             | 1458             | 185              |             |               |                |      |   |   |
| 1062         | 1062   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1062.4       | 1062.2 | 2    | 1495             | 1490             | 100              | 0.52        | 0.17          |                |      |   |   |
| 1062.2       | 1062   | 5    | 1490             | 1458             | 400              | 0.52        | 2.20          |                |      |   |   |
| 1062         | 1062   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1062         | 1053   | 3    | 1452             | 1448             | 280              |             |               |                |      |   |   |
| 1053         | 1053   | 11   |                  |                  |                  |             |               | Add Bank 3     |      |   |   |
| 1053         | 1053   | 12   |                  |                  |                  |             |               | Clear Bank 3   |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1053         | 1015   | 5    | 1448             | 1080             | 1280             | 0.35        | 14.13         |                |      |   |   |
| 1015         | 1015   | 10   |                  |                  |                  |             |               | Save to Bank 3 |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1070         | 1069   | 2    | 1605             | 1585             | 85               | 0.35        | 0.13          |                |      |   |   |
| 1069         | 1068   | 5    | 1585             | 1525             | 405              | 0.35        | 1.37          |                |      |   |   |
| 1068         | 1066   | 3    | 1519             | 1470             | 710              |             |               |                |      |   |   |
| 1066         | 1064   | 5    | 1470             | 1410             | 380              | 0.35        | 1.49          |                |      |   |   |
| 1064         | 1064   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1065.4       | 1065.2 | 2    | 1495             | 1493             | 75               | 0.52        | 0.15          |                |      |   |   |
| 1065.2       | 1065   | 5    | 1493             | 1438             | 780              | 0.52        | 4.38          |                |      |   |   |
| 1065         | 1064   | 3    | 1438             | 1410             | 120              |             |               |                |      |   |   |
| 1064         | 1064   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1065         | 1064   | 3    | 1432             | 1410             | 120              |             |               |                |      |   |   |
| 1064         | 1015   | 5    | 1410             | 1080             | 940              | 0.35        | 5.38          |                |      |   |   |



Job #:

Run Name:  
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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1015         | 1015   | 11   |                  |                  |                  |             |               | Add bank 2     |      |   |   |
| 1015         | 1015   | 11   |                  |                  |                  |             |               | Add bank 3     |      |   |   |
| 1015         | 1015   | 12   |                  |                  |                  |             |               | Clear bank 2   |      |   |   |
| 1015         | 1015   | 12   |                  |                  |                  |             |               | Clear bank 3   |      |   |   |
| 1015         | 1005   | 5    | 1080             | 950              | 830              |             |               | valley flow    |      |   |   |
| 1005         | 1005   | 11   |                  |                  |                  |             |               | Add bank 1     |      |   |   |
| 1005         | 1005   | 12   |                  |                  |                  |             |               | Clear bank 1   |      |   |   |
| 1005         | 1004   | 5    | 950              | 890              | 345              | 0.3         | 5.20          |                |      |   |   |
| 1004         | 1004   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1144         | 1142   | 2    | 1435             | 1380             | 80               | 0.35        | 0.34          |                |      |   |   |
| 1142         | 1004   | 5    | 1380             | 890              | 1510             | 0.32        | 23.01         |                |      |   |   |
| 1004         | 1004   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1004         | 1003   | 5    | 890              | 715              | 1700             | 0.3         | 62.54         |                |      |   |   |
| 1003         | 1002   | 5    | 715              | 685              | 530              | 0.25        | 5.54          |                |      |   |   |
| 1002         | 1002   | 10   |                  |                  |                  |             |               | Save to bank 1 |      |   |   |
| 1074.8       | 1074.6 | 2    | 1495             | 1493             | 80               | 0.52        | 0.15          |                |      |   |   |
| 1074.6       | 1074.4 | 6    | 1493             | 1478             | 595              | 0.52        | 2.89          | one side       |      |   |   |
| 1074.4       | 1074.2 | 3    | 1474.8           | 1474             | 80               |             |               |                |      |   |   |
| 1074.2       | 1074   | 3    | 1474             | 1443             | 350              |             |               |                |      |   |   |
| 1074         | 1074   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1079         | 1078   | 2    | 1465             | 1463.5           | 75               | 0.52        | 0.13          |                |      |   |   |
| 1078         | 1074   | 5    | 1463.5           | 1443             | 250              | 0.52        | 3.12          |                |      |   |   |
| 1074         | 1074   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1074         | 1073   | 3    | 1443             | 1430             | 65               |             |               |                |      |   |   |
| 1073         | 1072   | 5    | 1430             | 1095             | 860              | 0.32        | 6.89          |                |      |   |   |
| 1072         | 1072   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1081         | 1080   | 2    | 1445             | 1400             | 100              | 0.35        | 0.56          |                |      |   |   |
| 1080         | 1072   | 5    | 1400             | 1095             | 915              | 0.33        | 6.95          |                |      |   |   |
| 1072         | 1072   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1072         | 1071   | 5    | 1095             | 980              | 525              | 0.25        | 8.44          |                |      |   |   |
| 1071         | 1071   | 10   |                  |                  |                  |             |               | Save to bank 2 |      |   |   |
| 1106         | 1105   | 2    | 1494             | 1490             | 85               | 0.52        | 0.33          |                |      |   |   |
| 1105         | 1099   | 6    | 1490             | 1463             | 580              | 0.52        | 3.43          | 2 sides        |      |   |   |
| 1099         | 1095   | 3    | 1457             | 1450.9           | 340              |             |               |                |      |   |   |



Job #:

Run Name:  
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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1095         | 1095   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1098         | 1097   | 2    | 1493             | 1491             | 80               | 0.52        | 0.56          |                |      |   |   |
| 1097         | 1096   | 6    | 1490             | 1456.8           | 745              | 0.52        | 5.27          | two sides      |      |   |   |
| 1096         | 1095   | 3    | 1450.9           | 1450.5           | 40               |             |               |                |      |   |   |
| 1095         | 1095   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1095         | 1094   | 3    | 1450.5           | 1448             | 100              |             |               |                |      |   |   |
| 1094         | 1094   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1108         | 1107   | 2    | 1477             | 1475             | 65               | 0.52        | 0.09          |                |      |   |   |
| 1107         | 1094   | 6    | 1475             | 1455             | 750              | 0.52        | 1.33          | one side       |      |   |   |
| 1094         | 1094   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1094         | 1093   | 5    | 1448             | 1447.5           | 50               | 0.35        | 0.57          |                |      |   |   |
| 1093         | 1089   | 3    | 1441.5           | 1412             | 295              |             |               |                |      |   |   |
| 1089         | 1089   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1091         | 1090   | 2    | 1466             | 1460             | 100              | 0.52        | 0.14          |                |      |   |   |
| 1090         | 1089   | 5    | 1460             | 1418             | 540              | 0.52        | 5.57          |                |      |   |   |
| 1089         | 1089   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1089         | 1088   | 3    | 1412             | 1410             | 75               |             |               |                |      |   |   |
| 1088         | 1087   | 5    | 1410             | 1295             | 365              | 0.35        | 1.81          |                |      |   |   |
| 1087         | 1085   | 3    | 1289             | 1282             | 235              |             |               |                |      |   |   |
| 1085         | 1085   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1111         | 1110   | 2    | 1435             | 1395             | 100              | 0.35        | 0.42          |                |      |   |   |
| 1110         | 1109   | 5    | 1395             | 1290             | 320              | 0.33        | 1.94          |                |      |   |   |
| 1109         | 1085   | 3    | 1284             | 1282             | 230              |             |               |                |      |   |   |
| 1085         | 1085   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1085         | 1084   | 3    | 1282             | 1279             | 495              |             |               |                |      |   |   |
| 1084         | 1083   | 3    | 1279             | 1095             | 340              |             |               |                |      |   |   |
| 1083         | 1082   | 5    | 1095             | 1005             | 735              | 0.25        | 10.02         |                |      |   |   |
| 1082         | 1082   | 10   |                  |                  |                  |             |               | Save to bank 3 |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1115         | 1114   | 2    | 1281             | 1280             | 65               | 0.51        | 0.15          |                |      |   |   |
| 1114         | 1113   | 6    | 1280             | 1278             | 130              | 0.51        | 0.75          | 1 side         |      |   |   |
| 1113         | 1112.2 | 3    | 1272             | 1269             | 395              |             |               |                |      |   |   |
| 1112.2       | 1112.2 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 1112.6       | 1112.4 | 2    | 1278             | 1277             | 65               | 0.51        | 0.12          |                |      |   |   |
| 1112.4       | 1112.2 | 6    | 1277             | 1275             | 260              | 0.51        | 2.82          | one side       |      |   |   |
| 1112.2       | 1112.2 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 170  
San Diego, California 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* PROPOSED HYDROLOGY \*  
\* BASIN 10 WITH NO DETENTION \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-10.DAT  
TIME/DATE OF STUDY: 15:00 01/11/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1010.00 TO NODE 1009.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1480.00  
DOWNSTREAM ELEVATION(FEET) = 1470.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 1.70  
TOTAL AREA(ACRES) = 0.61 TOTAL RUNOFF(CFS) = 1.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1009.00 TO NODE 1008.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1470.00 DOWNSTREAM(FEET) = 1455.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.0500  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.146  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.43  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.32  
AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 1.16  
Tc(MIN.) = 7.42  
SUBAREA AREA(ACRES) = 2.18 SUBAREA RUNOFF(CFS) = 5.45  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 6.98

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 FLOW VELOCITY(FEET/SEC.) = 4.94  
LONGEST FLOWPATH FROM NODE 1010.00 TO NODE 1008.00 = 400.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1008.00 TO NODE 1007.00 IS CODE = 51

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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1455.00 DOWNSTREAM(FEET) = 1320.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 630.00 CHANNEL SLOPE = 0.2143  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.597

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.35  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.70  
AVERAGE FLOW DEPTH(FEET) = 0.40 TRAVEL TIME(MIN.) = 0.98  
Tc(MIN.) = 8.40  
SUBAREA AREA(ACRES) = 8.11 SUBAREA RUNOFF(CFS) = 18.72  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 10.9 PEAK FLOW RATE(CFS) = 25.17

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.51 FLOW VELOCITY(FEET/SEC.) = 12.15  
LONGEST FLOWPATH FROM NODE 1010.00 TO NODE 1007.00 = 1030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1007.00 TO NODE 1006.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1320.00 DOWNSTREAM(FEET) = 1160.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 695.00 CHANNEL SLOPE = 0.2302  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.235

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 47.61  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.10  
AVERAGE FLOW DEPTH(FEET) = 0.71 TRAVEL TIME(MIN.) = 0.77  
Tc(MIN.) = 9.17  
SUBAREA AREA(ACRES) = 20.56 SUBAREA RUNOFF(CFS) = 44.87  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 31.5 PEAK FLOW RATE(CFS) = 68.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.86 FLOW VELOCITY(FEET/SEC.) = 16.78  
LONGEST FLOWPATH FROM NODE 1010.00 TO NODE 1006.00 = 1725.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1006.00 TO NODE 1006.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.17  
RAINFALL INTENSITY(INCH/HR) = 6.24  
TOTAL STREAM AREA(ACRES) = 31.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 68.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 1014.00 TO NODE 1013.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1620.00  
DOWNSTREAM ELEVATION(FEET) = 1590.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.427  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.747  
SUBAREA RUNOFF(CFS) = 0.21  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.21

\*\*\*\*\*

FLOW PROCESS FROM NODE 1013.00 TO NODE 1012.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1590.00 DOWNSTREAM(FEET) = 1515.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 270.00 CHANNEL SLOPE = 0.2778  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.879  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.21  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.71  
AVERAGE FLOW DEPTH(FEET) = 0.08 TRAVEL TIME(MIN.) = 0.95

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Tc(MIN.) = 6.38  
SUBAREA AREA(ACRES) = 0.72 SUBAREA RUNOFF(CFS) = 1.99  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.18

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 5.74  
LONGEST FLOWPATH FROM NODE 1014.00 TO NODE 1012.00 = 345.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1012.00 TO NODE 1011.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1515.00 DOWNSTREAM(FEET) = 1450.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 565.00 CHANNEL SLOPE = 0.1150  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.909

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.70  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.53  
AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 1.44  
Tc(MIN.) = 7.82  
SUBAREA AREA(ACRES) = 3.73 SUBAREA RUNOFF(CFS) = 9.02  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 10.93

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 FLOW VELOCITY(FEET/SEC.) = 7.55  
LONGEST FLOWPATH FROM NODE 1014.00 TO NODE 1011.00 = 910.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1011.00 TO NODE 1006.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1450.00 DOWNSTREAM(FEET) = 1160.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1530.00 CHANNEL SLOPE = 0.1895  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.092

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500

P-10.TXT

S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 60.43
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.13
AVERAGE FLOW DEPTH(FEET) = 0.85 TRAVEL TIME(MIN.) = 1.68
Tc(MIN.) = 9.51
SUBAREA AREA(ACRES) = 46.29 SUBAREA RUNOFF(CFS) = 98.70
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350
TOTAL AREA(ACRES) = 50.8 PEAK FLOW RATE(CFS) = 108.34

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 1.15 FLOW VELOCITY(FEET/SEC.) = 17.79
LONGEST FLOWPATH FROM NODE 1014.00 TO NODE 1006.00 = 2440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1006.00 TO NODE 1006.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.51
RAINFALL INTENSITY(INCH/HR) = 6.09
TOTAL STREAM AREA(ACRES) = 50.81
PEAK FLOW RATE(CFS) AT CONFLUENCE = 108.34

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 175.42 Tc(MIN.) = 9.51
TOTAL AREA(ACRES) = 82.3
LONGEST FLOWPATH FROM NODE 1014.00 TO NODE 1006.00 = 2440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1006.00 TO NODE 1005.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1160.00 DOWNSTREAM(FEET) = 945.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1180.00 CHANNEL SLOPE = 0.1822  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.735  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 215.70  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 21.03  
AVERAGE FLOW DEPTH(FEET) = 1.64 TRAVEL TIME(MIN.) = 0.94  
Tc(MIN.) = 10.44  
SUBAREA AREA(ACRES) = 40.13 SUBAREA RUNOFF(CFS) = 80.54  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 122.4 PEAK FLOW RATE(CFS) = 245.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.74 FLOW VELOCITY(FEET/SEC.) = 21.74  
LONGEST FLOWPATH FROM NODE 1014.00 TO NODE 1005.00 = 3620.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1005.00 TO NODE 1005.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1027.00 TO NODE 1026.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1680.00  
DOWNSTREAM ELEVATION(FEET) = 1640.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.28  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1026.00 TO NODE 1025.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1640.00 DOWNSTREAM(FEET) = 1495.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 460.00 CHANNEL SLOPE = 0.3152  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.109  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.26  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.29  
AVERAGE FLOW DEPTH(FEET) = 0.11 TRAVEL TIME(MIN.) = 1.22  
Tc(MIN.) = 7.49  
SUBAREA AREA(ACRES) = 1.59 SUBAREA RUNOFF(CFS) = 3.96  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 4.20

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 7.75  
LONGEST FLOWPATH FROM NODE 1027.00 TO NODE 1025.00 = 560.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1025.00 TO NODE 1024.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1495.00 DOWNSTREAM(FEET) = 1485.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.41  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.20  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 7.62  
LONGEST FLOWPATH FROM NODE 1027.00 TO NODE 1024.00 = 660.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1024.00 TO NODE 1024.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<  
=====



\*\*\*\*\*

FLOW PROCESS FROM NODE 1035.00 TO NODE 1034.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00

UPSTREAM ELEVATION(FEET) = 1531.80

DOWNSTREAM ELEVATION(FEET) = 1531.20

ELEVATION DIFFERENCE(FEET) = 0.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.788

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.58

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 1034.00 TO NODE 1033.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1531.20 DOWNSTREAM ELEVATION(FEET) = 1511.00

STREET LENGTH(FEET) = 455.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.07

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.24

HALFSTREET FLOOD WIDTH(FEET) = 5.52

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.63

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86

STREET FLOW TRAVEL TIME(MIN.) = 2.09 Tc(MIN.) = 4.88

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 4.98  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 5.56

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.51  
FLOW VELOCITY(FEET/SEC.) = 4.08 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.13  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1033.00 = 515.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1033.00 TO NODE 1031.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1510.00 DOWNSTREAM(FEET) = 1500.00  
FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.56  
PIPE TRAVEL TIME(MIN.) = 1.16 Tc(MIN.) = 6.03  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1031.00 = 1030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1031.00 TO NODE 1031.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.03  
RAINFALL INTENSITY(INCH/HR) = 8.17  
TOTAL STREAM AREA(ACRES) = 0.67  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 1033.00 TO NODE 1032.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1510.00

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DOWNSTREAM ELEVATION(FEET) = 1508.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.996  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 1032.00 TO NODE 1031.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1508.00 DOWNSTREAM ELEVATION(FEET) = 1500.00  
STREET LENGTH(FEET) = 460.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.67  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.58  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.42  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.62  
STREET FLOW TRAVEL TIME(MIN.) = 3.17 Tc(MIN.) = 5.16  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.032

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.45 SUBAREA RUNOFF(CFS) = 3.66  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 4.47

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.44  
FLOW VELOCITY(FEET/SEC.) = 2.69 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.79  
LONGEST FLOWPATH FROM NODE 1033.00 TO NODE 1031.00 = 525.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1031.00 TO NODE 1031.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.16
RAINFALL INTENSITY(INCH/HR) = 9.03
TOTAL STREAM AREA(ACRES) = 0.55
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.47

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 9.61 Tc(MIN.) = 6.03
TOTAL AREA(ACRES) = 1.2
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1031.00 = 1030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1031.00 TO NODE 1029.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1500.00 DOWNSTREAM(FEET) = 1485.00
FLOW LENGTH(FEET) = 430.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.61
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.61
PIPE TRAVEL TIME(MIN.) = 0.68 Tc(MIN.) = 6.71
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1029.00 = 1460.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 1029.00 TO NODE 1029.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.71  
RAINFALL INTENSITY(INCH/HR) = 7.63  
TOTAL STREAM AREA(ACRES) = 1.22  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.61

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1031.00 TO NODE 1030.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1500.00  
DOWNSTREAM ELEVATION(FEET) = 1498.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.996  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1030.00 TO NODE 1029.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1498.00 DOWNSTREAM ELEVATION(FEET) = 1485.00  
STREET LENGTH(FEET) = 365.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.95  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.22  
 HALFSTREET FLOOD WIDTH(FEET) = 4.46  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.08  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.66  
 STREET FLOW TRAVEL TIME(MIN.) = 1.98 Tc(MIN.) = 3.97  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 0.35 SUBAREA RUNOFF(CFS) = 2.90  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.40

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.18  
 FLOW VELOCITY(FEET/SEC.) = 3.40 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.85  
 LONGEST FLOWPATH FROM NODE 1031.00 TO NODE 1029.00 = 430.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1029.00 TO NODE 1029.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 3.97  
 RAINFALL INTENSITY(INCH/HR) = 9.22  
 TOTAL STREAM AREA(ACRES) = 0.41  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.40

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.61         | 6.71      | 7.630                 | 1.22        |
| 2             | 3.40         | 3.97      | 9.222                 | 0.41        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.35        | 3.97      | 9.222                 |

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2 12.42 6.71 7.630

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.42 Tc(MIN.) = 6.71
TOTAL AREA(ACRES) = 1.6
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1029.00 = 1460.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1029.00 TO NODE 1024.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1485.00 DOWNSTREAM(FEET) = 1480.00
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.68
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.42
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.77
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1024.00 = 1520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1024.00 TO NODE 1024.00 IS CODE = 11

-----

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 12.42 6.77 7.584 1.63
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1024.00 = 1520.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 4.20 7.62 7.027 1.69
LONGEST FLOWPATH FROM NODE 1027.00 TO NODE 1024.00 = 660.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 16.16 6.77 7.584
2 15.71 7.62 7.027

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

P-10.TXT  
PEAK FLOW RATE(CFS) = 16.16 Tc(MIN.) = 6.77  
TOTAL AREA(ACRES) = 3.3

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1024.00 TO NODE 1024.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 2 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1024.00 TO NODE 1021.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1480.00 DOWNSTREAM(FEET) = 1475.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.94  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.16  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 6.82  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1021.00 = 1570.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1021.00 TO NODE 1021.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.82  
RAINFALL INTENSITY(INCH/HR) = 7.55  
TOTAL STREAM AREA(ACRES) = 3.32  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1023.00 TO NODE 1022.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1485.00  
DOWNSTREAM ELEVATION(FEET) = 1484.00



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ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.514  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 2.66  
TOTAL AREA(ACRES) = 0.32 TOTAL RUNOFF(CFS) = 2.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 1022.00 TO NODE 1021.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1479.00 DOWNSTREAM(FEET) = 1475.00  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.40  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.66  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 2.62  
LONGEST FLOWPATH FROM NODE 1023.00 TO NODE 1021.00 = 125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1021.00 TO NODE 1021.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.62  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.32  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.66

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.16        | 6.82      | 7.550                 | 3.32        |
| 2             | 2.66         | 2.62      | 9.222                 | 0.32        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.16        | 6.82      | 7.550                 |
| 2             | 2.66         | 2.62      | 9.222                 |

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|   |       |      |       |
|---|-------|------|-------|
| 1 | 8.87  | 2.62 | 9.222 |
| 2 | 18.33 | 6.82 | 7.550 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 18.33 Tc(MIN.) = 6.82

TOTAL AREA(ACRES) = 3.6

LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1021.00 = 1570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1021.00 TO NODE 1020.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1475.00 DOWNSTREAM(FEET) = 1440.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1167

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.205

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 23.77

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.75

AVERAGE FLOW DEPTH(FEET) = 0.58 TRAVEL TIME(MIN.) = 0.51

Tc(MIN.) = 7.33

SUBAREA AREA(ACRES) = 4.30 SUBAREA RUNOFF(CFS) = 10.84

AREA-AVERAGE RUNOFF COEFFICIENT = 0.485

TOTAL AREA(ACRES) = 7.9 PEAK FLOW RATE(CFS) = 27.75

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.64 FLOW VELOCITY(FEET/SEC.) = 10.17

LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1020.00 = 1870.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1020.00 TO NODE 1019.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1440.00 DOWNSTREAM(FEET) = 1430.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 140.00 CHANNEL SLOPE = 0.0714

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.040

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

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TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 29.48  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.70  
AVERAGE FLOW DEPTH(FEET) = 0.75 TRAVEL TIME(MIN.) = 0.27  
Tc(MIN.) = 7.60  
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 3.45  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.465  
TOTAL AREA(ACRES) = 9.3 PEAK FLOW RATE(CFS) = 30.56

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.77 FLOW VELOCITY(FEET/SEC.) = 8.78  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1019.00 = 2010.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1019.00 TO NODE 1019.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.60  
RAINFALL INTENSITY(INCH/HR) = 7.04  
TOTAL STREAM AREA(ACRES) = 9.34  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 1039.00 TO NODE 1038.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1690.00  
DOWNSTREAM ELEVATION(FEET) = 1665.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.605  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.567  
SUBAREA RUNOFF(CFS) = 1.02  
TOTAL AREA(ACRES) = 0.34 TOTAL RUNOFF(CFS) = 1.02

\*\*\*\*\*

FLOW PROCESS FROM NODE 1038.00 TO NODE 1037.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1665.00 DOWNSTREAM(FEET) = 1520.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 285.00 CHANNEL SLOPE = 0.5088  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.105  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.66  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.44  
AVERAGE FLOW DEPTH(FEET) = 0.15 TRAVEL TIME(MIN.) = 0.50  
Tc(MIN.) = 6.11  
SUBAREA AREA(ACRES) = 2.57 SUBAREA RUNOFF(CFS) = 7.29  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 2.9 PEAK FLOW RATE(CFS) = 8.25

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.21 FLOW VELOCITY(FEET/SEC.) = 11.45  
LONGEST FLOWPATH FROM NODE 1039.00 TO NODE 1037.00 = 365.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1037.00 TO NODE 1036.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1514.00 DOWNSTREAM(FEET) = 1490.00  
FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.80  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.25  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.17  
LONGEST FLOWPATH FROM NODE 1039.00 TO NODE 1036.00 = 450.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1036.00 TO NODE 1019.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1490.00 DOWNSTREAM(FEET) = 1430.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 335.00 CHANNEL SLOPE = 0.1791  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.544  
\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.08  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.55  
 AVERAGE FLOW DEPTH(FEET) = 0.32 TRAVEL TIME(MIN.) = 0.65  
 Tc(MIN.) = 6.83  
 SUBAREA AREA(ACRES) = 1.38 SUBAREA RUNOFF(CFS) = 3.64  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
 TOTAL AREA(ACRES) = 4.3 PEAK FLOW RATE(CFS) = 11.33

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.34 FLOW VELOCITY(FEET/SEC.) = 9.04  
 LONGEST FLOWPATH FROM NODE 1039.00 TO NODE 1019.00 = 785.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1019.00 TO NODE 1019.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.83  
 RAINFALL INTENSITY(INCH/HR) = 7.54  
 TOTAL STREAM AREA(ACRES) = 4.29  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.33

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 30.56        | 7.60      | 7.040                 | 9.34        |
| 2             | 11.33        | 6.83      | 7.544                 | 4.29        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 39.85        | 6.83      | 7.544                 |
| 2             | 41.14        | 7.60      | 7.040                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 41.14 Tc(MIN.) = 7.60  
 TOTAL AREA(ACRES) = 13.6  
 LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1019.00 = 2010.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1019.00 TO NODE 1018.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1430.00 DOWNSTREAM(FEET) = 1420.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 100.00 CHANNEL SLOPE = 0.1000
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.949

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.59
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.81
AVERAGE FLOW DEPTH(FEET) = 0.83 TRAVEL TIME(MIN.) = 0.15
Tc(MIN.) = 7.75
SUBAREA AREA(ACRES) = 0.37 SUBAREA RUNOFF(CFS) = 0.90
AREA-AVERAGE RUNOFF COEFFICIENT = 0.427
TOTAL AREA(ACRES) = 14.0 PEAK FLOW RATE(CFS) = 41.51

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.83 FLOW VELOCITY(FEET/SEC.) = 10.79
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1018.00 = 2110.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1018.00 TO NODE 1018.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*
FLOW PROCESS FROM NODE 1044.00 TO NODE 1043.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1733.00
DOWNSTREAM ELEVATION(FEET) = 1720.00
ELEVATION DIFFERENCE(FEET) = 13.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972
SUBAREA RUNOFF(CFS) = 0.78
TOTAL AREA(ACRES) = 0.28 TOTAL RUNOFF(CFS) = 0.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 1043.00 TO NODE 1042.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1720.00 DOWNSTREAM(FEET) = 1510.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 520.00 CHANNEL SLOPE = 0.4038  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.232

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.60  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.48  
AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 1.02  
Tc(MIN.) = 7.29  
SUBAREA AREA(ACRES) = 3.01 SUBAREA RUNOFF(CFS) = 7.62  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 8.33

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 FLOW VELOCITY(FEET/SEC.) = 10.67  
LONGEST FLOWPATH FROM NODE 1044.00 TO NODE 1042.00 = 620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1042.00 TO NODE 1041.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1504.00 DOWNSTREAM(FEET) = 1500.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.88  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.33  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 7.35  
LONGEST FLOWPATH FROM NODE 1044.00 TO NODE 1041.00 = 670.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1041.00 TO NODE 1040.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1500.00 DOWNSTREAM(FEET) = 1450.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 160.00 CHANNEL SLOPE = 0.3125  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.030

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.71  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.00  
AVERAGE FLOW DEPTH(FEET) = 0.25 TRAVEL TIME(MIN.) = 0.27  
Tc(MIN.) = 7.62  
SUBAREA AREA(ACRES) = 0.31 SUBAREA RUNOFF(CFS) = 0.76  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 3.6 PEAK FLOW RATE(CFS) = 8.86

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 FLOW VELOCITY(FEET/SEC.) = 9.91  
LONGEST FLOWPATH FROM NODE 1044.00 TO NODE 1040.00 = 830.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1040.00 TO NODE 1040.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.62  
RAINFALL INTENSITY(INCH/HR) = 7.03  
TOTAL STREAM AREA(ACRES) = 3.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.86

\*\*\*\*\*

FLOW PROCESS FROM NODE 1048.00 TO NODE 1047.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1715.00  
DOWNSTREAM ELEVATION(FEET) = 1675.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972



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SUBAREA RUNOFF(CFS) = 0.56  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.56

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1047.00 TO NODE 1046.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1675.00 DOWNSTREAM(FEET) = 1515.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 465.00 CHANNEL SLOPE = 0.3441  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.209

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.42  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.33  
AVERAGE FLOW DEPTH(FEET) = 0.14 TRAVEL TIME(MIN.) = 1.06  
Tc(MIN.) = 7.32  
SUBAREA AREA(ACRES) = 2.26 SUBAREA RUNOFF(CFS) = 5.70  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 6.21

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.20 FLOW VELOCITY(FEET/SEC.) = 9.07  
LONGEST FLOWPATH FROM NODE 1048.00 TO NODE 1046.00 = 565.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1046.00 TO NODE 1045.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1509.00 DOWNSTREAM(FEET) = 1500.00  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.58  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.21  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 7.39  
LONGEST FLOWPATH FROM NODE 1048.00 TO NODE 1045.00 = 630.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1045.00 TO NODE 1040.00 IS CODE = 51

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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1500.00 DOWNSTREAM(FEET) = 1450.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 195.00 CHANNEL SLOPE = 0.2564
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.938

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.69
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.58
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 0.38
Tc(MIN.) = 7.77
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.97
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350
TOTAL AREA(ACRES) = 2.9 PEAK FLOW RATE(CFS) = 6.94

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 FLOW VELOCITY(FEET/SEC.) = 8.57
LONGEST FLOWPATH FROM NODE 1048.00 TO NODE 1040.00 = 825.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1040.00 TO NODE 1040.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.77
RAINFALL INTENSITY(INCH/HR) = 6.94
TOTAL STREAM AREA(ACRES) = 2.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.94

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR)

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|   |       |      |       |
|---|-------|------|-------|
| 1 | 15.66 | 7.62 | 7.030 |
| 2 | 15.69 | 7.77 | 6.938 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.69 Tc(MIN.) = 7.77

TOTAL AREA(ACRES) = 6.5

LONGEST FLOWPATH FROM NODE 1044.00 TO NODE 1040.00 = 830.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1040.00 TO NODE 1018.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1450.00 DOWNSTREAM(FEET) = 1420.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 195.00 CHANNEL SLOPE = 0.1538

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 3.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.738

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.23

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.00

AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 0.36

Tc(MIN.) = 8.13

SUBAREA AREA(ACRES) = 0.46 SUBAREA RUNOFF(CFS) = 1.08

AREA-AVERAGE RUNOFF COEFFICIENT = 0.350

TOTAL AREA(ACRES) = 6.9 PEAK FLOW RATE(CFS) = 16.32

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 FLOW VELOCITY(FEET/SEC.) = 9.05

LONGEST FLOWPATH FROM NODE 1044.00 TO NODE 1018.00 = 1025.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1018.00 TO NODE 1018.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.32        | 8.13      | 6.738                 | 6.92        |

LONGEST FLOWPATH FROM NODE 1044.00 TO NODE 1018.00 = 1025.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM | RUNOFF | Tc | INTENSITY | AREA |
|--------|--------|----|-----------|------|
|--------|--------|----|-----------|------|

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 41.51 | 7.75   | 6.949       | 14.00  |

LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1018.00 = 2110.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 57.06        | 7.75      | 6.949                 |
| 2             | 56.56        | 8.13      | 6.738                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 57.06 Tc(MIN.) = 7.75  
TOTAL AREA(ACRES) = 20.9

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1018.00 TO NODE 1018.00 IS CODE = 12  
-----

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1018.00 TO NODE 1017.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1420.00 DOWNSTREAM(FEET) = 1355.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 370.00 CHANNEL SLOPE = 0.1757  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.720

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 62.69  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 14.92  
AVERAGE FLOW DEPTH(FEET) = 0.88 TRAVEL TIME(MIN.) = 0.41  
Tc(MIN.) = 8.17  
SUBAREA AREA(ACRES) = 4.79 SUBAREA RUNOFF(CFS) = 11.27  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.392  
TOTAL AREA(ACRES) = 25.7 PEAK FLOW RATE(CFS) = 67.68

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.92 FLOW VELOCITY(FEET/SEC.) = 15.19  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1017.00 = 2480.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1017.00 TO NODE 1016.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1355.00 DOWNSTREAM(FEET) = 1340.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 195.00 CHANNEL SLOPE = 0.0769  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.573  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 70.10  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.40  
AVERAGE FLOW DEPTH(FEET) = 1.16 TRAVEL TIME(MIN.) = 0.28  
Tc(MIN.) = 8.45  
SUBAREA AREA(ACRES) = 2.10 SUBAREA RUNOFF(CFS) = 4.83  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.389  
TOTAL AREA(ACRES) = 27.8 PEAK FLOW RATE(CFS) = 71.03

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.16 FLOW VELOCITY(FEET/SEC.) = 11.45  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1016.00 = 2675.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1016.00 TO NODE 1016.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.45  
RAINFALL INTENSITY(INCH/HR) = 6.57  
TOTAL STREAM AREA(ACRES) = 27.81  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 71.03

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1052.00 TO NODE 1051.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1615.00  
DOWNSTREAM ELEVATION(FEET) = 1605.00  
ELEVATION DIFFERENCE(FEET) = 10.00

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SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.47  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1051.00 TO NODE 1050.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1605.00 DOWNSTREAM(FEET) = 1535.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 250.00 CHANNEL SLOPE = 0.2800  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.432  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.20  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.79  
AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) = 0.72  
Tc(MIN.) = 6.99  
SUBAREA AREA(ACRES) = 1.32 SUBAREA RUNOFF(CFS) = 3.43  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 3.88

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 7.14  
LONGEST FLOWPATH FROM NODE 1052.00 TO NODE 1050.00 = 350.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1050.00 TO NODE 1049.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1524.00 DOWNSTREAM(FEET) = 1475.00  
FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.37  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.88  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.10  
LONGEST FLOWPATH FROM NODE 1052.00 TO NODE 1049.00 = 480.00 FEET.

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\*\*\*\*\*

FLOW PROCESS FROM NODE 1049.00 TO NODE 1016.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1475.00 DOWNSTREAM(FEET) = 1340.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 395.00 CHANNEL SLOPE = 0.3418  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.943

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.73  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.90  
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 0.66  
Tc(MIN.) = 7.76  
SUBAREA AREA(ACRES) = 3.17 SUBAREA RUNOFF(CFS) = 7.70  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 11.32

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 11.12  
LONGEST FLOWPATH FROM NODE 1052.00 TO NODE 1016.00 = 875.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1016.00 TO NODE 1016.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.76  
RAINFALL INTENSITY(INCH/HR) = 6.94  
TOTAL STREAM AREA(ACRES) = 4.66  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.32

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 71.03        | 8.45      | 6.573                 | 27.81       |
| 2             | 11.32        | 7.76      | 6.943                 | 4.66        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

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\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 76.58        | 7.76      | 6.943                 |
| 2             | 81.75        | 8.45      | 6.573                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 81.75 Tc(MIN.) = 8.45  
TOTAL AREA(ACRES) = 32.5  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1016.00 = 2675.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1016.00 TO NODE 1015.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1340.00 DOWNSTREAM(FEET) = 1080.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1015.00 CHANNEL SLOPE = 0.2562  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.165  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 95.35  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 19.16  
AVERAGE FLOW DEPTH(FEET) = 1.00 TRAVEL TIME(MIN.) = 0.88  
Tc(MIN.) = 9.33  
SUBAREA AREA(ACRES) = 12.60 SUBAREA RUNOFF(CFS) = 27.19  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.374  
TOTAL AREA(ACRES) = 45.1 PEAK FLOW RATE(CFS) = 103.87

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.04 FLOW VELOCITY(FEET/SEC.) = 19.60  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1015.00 = 3690.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1058.00 TO NODE 1057.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<



```

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1735.00
DOWNSTREAM ELEVATION(FEET) = 1712.00
ELEVATION DIFFERENCE(FEET) = 23.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972
SUBAREA RUNOFF(CFS) = 0.81
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.81

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*****
FLOW PROCESS FROM NODE 1057.00 TO NODE 1056.00 IS CODE = 51
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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====

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```

ELEVATION DATA: UPSTREAM(FEET) = 1712.00 DOWNSTREAM(FEET) = 1585.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 435.00 CHANNEL SLOPE = 0.2920
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.236

```

```

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.68
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.14
AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 1.01
Tc(MIN.) = 7.28
SUBAREA AREA(ACRES) = 2.26 SUBAREA RUNOFF(CFS) = 5.72
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 6.46

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 8.69
LONGEST FLOWPATH FROM NODE 1058.00 TO NODE 1056.00 = 535.00 FEET.

```

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*****
FLOW PROCESS FROM NODE 1056.00 TO NODE 1055.00 IS CODE = 31
-----

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```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

```

```

ELEVATION DATA: UPSTREAM(FEET) = 1579.00 DOWNSTREAM(FEET) = 1560.00
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

```

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DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.05  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.46  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.39  
LONGEST FLOWPATH FROM NODE 1058.00 TO NODE 1055.00 = 645.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1055.00 TO NODE 1054.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1560.00 DOWNSTREAM(FEET) = 1510.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 190.00 CHANNEL SLOPE = 0.2632  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.968  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.45  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.57  
AVERAGE FLOW DEPTH(FEET) = 0.28 TRAVEL TIME(MIN.) = 0.33  
Tc(MIN.) = 7.72  
SUBAREA AREA(ACRES) = 2.45 SUBAREA RUNOFF(CFS) = 5.98  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 12.19

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 FLOW VELOCITY(FEET/SEC.) = 10.34  
LONGEST FLOWPATH FROM NODE 1058.00 TO NODE 1054.00 = 835.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1054.00 TO NODE 1054.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.72  
RAINFALL INTENSITY(INCH/HR) = 6.97  
TOTAL STREAM AREA(ACRES) = 5.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1061.00 TO NODE 1060.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1750.00
DOWNSTREAM ELEVATION(FEET) = 1730.00
ELEVATION DIFFERENCE(FEET) = 20.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.605
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.567
SUBAREA RUNOFF(CFS) = 0.33
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.33

```

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*****
FLOW PROCESS FROM NODE 1060.00 TO NODE 1059.40 IS CODE = 51
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```

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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=====
ELEVATION DATA: UPSTREAM(FEET) = 1730.00 DOWNSTREAM(FEET) = 1545.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.3083
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.575

```

```

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.81
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.49
AVERAGE FLOW DEPTH(FEET) = 0.20 TRAVEL TIME(MIN.) = 1.18
Tc(MIN.) = 6.78
SUBAREA AREA(ACRES) = 4.11 SUBAREA RUNOFF(CFS) = 10.90
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350
TOTAL AREA(ACRES) = 4.2 PEAK FLOW RATE(CFS) = 11.19

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 10.66
LONGEST FLOWPATH FROM NODE 1061.00 TO NODE 1059.40 = 680.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 1059.40 TO NODE 1059.20 IS CODE = 31
-----

```

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1539.00 DOWNSTREAM(FEET) = 1535.00

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FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.63
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.19
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 6.83
LONGEST FLOWPATH FROM NODE 1061.00 TO NODE 1059.20 = 725.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1059.20 TO NODE 1054.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1535.00 DOWNSTREAM(FEET) = 1510.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 130.00 CHANNEL SLOPE = 0.1923
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 11.19
FLOW VELOCITY(FEET/SEC) = 8.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 7.10
LONGEST FLOWPATH FROM NODE 1061.00 TO NODE 1054.00 = 855.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1054.00 TO NODE 1054.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.10
RAINFALL INTENSITY(INCH/HR) = 7.36
TOTAL STREAM AREA(ACRES) = 4.22
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.19

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR)

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|   |       |      |       |
|---|-------|------|-------|
| 1 | 22.40 | 7.10 | 7.357 |
| 2 | 22.79 | 7.72 | 6.968 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 22.79 Tc(MIN.) = 7.72

TOTAL AREA(ACRES) = 9.2

LONGEST FLOWPATH FROM NODE 1061.00 TO NODE 1054.00 = 855.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1054.00 TO NODE 1053.20 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1504.00 DOWNSTREAM(FEET) = 1485.00

FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.3 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 24.88

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 22.79

PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 7.79

LONGEST FLOWPATH FROM NODE 1061.00 TO NODE 1053.20 = 955.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1053.20 TO NODE 1053.00 IS CODE = 52

-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1485.00 DOWNSTREAM(FEET) = 1448.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 175.00 CHANNEL SLOPE = 0.2114

NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION

CHANNEL FLOW THRU SUBAREA(CFS) = 22.79

FLOW VELOCITY(FEET/SEC) = 9.82 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 8.08

LONGEST FLOWPATH FROM NODE 1061.00 TO NODE 1053.00 = 1130.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1053.00 TO NODE 1053.00 IS CODE = 10

-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 1128.00 TO NODE 1126.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 1530.00  
DOWNSTREAM ELEVATION(FEET) = 1526.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.685  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.58  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 1126.00 TO NODE 1063.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1526.00 DOWNSTREAM ELEVATION(FEET) = 1465.00  
STREET LENGTH(FEET) = 720.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.48  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 6.31  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.30  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.34  
STREET FLOW TRAVEL TIME(MIN.) = 2.26 Tc(MIN.) = 3.95  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.18 SUBAREA RUNOFF(CFS) = 9.79  
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 10.37

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.57  
FLOW VELOCITY(FEET/SEC.) = 6.08 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.81  
LONGEST FLOWPATH FROM NODE 1128.00 TO NODE 1063.00 = 790.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1063.00 TO NODE 1062.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1464.00 DOWNSTREAM(FEET) = 1458.00  
FLOW LENGTH(FEET) = 185.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.53  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.37  
PIPE TRAVEL TIME(MIN.) = 0.29 Tc(MIN.) = 4.24  
LONGEST FLOWPATH FROM NODE 1128.00 TO NODE 1062.00 = 975.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1062.00 TO NODE 1062.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.24  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.25  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.37

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1062.40 TO NODE 1062.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1495.00  
DOWNSTREAM ELEVATION(FEET) = 1490.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.106  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.107

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SUBAREA RUNOFF(CFS) = 0.72  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 1062.20 TO NODE 1062.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1490.00 DOWNSTREAM(FEET) = 1458.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.0800  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.167

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.83  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.19  
AVERAGE FLOW DEPTH(FEET) = 0.26 TRAVEL TIME(MIN.) = 1.29  
Tc(MIN.) = 7.39  
SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 8.20  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 8.83

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 FLOW VELOCITY(FEET/SEC.) = 6.25  
LONGEST FLOWPATH FROM NODE 1062.40 TO NODE 1062.00 = 500.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1062.00 TO NODE 1062.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.39  
RAINFALL INTENSITY(INCH/HR) = 7.17  
TOTAL STREAM AREA(ACRES) = 2.37  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.83

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.37        | 4.24      | 9.222                 | 1.25        |
| 2             | 8.83         | 7.39      | 7.167                 | 2.37        |



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RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 15.44        | 4.24      | 9.222                 |
| 2             | 16.89        | 7.39      | 7.167                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.89 Tc(MIN.) = 7.39  
TOTAL AREA(ACRES) = 3.6  
LONGEST FLOWPATH FROM NODE 1128.00 TO NODE 1062.00 = 975.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1062.00 TO NODE 1053.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1452.00 DOWNSTREAM(FEET) = 1448.00  
FLOW LENGTH(FEET) = 280.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.49  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.89  
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 7.94  
LONGEST FLOWPATH FROM NODE 1128.00 TO NODE 1053.00 = 1255.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1053.00 TO NODE 1053.00 IS CODE = 11

-----

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.89        | 7.94      | 6.843                 | 3.62        |

LONGEST FLOWPATH FROM NODE 1128.00 TO NODE 1053.00 = 1255.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 22.79        | 8.08      | 6.764                 | 9.22        |

LONGEST FLOWPATH FROM NODE 1061.00 TO NODE 1053.00 = 1130.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| P-10.TXT      |              |           |                       |
|---------------|--------------|-----------|-----------------------|
| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
| 1             | 39.28        | 7.94      | 6.843                 |
| 2             | 39.49        | 8.08      | 6.764                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 39.49 Tc(MIN.) = 8.08  
TOTAL AREA(ACRES) = 12.8

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1053.00 TO NODE 1053.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1053.00 TO NODE 1015.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1448.00 DOWNSTREAM(FEET) = 1080.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1280.00 CHANNEL SLOPE = 0.2875  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.166

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 54.78  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 17.08  
AVERAGE FLOW DEPTH(FEET) = 0.72 TRAVEL TIME(MIN.) = 1.25  
Tc(MIN.) = 9.33  
SUBAREA AREA(ACRES) = 14.13 SUBAREA RUNOFF(CFS) = 30.49  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.390  
TOTAL AREA(ACRES) = 27.0 PEAK FLOW RATE(CFS) = 64.92

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.79 FLOW VELOCITY(FEET/SEC.) = 17.93  
LONGEST FLOWPATH FROM NODE 1128.00 TO NODE 1015.00 = 2535.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1070.00 TO NODE 1069.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00
UPSTREAM ELEVATION(FEET) = 1605.00
DOWNSTREAM ELEVATION(FEET) = 1585.00
ELEVATION DIFFERENCE(FEET) = 20.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.778
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.401
SUBAREA RUNOFF(CFS) = 0.38
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.38

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*****
FLOW PROCESS FROM NODE 1069.00 TO NODE 1068.00 IS CODE = 51

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-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1585.00 DOWNSTREAM(FEET) = 1525.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 405.00 CHANNEL SLOPE = 0.1481
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.270
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.14
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.65
AVERAGE FLOW DEPTH(FEET) = 0.14 TRAVEL TIME(MIN.) = 1.45
Tc(MIN.) = 7.23
SUBAREA AREA(ACRES) = 1.37 SUBAREA RUNOFF(CFS) = 3.49
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 3.82

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```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.19 FLOW VELOCITY(FEET/SEC.) = 5.82
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1068.00 = 490.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 1068.00 TO NODE 1066.00 IS CODE = 31

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-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====

ELEVATION DATA: UPSTREAM(FEET) = 1519.00 DOWNSTREAM(FEET) = 1470.00  
FLOW LENGTH(FEET) = 710.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.56  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.82  
PIPE TRAVEL TIME(MIN.) = 1.12 Tc(MIN.) = 8.35  
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1066.00 = 1200.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1066.00 TO NODE 1064.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1470.00 DOWNSTREAM(FEET) = 1410.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 380.00 CHANNEL SLOPE = 0.1579  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.182  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.43  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.70  
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 0.94  
Tc(MIN.) = 9.29  
SUBAREA AREA(ACRES) = 1.49 SUBAREA RUNOFF(CFS) = 3.22  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 6.47

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.26 FLOW VELOCITY(FEET/SEC.) = 7.18  
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1064.00 = 1580.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1064.00 TO NODE 1064.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.29  
RAINFALL INTENSITY(INCH/HR) = 6.18  
TOTAL STREAM AREA(ACRES) = 2.99  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1065.40 TO NODE 1065.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1495.00  
DOWNSTREAM ELEVATION(FEET) = 1493.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.520  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.770  
SUBAREA RUNOFF(CFS) = 0.61  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.61

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1065.20 TO NODE 1065.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1493.00 DOWNSTREAM(FEET) = 1438.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 780.00 CHANNEL SLOPE = 0.0705  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.421  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.00  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.80  
AVERAGE FLOW DEPTH(FEET) = 0.37 TRAVEL TIME(MIN.) = 2.24  
Tc(MIN.) = 8.76  
SUBAREA AREA(ACRES) = 4.38 SUBAREA RUNOFF(CFS) = 14.63  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 15.13

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.52 FLOW VELOCITY(FEET/SEC.) = 7.14  
LONGEST FLOWPATH FROM NODE 1065.40 TO NODE 1065.00 = 855.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1065.00 TO NODE 1064.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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=====
ELEVATION DATA: UPSTREAM(FEET) = 1438.00  DOWNSTREAM(FEET) = 1410.00
FLOW LENGTH(FEET) = 120.00  MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.11
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.13
PIPE TRAVEL TIME(MIN.) = 0.08  Tc(MIN.) = 8.85
LONGEST FLOWPATH FROM NODE 1065.40 TO NODE 1064.00 = 975.00 FEET.

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*****
FLOW PROCESS FROM NODE 1064.00 TO NODE 1064.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.85
RAINFALL INTENSITY(INCH/HR) = 6.38
TOTAL STREAM AREA(ACRES) = 4.53
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.13

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.47         | 9.29      | 6.182                 | 2.99        |
| 2             | 15.13        | 8.85      | 6.383                 | 4.53        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 21.28        | 8.85      | 6.383                 |
| 2             | 21.12        | 9.29      | 6.182                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 21.28  Tc(MIN.) = 8.85
TOTAL AREA(ACRES) = 7.5
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1064.00 = 1580.00 FEET.

```

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*****
FLOW PROCESS FROM NODE 1065.00 TO NODE 1064.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1432.00 DOWNSTREAM(FEET) = 1410.00
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.13
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 21.28
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 8.93
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1064.00 = 1700.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1064.00 TO NODE 1015.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1410.00 DOWNSTREAM(FEET) = 1080.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 940.00 CHANNEL SLOPE = 0.3511
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.902
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 26.85
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 14.79
AVERAGE FLOW DEPTH(FEET) = 0.46 TRAVEL TIME(MIN.) = 1.06
Tc(MIN.) = 9.99
SUBAREA AREA(ACRES) = 5.38 SUBAREA RUNOFF(CFS) = 11.11
AREA-AVERAGE RUNOFF COEFFICIENT = 0.410
TOTAL AREA(ACRES) = 12.9 PEAK FLOW RATE(CFS) = 31.19

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.50 FLOW VELOCITY(FEET/SEC.) = 15.57
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1015.00 = 2640.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

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1 31.19 9.99 5.902 12.90  
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1015.00 = 2640.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 103.87 9.33 6.165 45.07  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1015.00 = 3690.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY  
NUMBER (CFS) (MIN.) (INCH/HOUR)  
1 133.01 9.33 6.165  
2 130.62 9.99 5.902

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 133.01 Tc(MIN.) = 9.33

TOTAL AREA(ACRES) = 58.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 133.01 9.33 6.165 57.97  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1015.00 = 3690.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 64.92 9.33 6.166 26.97  
LONGEST FLOWPATH FROM NODE 1128.00 TO NODE 1015.00 = 2535.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY  
NUMBER (CFS) (MIN.) (INCH/HOUR)  
1 197.93 9.33 6.166  
2 197.93 9.33 6.165

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 197.93 Tc(MIN.) = 9.33

TOTAL AREA(ACRES) = 84.9

\*\*\*\*\*



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FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 1005.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1080.00 DOWNSTREAM(FEET) = 950.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 830.00 CHANNEL SLOPE = 0.1566  
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 197.93  
FLOW VELOCITY(FEET/SEC) = 18.49 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.75 Tc(MIN.) = 10.08  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1005.00 = 4520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1005.00 TO NODE 1005.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 197.93       | 10.08     | 5.866                 | 84.94       |

LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1005.00 = 4520.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 245.67       | 10.44     | 5.735                 | 122.40      |

LONGEST FLOWPATH FROM NODE 1014.00 TO NODE 1005.00 = 3620.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 435.11       | 10.08     | 5.866                 |
| 2             | 439.16       | 10.44     | 5.735                 |

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COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 439.16 Tc(MIN.) = 10.44  
TOTAL AREA(ACRES) = 207.3

\*\*\*\*\*

FLOW PROCESS FROM NODE 1005.00 TO NODE 1005.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1005.00 TO NODE 1004.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 950.00 DOWNSTREAM(FEET) = 890.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 345.00 CHANNEL SLOPE = 0.1739  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.654

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 443.57

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 24.95

AVERAGE FLOW DEPTH(FEET) = 2.32 TRAVEL TIME(MIN.) = 0.23

Tc(MIN.) = 10.67

SUBAREA AREA(ACRES) = 5.20 SUBAREA RUNOFF(CFS) = 8.82

AREA-AVERAGE RUNOFF COEFFICIENT = 0.363

TOTAL AREA(ACRES) = 212.5 PEAK FLOW RATE(CFS) = 439.16

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 2.31 FLOW VELOCITY(FEET/SEC.) = 24.87

LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1004.00 = 4865.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1004.00 TO NODE 1004.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 10.67

RAINFALL INTENSITY(INCH/HR) = 5.65

TOTAL STREAM AREA(ACRES) = 212.54

PEAK FLOW RATE(CFS) AT CONFLUENCE = 439.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1144.00 TO NODE 1142.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1435.00  
DOWNSTREAM ELEVATION(FEET) = 1380.00  
ELEVATION DIFFERENCE(FEET) = 55.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.605  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.567  
SUBAREA RUNOFF(CFS) = 1.02  
TOTAL AREA(ACRES) = 0.34 TOTAL RUNOFF(CFS) = 1.02

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1142.00 TO NODE 1004.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1380.00 DOWNSTREAM(FEET) = 890.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1510.00 CHANNEL SLOPE = 0.3245  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.199  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3200  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 27.83  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 14.51  
AVERAGE FLOW DEPTH(FEET) = 0.48 TRAVEL TIME(MIN.) = 1.73  
Tc(MIN.) = 7.34  
SUBAREA AREA(ACRES) = 23.01 SUBAREA RUNOFF(CFS) = 53.01  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.320  
TOTAL AREA(ACRES) = 23.4 PEAK FLOW RATE(CFS) = 53.87

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.69 FLOW VELOCITY(FEET/SEC.) = 17.78  
LONGEST FLOWPATH FROM NODE 1144.00 TO NODE 1004.00 = 1590.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1004.00 TO NODE 1004.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.34
RAINFALL INTENSITY(INCH/HR) = 7.20
TOTAL STREAM AREA(ACRES) = 23.35
PEAK FLOW RATE(CFS) AT CONFLUENCE = 53.87

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 481.47 Tc(MIN.) = 10.67
TOTAL AREA(ACRES) = 235.9
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1004.00 = 4865.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1004.00 TO NODE 1003.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 890.00 DOWNSTREAM(FEET) = 715.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1700.00 CHANNEL SLOPE = 0.1029
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.245
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 530.69
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 21.49
AVERAGE FLOW DEPTH(FEET) = 2.84 TRAVEL TIME(MIN.) = 1.32
Tc(MIN.) = 11.99

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SUBAREA AREA(ACRES) = 62.54 SUBAREA RUNOFF(CFS) = 98.41  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.346  
TOTAL AREA(ACRES) = 298.4 PEAK FLOW RATE(CFS) = 541.86

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 2.87 FLOW VELOCITY(FEET/SEC.) = 21.58  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1003.00 = 6565.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1003.00 TO NODE 1002.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 715.00 DOWNSTREAM(FEET) = 685.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 530.00 CHANNEL SLOPE = 0.0566  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.106

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 545.39  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 17.29  
AVERAGE FLOW DEPTH(FEET) = 3.29 TRAVEL TIME(MIN.) = 0.51  
Tc(MIN.) = 12.50  
SUBAREA AREA(ACRES) = 5.54 SUBAREA RUNOFF(CFS) = 7.07  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.344  
TOTAL AREA(ACRES) = 304.0 PEAK FLOW RATE(CFS) = 541.86

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 3.28 FLOW VELOCITY(FEET/SEC.) = 17.30  
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1002.00 = 7095.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1002.00 TO NODE 1002.00 IS CODE = 10

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 1074.80 TO NODE 1074.60 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1495.00  
DOWNSTREAM ELEVATION(FEET) = 1493.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.880  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.506  
SUBAREA RUNOFF(CFS) = 0.59  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 1074.60 TO NODE 1074.40 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1493.00 DOWNSTREAM ELEVATION(FEET) = 1478.00  
STREET LENGTH(FEET) = 595.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.20  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.22  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.78  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.32  
STREET FLOW TRAVEL TIME(MIN.) = 2.63 Tc(MIN.) = 9.51  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.093

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 2.89 SUBAREA RUNOFF(CFS) = 9.16  
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 9.63

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.41  
FLOW VELOCITY(FEET/SEC.) = 4.39 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.82  
LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1074.40 = 675.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 1074.40 TO NODE 1074.20 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1474.80 DOWNSTREAM(FEET) = 1474.00  
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.43  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.63  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 9.71  
LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1074.20 = 755.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1074.20 TO NODE 1074.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1474.00 DOWNSTREAM(FEET) = 1443.00  
FLOW LENGTH(FEET) = 350.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.98  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.63  
PIPE TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 10.10  
LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1074.00 = 1105.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1074.00 TO NODE 1074.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.10  
RAINFALL INTENSITY(INCH/HR) = 5.86  
TOTAL STREAM AREA(ACRES) = 3.04  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.63

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1079.00 TO NODE 1078.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1465.00  
DOWNSTREAM ELEVATION(FEET) = 1463.50  
ELEVATION DIFFERENCE(FEET) = 1.50  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.176  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.304  
SUBAREA RUNOFF(CFS) = 0.49  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 1078.00 TO NODE 1074.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1463.50 DOWNSTREAM(FEET) = 1443.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 250.00 CHANNEL SLOPE = 0.0820  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.854

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.06  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.60  
AVERAGE FLOW DEPTH(FEET) = 0.30 TRAVEL TIME(MIN.) = 0.74  
Tc(MIN.) = 7.92  
SUBAREA AREA(ACRES) = 3.12 SUBAREA RUNOFF(CFS) = 11.12  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
TOTAL AREA(ACRES) = 3.2 PEAK FLOW RATE(CFS) = 11.58

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.43 FLOW VELOCITY(FEET/SEC.) = 6.94  
LONGEST FLOWPATH FROM NODE 1079.00 TO NODE 1074.00 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1074.00 TO NODE 1074.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.92  
RAINFALL INTENSITY(INCH/HR) = 6.85



P-10.TXT

TOTAL STREAM AREA(ACRES) = 3.25  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.58

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.63         | 10.10     | 5.858                 | 3.04        |
| 2             | 11.58        | 7.92      | 6.854                 | 3.25        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.13        | 7.92      | 6.854                 |
| 2             | 19.53        | 10.10     | 5.858                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.53 Tc(MIN.) = 10.10  
TOTAL AREA(ACRES) = 6.3  
LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1074.00 = 1105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1074.00 TO NODE 1073.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1443.00 DOWNSTREAM(FEET) = 1430.00  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.39  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.53  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 10.15  
LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1073.00 = 1170.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1073.00 TO NODE 1072.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1430.00 DOWNSTREAM(FEET) = 1095.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 860.00 CHANNEL SLOPE = 0.3895  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

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MANNING'S FACTOR = 0.030    MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.514  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.63  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.11  
 AVERAGE FLOW DEPTH(FEET) = 0.44    TRAVEL TIME(MIN.) = 0.95  
 Tc(MIN.) = 11.10  
 SUBAREA AREA(ACRES) = 6.89    SUBAREA RUNOFF(CFS) = 12.16  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.415  
 TOTAL AREA(ACRES) = 13.2    PEAK FLOW RATE(CFS) = 30.19

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.48    FLOW VELOCITY(FEET/SEC.) = 15.98  
 LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1072.00 = 2030.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1072.00 TO NODE 1072.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.10  
 RAINFALL INTENSITY(INCH/HR) = 5.51  
 TOTAL STREAM AREA(ACRES) = 13.18  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.19

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1081.00 TO NODE 1080.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1445.00  
 DOWNSTREAM ELEVATION(FEET) = 1400.00  
 ELEVATION DIFFERENCE(FEET) = 45.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
 SUBAREA RUNOFF(CFS) = 1.56  
 TOTAL AREA(ACRES) = 0.56    TOTAL RUNOFF(CFS) = 1.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 1080.00 TO NODE 1072.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1400.00 DOWNSTREAM(FEET) = 1095.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 915.00 CHANNEL SLOPE = 0.3333
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.959

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.60
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.38
AVERAGE FLOW DEPTH(FEET) = 0.26 TRAVEL TIME(MIN.) = 1.47
Tc(MIN.) = 7.74
SUBAREA AREA(ACRES) = 6.95 SUBAREA RUNOFF(CFS) = 15.96
AREA-AVERAGE RUNOFF COEFFICIENT = 0.331
TOTAL AREA(ACRES) = 7.5 PEAK FLOW RATE(CFS) = 17.33

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 FLOW VELOCITY(FEET/SEC.) = 12.56
LONGEST FLOWPATH FROM NODE 1081.00 TO NODE 1072.00 = 1015.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1072.00 TO NODE 1072.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.74
RAINFALL INTENSITY(INCH/HR) = 6.96
TOTAL STREAM AREA(ACRES) = 7.51
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.33

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| P-10.TXT      |              |           |                       |
|---------------|--------------|-----------|-----------------------|
| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
| 1             | 41.25        | 7.74      | 6.959                 |
| 2             | 43.92        | 11.10     | 5.514                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 43.92 Tc(MIN.) = 11.10  
 TOTAL AREA(ACRES) = 20.7  
 LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1072.00 = 2030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1072.00 TO NODE 1071.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1095.00 DOWNSTREAM(FEET) = 980.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 525.00 CHANNEL SLOPE = 0.2190  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.336  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 49.55  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.08  
 AVERAGE FLOW DEPTH(FEET) = 0.74 TRAVEL TIME(MIN.) = 0.58  
 Tc(MIN.) = 11.68  
 SUBAREA AREA(ACRES) = 8.44 SUBAREA RUNOFF(CFS) = 11.26  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.346  
 TOTAL AREA(ACRES) = 29.1 PEAK FLOW RATE(CFS) = 53.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.77 FLOW VELOCITY(FEET/SEC.) = 15.44  
 LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1071.00 = 2555.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1071.00 TO NODE 1071.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1106.00 TO NODE 1105.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
 UPSTREAM ELEVATION(FEET) = 1494.00  
 DOWNSTREAM ELEVATION(FEET) = 1490.00  
 ELEVATION DIFFERENCE(FEET) = 4.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.744  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.432  
 SUBAREA RUNOFF(CFS) = 1.45  
 TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 1.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 1105.00 TO NODE 1099.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1490.00 DOWNSTREAM ELEVATION(FEET) = 1463.00  
 STREET LENGTH(FEET) = 580.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.60  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.30  
 HALFSTREET FLOOD WIDTH(FEET) = 8.57  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.46  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.33  
 STREET FLOW TRAVEL TIME(MIN.) = 2.17 Tc(MIN.) = 7.91  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.858

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
 SUBAREA AREA(ACRES) = 3.43 SUBAREA RUNOFF(CFS) = 12.23  
 TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 13.41

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 10.97  
 FLOW VELOCITY(FEET/SEC.) = 5.07 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.75

LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1099.00 = 665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1099.00 TO NODE 1095.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1457.00 DOWNSTREAM(FEET) = 1450.90
FLOW LENGTH(FEET) = 340.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.96
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 13.41
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 8.55
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1095.00 = 1005.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1095.00 TO NODE 1095.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.55
RAINFALL INTENSITY(INCH/HR) = 6.53
TOTAL STREAM AREA(ACRES) = 3.76
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 1098.00 TO NODE 1097.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5200
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1493.00
DOWNSTREAM ELEVATION(FEET) = 1491.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.880
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.506
SUBAREA RUNOFF(CFS) = 2.19
TOTAL AREA(ACRES) = 0.56 TOTAL RUNOFF(CFS) = 2.19

\*\*\*\*\*

FLOW PROCESS FROM NODE 1097.00 TO NODE 1096.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
-----

UPSTREAM ELEVATION(FEET) = 1491.00 DOWNSTREAM ELEVATION(FEET) = 1456.80  
STREET LENGTH(FEET) = 745.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.61  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.33  
HALFSTREET FLOOD WIDTH(FEET) = 9.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.77  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.55  
STREET FLOW TRAVEL TIME(MIN.) = 2.60 Tc(MIN.) = 9.48  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.103

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 5.27 SUBAREA RUNOFF(CFS) = 16.72  
TOTAL AREA(ACRES) = 5.8 PEAK FLOW RATE(CFS) = 18.50

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.53  
FLOW VELOCITY(FEET/SEC.) = 5.48 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.06  
LONGEST FLOWPATH FROM NODE 1098.00 TO NODE 1096.00 = 825.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1096.00 TO NODE 1095.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
-----

ELEVATION DATA: UPSTREAM(FEET) = 1450.90 DOWNSTREAM(FEET) = 1450.50  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.68  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1

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PIPE-FLOW(CFS) = 18.50  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 9.57  
LONGEST FLOWPATH FROM NODE 1098.00 TO NODE 1095.00 = 865.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1095.00 TO NODE 1095.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.57  
RAINFALL INTENSITY(INCH/HR) = 6.07  
TOTAL STREAM AREA(ACRES) = 5.83  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.50

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 13.41        | 8.55      | 6.526                 | 3.76        |
| 2             | 18.50        | 9.57      | 6.067                 | 5.83        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 29.93        | 8.55      | 6.526                 |
| 2             | 30.97        | 9.57      | 6.067                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 30.97 Tc(MIN.) = 9.57  
TOTAL AREA(ACRES) = 9.6  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1095.00 = 1005.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1095.00 TO NODE 1094.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1450.50 DOWNSTREAM(FEET) = 1448.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.24  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1



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PIPE-FLOW(CFS) = 30.97  
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 9.71  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1094.00 = 1105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1094.00 TO NODE 1094.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.71  
RAINFALL INTENSITY(INCH/HR) = 6.01  
TOTAL STREAM AREA(ACRES) = 9.59  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.97

\*\*\*\*\*

FLOW PROCESS FROM NODE 1108.00 TO NODE 1107.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1477.00  
DOWNSTREAM ELEVATION(FEET) = 1475.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.787  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.392  
SUBAREA RUNOFF(CFS) = 0.39  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.39

\*\*\*\*\*

FLOW PROCESS FROM NODE 1107.00 TO NODE 1094.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1475.00 DOWNSTREAM ELEVATION(FEET) = 1455.00  
STREET LENGTH(FEET) = 750.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

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STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.52  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.04  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.29  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.95  
STREET FLOW TRAVEL TIME(MIN.) = 3.80 Tc(MIN.) = 9.58  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.061

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 1.33 SUBAREA RUNOFF(CFS) = 4.19  
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 4.48

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.41  
FLOW VELOCITY(FEET/SEC.) = 3.73 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.25  
LONGEST FLOWPATH FROM NODE 1108.00 TO NODE 1094.00 = 815.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1094.00 TO NODE 1094.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.58  
RAINFALL INTENSITY(INCH/HR) = 6.06  
TOTAL STREAM AREA(ACRES) = 1.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.48

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 30.97        | 9.71      | 6.012                 | 9.59        |
| 2             | 4.48         | 9.58      | 6.061                 | 1.42        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM | RUNOFF | Tc | INTENSITY |
|--------|--------|----|-----------|
|--------|--------|----|-----------|

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) |
|--------|-------|--------|-------------|
| 1      | 35.19 | 9.58   | 6.061       |
| 2      | 35.41 | 9.71   | 6.012       |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 35.41 Tc(MIN.) = 9.71  
TOTAL AREA(ACRES) = 11.0  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1094.00 = 1105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1094.00 TO NODE 1093.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1448.00 DOWNSTREAM(FEET) = 1447.50  
CHANNEL LENGTH THRU SUBAREA(FEET) = 50.00 CHANNEL SLOPE = 0.0100  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.939  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 36.00  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.51  
AVERAGE FLOW DEPTH(FEET) = 1.38 TRAVEL TIME(MIN.) = 0.18  
Tc(MIN.) = 9.89  
SUBAREA AREA(ACRES) = 0.57 SUBAREA RUNOFF(CFS) = 1.18  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.512  
TOTAL AREA(ACRES) = 11.6 PEAK FLOW RATE(CFS) = 35.41

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.37 FLOW VELOCITY(FEET/SEC.) = 4.50  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1093.00 = 1155.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1093.00 TO NODE 1089.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1441.50 DOWNSTREAM(FEET) = 1412.00  
FLOW LENGTH(FEET) = 295.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.66  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 35.41  
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 10.12

LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1089.00 = 1450.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1089.00 TO NODE 1089.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.12
RAINFALL INTENSITY(INCH/HR) = 5.85
TOTAL STREAM AREA(ACRES) = 11.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 35.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 1091.00 TO NODE 1090.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5200
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1466.00
DOWNSTREAM ELEVATION(FEET) = 1460.00
ELEVATION DIFFERENCE(FEET) = 6.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.746
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.431
SUBAREA RUNOFF(CFS) = 0.61
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 1090.00 TO NODE 1089.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1460.00 DOWNSTREAM(FEET) = 1418.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 540.00 CHANNEL SLOPE = 0.0778
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.373
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5200
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.32
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.78
AVERAGE FLOW DEPTH(FEET) = 0.43 TRAVEL TIME(MIN.) = 1.33

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Tc(MIN.) = 7.07  
SUBAREA AREA(ACRES) = 5.57 SUBAREA RUNOFF(CFS) = 21.36  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
TOTAL AREA(ACRES) = 5.7 PEAK FLOW RATE(CFS) = 21.89

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.63 FLOW VELOCITY(FEET/SEC.) = 8.18  
LONGEST FLOWPATH FROM NODE 1091.00 TO NODE 1089.00 = 640.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1089.00 TO NODE 1089.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.07  
RAINFALL INTENSITY(INCH/HR) = 7.37  
TOTAL STREAM AREA(ACRES) = 5.71  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.89

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 35.41        | 10.12     | 5.853                 | 11.58       |
| 2             | 21.89        | 7.07      | 7.373                 | 5.71        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 50.00        | 7.07      | 7.373                 |
| 2             | 52.78        | 10.12     | 5.853                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 52.78 Tc(MIN.) = 10.12  
TOTAL AREA(ACRES) = 17.3  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1089.00 = 1450.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1089.00 TO NODE 1088.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

P-10.TXT

ELEVATION DATA: UPSTREAM(FEET) = 1412.00 DOWNSTREAM(FEET) = 1410.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.48  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 52.78  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.20  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1088.00 = 1525.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1088.00 TO NODE 1087.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1410.00 DOWNSTREAM(FEET) = 1295.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 365.00 CHANNEL SLOPE = 0.3151  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.697  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 54.59  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 17.57  
AVERAGE FLOW DEPTH(FEET) = 0.70 TRAVEL TIME(MIN.) = 0.35  
Tc(MIN.) = 10.55  
SUBAREA AREA(ACRES) = 1.81 SUBAREA RUNOFF(CFS) = 3.61  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.499  
TOTAL AREA(ACRES) = 19.1 PEAK FLOW RATE(CFS) = 54.28

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.70 FLOW VELOCITY(FEET/SEC.) = 17.65  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1087.00 = 1890.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1087.00 TO NODE 1085.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1289.00 DOWNSTREAM(FEET) = 1282.00  
FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.23  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 54.28  
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 10.81

LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1085.00 = 2125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1085.00 TO NODE 1085.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.81
RAINFALL INTENSITY(INCH/HR) = 5.61
TOTAL STREAM AREA(ACRES) = 19.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 54.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 1111.00 TO NODE 1110.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1435.00
DOWNSTREAM ELEVATION(FEET) = 1395.00
ELEVATION DIFFERENCE(FEET) = 40.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972
SUBAREA RUNOFF(CFS) = 1.17
TOTAL AREA(ACRES) = 0.42 TOTAL RUNOFF(CFS) = 1.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 1110.00 TO NODE 1109.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1395.00 DOWNSTREAM(FEET) = 1290.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 320.00 CHANNEL SLOPE = 0.3281
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.424
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.55
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.29

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AVERAGE FLOW DEPTH(FEET) = 0.15 TRAVEL TIME(MIN.) = 0.73  
Tc(MIN.) = 7.00  
SUBAREA AREA(ACRES) = 1.94 SUBAREA RUNOFF(CFS) = 4.75  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.334  
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 5.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.20 FLOW VELOCITY(FEET/SEC.) = 8.82  
LONGEST FLOWPATH FROM NODE 1111.00 TO NODE 1109.00 = 420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1109.00 TO NODE 1085.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1284.00 DOWNSTREAM(FEET) = 1282.00  
FLOW LENGTH(FEET) = 230.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.56  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.84  
PIPE TRAVEL TIME(MIN.) = 0.69 Tc(MIN.) = 7.69  
LONGEST FLOWPATH FROM NODE 1111.00 TO NODE 1085.00 = 650.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1085.00 TO NODE 1085.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.69  
RAINFALL INTENSITY(INCH/HR) = 6.99  
TOTAL STREAM AREA(ACRES) = 2.36  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.84

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 54.28        | 10.81     | 5.609                 | 19.10       |
| 2             | 5.84         | 7.69      | 6.987                 | 2.36        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*



P-10.TXT

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 49.42        | 7.69      | 6.987                 |
| 2             | 58.97        | 10.81     | 5.609                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 58.97 Tc(MIN.) = 10.81  
TOTAL AREA(ACRES) = 21.5  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1085.00 = 2125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1085.00 TO NODE 1084.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1282.00 DOWNSTREAM(FEET) = 1279.00  
FLOW LENGTH(FEET) = 495.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 30.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.37  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 58.97  
PIPE TRAVEL TIME(MIN.) = 0.99 Tc(MIN.) = 11.79  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1084.00 = 2620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1084.00 TO NODE 1083.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1279.00 DOWNSTREAM(FEET) = 1095.00  
FLOW LENGTH(FEET) = 340.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 46.13  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 58.97  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 11.91  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1083.00 = 2960.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1083.00 TO NODE 1082.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1095.00 DOWNSTREAM(FEET) = 1005.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 735.00 CHANNEL SLOPE = 0.1224

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CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.017  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 65.26  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.15  
 AVERAGE FLOW DEPTH(FEET) = 0.99 TRAVEL TIME(MIN.) = 0.93  
 Tc(MIN.) = 12.85  
 SUBAREA AREA(ACRES) = 10.02 SUBAREA RUNOFF(CFS) = 12.57  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.407  
 TOTAL AREA(ACRES) = 31.5 PEAK FLOW RATE(CFS) = 64.32

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.99 FLOW VELOCITY(FEET/SEC.) = 13.10  
 LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1082.00 = 3695.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1082.00 TO NODE 1082.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1115.00 TO NODE 1114.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 1281.00  
 DOWNSTREAM ELEVATION(FEET) = 1280.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
 SUBAREA RUNOFF(CFS) = 0.55  
 TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 1114.00 TO NODE 1113.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1280.00 DOWNSTREAM ELEVATION(FEET) = 1278.00

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STREET LENGTH(FEET) = 130.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.82  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.84  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.48  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.70  
STREET FLOW TRAVEL TIME(MIN.) = 0.87 Tc(MIN.) = 8.29  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.656  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.75 SUBAREA RUNOFF(CFS) = 2.55  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 3.05

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.90  
FLOW VELOCITY(FEET/SEC.) = 2.78 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.90  
LONGEST FLOWPATH FROM NODE 1115.00 TO NODE 1113.00 = 195.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1113.00 TO NODE 1112.20 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1272.00 DOWNSTREAM(FEET) = 1269.00  
FLOW LENGTH(FEET) = 395.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.49  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.05  
PIPE TRAVEL TIME(MIN.) = 1.47 Tc(MIN.) = 9.76  
LONGEST FLOWPATH FROM NODE 1115.00 TO NODE 1112.20 = 590.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 1112.20 TO NODE 1112.20 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.76  
RAINFALL INTENSITY(INCH/HR) = 5.99  
TOTAL STREAM AREA(ACRES) = 0.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1112.60 TO NODE 1112.40 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1278.00  
DOWNSTREAM ELEVATION(FEET) = 1277.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 0.44  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.44

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1112.40 TO NODE 1112.20 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1277.00 DOWNSTREAM ELEVATION(FEET) = 1275.00  
STREET LENGTH(FEET) = 260.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

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\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.92

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.41

HALFSTREET FLOOD WIDTH(FEET) = 13.97

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.38

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.96

STREET FLOW TRAVEL TIME(MIN.) = 1.82 Tc(MIN.) = 9.24

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.206

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.510

SUBAREA AREA(ACRES) = 2.82 SUBAREA RUNOFF(CFS) = 8.93

TOTAL AREA(ACRES) = 2.9 PEAK FLOW RATE(CFS) = 9.30

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 17.97

FLOW VELOCITY(FEET/SEC.) = 2.78 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.35

LONGEST FLOWPATH FROM NODE 1112.60 TO NODE 1112.20 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1112.20 TO NODE 1112.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.24

RAINFALL INTENSITY(INCH/HR) = 6.21

TOTAL STREAM AREA(ACRES) = 2.94

PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.30

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.05         | 9.76      | 5.992                 | 0.90        |
| 2             | 9.30         | 9.24      | 6.206                 | 2.94        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.20        | 9.24      | 6.206                 |
| 2             | 12.04        | 9.76      | 5.992                 |

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COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.20 Tc(MIN.) = 9.24  
TOTAL AREA(ACRES) = 3.8  
LONGEST FLOWPATH FROM NODE 1115.00 TO NODE 1112.20 = 590.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1112.20 TO NODE 1112.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1274.00 DOWNSTREAM(FEET) = 1245.00  
FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.08  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.20  
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 9.38  
LONGEST FLOWPATH FROM NODE 1115.00 TO NODE 1112.00 = 765.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1112.00 TO NODE 1082.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1245.00 DOWNSTREAM(FEET) = 1005.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 805.00 CHANNEL SLOPE = 0.2981  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.726  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 18.40  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 12.41  
AVERAGE FLOW DEPTH(FEET) = 0.39 TRAVEL TIME(MIN.) = 1.08  
Tc(MIN.) = 10.47  
SUBAREA AREA(ACRES) = 7.43 SUBAREA RUNOFF(CFS) = 12.34  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.365  
TOTAL AREA(ACRES) = 11.3 PEAK FLOW RATE(CFS) = 23.55

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.45 FLOW VELOCITY(FEET/SEC.) = 13.52  
LONGEST FLOWPATH FROM NODE 1115.00 TO NODE 1082.00 = 1570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1082.00 TO NODE 1082.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 23.55        | 10.47     | 5.726                 | 11.27       |

LONGEST FLOWPATH FROM NODE 1115.00 TO NODE 1082.00 = 1570.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 64.32        | 12.85     | 5.017                 | 31.48       |

LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1082.00 = 3695.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 75.96        | 10.47     | 5.726                 |
| 2             | 84.96        | 12.85     | 5.017                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 84.96 Tc(MIN.) = 12.85  
TOTAL AREA(ACRES) = 42.8

\*\*\*\*\*

FLOW PROCESS FROM NODE 1082.00 TO NODE 1082.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1082.00 TO NODE 1071.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1005.00 DOWNSTREAM(FEET) = 980.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 155.00 CHANNEL SLOPE = 0.1613  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.976  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 85.32

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TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.65  
AVERAGE FLOW DEPTH(FEET) = 1.06 TRAVEL TIME(MIN.) = 0.17  
Tc(MIN.) = 13.01  
SUBAREA AREA(ACRES) = 0.59 SUBAREA RUNOFF(CFS) = 0.73  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.394  
TOTAL AREA(ACRES) = 43.3 PEAK FLOW RATE(CFS) = 84.99

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.06 FLOW VELOCITY(FEET/SEC.) = 15.71  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1071.00 = 3850.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1071.00 TO NODE 1071.00 IS CODE = 11  
-----  
>>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*  
STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 84.99 13.01 4.976 43.34  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1071.00 = 3850.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*  
STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 53.76 11.68 5.336 29.13  
LONGEST FLOWPATH FROM NODE 1074.80 TO NODE 1071.00 = 2555.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*  
STREAM RUNOFF Tc INTENSITY  
NUMBER (CFS) (MIN.) (INCH/HOUR)  
1 130.04 11.68 5.336  
2 135.13 13.01 4.976

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 135.13 Tc(MIN.) = 13.01  
TOTAL AREA(ACRES) = 72.5

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1071.00 TO NODE 1071.00 IS CODE = 12  
-----  
>>>>>CLEAR MEMORY BANK # 2 <<<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1071.00 TO NODE 1002.00 IS CODE = 51  
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P-10.TXT

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 980.00 DOWNSTREAM(FEET) = 700.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 2100.00 CHANNEL SLOPE = 0.1333  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.530

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2600  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 154.29  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 17.17  
AVERAGE FLOW DEPTH(FEET) = 1.50 TRAVEL TIME(MIN.) = 2.04  
Tc(MIN.) = 15.05  
SUBAREA AREA(ACRES) = 32.48 SUBAREA RUNOFF(CFS) = 38.26  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.339  
TOTAL AREA(ACRES) = 104.9 PEAK FLOW RATE(CFS) = 161.28

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.53 FLOW VELOCITY(FEET/SEC.) = 17.38  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1002.00 = 5950.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1002.00 TO NODE 1002.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.05  
RAINFALL INTENSITY(INCH/HR) = 4.53  
TOTAL STREAM AREA(ACRES) = 104.95  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 161.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 1117.00 TO NODE 1116.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1365.00  
DOWNSTREAM ELEVATION(FEET) = 1325.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267

P-10.TXT

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972

SUBAREA RUNOFF(CFS) = 0.59

TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 1116.00 TO NODE 1002.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1325.00 DOWNSTREAM(FEET) = 700.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 2240.00 CHANNEL SLOPE = 0.2790

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.196

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2700

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.47

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 12.46

AVERAGE FLOW DEPTH(FEET) = 0.41 TRAVEL TIME(MIN.) = 3.00

Tc(MIN.) = 9.26

SUBAREA AREA(ACRES) = 21.97 SUBAREA RUNOFF(CFS) = 36.75

AREA-AVERAGE RUNOFF COEFFICIENT = 0.271

TOTAL AREA(ACRES) = 22.2 PEAK FLOW RATE(CFS) = 37.21

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.59 FLOW VELOCITY(FEET/SEC.) = 15.08

LONGEST FLOWPATH FROM NODE 1117.00 TO NODE 1002.00 = 2340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1002.00 TO NODE 1002.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.26

RAINFALL INTENSITY(INCH/HR) = 6.20

TOTAL STREAM AREA(ACRES) = 22.18

PEAK FLOW RATE(CFS) AT CONFLUENCE = 37.21

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 161.28       | 15.05     | 4.530                 | 104.95      |

2 37.21 9.26 P-10.TXT  
6.196 22.18

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 136.47       | 9.26      | 6.196                 |
| 2             | 188.49       | 15.05     | 4.530                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 188.49 Tc(MIN.) = 15.05  
TOTAL AREA(ACRES) = 127.1  
LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1002.00 = 5950.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1002.00 TO NODE 1002.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 188.49       | 15.05     | 4.530                 | 127.13      |

LONGEST FLOWPATH FROM NODE 1106.00 TO NODE 1002.00 = 5950.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 541.86       | 12.50     | 5.106                 | 303.97      |

LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1002.00 = 7095.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 698.45       | 12.50     | 5.106                 |
| 2             | 669.27       | 15.05     | 4.530                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 698.45 Tc(MIN.) = 12.50  
TOTAL AREA(ACRES) = 431.1

\*\*\*\*\*

FLOW PROCESS FROM NODE 1002.00 TO NODE 1001.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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=====
ELEVATION DATA: UPSTREAM(FEET) = 700.00 DOWNSTREAM(FEET) = 675.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 955.00 CHANNEL SLOPE = 0.0262
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.826
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2700
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 726.61
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.92
AVERAGE FLOW DEPTH(FEET) = 4.41 TRAVEL TIME(MIN.) = 1.14
Tc(MIN.) = 13.65
SUBAREA AREA(ACRES) = 43.22 SUBAREA RUNOFF(CFS) = 56.31
AREA-AVERAGE RUNOFF COEFFICIENT = 0.333
TOTAL AREA(ACRES) = 474.3 PEAK FLOW RATE(CFS) = 762.31

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```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 4.50 FLOW VELOCITY(FEET/SEC.) = 14.09
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 1001.00 = 8050.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 1001.00 TO NODE 10.00 IS CODE = 41

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-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

```

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=====
ELEVATION DATA: UPSTREAM(FEET) = 675.00 DOWNSTREAM(FEET) = 550.00
FLOW LENGTH(FEET) = 755.00 MANNING'S N = 0.015
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 38.58
(PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW
AT DEPTH = 0.94 * DIAMETER)
GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 762.31
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 13.97
LONGEST FLOWPATH FROM NODE 1035.00 TO NODE 10.00 = 8805.00 FEET.

```

```

=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 474.3 TC(MIN.) = 13.97
PEAK FLOW RATE(CFS) = 762.31

```

```

=====
END OF RATIONAL METHOD ANALYSIS

```





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 19.0 Release Date: 06/01/2012 License ID 1355

Analysis prepared by:

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Suite 170  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* PROPOSED HYDROLOGY \*  
\* SUBBASIN 11 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-11.DAT  
TIME/DATE OF STUDY: 11:32 08/22/2014

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0312      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1121.00 TO NODE 1120.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1275.00  
DOWNSTREAM ELEVATION(FEET) = 1235.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

P-11. TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.45  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1120.00 TO NODE 1119.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1235.00 DOWNSTREAM(FEET) = 850.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 750.00 CHANNEL SLOPE = 0.5133  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING' S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.018  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.26  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.13  
AVERAGE FLOW DEPTH(FEET) = 0.14 TRAVEL TIME(MIN.) = 1.37  
Tc(MIN.) = 7.64  
SUBAREA AREA(ACRES) = 3.59 SUBAREA RUNOFF(CFS) = 7.56  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.302  
TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 7.95

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.21 FLOW VELOCITY(FEET/SEC.) = 11.14  
LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 1119.00 = 850.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1119.00 TO NODE 1103.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 850.00 DOWNSTREAM(FEET) = 750.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 535.00 CHANNEL SLOPE = 0.1869  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING' S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.546  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3000  
S. C. S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.39  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.26  
AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 0.87  
Tc(MIN.) = 8.50  
SUBAREA AREA(ACRES) = 8.59 SUBAREA RUNOFF(CFS) = 16.87  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.301  
TOTAL AREA(ACRES) = 12.3 PEAK FLOW RATE(CFS) = 24.29

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.52 FLOW VELOCITY(FEET/SEC.) = 11.51  
LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 1103.00 = 1385.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1103.00 TO NODE 1103.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

P-11. TXT  
TIME OF CONCENTRATION(MIN. ) = 8.50  
RAINFALL INTENSITY(INCH/HR) = 6.55  
TOTAL STREAM AREA(ACRES) = 12.34  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 24.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1124.00 TO NODE 1123.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 1165.00  
DOWNSTREAM ELEVATION(FEET) = 1145.00  
ELEVATION DIFFERENCE(FEET) = 20.00  
SUBAREA OVERLAND TIME OF FLOW(MIN. ) = 5.243  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.944  
SUBAREA RUNOFF(CFS) = 0.19  
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1123.00 TO NODE 1122.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVEL TIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1145.00 DOWNSTREAM(FEET) = 765.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 690.00 CHANNEL SLOPE = 0.5507  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING' S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.074  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .2900  
S. C. S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.01  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC. ) = 12.76  
AVERAGE FLOW DEPTH(FEET) = 0.25 TRAVEL TIME(MIN. ) = 0.90  
Tc(MIN. ) = 6.14  
SUBAREA AREA(ACRES) = 9.16 SUBAREA RUNOFF(CFS) = 21.45  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.290  
TOTAL AREA(ACRES) = 9.2 PEAK FLOW RATE(CFS) = 21.62

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 FLOW VELOCITY(FEET/SEC. ) = 16.06  
LONGEST FLOWPATH FROM NODE 1124.00 TO NODE 1122.00 = 760.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1122.00 TO NODE 1103.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 759.00 DOWNSTREAM(FEET) = 744.00  
FLOW LENGTH(FEET) = 365.00 MANNING' S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC. ) = 13.75  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 21.62  
PIPE TRAVEL TIME(MIN. ) = 0.44 Tc(MIN. ) = 6.59  
LONGEST FLOWPATH FROM NODE 1124.00 TO NODE 1103.00 = 1125.00 FEET.



\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1103.00 TO NODE 1103.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.59  
 RAINFALL INTENSITY(INCH/HR) = 7.72  
 TOTAL STREAM AREA(ACRES) = 9.22  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.62

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 24.29        | 8.50      | 6.546                 | 12.34       |
| 2             | 21.62        | 6.59      | 7.720                 | 9.22        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 40.43        | 6.59      | 7.720                 |
| 2             | 42.62        | 8.50      | 6.546                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 42.62 Tc(MIN.) = 8.50  
 TOTAL AREA(ACRES) = 21.6  
 LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 1103.00 = 1385.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1103.00 TO NODE 11.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 744.00 DOWNSTREAM(FEET) = 625.00  
 FLOW LENGTH(FEET) = 615.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 28.27  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 42.62  
 PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 8.87  
 LONGEST FLOWPATH FROM NODE 1121.00 TO NODE 11.00 = 2000.00 FEET.

-----  
 END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 21.6 TC(MIN.) = 8.87  
 PEAK FLOW RATE(CFS) = 42.62  
 =====

-----  
 END OF RATIONAL METHOD ANALYSIS  
 -----

□



| Node to Node |        | Code | Elev 1<br>(feet)                  | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments              | BANK |   |   |  |
|--------------|--------|------|-----------------------------------|------------------|------------------|-------------|---------------|-----------------------|------|---|---|--|
|              |        |      |                                   |                  |                  |             |               |                       | 1    | 2 | 3 |  |
| 1321         | 1320   | 2    | 1278                              | 1275             | 95               | 0.57        | 0.22          |                       |      |   |   |  |
| 1320         | 1319   | 6    | 1275                              | 1269             | 655              | 0.52        | 4.03          | 2 sides               |      |   |   |  |
| 1319         | 1313   | 3    | 1263                              | 1262             | 75               |             |               |                       |      |   |   |  |
| 1313         | 1313   | 1    |                                   |                  |                  |             |               | 1 of 2                |      |   |   |  |
| 1316         | 1315   | 2    | 1282                              | 1279.5           | 87               | 0.51        | 0.09          |                       |      |   |   |  |
| 1315         | 1314   | 6    | 1279.5                            | 1269.5           | 360              | 0.51        | 2.93          | 2 sides               |      |   |   |  |
| 1314         | 1313   | 3    | 1263                              | 1262             | 70               |             |               |                       |      |   |   |  |
| 1313         | 1313   | 1    |                                   |                  |                  |             |               | 2 of 2                |      |   |   |  |
| 1313         | 1309   | 3    | 1262                              | 1261             | 120              |             |               |                       |      |   |   |  |
| 1309         | 1309   | 1    |                                   |                  |                  |             |               | 1 of 3                |      |   |   |  |
| 1312         | 1311   | 2    | 1275                              | 1274             | 65               | 0.51        | 0.11          |                       |      |   |   |  |
| 1311         | 1310   | 5    | 1274                              | 1269             | 335              | 0.51        | 0.51          |                       |      |   |   |  |
| 1310         | 1309   | 3    | 1263                              | 1261             | 30               |             |               |                       |      |   |   |  |
| 1309         | 1309   | 1    |                                   |                  |                  |             |               | 2 of 3                |      |   |   |  |
| 1318         | 1317   | 2    | 1275                              | 1270             | 85               | 0.51        | 0.15          |                       |      |   |   |  |
| 1317         | 1309   | 6    | 1270                              | 1267             | 250              | 0.51        | 0.47          | Two sides             |      |   |   |  |
| 1309         | 1309   | 1    |                                   |                  |                  |             |               | 3 of 3                |      |   |   |  |
| 1309         | 1308   | 3    | 1261                              | 1260.5           | 45               |             |               |                       |      |   |   |  |
| 1308         | 1307   | 5    | 1260.5                            | 1257.5           | 590              | 0.53        | 1.05          |                       |      |   |   |  |
| 1307         | 1307   | 1    |                                   |                  |                  |             |               | 1 of 2                |      |   |   |  |
| 1323         | 1322   | 2    | 1274                              | 1272             | 80               | 0.57        | 0.15          |                       |      |   |   |  |
| 1322         | 1306   | 6    | 1272                              | 1267             | 315              | 0.57        | 4.48          | 1 side                |      |   |   |  |
| 1306         | 1307   | 3    | 1263                              | 1257.5           | 120              |             |               |                       |      |   |   |  |
| 1307         | 1307   | 1    |                                   |                  |                  |             |               | 2 of 2                |      |   |   |  |
| 1307         | 1307   | 7    | Tc= 14.56, A = 14.1, Q = 13.1 cfs |                  |                  |             |               |                       |      |   |   |  |
| 1307         | 1305.5 | 3    | 1257.5                            | 1255.2           | 115              |             |               |                       |      |   |   |  |
| 1305.5       | 1305.5 | 1    |                                   |                  |                  |             |               | 1 of 2                |      |   |   |  |
| 1305.8       | 1305.7 | 2    | 1287                              | 1285             | 100              | 0.51        | 0.13          |                       |      |   |   |  |
| 1305.7       | 1305.6 | 6    | 1285                              | 1275             | 570              | 0.56        | 4.71          | one side              |      |   |   |  |
| 1305.6       | 1305.5 | 3    | 1269                              | 1255.2           | 525              |             |               |                       |      |   |   |  |
| 1305.5       | 1305.5 | 1    |                                   |                  |                  |             |               | 2 of 2                |      |   |   |  |
| 1305.5       | 1305   | 3    | 1255.2                            | 1252.7           | 125              |             |               |                       |      |   |   |  |
| 1305         | 1304   | 3    | 1252.7                            | 1105             | 320              |             |               |                       |      |   |   |  |
| 1304         | 1303   | 5    | 1105                              | 835              | 1225             | 0.34        | 13.15         |                       |      |   |   |  |
| 1303         | 1303   | 10   |                                   |                  |                  |             |               | save to bank 1 - 1303 |      |   |   |  |



| Node to Node |        | Code | Elev 1<br>(feet)      | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments              | BANK |   |   |
|--------------|--------|------|-----------------------|------------------|------------------|-------------|---------------|-----------------------|------|---|---|
|              |        |      |                       |                  |                  |             |               |                       | 1    | 2 | 3 |
| 2564         | 2563   | 2    | 1273                  | 1271             | 80               | 0.54        | 0.16          |                       |      |   |   |
| 2563         | 2563.1 | 6    | 1271                  | 1269             | 230              | 0.51        | 1.93          | 2 SIDES               |      |   |   |
| 2563.1       | 2562   | 3    | 1266                  | 1261             | 210              |             |               |                       |      |   |   |
| 2562         | 2562   | 1    |                       |                  |                  |             |               | 1 OF 2                |      |   |   |
| 2563.1       | 2563.2 | 2    | 1269                  | 1268             | 65               | 0.51        | 0.55          |                       |      |   |   |
| 2563.2       | 2562   | 6    | 1268                  | 1267             | 120              | 0.51        | 0.55          | 2 SIDES               |      |   |   |
| 2562         | 2562   | 1    |                       |                  |                  |             |               | 2 OF 2                |      |   |   |
| 2562         | 2558   | 3    | 1261                  | 1260             | 140              |             |               |                       |      |   |   |
| 2558         | 2558   | 10   |                       |                  |                  |             |               | SAVE TO BANK 2 - 2558 |      |   |   |
| 2561         | 2560   | 2    | 1275                  | 1274             | 50               | 0.51        | 0.13          |                       |      |   |   |
| 2560         | 2560.1 | 6    | 1274                  | 1269             | 315              | 0.51        | 1.96          | 2 SIDES               |      |   |   |
| 2560.1       | 2559   | 3    | 1263                  | 1262             | 160              |             |               |                       |      |   |   |
| 2559         | 2559   | 1    |                       |                  |                  |             |               | 1 OF 2                |      |   |   |
| 2560.1       | 2560.2 | 2    | 1269                  | 1268.8           | 50               | 0.51        | 0.4           |                       |      |   |   |
| 2560.2       | 2559   | 6    | 1268.8                | 1268             | 115              | 0.51        | 0.97          | 2 SIDES               |      |   |   |
| 2559         | 2559   | 1    |                       |                  |                  |             |               | 2 OF 2                |      |   |   |
| 2559         | 2558   | 3    | 1262                  | 1260             | 40               |             |               |                       |      |   |   |
| 2558         | 2558   | 11   |                       |                  |                  |             |               | ADD BANK 2 - 2558     |      |   |   |
| 2558         | 2558   | 12   |                       |                  |                  |             |               | CLEAR BANK 2          |      |   |   |
| 2558         | 2554   | 3    | 1260                  | 1257.8           | 225              |             |               |                       |      |   |   |
| 2554         | 2554   | 1    |                       |                  |                  |             |               | 1 OF 2                |      |   |   |
| 2557         | 2556   | 2    | 1271                  | 1270             | 65               | 0.51        | 0.16          |                       |      |   |   |
| 2556         | 2555   | 6    | 1270                  | 1264             | 488              | 0.51        | 3.46          | 1 SIDE                |      |   |   |
| 2555         | 2554   | 3    | 1258                  | 1257.8           | 10               |             |               |                       |      |   |   |
| 2554         | 2554   | 1    |                       |                  |                  |             |               | 2 OF 2                |      |   |   |
| 2554         | 2552.5 | 3    | 1257.8                | 1252.8           | 515              |             |               |                       |      |   |   |
| 2552.5       | 2552.5 | 7    | Tc=10.84 A=10.3 Q=9.1 |                  |                  |             |               |                       |      |   |   |
| 2552.5       | 2552   | 5    | 1252.8                | 1250.8           | 185              |             |               | VALLEY                |      |   |   |
| 2552         | 1303   | 5    | 1250.8                | 835              | 1400             |             |               | MTN                   |      |   |   |
| 2552         | 1303   | 8    |                       |                  |                  | 0.27        | 20.83         |                       |      |   |   |
| 1303         | 1303   | 10   |                       |                  |                  |             |               | save to bank 2 - 1303 |      |   |   |
| 1335         | 1334   | 2    | 1293                  | 1291             | 83               | 0.57        | 0.13          |                       |      |   |   |
| 1334         | 1333.8 | 6    | 1291                  | 1280             | 270              | 0.57        | 1.74          | 1 SIDE                |      |   |   |
| 1333.8       | 1333.8 | 1    |                       |                  |                  |             |               | 1 of 2                |      |   |   |
| 1334.8       | 1334.6 | 2    | 1287                  | 1285             | 80               | 0.57        | 0.11          |                       |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet)   | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments              | BANK |   |   |
|--------------|--------|------|--------------------|------------------|------------------|-------------|---------------|-----------------------|------|---|---|
|              |        |      |                    |                  |                  |             |               |                       | 1    | 2 | 3 |
| 1334.6       | 1334.4 | 6    | 1285               | 1284             | 50               | 0.55        | 0.46          | 2 SIDES               |      |   |   |
| 1334.4       | 1333.8 | 3    | 1278               | 1276             | 200              |             |               |                       |      |   |   |
| 1333.8       | 1333.8 | 1    |                    |                  |                  |             |               | 2 of 2                |      |   |   |
| 1333.8       | 1333.4 | 3    | 1276               | 1273             | 100              |             |               |                       |      |   |   |
| 1333.4       | 1333.4 | 1    |                    |                  |                  |             |               | 1 of 2                |      |   |   |
| 1333         | 1333   | 2    | 1281               | 1280             | 80               | 0.56        | 0.29          |                       |      |   |   |
| 1333         | 1333.4 | 3    | 1274               | 1273             | 50               |             |               |                       |      |   |   |
| 1333.4       | 1333.4 | 1    |                    |                  |                  |             |               | 2 of 2                |      |   |   |
| 1333.4       | 1332   | 3    | 1273               | 1267             | 210              |             |               |                       |      |   |   |
| 1332         | 1332   | 1    |                    |                  |                  |             |               | 1 of 2                |      |   |   |
| 1337         | 1336   | 2    | 1278               | 1276             | 80               | 0.51        | 0.07          |                       |      |   |   |
| 1336         | 1335   | 6    | 1276               | 1273             | 240              | 0.51        | 0.53          | 2 SIDES               |      |   |   |
| 1335         | 1332   | 3    | 1268               | 1267             | 30               |             |               |                       |      |   |   |
| 1332         | 1332   | 1    |                    |                  |                  |             |               | 2 of 2                |      |   |   |
| 1332         | 1330   | 3    | 1267               | 1265             | 150              |             |               |                       |      |   |   |
| 1330         | 1330   | 10   | clean - left flow  |                  |                  |             |               | save to bank 3 - 1330 |      |   |   |
| 1353         | 1352   | 2    | 1284               | 1282             | 80               | 0.51        | 0.14          |                       |      |   |   |
| 1352         | 1351   | 6    | 1282               | 1278             | 270              | 0.51        | 0.79          | 2 SIDES               |      |   |   |
| 1351         | 1350.4 | 3    | 1272               | 1267             | 280              |             |               |                       |      |   |   |
| 1350.4       | 1350.4 | 1    |                    |                  |                  |             |               | 1 of 2                |      |   |   |
| 1350.8       | 1350.6 | 2    | 1278               | 1276             | 80               | 0.51        | 0.10          |                       |      |   |   |
| 1350.6       | 1350.4 | 6    | 1276               | 1267             | 160              | 0.52        | 2.00          | 1 SIDE                |      |   |   |
| 1350.4       | 1350.4 | 1    |                    |                  |                  |             |               | 2 of 2                |      |   |   |
| 1350.4       | 1346   | 3    | 1267               | 1265             | 60               |             |               | WQ in                 |      |   |   |
| 1346         | 1330   | 3    | 1265               | 1255             | 850              |             |               | WQ out                |      |   |   |
| 1330         | 1330   | 11   | clean - right flow |                  |                  |             |               | add bank 3            |      |   |   |
| 1330         | 1330   | 12   |                    |                  |                  |             |               | clear bank 3          |      |   |   |
| 1330         | 1326   | 5    | 1255               | 1120             | 410              |             |               | MTN                   |      |   |   |
| 1330         | 1326   | 8    |                    |                  |                  | 0.3         | 2.34          |                       |      |   |   |
| 1326         | 1326   | 1    |                    |                  |                  |             |               | 1 of 2                |      |   |   |
| 1328         | 1327   | 2    | 1325               | 1315             | 80               | 0.35        | 0.24          |                       |      |   |   |
| 1327         | 1326   | 5    | 1315               | 1120             | 1075             |             |               | MTN                   |      |   |   |
| 1327         | 1326   | 8    |                    |                  |                  | 0.3         | 6.90          |                       |      |   |   |
| 1326         | 1326   | 1    |                    |                  |                  |             |               | 2 of 2                |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1326         | 1303   | 5    | 1120             | 835              | 965              |             |               | MTN            |      |   |   |
| 1326         | 1303   | 8    |                  |                  |                  | 0.27        | 8.99          |                |      |   |   |
| 1303         | 1303   | 11   |                  |                  |                  |             |               | add bank 1     |      |   |   |
| 1303         | 1303   | 11   |                  |                  |                  |             |               | add bank 2     |      |   |   |
| 1303         | 1303   | 12   |                  |                  |                  |             |               | clear bank 1   |      |   |   |
| 1303         | 1303   | 12   |                  |                  |                  |             |               | clear bank 2   |      |   |   |
| 1303         | 1302   | 5    | 835              | 775              | 520              |             |               | MTN            |      |   |   |
| 1303         | 1302   | 8    |                  |                  |                  | 0.29        | 9.18          |                |      |   |   |
| 1302         | 1302   | 10   |                  |                  |                  |             |               | save to bank 1 |      |   |   |
| 1339         | 1338   | 2    | 1284             | 1282             | 85               | 0.51        | 0.06          |                |      |   |   |
| 1338         | 1337.8 | 6    | 1282             | 1276             | 165              | 0.51        | 0.98          |                |      |   |   |
| 1337.8       | 1337.6 | 3    | 1270             | 1266             | 255              |             |               |                |      |   |   |
| 1337.6       | 1337.6 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1345         | 1344   | 2    | 1277             | 1275             | 80               | 0.51        | 0.13          |                |      |   |   |
| 1344         | 1343.8 | 6    | 1275             | 1272             | 210              | 0.52        | 0.69          | 1 SIDE         |      |   |   |
| 1343.8       | 1337.6 | 3    | 1266.5           | 1266             | 50               |             |               |                |      |   |   |
| 1337.6       | 1337.6 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1337.6       | 1345.6 | 3    | 1266             | 1264             | 125              |             |               |                |      |   |   |
| 1345.6       | 1345.6 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1345.9       | 1345.8 | 2    | 1280             | 1278             | 100              | 0.57        | 0.13          |                |      |   |   |
| 1345.8       | 1343   | 6    | 1278             | 1269.5           | 315              | 0.56        | 1.25          | 1 SIDE         |      |   |   |
| 1343         | 1345.6 | 3    | 1264.5           | 1264             | 40               |             |               |                |      |   |   |
| 1345.6       | 1345.6 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1345.6       | 1346.8 | 3    | 1264             | 1262             | 170              |             |               |                |      |   |   |
| 1346.8       | 1346.8 | 1    |                  |                  |                  |             |               | 1 of 3         |      |   |   |
| 1348         | 1347   | 2    | 1275             | 1273             | 80               | 0.51        | 0.10          |                |      |   |   |
| 1347         | 1346.9 | 6    | 1273             | 1265             | 150              | 0.52        | 0.97          | 2 SIDES        |      |   |   |
| 1346.9       | 1346.8 | 3    | 1262.5           | 1262             | 50               |             |               |                |      |   |   |
| 1346.8       | 1346.8 | 1    |                  |                  |                  |             |               | 2 of 3         |      |   |   |
| 1347.6       | 1347.5 | 2    | 1270             | 1268             | 100              | 0.57        | 0.15          | 1 SIDE         |      |   |   |
| 1347.5       | 1347.4 | 6    | 1268             | 1265             | 110              | 0.54        | 1.69          |                |      |   |   |
| 1347.4       | 1346.8 | 3    | 1262.5           | 1262             | 40               |             |               |                |      |   |   |
| 1346.8       | 1346.8 | 1    |                  |                  |                  |             |               | 3 of 3         |      |   |   |
| 1346.8       | 1342   | 3    | 1262             | 1261.5           | 50               |             |               |                |      |   |   |
| 1342         | 1342   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments            | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|---------------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                     | 1    | 2 | 3 |
| 1347.9       | 1347.8 | 2    | 1272             | 1270             | 85               | 0.51        | 0.10          |                     |      |   |   |
| 1347.8       | 1347.7 | 6    | 1270             | 1269             | 100              | 0.51        | 0.80          | 2 SIDES             |      |   |   |
| 1347.7       | 1342   | 3    | 1263             | 1261.5           | 150              |             |               |                     |      |   |   |
| 1342         | 1342   | 1    |                  |                  |                  |             |               | 2 of 2              |      |   |   |
| 1342         | 1341.5 | 3    | 1261.5           | 1260             | 150              |             |               |                     |      |   |   |
| 1341.5       | 1341   | 5    | 1260             | 1259.5           | 50               |             |               |                     |      |   |   |
| 1341.5       | 1341   | 8    |                  |                  |                  | 0.35        | 0.51          | WQ in               |      |   |   |
| 1341         | 1340.8 | 3    | 1253             | 1215             | 100              |             |               | WQ out              |      |   |   |
| 1340.8       | 1340   | 5    | 1215             | 1030             | 800              |             |               |                     |      |   |   |
| 1340.8       | 1340   | 8    |                  |                  |                  | 0.27        | 6.19          |                     |      |   |   |
| 1340         | 1340   | 1    |                  |                  |                  |             |               | 1 of 2              |      |   |   |
| 1356.1       | 1350   | 2    | 1280             | 1235             | 100              | 0.57        | 0.29          |                     |      |   |   |
| 1350         | 1340   | 5    | 1235             | 1030             | 600              |             |               |                     |      |   |   |
| 1350         | 1340   | 8    |                  |                  |                  | 0.28        | 5.56          |                     |      |   |   |
| 1340         | 1340   | 1    |                  |                  |                  |             |               | 2 of 2              |      |   |   |
| 1340         | 1302   | 5    | 1030             | 775              | 1505             |             |               |                     |      |   |   |
| 1340         | 1302   | 8    |                  |                  |                  | 0.28        | 25.68         |                     |      |   |   |
| 1302         | 1302   | 11   |                  |                  |                  |             |               | add bank 1          |      |   |   |
| 1302         | 1301   | 5    | 775              | 760              | 220              |             |               |                     |      |   |   |
| 1301         | 13     | 4    | 760              | 670              | 665              |             |               | Ex 36" RCP Caltrans |      |   |   |
|              |        |      |                  |                  |                  |             | 142.57        |                     |      |   |   |

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* PROPOSED HYDROLOGY \*  
\* SUB BASIN 13 - WITH DETENTION AT NODE 1307 AND 2552.5 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-13D.DAT  
TIME/DATE OF STUDY: 13:27 02/23/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|--|--------------|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020                                       | 0.50                   | 1.50 0.0312                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1321.00 TO NODE 1320.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 1278.00

DOWNSTREAM ELEVATION(FEET) = 1275.00

ELEVATION DIFFERENCE(FEET) = 3.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914

SUBAREA RUNOFF(CFS) = 0.99

TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 0.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 1320.00 TO NODE 1319.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1275.00 DOWNSTREAM ELEVATION(FEET) = 1269.00

STREET LENGTH(FEET) = 655.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.94

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.36

HALFSTREET FLOOD WIDTH(FEET) = 11.66

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.35

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.85

STREET FLOW TRAVEL TIME(MIN.) = 4.64 Tc(MIN.) = 10.98

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.552

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200

S.C.S. CURVE NUMBER (AMC II) = 0



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AREA-AVERAGE RUNOFF COEFFICIENT = 0.523  
SUBAREA AREA(ACRES) = 4.03 SUBAREA RUNOFF(CFS) = 11.63  
TOTAL AREA(ACRES) = 4.2 PEAK FLOW RATE(CFS) = 12.33

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.78  
FLOW VELOCITY(FEET/SEC.) = 2.68 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.13  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1319.00 = 750.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1319.00 TO NODE 1313.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1262.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.83  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.33  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 11.14  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1313.00 = 825.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1313.00 TO NODE 1313.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.14  
RAINFALL INTENSITY(INCH/HR) = 5.50  
TOTAL STREAM AREA(ACRES) = 4.25  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 1316.00 TO NODE 1315.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 87.00  
UPSTREAM ELEVATION(FEET) = 1282.00  
DOWNSTREAM ELEVATION(FEET) = 1279.50  
ELEVATION DIFFERENCE(FEET) = 2.50

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SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.968  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.445  
SUBAREA RUNOFF(CFS) = 0.34  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 1315.00 TO NODE 1314.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1279.50 DOWNSTREAM ELEVATION(FEET) = 1269.50  
STREET LENGTH(FEET) = 360.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.16  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.04  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.37  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.97  
STREET FLOW TRAVEL TIME(MIN.) = 1.78 Tc(MIN.) = 8.75  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.430

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 2.93 SUBAREA RUNOFF(CFS) = 9.61  
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 9.90

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.72  
FLOW VELOCITY(FEET/SEC.) = 3.91 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.33  
LONGEST FLOWPATH FROM NODE 1316.00 TO NODE 1314.00 = 447.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1314.00 TO NODE 1313.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1263.00  DOWNSTREAM(FEET) = 1262.00
FLOW LENGTH(FEET) = 70.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.54
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.90
PIPE TRAVEL TIME(MIN.) = 0.15  Tc(MIN.) = 8.90
LONGEST FLOWPATH FROM NODE 1316.00 TO NODE 1313.00 = 517.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 1313.00 TO NODE 1313.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.90
RAINFALL INTENSITY(INCH/HR) = 6.36
TOTAL STREAM AREA(ACRES) = 3.02
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.90

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.33        | 11.14     | 5.500                 | 4.25        |
| 2             | 9.90         | 8.90      | 6.357                 | 3.02        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.75        | 8.90      | 6.357                 |
| 2             | 20.90        | 11.14     | 5.500                 |

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 20.90  Tc(MIN.) = 11.14
TOTAL AREA(ACRES) = 7.3
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1313.00 = 825.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 1313.00 TO NODE 1309.00 IS CODE = 31
-----

```

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

```

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1262.00  DOWNSTREAM(FEET) = 1261.00
FLOW LENGTH(FEET) = 120.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.46
ESTIMATED PIPE DIAMETER(INCH) = 27.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.90
PIPE TRAVEL TIME(MIN.) = 0.27  Tc(MIN.) = 11.41
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1309.00 = 945.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 1309.00 TO NODE 1309.00 IS CODE = 1
-----

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.41
RAINFALL INTENSITY(INCH/HR) = 5.42
TOTAL STREAM AREA(ACRES) = 7.27
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.90

```

```

*****
FLOW PROCESS FROM NODE 1312.00 TO NODE 1311.00 IS CODE = 21
-----

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 1275.00
DOWNSTREAM ELEVATION(FEET) = 1274.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151
SUBAREA RUNOFF(CFS) = 0.40
TOTAL AREA(ACRES) = 0.11  TOTAL RUNOFF(CFS) = 0.40

```

```

*****
FLOW PROCESS FROM NODE 1311.00 TO NODE 1310.00 IS CODE = 51
-----

```

```

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1274.00  DOWNSTREAM(FEET) = 1269.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 335.00  CHANNEL SLOPE = 0.0149

```

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CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.718  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.15  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.82  
AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 3.07  
Tc(MIN.) = 10.49  
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 1.49  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.81

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.24 FLOW VELOCITY(FEET/SEC.) = 2.15  
LONGEST FLOWPATH FROM NODE 1312.00 TO NODE 1310.00 = 400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1310.00 TO NODE 1309.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1261.00  
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.40  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.81  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 10.55  
LONGEST FLOWPATH FROM NODE 1312.00 TO NODE 1309.00 = 430.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1309.00 TO NODE 1309.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.55  
RAINFALL INTENSITY(INCH/HR) = 5.70  
TOTAL STREAM AREA(ACRES) = 0.62  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.81

\*\*\*\*\*

FLOW PROCESS FROM NODE 1318.00 TO NODE 1317.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1275.00  
DOWNSTREAM ELEVATION(FEET) = 1270.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.424  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.750  
SUBAREA RUNOFF(CFS) = 0.67  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.67

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1317.00 TO NODE 1309.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1270.00 DOWNSTREAM ELEVATION(FEET) = 1267.00  
STREET LENGTH(FEET) = 250.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.51  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.23  
HALFSTREET FLOOD WIDTH(FEET) = 5.32  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.89  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.44  
STREET FLOW TRAVEL TIME(MIN.) = 2.21 Tc(MIN.) = 7.63  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.021

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.68  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.22

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 6.58  
FLOW VELOCITY(FEET/SEC.) = 2.01 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.52  
LONGEST FLOWPATH FROM NODE 1318.00 TO NODE 1309.00 = 335.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1309.00 TO NODE 1309.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.63  
RAINFALL INTENSITY(INCH/HR) = 7.02  
TOTAL STREAM AREA(ACRES) = 0.62  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.22

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.90        | 11.41     | 5.417                 | 7.27        |
| 2             | 1.81         | 10.55     | 5.698                 | 0.62        |
| 3             | 2.22         | 7.63      | 7.021                 | 0.62        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.65        | 7.63      | 7.021                 |
| 2             | 23.48        | 10.55     | 5.698                 |
| 3             | 24.33        | 11.41     | 5.417                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 24.33 Tc(MIN.) = 11.41  
TOTAL AREA(ACRES) = 8.5  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1309.00 = 945.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1309.00 TO NODE 1308.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1261.00 DOWNSTREAM(FEET) = 1260.50

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FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.63  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 24.33  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 11.50  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1308.00 = 990.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1308.00 TO NODE 1307.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1260.50 DOWNSTREAM(FEET) = 1257.50  
CHANNEL LENGTH THRU SUBAREA(FEET) = 590.00 CHANNEL SLOPE = 0.0051  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.628

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5300  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.62  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.21  
AVERAGE FLOW DEPTH(FEET) = 1.38 TRAVEL TIME(MIN.) = 3.06  
Tc(MIN.) = 14.56  
SUBAREA AREA(ACRES) = 1.05 SUBAREA RUNOFF(CFS) = 2.58  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.518  
TOTAL AREA(ACRES) = 9.6 PEAK FLOW RATE(CFS) = 24.33

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.35 FLOW VELOCITY(FEET/SEC.) = 3.17  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1307.00 = 1580.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1307.00 TO NODE 1307.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.56  
RAINFALL INTENSITY(INCH/HR) = 4.63  
TOTAL STREAM AREA(ACRES) = 9.56  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 24.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 1323.00 TO NODE 1322.00 IS CODE = 21



-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1274.00  
DOWNSTREAM ELEVATION(FEET) = 1272.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.287  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.955  
SUBAREA RUNOFF(CFS) = 0.68  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.68

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1322.00 TO NODE 1306.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1272.00 DOWNSTREAM ELEVATION(FEET) = 1267.00  
STREET LENGTH(FEET) = 315.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.62  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.44  
HALFSTREET FLOOD WIDTH(FEET) = 15.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.69  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.63  
STREET FLOW TRAVEL TIME(MIN.) = 1.42 Tc(MIN.) = 7.71  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.973

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 4.48 SUBAREA RUNOFF(CFS) = 17.81  
TOTAL AREA(ACRES) = 4.6 PEAK FLOW RATE(CFS) = 18.40

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.00  
FLOW VELOCITY(FEET/SEC.) = 4.00 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.94  
LONGEST FLOWPATH FROM NODE 1323.00 TO NODE 1306.00 = 395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1306.00 TO NODE 1307.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1257.50  
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.58  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 18.40  
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 7.86  
LONGEST FLOWPATH FROM NODE 1323.00 TO NODE 1307.00 = 515.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1307.00 TO NODE 1307.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.86  
RAINFALL INTENSITY(INCH/HR) = 6.89  
TOTAL STREAM AREA(ACRES) = 4.63  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.40

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 24.33        | 14.56     | 4.628                 | 9.56        |
| 2             | 18.40        | 7.86      | 6.889                 | 4.63        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 34.75        | 7.86      | 6.889                 |
| 2             | 36.69        | 14.56     | 4.628                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 36.69 Tc(MIN.) = 14.56  
TOTAL AREA(ACRES) = 14.2  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1307.00 = 1580.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1307.00 TO NODE 1307.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 14.56 RAIN INTENSITY(INCH/HOUR) = 4.63  
TOTAL AREA(ACRES) = 14.10 TOTAL RUNOFF(CFS) = 13.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1307.00 TO NODE 1305.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1257.50 DOWNSTREAM(FEET) = 1255.20  
FLOW LENGTH(FEET) = 115.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.06  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 13.10  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 14.77  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1305.50 = 1695.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1305.50 TO NODE 1305.50 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.77  
RAINFALL INTENSITY(INCH/HR) = 4.59  
TOTAL STREAM AREA(ACRES) = 14.10  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1305.80 TO NODE 1305.70 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1287.00  
 DOWNSTREAM ELEVATION(FEET) = 1285.00  
 ELEVATION DIFFERENCE(FEET) = 2.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.539  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
           THE MAXIMUM OVERLAND FLOW LENGTH = 80.00  
           (Reference: Table 3-1B of Hydrology Manual)  
           THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.076  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.13    TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1305.70 TO NODE 1305.60 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1285.00    DOWNSTREAM ELEVATION(FEET) = 1275.00  
 STREET LENGTH(FEET) = 570.00    CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.22  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.42  
 HALFSTREET FLOOD WIDTH(FEET) = 14.53  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.69  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.54  
 STREET FLOW TRAVEL TIME(MIN.) = 2.58    Tc(MIN.) = 10.12  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.853

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5600  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.559  
 SUBAREA AREA(ACRES) = 4.71    SUBAREA RUNOFF(CFS) = 15.44  
 TOTAL AREA(ACRES) = 4.8    PEAK FLOW RATE(CFS) = 15.83

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.00  
FLOW VELOCITY(FEET/SEC.) = 4.20 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.04  
LONGEST FLOWPATH FROM NODE 1305.80 TO NODE 1305.60 = 670.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1305.60 TO NODE 1305.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1269.00 DOWNSTREAM(FEET) = 1255.20  
FLOW LENGTH(FEET) = 525.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.83  
PIPE TRAVEL TIME(MIN.) = 0.84 Tc(MIN.) = 10.96  
LONGEST FLOWPATH FROM NODE 1305.80 TO NODE 1305.50 = 1195.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1305.50 TO NODE 1305.50 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.96  
RAINFALL INTENSITY(INCH/HR) = 5.56  
TOTAL STREAM AREA(ACRES) = 4.84  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.83

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 13.10        | 14.77     | 4.585                 | 14.10       |
| 2             | 15.83        | 10.96     | 5.560                 | 4.84        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 25.54        | 10.96     | 5.560                 |
| 2             | 26.15        | 14.77     | 4.585                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.15 Tc(MIN.) = 14.77  
TOTAL AREA(ACRES) = 18.9  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1305.50 = 1695.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1305.50 TO NODE 1305.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1255.20 DOWNSTREAM(FEET) = 1252.70  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.87  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.15  
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 14.96  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1305.00 = 1820.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1305.00 TO NODE 1304.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1252.70 DOWNSTREAM(FEET) = 1105.00  
FLOW LENGTH(FEET) = 320.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 35.84  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.15  
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 15.11  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1304.00 = 2140.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1304.00 TO NODE 1303.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1105.00 DOWNSTREAM(FEET) = 835.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1225.00 CHANNEL SLOPE = 0.2204  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.252

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3400  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 35.65  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.70  
 AVERAGE FLOW DEPTH(FEET) = 0.62 TRAVEL TIME(MIN.) = 1.49  
 Tc(MIN.) = 16.60  
 SUBAREA AREA(ACRES) = 13.15 SUBAREA RUNOFF(CFS) = 19.01  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.312  
 TOTAL AREA(ACRES) = 32.1 PEAK FLOW RATE(CFS) = 42.55

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.68 FLOW VELOCITY(FEET/SEC.) = 14.46  
 LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1303.00 = 3365.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1303.00 TO NODE 1303.00 IS CODE = 10

-----  
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1<<<<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2564.00 TO NODE 2563.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 =====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5400  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 1273.00  
 DOWNSTREAM ELEVATION(FEET) = 1271.00  
 ELEVATION DIFFERENCE(FEET) = 2.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.643  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.677  
 SUBAREA RUNOFF(CFS) = 0.66  
 TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.66

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2563.00 TO NODE 2563.10 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<<  
 =====

UPSTREAM ELEVATION(FEET) = 1271.00 DOWNSTREAM ELEVATION(FEET) = 1269.00  
 STREET LENGTH(FEET) = 230.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.89  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.24  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.00  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.62  
STREET FLOW TRAVEL TIME(MIN.) = 1.91 Tc(MIN.) = 8.56  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.521

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.512  
SUBAREA AREA(ACRES) = 1.93 SUBAREA RUNOFF(CFS) = 6.42  
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 6.98

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.84  
FLOW VELOCITY(FEET/SEC.) = 2.30 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.83  
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2563.10 = 310.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2563.10 TO NODE 2562.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1266.00 DOWNSTREAM(FEET) = 1261.00  
FLOW LENGTH(FEET) = 210.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.49  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.98  
PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 8.97  
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2562.00 = 520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2562.00 TO NODE 2562.00 IS CODE = 1



>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.97
RAINFALL INTENSITY(INCH/HR) = 6.33
TOTAL STREAM AREA(ACRES) = 2.09
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.98

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*****
FLOW PROCESS FROM NODE 2563.10 TO NODE 2563.20 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 1269.00
DOWNSTREAM ELEVATION(FEET) = 1268.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151
SUBAREA RUNOFF(CFS) = 2.01
TOTAL AREA(ACRES) = 0.55 TOTAL RUNOFF(CFS) = 2.01

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*****
FLOW PROCESS FROM NODE 2563.20 TO NODE 2562.00 IS CODE = 62
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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

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=====
UPSTREAM ELEVATION(FEET) = 1268.00 DOWNSTREAM ELEVATION(FEET) = 1267.00
STREET LENGTH(FEET) = 120.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

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```

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

```

```

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.92
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29

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HALFSTREET FLOOD WIDTH(FEET) = 8.17  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.86  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.54  
 STREET FLOW TRAVEL TIME(MIN.) = 1.08 Tc(MIN.) = 8.49  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.553  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
 SUBAREA AREA(ACRES) = 0.55 SUBAREA RUNOFF(CFS) = 1.84  
 TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 3.68

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.10  
 FLOW VELOCITY(FEET/SEC.) = 1.94 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.60  
 LONGEST FLOWPATH FROM NODE 2563.10 TO NODE 2562.00 = 185.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2562.00 TO NODE 2562.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.49  
 RAINFALL INTENSITY(INCH/HR) = 6.55  
 TOTAL STREAM AREA(ACRES) = 1.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.68

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.98         | 8.97      | 6.326                 | 2.09        |
| 2             | 3.68         | 8.49      | 6.553                 | 1.10        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 10.29        | 8.49      | 6.553                 |
| 2             | 10.53        | 8.97      | 6.326                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 10.53 Tc(MIN.) = 8.97  
 TOTAL AREA(ACRES) = 3.2

LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2562.00 = 520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2562.00 TO NODE 2558.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1261.00 DOWNSTREAM(FEET) = 1260.00
FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.90
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.53
PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 9.36
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2558.00 = 660.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2558.00 TO NODE 2558.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2561.00 TO NODE 2560.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00
UPSTREAM ELEVATION(FEET) = 1275.00
DOWNSTREAM ELEVATION(FEET) = 1274.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.960
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.234
SUBAREA RUNOFF(CFS) = 0.55
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 2560.00 TO NODE 2560.10 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1274.00 DOWNSTREAM ELEVATION(FEET) = 1269.00
STREET LENGTH(FEET) = 315.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.96

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.29

HALFSTREET FLOOD WIDTH(FEET) = 8.11

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.55

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.74

STREET FLOW TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 8.02

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.801

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.510

SUBAREA AREA(ACRES) = 1.96 SUBAREA RUNOFF(CFS) = 6.80

TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 7.25

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.59

FLOW VELOCITY(FEET/SEC.) = 2.92 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.99

LONGEST FLOWPATH FROM NODE 2561.00 TO NODE 2560.10 = 365.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2560.10 TO NODE 2559.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1262.00

FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.06

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 7.25

PIPE TRAVEL TIME(MIN.) = 0.53 Tc(MIN.) = 8.54

LONGEST FLOWPATH FROM NODE 2561.00 TO NODE 2559.00 = 525.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2559.00 TO NODE 2559.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.54  
RAINFALL INTENSITY(INCH/HR) = 6.53  
TOTAL STREAM AREA(ACRES) = 2.09  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.25

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2560.10 TO NODE 2560.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00  
UPSTREAM ELEVATION(FEET) = 1269.00  
DOWNSTREAM ELEVATION(FEET) = 1268.80  
ELEVATION DIFFERENCE(FEET) = 0.20  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.461  
WARNING: THE MINIMUM OVERLAND FLOW SLOPE, 0.5%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.112  
SUBAREA RUNOFF(CFS) = 1.25  
TOTAL AREA(ACRES) = 0.40 TOTAL RUNOFF(CFS) = 1.25

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2560.20 TO NODE 2559.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1268.80 DOWNSTREAM ELEVATION(FEET) = 1268.00  
STREET LENGTH(FEET) = 115.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.65

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STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.17  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.69  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.49  
STREET FLOW TRAVEL TIME(MIN.) = 1.14 Tc(MIN.) = 10.60  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.681

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.97 SUBAREA RUNOFF(CFS) = 2.81  
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 3.97

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.77  
FLOW VELOCITY(FEET/SEC.) = 1.85 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.60  
LONGEST FLOWPATH FROM NODE 2560.10 TO NODE 2559.00 = 165.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2559.00 TO NODE 2559.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.60  
RAINFALL INTENSITY(INCH/HR) = 5.68  
TOTAL STREAM AREA(ACRES) = 1.37  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.97

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 7.25         | 8.54      | 6.528                 | 2.09        |
| 2             | 3.97         | 10.60     | 5.681                 | 1.37        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 10.45        | 8.54      | 6.528                 |
| 2             | 10.28        | 10.60     | 5.681                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

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PEAK FLOW RATE(CFS) = 10.45 Tc(MIN.) = 8.54  
TOTAL AREA(ACRES) = 3.5  
LONGEST FLOWPATH FROM NODE 2561.00 TO NODE 2559.00 = 525.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2559.00 TO NODE 2558.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1262.00 DOWNSTREAM(FEET) = 1260.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.41  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.45  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 8.60  
LONGEST FLOWPATH FROM NODE 2561.00 TO NODE 2558.00 = 565.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2558.00 TO NODE 2558.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.45        | 8.60      | 6.501                 | 3.46        |

LONGEST FLOWPATH FROM NODE 2561.00 TO NODE 2558.00 = 565.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.53        | 9.36      | 6.153                 | 3.19        |

LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2558.00 = 660.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 20.12        | 8.60      | 6.501                 |
| 2             | 20.42        | 9.36      | 6.153                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 20.42 Tc(MIN.) = 9.36  
TOTAL AREA(ACRES) = 6.7

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2558.00 TO NODE 2558.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2558.00 TO NODE 2554.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1260.00 DOWNSTREAM(FEET) = 1257.80  
FLOW LENGTH(FEET) = 225.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.69  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.42  
PIPE TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 9.85  
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2554.00 = 885.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2554.00 TO NODE 2554.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

-----  
TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.85  
RAINFALL INTENSITY(INCH/HR) = 5.95  
TOTAL STREAM AREA(ACRES) = 6.65  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2557.00 TO NODE 2556.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1271.00  
DOWNSTREAM ELEVATION(FEET) = 1270.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 0.58



TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 2556.00 TO NODE 2555.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1270.00 DOWNSTREAM ELEVATION(FEET) = 1264.00
STREET LENGTH(FEET) = 488.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.77
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.53
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.96
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.17
STREET FLOW TRAVEL TIME(MIN.) = 2.75 Tc(MIN.) = 10.16
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.836

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510
SUBAREA AREA(ACRES) = 3.46 SUBAREA RUNOFF(CFS) = 10.30
TOTAL AREA(ACRES) = 3.6 PEAK FLOW RATE(CFS) = 10.77

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.34
FLOW VELOCITY(FEET/SEC.) = 3.45 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.63
LONGEST FLOWPATH FROM NODE 2557.00 TO NODE 2555.00 = 553.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2555.00 TO NODE 2554.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1258.00 DOWNSTREAM(FEET) = 1257.80

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FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.78  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.77  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 10.18  
LONGEST FLOWPATH FROM NODE 2557.00 TO NODE 2554.00 = 563.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2554.00 TO NODE 2554.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.18  
RAINFALL INTENSITY(INCH/HR) = 5.83  
TOTAL STREAM AREA(ACRES) = 3.62  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.77

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.42        | 9.85      | 5.955                 | 6.65        |
| 2             | 10.77        | 10.18     | 5.829                 | 3.62        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 30.84        | 9.85      | 5.955                 |
| 2             | 30.76        | 10.18     | 5.829                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 30.84 Tc(MIN.) = 9.85  
TOTAL AREA(ACRES) = 10.3  
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2554.00 = 885.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2554.00 TO NODE 2552.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1257.80 DOWNSTREAM(FEET) = 1252.80

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FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.69  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 30.84  
PIPE TRAVEL TIME(MIN.) = 0.99 Tc(MIN.) = 10.84  
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2552.50 = 1400.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2552.50 TO NODE 2552.50 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 10.84 RAIN INTENSITY(INCH/HOUR) = 5.60  
TOTAL AREA(ACRES) = 10.30 TOTAL RUNOFF(CFS) = 9.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2552.50 TO NODE 2552.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1252.80 DOWNSTREAM(FEET) = 1250.80  
CHANNEL LENGTH THRU SUBAREA(FEET) = 185.00 CHANNEL SLOPE = 0.0108  
CHANNEL FLOW THRU SUBAREA(CFS) = 9.10  
FLOW VELOCITY(FEET/SEC) = 2.54 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.22 Tc(MIN.) = 12.06  
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 2552.00 = 1585.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2552.00 TO NODE 1303.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1250.80 DOWNSTREAM(FEET) = 835.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1400.00 CHANNEL SLOPE = 0.2970  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1943 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 9.10  
FLOW VELOCITY(FEET/SEC) = 5.15 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.53 Tc(MIN.) = 16.59  
LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 1303.00 = 2985.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2552.00 TO NODE 1303.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.255
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2329
SUBAREA AREA(ACRES) = 20.83 SUBAREA RUNOFF(CFS) = 23.93
TOTAL AREA(ACRES) = 31.1 TOTAL RUNOFF(CFS) = 30.85
TC(MIN.) = 16.59

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*****
FLOW PROCESS FROM NODE 1303.00 TO NODE 1303.00 IS CODE = 10
-----

```

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

```

*****
FLOW PROCESS FROM NODE 1335.00 TO NODE 1334.00 IS CODE = 21
-----

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 83.00
UPSTREAM ELEVATION(FEET) = 1293.00
DOWNSTREAM ELEVATION(FEET) = 1291.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.483
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.799
SUBAREA RUNOFF(CFS) = 0.58
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.58

```

```

*****
FLOW PROCESS FROM NODE 1334.00 TO NODE 1333.80 IS CODE = 62
-----

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```

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

```

```

=====
UPSTREAM ELEVATION(FEET) = 1291.00 DOWNSTREAM ELEVATION(FEET) = 1280.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

```

```

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

```

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SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.10  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.10  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.33  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.33  
STREET FLOW TRAVEL TIME(MIN.) = 1.04 Tc(MIN.) = 7.52  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.085

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.74 SUBAREA RUNOFF(CFS) = 7.03  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 7.55

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.84  
FLOW VELOCITY(FEET/SEC.) = 4.97 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.80  
LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1333.80 = 353.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1333.80 TO NODE 1333.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.52  
RAINFALL INTENSITY(INCH/HR) = 7.09  
TOTAL STREAM AREA(ACRES) = 1.87  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.55

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1334.80 TO NODE 1334.60 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1287.00  
DOWNSTREAM ELEVATION(FEET) = 1285.00

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ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.287  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.955  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1334.60 TO NODE 1334.40 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1285.00 DOWNSTREAM ELEVATION(FEET) = 1284.00  
STREET LENGTH(FEET) = 50.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.47  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.22  
HALFSTREET FLOOD WIDTH(FEET) = 4.46  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.32  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.50  
STREET FLOW TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 6.65  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.675

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.554  
SUBAREA AREA(ACRES) = 0.46 SUBAREA RUNOFF(CFS) = 1.94  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.42

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.05  
FLOW VELOCITY(FEET/SEC.) = 2.50 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.62  
LONGEST FLOWPATH FROM NODE 1334.80 TO NODE 1334.40 = 130.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1334.40 TO NODE 1333.80 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1278.00 DOWNSTREAM(FEET) = 1276.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.65
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.42
PIPE TRAVEL TIME(MIN.) = 0.72 Tc(MIN.) = 7.36
LONGEST FLOWPATH FROM NODE 1334.80 TO NODE 1333.80 = 330.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1333.80 TO NODE 1333.80 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.36
RAINFALL INTENSITY(INCH/HR) = 7.18
TOTAL STREAM AREA(ACRES) = 0.57
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.42

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 9.94 Tc(MIN.) = 7.52
TOTAL AREA(ACRES) = 2.4
LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1333.80 = 353.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1333.80 TO NODE 1333.40 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1276.00 DOWNSTREAM(FEET) = 1273.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.11  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.94  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 7.69  
LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1333.40 = 453.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1333.40 TO NODE 1333.40 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.69  
RAINFALL INTENSITY(INCH/HR) = 6.99  
TOTAL STREAM AREA(ACRES) = 2.44  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.94

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1333.00 TO NODE 1333.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1281.00  
DOWNSTREAM ELEVATION(FEET) = 1280.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.482  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 68.75  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.111  
SUBAREA RUNOFF(CFS) = 1.15  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 1.15

\*\*\*\*\*



FLOW PROCESS FROM NODE 1333.00 TO NODE 1333.40 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1274.00 DOWNSTREAM(FEET) = 1273.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.81
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.15
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 7.65
LONGEST FLOWPATH FROM NODE 1333.00 TO NODE 1333.40 = 130.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1333.40 TO NODE 1333.40 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.65
RAINFALL INTENSITY(INCH/HR) = 7.01
TOTAL STREAM AREA(ACRES) = 0.29
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.15

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 11.09 Tc(MIN.) = 7.69
TOTAL AREA(ACRES) = 2.7
LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1333.40 = 453.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1333.40 TO NODE 1332.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1273.00 DOWNSTREAM(FEET) = 1267.00  
FLOW LENGTH(FEET) = 210.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.18  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.09  
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 8.03  
LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1332.00 = 663.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1332.00 TO NODE 1332.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.03  
RAINFALL INTENSITY(INCH/HR) = 6.79  
TOTAL STREAM AREA(ACRES) = 2.73  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.09

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1337.00 TO NODE 1336.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1278.00  
DOWNSTREAM ELEVATION(FEET) = 1276.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.27  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1336.00 TO NODE 1335.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1276.00 DOWNSTREAM ELEVATION(FEET) = 1273.00  
STREET LENGTH(FEET) = 240.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.11  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.21  
HALFSTREET FLOOD WIDTH(FEET) = 4.32  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.82  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.39  
STREET FLOW TRAVEL TIME(MIN.) = 2.20 Tc(MIN.) = 9.20  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.224

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.53 SUBAREA RUNOFF(CFS) = 1.68  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.90

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 5.98  
FLOW VELOCITY(FEET/SEC.) = 2.00 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.49  
LONGEST FLOWPATH FROM NODE 1337.00 TO NODE 1335.00 = 320.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1335.00 TO NODE 1332.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1268.00 DOWNSTREAM(FEET) = 1267.00  
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.67  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.90

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PIPE TRAVEL TIME(MIN.) = 0.07    Tc(MIN.) = 9.27  
 LONGEST FLOWPATH FROM NODE 1337.00 TO NODE 1332.00 = 350.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1332.00 TO NODE 1332.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.27  
 RAINFALL INTENSITY(INCH/HR) = 6.19  
 TOTAL STREAM AREA(ACRES) = 0.60  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.90

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.09        | 8.03      | 6.793                 | 2.73        |
| 2             | 1.90         | 9.27      | 6.191                 | 0.60        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.74        | 8.03      | 6.793                 |
| 2             | 12.02        | 9.27      | 6.191                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 12.74    Tc(MIN.) = 8.03  
 TOTAL AREA(ACRES) = 3.3  
 LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1332.00 = 663.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1332.00 TO NODE 1330.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1267.00    DOWNSTREAM(FEET) = 1265.00  
 FLOW LENGTH(FEET) = 150.00    MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.89  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00    NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 12.74

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PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 8.35  
LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1330.00 = 813.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1330.00 TO NODE 1330.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1353.00 TO NODE 1352.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 1284.00

DOWNSTREAM ELEVATION(FEET) = 1282.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423

SUBAREA RUNOFF(CFS) = 0.53

TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1352.00 TO NODE 1351.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 1282.00 DOWNSTREAM ELEVATION(FEET) = 1278.00

STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.79

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.24

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HALFSTREET FLOOD WIDTH(FEET) = 5.52  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.12  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.50  
 STREET FLOW TRAVEL TIME(MIN.) = 2.12 Tc(MIN.) = 9.12  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.259  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
 SUBAREA AREA(ACRES) = 0.79 SUBAREA RUNOFF(CFS) = 2.52  
 TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.97

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.18  
 FLOW VELOCITY(FEET/SEC.) = 2.34 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.63  
 LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1351.00 = 350.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1351.00 TO NODE 1350.40 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1272.00 DOWNSTREAM(FEET) = 1267.00  
 FLOW LENGTH(FEET) = 280.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.07  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.97  
 PIPE TRAVEL TIME(MIN.) = 0.77 Tc(MIN.) = 9.89  
 LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1350.40 = 630.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1350.40 TO NODE 1350.40 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.89  
 RAINFALL INTENSITY(INCH/HR) = 5.94  
 TOTAL STREAM AREA(ACRES) = 0.93  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.97

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1350.80 TO NODE 1350.60 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====
\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1278.00
DOWNSTREAM ELEVATION(FEET) = 1276.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423
SUBAREA RUNOFF(CFS) = 0.38
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 1350.60 TO NODE 1350.40 IS CODE = 62

-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 1276.00 DOWNSTREAM ELEVATION(FEET) = 1267.00
STREET LENGTH(FEET) = 160.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.06
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 8.44
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.88
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.44
STREET FLOW TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 7.54
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.072

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520
SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 7.36
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 7.72

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.16  
FLOW VELOCITY(FEET/SEC.) = 5.66 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.98  
LONGEST FLOWPATH FROM NODE 1350.80 TO NODE 1350.40 = 240.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1350.40 TO NODE 1350.40 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.54  
RAINFALL INTENSITY(INCH/HR) = 7.07  
TOTAL STREAM AREA(ACRES) = 2.10  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.72

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 2.97         | 9.89      | 5.940                 | 0.93        |
| 2             | 7.72         | 7.54      | 7.072                 | 2.10        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 9.98         | 7.54      | 7.072                 |
| 2             | 9.45         | 9.89      | 5.940                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 9.98 Tc(MIN.) = 7.54  
TOTAL AREA(ACRES) = 3.0  
LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1350.40 = 630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1350.40 TO NODE 1346.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1267.00 DOWNSTREAM(FEET) = 1265.00  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.5 INCHES



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PIPE-FLOW VELOCITY(FEET/SEC.) = 10.54  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.98  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 7.64  
LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1346.00 = 690.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1346.00 TO NODE 1330.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1265.00 DOWNSTREAM(FEET) = 1255.00  
FLOW LENGTH(FEET) = 850.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.94  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.98  
PIPE TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 9.68  
LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1330.00 = 1540.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1330.00 TO NODE 1330.00 IS CODE = 11  
-----

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.98         | 9.68      | 6.022                 | 3.03        |

LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1330.00 = 1540.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.74        | 8.35      | 6.625                 | 3.33        |

LONGEST FLOWPATH FROM NODE 1335.00 TO NODE 1330.00 = 813.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 21.35        | 8.35      | 6.625                 |
| 2             | 21.56        | 9.68      | 6.022                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 21.56 Tc(MIN.) = 9.68  
TOTAL AREA(ACRES) = 6.4

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1330.00 TO NODE 1330.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1330.00 TO NODE 1326.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1255.00 DOWNSTREAM(FEET) = 1120.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 410.00 CHANNEL SLOPE = 0.3293  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2016 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 21.56  
FLOW VELOCITY(FEET/SEC) = 6.99 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.98 Tc(MIN.) = 10.66  
LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1326.00 = 1950.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1330.00 TO NODE 1326.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.660  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4733  
SUBAREA AREA(ACRES) = 2.34 SUBAREA RUNOFF(CFS) = 3.97  
TOTAL AREA(ACRES) = 8.7 TOTAL RUNOFF(CFS) = 23.30  
TC(MIN.) = 10.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1326.00 TO NODE 1326.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

-----  
TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.66  
RAINFALL INTENSITY(INCH/HR) = 5.66  
TOTAL STREAM AREA(ACRES) = 8.70  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1328.00 TO NODE 1327.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1325.00  
DOWNSTREAM ELEVATION(FEET) = 1315.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.605  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.567  
SUBAREA RUNOFF(CFS) = 0.72  
TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.72

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1327.00 TO NODE 1326.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1315.00 DOWNSTREAM(FEET) = 1120.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1075.00 CHANNEL SLOPE = 0.1814  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1507 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.72  
FLOW VELOCITY(FEET/SEC) = 2.17 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 8.24 Tc(MIN.) = 13.85  
LONGEST FLOWPATH FROM NODE 1328.00 TO NODE 1326.00 = 1155.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1327.00 TO NODE 1326.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.780  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3017  
SUBAREA AREA(ACRES) = 6.90 SUBAREA RUNOFF(CFS) = 9.90  
TOTAL AREA(ACRES) = 7.1 TOTAL RUNOFF(CFS) = 10.30  
TC(MIN.) = 13.85

\*\*\*\*\*

FLOW PROCESS FROM NODE 1326.00 TO NODE 1326.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 13.85
RAINFALL INTENSITY(INCH/HR) = 4.78
TOTAL STREAM AREA(ACRES) = 7.14
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.30

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 31.23 Tc(MIN.) = 10.66
TOTAL AREA(ACRES) = 15.8
LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1326.00 = 1950.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1326.00 TO NODE 1303.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1120.00 DOWNSTREAM(FEET) = 835.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 965.00 CHANNEL SLOPE = 0.2953
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1938 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 31.23
FLOW VELOCITY(FEET/SEC) = 7.76 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.07 Tc(MIN.) = 12.73
LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1303.00 = 2915.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1326.00 TO NODE 1303.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.046  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3503  
SUBAREA AREA(ACRES) = 8.99 SUBAREA RUNOFF(CFS) = 12.25  
TOTAL AREA(ACRES) = 24.8 TOTAL RUNOFF(CFS) = 43.90  
TC(MIN.) = 12.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1303.00 TO NODE 1303.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 43.90        | 12.73     | 5.046                 | 24.83       |

LONGEST FLOWPATH FROM NODE 1353.00 TO NODE 1303.00 = 2915.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 42.55        | 16.60     | 4.252                 | 32.09       |

LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1303.00 = 3365.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 76.53        | 12.73     | 5.046                 |
| 2             | 79.54        | 16.60     | 4.252                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 79.54 Tc(MIN.) = 16.60  
TOTAL AREA(ACRES) = 56.9

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1303.00 TO NODE 1303.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 79.54        | 16.60     | 4.252                 | 56.92       |

LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1303.00 = 3365.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 30.85        | 16.59     | 4.255                 | 31.13       |

LONGEST FLOWPATH FROM NODE 2564.00 TO NODE 1303.00 = 2985.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 110.31       | 16.59     | 4.255                 |
| 2             | 110.37       | 16.60     | 4.252                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 110.37 Tc(MIN.) = 16.60  
 TOTAL AREA(ACRES) = 88.1

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1303.00 TO NODE 1303.00 IS CODE = 12  
 -----

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1303.00 TO NODE 1303.00 IS CODE = 12  
 -----

>>>>CLEAR MEMORY BANK # 2 <<<<<

=====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1303.00 TO NODE 1302.00 IS CODE = 53  
 -----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 835.00 DOWNSTREAM(FEET) = 775.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 520.00 CHANNEL SLOPE = 0.1154  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1115 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 110.37  
 FLOW VELOCITY(FEET/SEC) = 8.96 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 0.97 Tc(MIN.) = 17.57  
 LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1302.00 = 3885.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1303.00 TO NODE 1302.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.100  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2943  
SUBAREA AREA(ACRES) = 9.18 SUBAREA RUNOFF(CFS) = 10.91  
TOTAL AREA(ACRES) = 97.2 TOTAL RUNOFF(CFS) = 117.32  
TC(MIN.) = 17.57

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1302.00 TO NODE 1302.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1<<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1339.00 TO NODE 1338.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1284.00  
DOWNSTREAM ELEVATION(FEET) = 1282.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.362  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.185  
SUBAREA RUNOFF(CFS) = 0.22  
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.22

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1338.00 TO NODE 1337.80 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1282.00 DOWNSTREAM ELEVATION(FEET) = 1276.00  
STREET LENGTH(FEET) = 165.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.89  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.21  
HALFSTREET FLOOD WIDTH(FEET) = 4.32  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.10  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.66  
STREET FLOW TRAVEL TIME(MIN.) = 0.89 Tc(MIN.) = 8.25  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.676

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.98 SUBAREA RUNOFF(CFS) = 3.34  
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 3.54

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.31  
FLOW VELOCITY(FEET/SEC.) = 3.43 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.87  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1337.80 = 250.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1337.80 TO NODE 1337.60 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1270.00 DOWNSTREAM(FEET) = 1266.00  
FLOW LENGTH(FEET) = 255.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.09  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.54  
PIPE TRAVEL TIME(MIN.) = 0.70 Tc(MIN.) = 8.95  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1337.60 = 505.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1337.60 TO NODE 1337.60 IS CODE = 1  
-----



>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.95  
RAINFALL INTENSITY(INCH/HR) = 6.34  
TOTAL STREAM AREA(ACRES) = 1.04  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 1345.00 TO NODE 1344.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1277.00  
DOWNSTREAM ELEVATION(FEET) = 1275.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.49  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 1344.00 TO NODE 1343.80 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1275.00 DOWNSTREAM ELEVATION(FEET) = 1272.00  
STREET LENGTH(FEET) = 210.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.67  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28

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HALFSTREET FLOOD WIDTH(FEET) = 7.71  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.34  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.66  
 STREET FLOW TRAVEL TIME(MIN.) = 1.49 Tc(MIN.) = 8.49  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.553  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.518  
 SUBAREA AREA(ACRES) = 0.69 SUBAREA RUNOFF(CFS) = 2.35  
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.79

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.70  
 FLOW VELOCITY(FEET/SEC.) = 2.63 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.84  
 LONGEST FLOWPATH FROM NODE 1345.00 TO NODE 1343.80 = 290.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1343.80 TO NODE 1337.60 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1266.50 DOWNSTREAM(FEET) = 1266.00  
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.83  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.79  
 PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 8.66  
 LONGEST FLOWPATH FROM NODE 1345.00 TO NODE 1337.60 = 340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1337.60 TO NODE 1337.60 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.66  
 RAINFALL INTENSITY(INCH/HR) = 6.47  
 TOTAL STREAM AREA(ACRES) = 0.82  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.79

\*\* CONFLUENCE DATA \*\*

| STREAM | RUNOFF | Tc | INTENSITY | AREA |
|--------|--------|----|-----------|------|
|--------|--------|----|-----------|------|

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 3.54  | 8.95   | 6.336       | 1.04   |
| 2      | 2.79  | 8.66   | 6.468       | 0.82   |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 6.21         | 8.66      | 6.468                 |
| 2             | 6.27         | 8.95      | 6.336                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.27 Tc(MIN.) = 8.95  
TOTAL AREA(ACRES) = 1.9  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1337.60 = 505.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1337.60 TO NODE 1345.60 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1266.00 DOWNSTREAM(FEET) = 1264.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.27  
PIPE TRAVEL TIME(MIN.) = 0.29 Tc(MIN.) = 9.24  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1345.60 = 630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1345.60 TO NODE 1345.60 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.24  
RAINFALL INTENSITY(INCH/HR) = 6.21  
TOTAL STREAM AREA(ACRES) = 1.86  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 1345.90 TO NODE 1345.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1280.00

DOWNSTREAM ELEVATION(FEET) = 1278.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.773

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 80.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.582

SUBAREA RUNOFF(CFS) = 0.56

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 1345.80 TO NODE 1343.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1278.00 DOWNSTREAM ELEVATION(FEET) = 1269.50

STREET LENGTH(FEET) = 315.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.89

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.30

HALFSTREET FLOOD WIDTH(FEET) = 8.57

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.39

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.01

STREET FLOW TRAVEL TIME(MIN.) = 1.55 Tc(MIN.) = 8.32

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.640

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5600

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.561  
SUBAREA AREA(ACRES) = 1.25 SUBAREA RUNOFF(CFS) = 4.65  
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 5.14

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 10.97  
FLOW VELOCITY(FEET/SEC.) = 3.89 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.34  
LONGEST FLOWPATH FROM NODE 1345.90 TO NODE 1343.00 = 415.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1343.00 TO NODE 1345.60 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1264.50 DOWNSTREAM(FEET) = 1264.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.18  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.14  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 8.43  
LONGEST FLOWPATH FROM NODE 1345.90 TO NODE 1345.60 = 455.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1345.60 TO NODE 1345.60 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.43  
RAINFALL INTENSITY(INCH/HR) = 6.58  
TOTAL STREAM AREA(ACRES) = 1.38  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.14

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.27         | 9.24      | 6.205                 | 1.86        |
| 2             | 5.14         | 8.43      | 6.585                 | 1.38        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.05        | 8.43      | 6.585                 |
| 2             | 11.11        | 9.24      | 6.205                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.11 Tc(MIN.) = 9.24  
TOTAL AREA(ACRES) = 3.2  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1345.60 = 630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1345.60 TO NODE 1346.80 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1262.00  
FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.29  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.11  
PIPE TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 9.63  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1346.80 = 800.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1346.80 TO NODE 1346.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.63  
RAINFALL INTENSITY(INCH/HR) = 6.04  
TOTAL STREAM AREA(ACRES) = 3.24  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.11

\*\*\*\*\*

FLOW PROCESS FROM NODE 1348.00 TO NODE 1347.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1275.00

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DOWNSTREAM ELEVATION(FEET) = 1273.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.38  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 1347.00 TO NODE 1346.90 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1273.00 DOWNSTREAM ELEVATION(FEET) = 1265.00  
STREET LENGTH(FEET) = 150.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.14  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.21  
HALFSTREET FLOOD WIDTH(FEET) = 4.12  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.72  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.78  
STREET FLOW TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 7.67  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.997

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.519  
SUBAREA AREA(ACRES) = 0.97 SUBAREA RUNOFF(CFS) = 3.53  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 3.89

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 5.98  
FLOW VELOCITY(FEET/SEC.) = 4.08 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.00  
LONGEST FLOWPATH FROM NODE 1348.00 TO NODE 1346.90 = 230.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1346.90 TO NODE 1346.80 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1262.50 DOWNSTREAM(FEET) = 1262.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.29  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.89  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 7.83  
LONGEST FLOWPATH FROM NODE 1348.00 TO NODE 1346.80 = 280.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1346.80 TO NODE 1346.80 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.83  
RAINFALL INTENSITY(INCH/HR) = 6.91  
TOTAL STREAM AREA(ACRES) = 1.07  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.89

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1347.60 TO NODE 1347.50 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1270.00  
DOWNSTREAM ELEVATION(FEET) = 1268.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.773  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 80.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.582  
SUBAREA RUNOFF(CFS) = 0.65  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.65

\*\*\*\*\*



FLOW PROCESS FROM NODE 1347.50 TO NODE 1347.40 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1268.00 DOWNSTREAM ELEVATION(FEET) = 1265.00
STREET LENGTH(FEET) = 110.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.96
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 9.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.69
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.19
STREET FLOW TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 7.27
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.244

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5400
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.542
SUBAREA AREA(ACRES) = 1.69 SUBAREA RUNOFF(CFS) = 6.61
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 7.23

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.59
FLOW VELOCITY(FEET/SEC.) = 4.24 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.60
LONGEST FLOWPATH FROM NODE 1347.60 TO NODE 1347.40 = 210.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1347.40 TO NODE 1346.80 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1262.50 DOWNSTREAM(FEET) = 1262.00
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.71

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ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.23  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 7.37  
LONGEST FLOWPATH FROM NODE 1347.60 TO NODE 1346.80 = 250.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1346.80 TO NODE 1346.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.37  
RAINFALL INTENSITY(INCH/HR) = 7.18  
TOTAL STREAM AREA(ACRES) = 1.84  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.23

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.11        | 9.63      | 6.043                 | 3.24        |
| 2             | 3.89         | 7.83      | 6.906                 | 1.07        |
| 3             | 7.23         | 7.37      | 7.181                 | 1.84        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 20.24        | 7.37      | 7.181                 |
| 2             | 20.56        | 7.83      | 6.906                 |
| 3             | 20.60        | 9.63      | 6.043                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 20.60 Tc(MIN.) = 9.63  
TOTAL AREA(ACRES) = 6.2  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1346.80 = 800.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1346.80 TO NODE 1342.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1262.00 DOWNSTREAM(FEET) = 1261.50  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013

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DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.78  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.60  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 9.74  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1342.00 = 850.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1342.00 TO NODE 1342.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.74  
RAINFALL INTENSITY(INCH/HR) = 6.00  
TOTAL STREAM AREA(ACRES) = 6.15  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.60

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1347.90 TO NODE 1347.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1272.00  
DOWNSTREAM ELEVATION(FEET) = 1270.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.362  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.185  
SUBAREA RUNOFF(CFS) = 0.37  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1347.80 TO NODE 1347.70 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1270.00 DOWNSTREAM ELEVATION(FEET) = 1269.00  
STREET LENGTH(FEET) = 100.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.72

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.25

HALFSTREET FLOOD WIDTH(FEET) = 6.05

AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.78

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.44

STREET FLOW TRAVEL TIME(MIN.) = 0.94 Tc(MIN.) = 8.30

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.652

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.510

SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 2.71

TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 3.05

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.04

FLOW VELOCITY(FEET/SEC.) = 2.00 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.57

LONGEST FLOWPATH FROM NODE 1347.90 TO NODE 1342.70 = 185.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1347.70 TO NODE 1342.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1261.50

FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.96

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 3.05

PIPE TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 8.80

LONGEST FLOWPATH FROM NODE 1347.90 TO NODE 1342.00 = 335.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1342.00 TO NODE 1342.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.80  
RAINFALL INTENSITY(INCH/HR) = 6.40  
TOTAL STREAM AREA(ACRES) = 0.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.05

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.60        | 9.74      | 6.000                 | 6.15        |
| 2             | 3.05         | 8.80      | 6.403                 | 0.90        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 22.35        | 8.80      | 6.403                 |
| 2             | 23.46        | 9.74      | 6.000                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 23.46 Tc(MIN.) = 9.74  
TOTAL AREA(ACRES) = 7.1  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1342.00 = 850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1342.00 TO NODE 1341.50 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1261.50 DOWNSTREAM(FEET) = 1260.00  
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.21  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 23.46  
PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 10.04  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1341.50 = 1000.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1341.50 TO NODE 1341.00 IS CODE = 52

-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====  
ELEVATION DATA: UPSTREAM(FEET) = 1260.00 DOWNSTREAM(FEET) = 1259.50  
CHANNEL LENGTH THRU SUBAREA(FEET) = 50.00 CHANNEL SLOPE = 0.0100  
CHANNEL FLOW THRU SUBAREA(CFS) = 23.46  
FLOW VELOCITY(FEET/SEC) = 3.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 10.31  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1341.00 = 1050.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1341.50 TO NODE 1341.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.783  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5186  
SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 1.03  
TOTAL AREA(ACRES) = 7.6 TOTAL RUNOFF(CFS) = 23.46  
TC(MIN.) = 10.31  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1341.00 TO NODE 1340.80 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
ELEVATION DATA: UPSTREAM(FEET) = 1253.00 DOWNSTREAM(FEET) = 1215.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 32.43  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 23.46  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 10.36  
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1340.80 = 1150.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1340.80 TO NODE 1340.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====  
ELEVATION DATA: UPSTREAM(FEET) = 1215.00 DOWNSTREAM(FEET) = 1030.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 800.00 CHANNEL SLOPE = 0.2313  
SLOPE ADJUSTMENT CURVE USED:

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EFFECTIVE SLOPE = .1737 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 23.46
FLOW VELOCITY(FEET/SEC) = 6.68 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.00 Tc(MIN.) = 12.36
LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1340.00 = 1950.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1340.80 TO NODE 1340.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.145
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4067
SUBAREA AREA(ACRES) = 6.19 SUBAREA RUNOFF(CFS) = 8.60
TOTAL AREA(ACRES) = 13.8 TOTAL RUNOFF(CFS) = 28.77
TC(MIN.) = 12.36

\*\*\*\*\*
FLOW PROCESS FROM NODE 1340.00 TO NODE 1340.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.36
RAINFALL INTENSITY(INCH/HR) = 5.14
TOTAL STREAM AREA(ACRES) = 13.75
PEAK FLOW RATE(CFS) AT CONFLUENCE = 28.77

\*\*\*\*\*
FLOW PROCESS FROM NODE 1356.10 TO NODE 1350.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1280.00
DOWNSTREAM ELEVATION(FEET) = 1235.00
ELEVATION DIFFERENCE(FEET) = 45.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.428
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.52  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 1.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 1350.00 TO NODE 1340.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1235.00 DOWNSTREAM(FEET) = 1030.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.3417  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2038 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.52  
FLOW VELOCITY(FEET/SEC) = 2.91 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.44 Tc(MIN.) = 7.87  
LONGEST FLOWPATH FROM NODE 1356.10 TO NODE 1340.00 = 700.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1350.00 TO NODE 1340.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.885  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2941  
SUBAREA AREA(ACRES) = 5.66 SUBAREA RUNOFF(CFS) = 10.91  
TOTAL AREA(ACRES) = 5.9 TOTAL RUNOFF(CFS) = 12.05  
TC(MIN.) = 7.87

\*\*\*\*\*

FLOW PROCESS FROM NODE 1340.00 TO NODE 1340.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.87  
RAINFALL INTENSITY(INCH/HR) = 6.88  
TOTAL STREAM AREA(ACRES) = 5.95  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.05

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|



|   |       |       | P-13d.TXT |       |
|---|-------|-------|-----------|-------|
| 1 | 28.77 | 12.36 | 5.145     | 13.75 |
| 2 | 12.05 | 7.87  | 6.885     | 5.95  |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 33.55        | 7.87      | 6.885                 |
| 2             | 37.77        | 12.36     | 5.145                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 37.77 Tc(MIN.) = 12.36  
 TOTAL AREA(ACRES) = 19.7  
 LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1340.00 = 1950.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1340.00 TO NODE 1302.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1030.00 DOWNSTREAM(FEET) = 775.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1505.00 CHANNEL SLOPE = 0.1694  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1447 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 37.77  
 FLOW VELOCITY(FEET/SEC) = 7.14 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 3.51 Tc(MIN.) = 15.87  
 LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1302.00 = 3455.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1340.00 TO NODE 1302.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.378  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3202  
 SUBAREA AREA(ACRES) = 25.68 SUBAREA RUNOFF(CFS) = 31.48  
 TOTAL AREA(ACRES) = 45.4 TOTAL RUNOFF(CFS) = 63.62  
 TC(MIN.) = 15.87

\*\*\*\*\*

FLOW PROCESS FROM NODE 1302.00 TO NODE 1302.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 63.62        | 15.87     | 4.378                 | 45.38       |

LONGEST FLOWPATH FROM NODE 1339.00 TO NODE 1302.00 = 3455.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 117.32       | 17.57     | 4.100                 | 97.23       |

LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1302.00 = 3885.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 169.59       | 15.87     | 4.378                 |
| 2             | 176.90       | 17.57     | 4.100                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 176.90 Tc(MIN.) = 17.57  
TOTAL AREA(ACRES) = 142.6

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1302.00 TO NODE 1302.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1302.00 TO NODE 1301.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 775.00 DOWNSTREAM(FEET) = 760.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 220.00 CHANNEL SLOPE = 0.0682  
CHANNEL FLOW THRU SUBAREA(CFS) = 176.90  
FLOW VELOCITY(FEET/SEC) = 14.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 17.82  
LONGEST FLOWPATH FROM NODE 1321.00 TO NODE 1301.00 = 4105.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1301.00 TO NODE 13.00 IS CODE = 41

P-13d.TXT

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|                                  |                   |                    |                       |
|----------------------------------|-------------------|--------------------|-----------------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 760.00            | DOWNSTREAM(FEET) = | 670.00                |
| FLOW LENGTH(FEET) =              | 665.00            | MANNING'S N =      | 0.013                 |
| DEPTH OF FLOW IN                 | 36.0 INCH PIPE IS | 23.5 INCHES        |                       |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 36.23             |                    |                       |
| GIVEN PIPE DIAMETER(INCH) =      | 36.00             | NUMBER OF PIPES =  | 1                     |
| PIPE-FLOW(CFS) =                 | 176.90            |                    |                       |
| PIPE TRAVEL TIME(MIN.) =         | 0.31              | Tc(MIN.) =         | 18.12                 |
| LONGEST FLOWPATH FROM NODE       | 1321.00           | TO NODE            | 13.00 = 4770.00 FEET. |

=====

END OF STUDY SUMMARY:

|                     |   |        |            |       |
|---------------------|---|--------|------------|-------|
| TOTAL AREA(ACRES)   | = | 142.6  | TC(MIN.) = | 18.12 |
| PEAK FLOW RATE(CFS) | = | 176.90 |            |       |

=====

END OF RATIONAL METHOD ANALYSIS

↑



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL

(c) Copyright 1982-2012 Advanced Engineering Software (aes)  
Ver. 19.0 Release Date: 06/01/2012 License ID 1355

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUBBASIN # 15 \*  
\* 2660-02 - AUGUST 2014 \*  
\*\*\*\*\*

FILE NAME: MERR15-P. DAT  
TIME/DATE OF STUDY: 14:59 08/19/2014

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1510.00 TO NODE 1509.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1530.00  
DOWNSTREAM ELEVATION(FEET) = 1510.00  
ELEVATION DIFFERENCE(FEET) = 20.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.945  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.247  
SUBAREA RUNOFF(CFS) = 0.49  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1509.00 TO NODE 1508.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

|   |         |                       |         |
|---|---------|-----------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =                        | 1510.00 | DOWNSTREAM(FEET) =    | 1345.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) =                     | 500.00  | CHANNEL SLOPE =       | 0.3300  |
| CHANNEL BASE(FEET) =                                    | 3.00    | "Z" FACTOR =          | 2.000   |
| MANNING' S FACTOR =                                     | 0.030   | MAXIMUM DEPTH(FEET) = | 10.00   |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =                | 7.313   |                       |         |
| *USER SPECIFIED(SUBAREA):                               |         |                       |         |
| RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT =    | .3200   |                       |         |
| S. C. S. CURVE NUMBER (AMC II) =                        | 0       |                       |         |
| TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =        | 2.96    |                       |         |
| TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = | 6.84    |                       |         |
| AVERAGE FLOW DEPTH(FEET) =                              | 0.13    | TRAVEL TIME(MIN.) =   | 1.22    |
| Tc(MIN.) =  | 7.16    |                       |         |
| SUBAREA AREA(ACRES) =                                   | 2.10    | SUBAREA RUNOFF(CFS) = | 4.91    |
| AREA-AVERAGE RUNOFF COEFFICIENT =                       | 0.322   |                       |         |
| TOTAL AREA(ACRES) =                                     | 2.3     | PEAK FLOW RATE(CFS) = | 5.35    |

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.19 FLOW VELOCITY(FEET/SEC.) = 8.53  
LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1508.00 = 590.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1508.00 TO NODE 1507.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<<

=====

|  |                   |                    |         |
|--|-------------------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =                     | 1345.00           | DOWNSTREAM(FEET) = | 1285.00 |
| FLOW LENGTH(FEET) =                                  | 95.00             | MANNING' S N =     | 0.013   |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO           | 18.000            |                    |         |
| DEPTH OF FLOW IN                                     | 18.0 INCH PIPE IS | 3.2 INCHES         |         |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                      | 25.53             |                    |         |
| ESTIMATED PIPE DIAMETER(INCH) =                      | 18.00             | NUMBER OF PIPES =  | 1       |
| PIPE-FLOW(CFS) =                                     | 5.35              |                    |         |
| PIPE TRAVEL TIME(MIN.) =                             | 0.06              | Tc(MIN.) =         | 7.22    |
| LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1507.00 = | 685.00 FEET.      |                    |         |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1507.00 TO NODE 1506.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

|   |         |                       |         |
|---|---------|-----------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =                        | 1285.00 | DOWNSTREAM(FEET) =    | 1135.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) =                     | 575.00  | CHANNEL SLOPE =       | 0.2609  |
| CHANNEL BASE(FEET) =                                    | 3.00    | "Z" FACTOR =          | 2.000   |
| MANNING' S FACTOR =                                     | 0.030   | MAXIMUM DEPTH(FEET) = | 10.00   |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =                | 6.697   |                       |         |
| *USER SPECIFIED(SUBAREA):                               |         |                       |         |
| RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT =    | .2500   |                       |         |
| S. C. S. CURVE NUMBER (AMC II) =                        | 0       |                       |         |
| TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =        | 9.90    |                       |         |
| TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = | 9.73    |                       |         |
| AVERAGE FLOW DEPTH(FEET) =                              | 0.29    | TRAVEL TIME(MIN.) =   | 0.99    |

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Tc(MIN. ) = 8.21  
SUBAREA AREA(ACRES) = 5.42 SUBAREA RUNOFF(CFS) = 9.07  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.271  
TOTAL AREA(ACRES) = 7.7 PEAK FLOW RATE(CFS) = 13.97

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.35 FLOW VELOCITY(FEET/SEC. ) = 10.86  
LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1506.00 = 1260.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1506.00 TO NODE 1505.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 904.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 960.00 CHANNEL SLOPE = 0.2406  
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 13.97  
FLOW VELOCITY(FEET/SEC) = 8.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN. ) = 1.86 Tc(MIN. ) = 10.07  
LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1505.00 = 2220.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1506.00 TO NODE 1505.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.872  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2570  
SUBAREA AREA(ACRES) = 15.66 SUBAREA RUNOFF(CFS) = 22.99  
TOTAL AREA(ACRES) = 23.4 TOTAL RUNOFF(CFS) = 35.24  
TC(MIN. ) = 10.07

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1505.00 TO NODE 1504.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 904.00 DOWNSTREAM(FEET) = 857.00  
FLOW LENGTH(FEET) = 220.00 MANNING'S N = 0.015  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 9.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC. ) = 25.23  
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 35.24  
PIPE TRAVEL TIME(MIN. ) = 0.15 Tc(MIN. ) = 10.21  
LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1504.00 = 2440.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1504.00 TO NODE 1504.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN. ) = 10.21  
RAINFALL INTENSITY(INCH/HR) = 5.82  
TOTAL STREAM AREA(ACRES) = 23.35  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 35.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1504.30 TO NODE 1504.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1225.00  
DOWNSTREAM ELEVATION(FEET) = 1195.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.28  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1504.20 TO NODE 1504.10 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1195.00 DOWNSTREAM(FEET) = 891.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1110.00 CHANNEL SLOPE = 0.2739  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1880 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.28  
FLOW VELOCITY(FEET/SEC) = 2.43 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 7.62 Tc(MIN.) = 14.72  
LONGEST FLOWPATH FROM NODE 1504.30 TO NODE 1504.10 = 1210.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1504.20 TO NODE 1504.10 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.595  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 5.31 SUBAREA RUNOFF(CFS) = 6.10  
TOTAL AREA(ACRES) = 5.5 TOTAL RUNOFF(CFS) = 6.27  
TC(MIN.) = 14.72

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1504.10 TO NODE 1504.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 891.00 DOWNSTREAM(FEET) = 857.00  
FLOW LENGTH(FEET) = 574.00 MANNING'S N = 0.015  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 6.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.13  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.27  
PIPE TRAVEL TIME(MIN.) = 0.94 Tc(MIN.) = 15.67  
LONGEST FLOWPATH FROM NODE 1504.30 TO NODE 1504.00 = 1784.00 FEET.



\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1504.00 TO NODE 1504.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 15.67  
 RAINFALL INTENSITY(INCH/HR) = 4.41  
 TOTAL STREAM AREA(ACRES) = 5.46  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.27

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 35.24        | 10.21     | 5.818                 | 23.35       |
| 2             | 6.27         | 15.67     | 4.415                 | 5.46        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 39.33        | 10.21     | 5.818                 |
| 2             | 33.01        | 15.67     | 4.415                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 39.33 Tc(MIN.) = 10.21  
 TOTAL AREA(ACRES) = 28.8  
 LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1504.00 = 2440.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1504.00 TO NODE 1500.00 IS CODE = 41

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 857.00 DOWNSTREAM(FEET) = 846.00  
 FLOW LENGTH(FEET) = 234.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 42.0 INCH PIPE IS 12.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.55  
 GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 39.33  
 PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 10.45  
 LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1500.00 = 2674.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1500.00 TO NODE 1500.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.45  
 RAINFALL INTENSITY(INCH/HR) = 5.73  
 TOTAL STREAM AREA(ACRES) = 28.81  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 39.33

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1503.00 TO NODE 1502.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1290.00  
DOWNSTREAM ELEVATION(FEET) = 1260.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.44  
TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.44

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1502.00 TO NODE 1501.00 IS CODE = 53

-----  
>>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA<<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1260.00 DOWNSTREAM(FEET) = 902.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 820.00 CHANNEL SLOPE = 0.4366  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2184 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.44  
FLOW VELOCITY(FEET/SEC) = 2.62 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.22 Tc(MIN.) = 12.32  
LONGEST FLOWPATH FROM NODE 1503.00 TO NODE 1501.00 = 920.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1502.00 TO NODE 1501.00 IS CODE = 81

-----  
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.153  
\*USER SPECIFIED(SUBAREA):  
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .2500  
S. C. S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 7.10 SUBAREA RUNOFF(CFS) = 9.15  
TOTAL AREA(ACRES) = 7.3 TOTAL RUNOFF(CFS) = 9.46  
TC(MIN.) = 12.32

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1501.00 TO NODE 1500.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 902.00 DOWNSTREAM(FEET) = 846.00  
FLOW LENGTH(FEET) = 344.00 MANNING'S N = 0.015  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 5.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.34  
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.46  
PIPE TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 12.68  
LONGEST FLOWPATH FROM NODE 1503.00 TO NODE 1500.00 = 1264.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1500.00 TO NODE 1500.00 IS CODE = 1

-----  
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.68  
 RAINFALL INTENSITY(INCH/HR) = 5.06  
 TOTAL STREAM AREA(ACRES) = 7.34  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.46

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 39.33        | 10.45     | 5.733                 | 28.81       |
| 2             | 9.46         | 12.68     | 5.061                 | 7.34        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 47.12        | 10.45     | 5.733                 |
| 2             | 44.18        | 12.68     | 5.061                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 47.12 Tc(MIN.) = 10.45  
 TOTAL AREA(ACRES) = 36.2  
 LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 1500.00 = 2674.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1500.00 TO NODE 15.00 IS CODE = 41  
 -----

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 846.00 DOWNSTREAM(FEET) = 791.00  
 FLOW LENGTH(FEET) = 162.00 MANNING'S N = 0.024  
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 10.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 22.48  
 GIVEN PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 47.12  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 10.57  
 LONGEST FLOWPATH FROM NODE 1510.00 TO NODE 15.00 = 2836.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 36.2 TC(MIN.) = 10.57  
 PEAK FLOW RATE(CFS) = 47.12  
 =====

=====

END OF RATIONAL METHOD ANALYSIS

□



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* PROPOSED HYDROLOGY \*  
\* BASIN 16 - WITH DETENTION \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-16D.DAT  
TIME/DATE OF STUDY: 16:58 09/09/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0312 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1607.00 TO NODE 1606.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8800

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 67.00

UPSTREAM ELEVATION(FEET) = 1344.00

DOWNSTREAM ELEVATION(FEET) = 1343.20

ELEVATION DIFFERENCE(FEET) = 0.80

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.055

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.89

TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.89

\*\*\*\*\*

FLOW PROCESS FROM NODE 1606.00 TO NODE 1605.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1343.20 DOWNSTREAM ELEVATION(FEET) = 1310.00

STREET LENGTH(FEET) = 625.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.67

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.31

HALFSTREET FLOOD WIDTH(FEET) = 9.10

AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.93

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.52

STREET FLOW TRAVEL TIME(MIN.) = 2.11 Tc(MIN.) = 5.17

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.028

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8800

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
SUBAREA AREA(ACRES) = 0.95 SUBAREA RUNOFF(CFS) = 7.55  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 8.42

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.72  
FLOW VELOCITY(FEET/SEC.) = 5.65 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.04  
LONGEST FLOWPATH FROM NODE 1607.00 TO NODE 1605.00 = 692.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1605.00 TO NODE 1604.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1310.00 DOWNSTREAM(FEET) = 1308.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 30.00 CHANNEL SLOPE = 0.0667  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.42  
FLOW VELOCITY(FEET/SEC) = 6.18 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 5.25  
LONGEST FLOWPATH FROM NODE 1607.00 TO NODE 1604.00 = 722.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1604.00 TO NODE 1604.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 5.28 RAIN INTENSITY(INCH/HOUR) = 8.90  
TOTAL AREA(ACRES) = 1.06 TOTAL RUNOFF(CFS) = 1.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 1604.00 TO NODE 1603.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1305.00 DOWNSTREAM(FEET) = 1280.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.38  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.00  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 5.38  
LONGEST FLOWPATH FROM NODE 1607.00 TO NODE 1603.00 = 797.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 1603.00 TO NODE 1602.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1280.00 DOWNSTREAM(FEET) = 1245.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 135.00 CHANNEL SLOPE = 0.2593  
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.00  
FLOW VELOCITY(FEET/SEC) = 4.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 5.86  
LONGEST FLOWPATH FROM NODE 1607.00 TO NODE 1602.00 = 932.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1602.00 TO NODE 1602.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.86  
RAINFALL INTENSITY(INCH/HR) = 8.33  
TOTAL STREAM AREA(ACRES) = 1.06  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1610.00 TO NODE 1609.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1590.00  
DOWNSTREAM ELEVATION(FEET) = 1575.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.945  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.247  
SUBAREA RUNOFF(CFS) = 0.61  
TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 0.61

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1609.00 TO NODE 1608.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<



>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1575.00 DOWNSTREAM(FEET) = 1315.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 550.00 CHANNEL SLOPE = 0.4727
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.540
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.78
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.34
AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 0.89
Tc(MIN.) = 6.83
SUBAREA AREA(ACRES) = 5.42 SUBAREA RUNOFF(CFS) = 12.26
AREA-AVERAGE RUNOFF COEFFICIENT = 0.302
TOTAL AREA(ACRES) = 5.6 PEAK FLOW RATE(CFS) = 12.81

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.28 FLOW VELOCITY(FEET/SEC.) = 12.89
LONGEST FLOWPATH FROM NODE 1610.00 TO NODE 1608.00 = 640.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 1608.00 TO NODE 1602.00 IS CODE = 31

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1315.00 DOWNSTREAM(FEET) = 1245.00
FLOW LENGTH(FEET) = 605.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.85
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.81
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 7.40
LONGEST FLOWPATH FROM NODE 1610.00 TO NODE 1602.00 = 1245.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 1602.00 TO NODE 1602.00 IS CODE = 1

```

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.40
RAINFALL INTENSITY(INCH/HR) = 7.16

```

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TOTAL STREAM AREA(ACRES) = 5.63  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.81

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 1.00         | 5.86      | 8.329                 | 1.06        |
| 2             | 12.81        | 7.40      | 7.163                 | 5.63        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.14        | 5.86      | 8.329                 |
| 2             | 13.67        | 7.40      | 7.163                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.67 Tc(MIN.) = 7.40  
TOTAL AREA(ACRES) = 6.7  
LONGEST FLOWPATH FROM NODE 1610.00 TO NODE 1602.00 = 1245.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1602.00 TO NODE 1601.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1245.00 DOWNSTREAM(FEET) = 945.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1085.00 CHANNEL SLOPE = 0.2765  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.449

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 28.61  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.82  
AVERAGE FLOW DEPTH(FEET) = 0.51 TRAVEL TIME(MIN.) = 1.31  
Tc(MIN.) = 8.71  
SUBAREA AREA(ACRES) = 17.11 SUBAREA RUNOFF(CFS) = 29.79  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.270  
TOTAL AREA(ACRES) = 23.8 PEAK FLOW RATE(CFS) = 41.48

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.63 FLOW VELOCITY(FEET/SEC.) = 15.50  
LONGEST FLOWPATH FROM NODE 1610.00 TO NODE 1601.00 = 2330.00 FEET.

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\*\*\*\*\*

FLOW PROCESS FROM NODE 1601.00 TO NODE 16.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|  |             |                    |        |
|--|-------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =           | 950.00      | DOWNSTREAM(FEET) = | 850.00 |
| FLOW LENGTH(FEET) =                        | 605.00      | MANNING'S N =      | 0.015  |
| DEPTH OF FLOW IN 42.0 INCH PIPE IS         | 10.0 INCHES |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =            | 23.76       |                    |        |
| GIVEN PIPE DIAMETER(INCH) =                | 42.00       | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                           | 41.48       |                    |        |
| PIPE TRAVEL TIME(MIN.) =                   | 0.42        | Tc(MIN.) =         | 9.13   |
| LONGEST FLOWPATH FROM NODE 1610.00 TO NODE | 16.00 =     | 2935.00 FEET.      |        |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 23.8 TC(MIN.) = 9.13  
PEAK FLOW RATE(CFS) = 41.48

=====

END OF RATIONAL METHOD ANALYSIS







Job Name: Newland Sierra

Job #: 2660-02

Run Name:

P-19.dat

Page 2 of 5

| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1979         | 1978   | 3    | 1195             | 1179             | 220              |             |               |                |      |   |   |
| 1978         | 1978   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1978.4       | 1978.2 | 2    | 1235             | 1228             | 75               | 0.6         | 0.16          |                |      |   |   |
| 1978.2       | 1978   | 6    | 1228             | 1185             | 610              | 0.59        | 1.15          | 2 sides        |      |   |   |
| 1978         | 1978   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1978         | 1977   | 3    | 1179             | 1178             | 60               |             |               |                |      |   |   |
| 1977         | 1977   | 11   |                  |                  |                  |             |               | add bank 1     |      |   |   |
| 1977         | 1977   | 12   |                  |                  |                  |             |               | clear bank 1   |      |   |   |
| 1977         | 1976   | 3    | 1178             | 1104             | 700              |             |               |                |      |   |   |
| 1976         | 1976   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1976.4       | 1976.2 | 2    | 1186             | 1180             | 80               | 0.88        | 0.22          |                |      |   |   |
| 1976.2       | 1976   | 6    | 1184             | 1115             | 780              | 0.89        | 1.36          | 1 side         |      |   |   |
| 1976         | 1976   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1976         | 1975   | 3    | 1109             | 1070             | 625              |             |               |                |      |   |   |
| 1975         | 1906.5 | 5    | 1070             | 1054             | 165              | 0.25        | 4.08          |                |      |   |   |
| 1906.5       | 1906   | 3    | 1048             | 1047             | 25               |             |               |                |      |   |   |
| 1906         | 1906   | 10   |                  |                  |                  |             |               | save to bank 1 |      |   |   |
| 1968         | 1967   | 2    | 1320             | 1315             | 90               | 0.25        | 0.07          |                |      |   |   |
| 1967         | 1964   | 5    | 1315             | 1270             | 730              | 0.27        | 0.74          |                |      |   |   |
| 1964         | 1963   | 3    | 1264             | 1262             | 25               |             |               |                |      |   |   |
| 1963         | 1963   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1974         | 1973   | 2    | 1310             | 1305             | 75               | 0.35        | 0.19          |                |      |   |   |
| 1973         | 1972   | 5    | 1305             | 1270             | 580              | 0.27        | 2.32          |                |      |   |   |
| 1972         | 1963   | 3    | 1264             | 1262             | 60               |             |               |                |      |   |   |
| 1963         | 1963   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1963         | 1963.5 | 3    | 1262             | 1261.5           | 26               |             |               |                |      |   |   |
| 1963.5       | 1963.5 | 10   |                  |                  |                  |             |               | save to bank 2 |      |   |   |
| 1971         | 1970   | 2    | 1589             | 1558             | 100              | 0.35        | 0.44          |                |      |   |   |
| 1970         | 1969   | 5    | 1558             | 1326             | 1020             | 0.27        | 7.17          |                |      |   |   |
| 1969         | 1969   | 1    |                  |                  |                  |             |               | 1 of 3         |      |   |   |
| 1951         | 1950   | 2    | 1600             | 1529             | 100              | 0.35        | 0.14          |                |      |   |   |
| 1950         | 1969   | 5    | 1529             | 1272             | 900              | 0.35        | 4.85          |                |      |   |   |
| 1969         | 1969   | 1    |                  |                  |                  |             |               | 2 of 3         |      |   |   |
| 1958         | 1957   | 2    | 1435             | 1405             | 100              | 0.35        | 0.18          |                |      |   |   |



Job Name: Newland Sierra

Job #: 2660-02

Run Name:  
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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1957         | 1956   | 5    | 1405             | 1275             | 1125             | 0.35        | 4.29          |                |      |   |   |
| 1956         | 1969   | 3    | 1269             | 1264             | 165              |             |               |                |      |   |   |
| 1969         | 1969   | 1    |                  |                  |                  |             |               | 3 of 3         |      |   |   |
| 1969         | 1963.5 | 3    | 1264             | 1261.5           | 155              |             |               |                |      |   |   |
| 1963.5       | 1963.5 | 11   |                  |                  |                  |             |               | add bank 2     |      |   |   |
| 1963.5       | 193.5  | 12   |                  |                  |                  |             |               | clear bank 2   |      |   |   |
| 1963.5       | 1959   | 3    | 1261.5           | 1179             | 829              |             |               |                |      |   |   |
| 1959         | 1959   | 1    |                  |                  |                  |             |               | 1 of 3         |      |   |   |
| 1962         | 1961   | 2    | 1250             | 1240             | 65               | 0.63        | 0.03          |                |      |   |   |
| 1961         | 1960   | 5    | 1240             | 1190             | 490              | 0.62        | 1.20          |                |      |   |   |
| 1960         | 1959   | 3    | 1184             | 1179             | 25               |             |               |                |      |   |   |
| 1959         | 1959   | 1    |                  |                  |                  |             |               | 2 of 3         |      |   |   |
| 1959.6       | 1959.4 | 2    | 1370             | 1326             | 100              | 0.35        | 0.21          |                |      |   |   |
| 1959.4       | 1959.2 | 5    | 1326             | 1190             | 1185             | 0.35        | 2.83          |                |      |   |   |
| 1959         | 1959   | 1    |                  |                  |                  |             |               | 3 of 3         |      |   |   |
| 1959         | 1924   | 3    | 1179             | 1176             | 65               |             |               |                |      |   |   |
| 1924         | 1924   | 10   |                  |                  |                  |             |               | save to bank 2 |      |   |   |
| 1993         | 1992   | 2    | 1276             | 1273             | 194              | 0.35        | 0.07          |                |      |   |   |
| 1992         | 1933   | 5    | 1273             | 1267             | 255              | 0.35        | 0.31          |                |      |   |   |
| 1933         | 1933   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1935         | 1934   | 2    | 1235             | 1234             | 70               | 0.33        | 0.18          |                |      |   |   |
| 1934         | 1933   | 5    | 1234             | 1233             | 165              | 0.33        | 0.40          |                |      |   |   |
| 1933         | 1933   | 1    |                  |                  |                  |             |               | 3 of 3         |      |   |   |
| 1933         | 1932   | 3    | 1227             | 1226             | 40               |             |               |                |      |   |   |
| 1932         | 1925   | 3    | 1226             | 1194             | 490              |             |               |                |      |   |   |
| 1925         | 1925   | 10   |                  |                  |                  |             |               | save to bank 3 |      |   |   |
| 1931         | 1930   | 2    | 1280             | 1258             | 100              | 0.35        | 0.26          |                |      |   |   |
| 1930         | 1929   | 5    | 1258             | 1214             | 200              | 0.31        | 3.39          |                |      |   |   |
| 1929         | 1926   | 3    | 1208             | 1207             | 160              |             |               |                |      |   |   |
| 1926         | 1926   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1928         | 1927   | 2    | 1223             | 1221             | 80               | 0.58        | 0.11          |                |      |   |   |
| 1927         | 1926   | 5    | 1221             | 1216             | 260              | 0.58        | 1.90          |                |      |   |   |
| 1926         | 1926   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |



Job Name: Newland Sierra

Job #: 2660-02

Run Name:  
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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1926         | 1925   | 3    | 1210             | 1196             | 195              |             |               |                |      |   |   |
| 1925         | 1925   | 11   |                  |                  |                  |             |               | add bank 3     |      |   |   |
| 1925         | 1925   | 12   |                  |                  |                  |             |               | clear bank 3   |      |   |   |
| 1925         | 1924   | 3    | 1196             | 1178             | 285              |             |               |                |      |   |   |
| 1924         | 1924   | 11   |                  |                  |                  |             |               | add bank 2     |      |   |   |
| 1924         | 1924   | 12   |                  |                  |                  |             |               | clear bank 2   |      |   |   |
| 1924         | 1912   | 3    | 1178             | 1087.4           | 690              |             |               |                |      |   |   |
| 1912         | 1912   | 10   |                  |                  |                  |             |               | Save to bank 2 |      |   |   |
| 1921.5       | 1921   | 2    | 1201             | 1200             | 65               | 0.25        | 0.05          |                |      |   |   |
| 1921         | 1920   | 5    | 1200             | 1195             | 475              | 0.25        | 0.82          | brow ditch     |      |   |   |
| 1920         | 1917   | 3    | 1189             | 1183             | 25               |             |               |                |      |   |   |
| 1917         | 1917   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1919         | 1918   | 2    | 1200             | 1198             | 80               | 0.58        | 0.11          |                |      |   |   |
| 1918         | 1917   | 6    | 1198             | 1189             | 545              | 0.58        | 2.71          |                |      |   |   |
| 1917         | 1917   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1917         | 1914   | 3    | 1189             | 1173             | 215              |             |               |                |      |   |   |
| 1914         | 1914   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1916         | 1915   | 2    | 1193             | 1189             | 95               | 0.58        | 0.23          |                |      |   |   |
| 1915         | 1914   | 6    | 1189             | 1179             | 780              | 0.58        | 3.23          |                |      |   |   |
| 1914         | 1914   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1914         | 1913   | 3    | 1173             | 1089             | 130              |             |               |                |      |   |   |
| 1913         | 1913   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1923         | 1922   | 2    | 1180             | 1168             | 90               | 0.25        | 0.06          |                |      |   |   |
| 1922         | 1913   | 5    | 1168             | 1095             | 675              | 0.25        | 0.67          |                |      |   |   |
| 1913         | 1913   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 1913         | 1912   | 3    | 1089             | 1087.4           | 160              |             |               |                |      |   |   |
| 1912         | 1912   | 11   |                  |                  |                  |             |               | Add bank 2     |      |   |   |
| 1912         | 1912   | 12   |                  |                  |                  |             |               | Clear bank 2   |      |   |   |
| 1912         | 1911   | 3    | 1087.4           | 1079             | 220              |             |               |                |      |   |   |
| 1911         | 1911   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 1911.4       | 1911.2 | 2    | 1150             | 1140             | 70               | 0.3         | 0.08          |                |      |   |   |
| 1911.2       | 1911   | 5    | 1140             | 1085             | 250              | 0.25        | 0.53          |                |      |   |   |
| 1911         | 1911   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2014 Advanced Engineering Software (aes)
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering
6390 Greenwich Drive
Suite 200
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*
\* PROPOSED HYDROLOGY \*
\* SUB BASIN 19 WITH DETENTION \*
\* \*
\*\*\*\*\*

FILE NAME: P-19D.DAT
TIME/DATE OF STUDY: 15:25 01/20/2016

-----
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS
\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

Table with 10 columns: NO., WIDTH (FT), CROWN TO CROSSFALL (FT), STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY, CURB HEIGHT (FT), GUTTER WIDTH (FT), GUTTER LIP (FT), GUTTER GEOMETRIES: HIKE (FT), MANNING FACTOR (n). Row 1: 1, 18.0, 8.0, 0.020/0.020/0.020, 0.50, 1.50, 0.0313, 0.125, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2025.00 TO NODE 2024.00 IS CODE = 21

-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1295.00
DOWNSTREAM ELEVATION(FEET) = 1293.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.006
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

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THE MAXIMUM OVERLAND FLOW LENGTH = 80.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.193

SUBAREA RUNOFF(CFS) = 0.72

TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.72

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2024.00 TO NODE 2023.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1293.00 DOWNSTREAM(FEET) = 1275.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 930.00 CHANNEL SLOPE = 0.0194  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.206  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 18.68  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.80  
AVERAGE FLOW DEPTH(FEET) = 0.83 TRAVEL TIME(MIN.) = 3.23  
Tc(MIN.) = 9.24  
SUBAREA AREA(ACRES) = 9.04 SUBAREA RUNOFF(CFS) = 35.35  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
TOTAL AREA(ACRES) = 9.2 PEAK FLOW RATE(CFS) = 35.89

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.17 FLOW VELOCITY(FEET/SEC.) = 5.73  
LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 2023.00 = 1030.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2023.00 TO NODE 2020.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1269.00 DOWNSTREAM(FEET) = 1259.00  
FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.30  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 35.89  
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 9.51  
LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 2020.00 = 1280.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2020.00 TO NODE 2020.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.51  
RAINFALL INTENSITY(INCH/HR) = 6.09  
TOTAL STREAM AREA(ACRES) = 9.18  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 35.89

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2022.00 TO NODE 2021.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====
\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00
UPSTREAM ELEVATION(FEET) = 1284.00
DOWNSTREAM ELEVATION(FEET) = 1283.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.748
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.35

\*\*\*\*\*
FLOW PROCESS FROM NODE 2021.00 TO NODE 2020.00 IS CODE = 62
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 1283.00 DOWNSTREAM ELEVATION(FEET) = 1265.00
STREET LENGTH(FEET) = 315.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.34
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.17
HALFSTREET FLOOD WIDTH(FEET) = 2.26
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.97
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.68
STREET FLOW TRAVEL TIME(MIN.) = 1.32 Tc(MIN.) = 6.07
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.136

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630
SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 2.00
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 2.31

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 4.26
FLOW VELOCITY(FEET/SEC.) = 3.85 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.81
LONGEST FLOWPATH FROM NODE 2022.00 TO NODE 2020.00 = 365.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2020.00 TO NODE 2020.00 IS CODE = 1
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.07

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RAINFALL INTENSITY(INCH/HR) = 8.14  
 TOTAL STREAM AREA(ACRES) = 0.45  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.31

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 35.89        | 9.51      | 6.091                 | 9.18        |
| 2             | 2.31         | 6.07      | 8.136                 | 0.45        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 25.22        | 6.07      | 8.136                 |
| 2             | 37.62        | 9.51      | 6.091                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 37.62 Tc(MIN.) = 9.51  
 TOTAL AREA(ACRES) = 9.6  
 LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 2020.00 = 1280.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2020.00 TO NODE 2017.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1259.00 DOWNSTREAM(FEET) = 1258.00  
 FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.39  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 37.62  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 9.57  
 LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 2017.00 = 1325.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2017.00 TO NODE 2017.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.57  
 RAINFALL INTENSITY(INCH/HR) = 6.07  
 TOTAL STREAM AREA(ACRES) = 9.63  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 37.62

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2019.00 TO NODE 2018.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
 UPSTREAM ELEVATION(FEET) = 1310.00  
 DOWNSTREAM ELEVATION(FEET) = 1305.00  
 ELEVATION DIFFERENCE(FEET) = 5.00

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SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.219  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.14  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 1.14

\*\*\*\*\*

FLOW PROCESS FROM NODE 2018.00 TO NODE 2017.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

UPSTREAM ELEVATION(FEET) = 1305.00 DOWNSTREAM ELEVATION(FEET) = 1270.00  
STREET LENGTH(FEET) = 590.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.03

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.17  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.25  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.63  
STREET FLOW TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 4.09  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.889  
SUBAREA AREA(ACRES) = 0.95 SUBAREA RUNOFF(CFS) = 7.80  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 8.93

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.72  
FLOW VELOCITY(FEET/SEC.) = 5.99 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.16  
LONGEST FLOWPATH FROM NODE 2019.00 TO NODE 2017.00 = 685.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2017.00 TO NODE 2017.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.09  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.09  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.93

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 37.62        | 9.57      | 6.066                 | 9.63        |

2 8.93 4.09 P-19d.TXT 9.222 1.09

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 33.68        | 4.09      | 9.222                 |
| 2             | 43.50        | 9.57      | 6.066                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 43.50 Tc(MIN.) = 9.57  
TOTAL AREA(ACRES) = 10.7  
LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 2017.00 = 1325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2017.00 TO NODE 2014.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1258.00 DOWNSTREAM(FEET) = 1179.00  
FLOW LENGTH(FEET) = 855.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.62  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 43.50  
PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 10.23  
LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 2014.00 = 2180.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2014.00 TO NODE 2014.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.23  
RAINFALL INTENSITY(INCH/HR) = 5.81  
TOTAL STREAM AREA(ACRES) = 10.72  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 2016.00 TO NODE 2015.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 1270.00  
DOWNSTREAM ELEVATION(FEET) = 1264.00  
ELEVATION DIFFERENCE(FEET) = 6.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.472  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.41  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 1.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 2015.00 TO NODE 2014.00 IS CODE = 62

-----  
 >>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1264.00 DOWNSTREAM ELEVATION(FEET) = 1185.00  
 STREET LENGTH(FEET) = 810.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.42  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.33  
 HALFSTREET FLOOD WIDTH(FEET) = 10.34  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.09  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.36  
 STREET FLOW TRAVEL TIME(MIN.) = 1.90 Tc(MIN.) = 3.38  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.69 SUBAREA RUNOFF(CFS) = 14.03  
 TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 15.44

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.28  
 FLOW VELOCITY(FEET/SEC.) = 8.20 DEPTH\*VELOCITY(FT\*FT/SEC.) = 3.21  
 LONGEST FLOWPATH FROM NODE 2016.00 TO NODE 2014.00 = 880.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2014.00 TO NODE 2014.00 IS CODE = 1

-----  
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 3.38  
 RAINFALL INTENSITY(INCH/HR) = 9.22  
 TOTAL STREAM AREA(ACRES) = 1.86  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.44

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 43.50        | 10.23     | 5.811                 | 10.72       |
| 2             | 15.44        | 3.38      | 9.222                 | 1.86        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 43.50        | 10.23     | 5.811                 |
| 2             | 15.44        | 3.38      | 9.222                 |

|   |       |       |           |
|---|-------|-------|-----------|
|   |       |       | P-19d.TXT |
| 1 | 42.85 | 3.38  | 9.222     |
| 2 | 53.23 | 10.23 | 5.811     |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 53.23 Tc(MIN.) = 10.23  
 TOTAL AREA(ACRES) = 12.6  
 LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 2014.00 = 2180.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2014.00 TO NODE 1977.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1185.00 DOWNSTREAM(FEET) = 1183.00  
 FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 17.52  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 53.23  
 PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 10.27  
 LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1977.00 = 2225.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1977.00 TO NODE 1977.00 IS CODE = 10

-----  
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1989.00 TO NODE 1988.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 1284.00  
 DOWNSTREAM ELEVATION(FEET) = 1283.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.431  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
 THE MAXIMUM OVERLAND FLOW LENGTH = 70.00  
 (Reference: Table 3-1B of Hydrology Manual)  
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.840  
 SUBAREA RUNOFF(CFS) = 0.44  
 TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.44

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1988.00 TO NODE 1987.00 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1283.00 DOWNSTREAM ELEVATION(FEET) = 1235.00  
 STREET LENGTH(FEET) = 490.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020



SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.83  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.18  
HALFSTREET FLOOD WIDTH(FEET) = 2.46  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.13  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.90  
STREET FLOW TRAVEL TIME(MIN.) = 1.59 Tc(MIN.) = 8.02  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.797  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
SUBAREA AREA(ACRES) = 0.65 SUBAREA RUNOFF(CFS) = 2.78  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 3.17

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 4.39  
FLOW VELOCITY(FEET/SEC.) = 5.10 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.09  
LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1987.00 = 565.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1987.00 TO NODE 1983.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1229.00 DOWNSTREAM(FEET) = 1214.00  
FLOW LENGTH(FEET) = 165.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.04  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.17  
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 8.27  
LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1983.00 = 730.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1983.00 TO NODE 1983.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.27  
RAINFALL INTENSITY(INCH/HR) = 6.66  
TOTAL STREAM AREA(ACRES) = 0.74  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.17

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1986.00 TO NODE 1985.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5900  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

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UPSTREAM ELEVATION(FEET) = 1228.00  
DOWNSTREAM ELEVATION(FEET) = 1226.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.050  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.155  
SUBAREA RUNOFF(CFS) = 0.48  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.48

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1985.00 TO NODE 1984.00 IS CODE = 51

-----  
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1226.00 DOWNSTREAM(FEET) = 1221.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 185.00 CHANNEL SLOPE = 0.0270  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.377  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5800  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.99  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.03  
AVERAGE FLOW DEPTH(FEET) = 0.28 TRAVEL TIME(MIN.) = 1.02  
Tc(MIN.) = 7.07  
SUBAREA AREA(ACRES) = 1.17 SUBAREA RUNOFF(CFS) = 5.01  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.581  
TOTAL AREA(ACRES) = 1.3 PEAK FLOW RATE(CFS) = 5.44

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 FLOW VELOCITY(FEET/SEC.) = 3.73  
LONGEST FLOWPATH FROM NODE 1986.00 TO NODE 1984.00 = 265.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1984.00 TO NODE 1983.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1215.00 DOWNSTREAM(FEET) = 1214.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.44  
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.26  
LONGEST FLOWPATH FROM NODE 1986.00 TO NODE 1983.00 = 340.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1983.00 TO NODE 1983.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.26  
RAINFALL INTENSITY(INCH/HR) = 7.25  
TOTAL STREAM AREA(ACRES) = 1.27  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.44

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.17         | 8.27      | 6.664                 | 0.74        |
| 2             | 5.44         | 7.26      | 7.249                 | 1.27        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 8.22         | 7.26      | 7.249                 |
| 2             | 8.17         | 8.27      | 6.664                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.22 Tc(MIN.) = 7.26  
TOTAL AREA(ACRES) = 2.0  
LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1983.00 = 730.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1983.00 TO NODE 1979.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1214.00 DOWNSTREAM(FEET) = 1194.00  
FLOW LENGTH(FEET) = 335.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.44  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.22  
PIPE TRAVEL TIME(MIN.) = 0.45 Tc(MIN.) = 7.71  
LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1979.00 = 1065.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1979.00 TO NODE 1979.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.71  
RAINFALL INTENSITY(INCH/HR) = 6.97  
TOTAL STREAM AREA(ACRES) = 2.01  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.22

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1982.00 TO NODE 1981.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1267.00  
DOWNSTREAM ELEVATION(FEET) = 1264.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.373  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.803  
SUBAREA RUNOFF(CFS) = 0.78

TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.78

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1981.00 TO NODE 1980.00 IS CODE = 51

-----  
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1239.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 725.00 CHANNEL SLOPE = 0.0345  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.052  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.89  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.48  
AVERAGE FLOW DEPTH(FEET) = 0.64 TRAVEL TIME(MIN.) = 2.21  
Tc(MIN.) = 7.58  
SUBAREA AREA(ACRES) = 6.28 SUBAREA RUNOFF(CFS) = 27.90  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
TOTAL AREA(ACRES) = 6.4 PEAK FLOW RATE(CFS) = 28.52

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.90 FLOW VELOCITY(FEET/SEC.) = 6.63  
LONGEST FLOWPATH FROM NODE 1982.00 TO NODE 1980.00 = 815.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1980.00 TO NODE 1979.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1233.00 DOWNSTREAM(FEET) = 1195.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.11  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 28.52  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 7.63  
LONGEST FLOWPATH FROM NODE 1982.00 TO NODE 1979.00 = 915.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1979.00 TO NODE 1979.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.63  
RAINFALL INTENSITY(INCH/HR) = 7.02  
TOTAL STREAM AREA(ACRES) = 6.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 28.52

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.22         | 7.71      | 6.974                 | 2.01        |
| 2             | 28.52        | 7.63      | 7.023                 | 6.42        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 36.69        | 7.63      | 7.023                 |
| 2             | 36.55        | 7.71      | 6.974                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 36.69 Tc(MIN.) = 7.63  
 TOTAL AREA(ACRES) = 8.4  
 LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1979.00 = 1065.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1979.00 TO NODE 1978.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1195.00 DOWNSTREAM(FEET) = 1179.00  
 FLOW LENGTH(FEET) = 220.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.09  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 36.69  
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.82  
 LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1978.00 = 1285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1978.00 TO NODE 1978.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.82  
 RAINFALL INTENSITY(INCH/HR) = 6.91  
 TOTAL STREAM AREA(ACRES) = 8.43  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.69

\*\*\*\*\*

FLOW PROCESS FROM NODE 1978.40 TO NODE 1978.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 1235.00  
 DOWNSTREAM ELEVATION(FEET) = 1228.00  
 ELEVATION DIFFERENCE(FEET) = 7.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.702  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.89  
 TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.89

\*\*\*\*\*

FLOW PROCESS FROM NODE 1978.20 TO NODE 1978.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1228.00 DOWNSTREAM ELEVATION(FEET) = 1185.00  
 STREET LENGTH(FEET) = 610.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.70  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.23  
 HALFSTREET FLOOD WIDTH(FEET) = 5.38  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.53  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.06  
 STREET FLOW TRAVEL TIME(MIN.) = 2.24 Tc(MIN.) = 5.94  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.248

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5900  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.591  
 SUBAREA AREA(ACRES) = 1.15 SUBAREA RUNOFF(CFS) = 5.60  
 TOTAL AREA(ACRES) = 1.3 PEAK FLOW RATE(CFS) = 6.39

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.18  
 FLOW VELOCITY(FEET/SEC.) = 5.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.36  
 LONGEST FLOWPATH FROM NODE 1978.40 TO NODE 1978.00 = 685.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1978.00 TO NODE 1978.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.94  
 RAINFALL INTENSITY(INCH/HR) = 8.25  
 TOTAL STREAM AREA(ACRES) = 1.31  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.39

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 36.69        | 7.82      | 6.911                 | 8.43        |
| 2             | 6.39         | 5.94      | 8.248                 | 1.31        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 37.13        | 5.94      | 8.248                 |
| 2             | 42.04        | 7.82      | 6.911                 |

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COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 42.04 Tc(MIN.) = 7.82

TOTAL AREA(ACRES) = 9.7

LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1978.00 = 1285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1978.00 TO NODE 1977.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1179.00 DOWNSTREAM(FEET) = 1178.00

FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 11.46

ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 42.04

PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 7.91

LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1977.00 = 1345.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1977.00 TO NODE 1977.00 IS CODE = 11

>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

|   |       |      |       |      |
|---|-------|------|-------|------|
| 1 | 42.04 | 7.91 | 6.862 | 9.74 |
|---|-------|------|-------|------|

LONGEST FLOWPATH FROM NODE 1989.00 TO NODE 1977.00 = 1345.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

|   |       |       |       |       |
|---|-------|-------|-------|-------|
| 1 | 53.23 | 10.27 | 5.796 | 12.58 |
|---|-------|-------|-------|-------|

LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1977.00 = 2225.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
|---------------|--------------|-----------|-----------------------|

|   |       |      |       |
|---|-------|------|-------|
| 1 | 83.01 | 7.91 | 6.862 |
|---|-------|------|-------|

|   |       |       |       |
|---|-------|-------|-------|
| 2 | 88.73 | 10.27 | 5.796 |
|---|-------|-------|-------|

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 88.73 Tc(MIN.) = 10.27

TOTAL AREA(ACRES) = 22.3

\*\*\*\*\*

FLOW PROCESS FROM NODE 1977.00 TO NODE 1977.00 IS CODE = 12

>>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1977.00 TO NODE 1976.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1178.00 DOWNSTREAM(FEET) = 1104.00

FLOW LENGTH(FEET) = 700.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.6 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 27.29  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 88.73  
PIPE TRAVEL TIME(MIN.) = 0.43 Tc(MIN.) = 10.70  
LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1976.00 = 2925.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1976.00 TO NODE 1976.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.70  
RAINFALL INTENSITY(INCH/HR) = 5.65  
TOTAL STREAM AREA(ACRES) = 22.32  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 88.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1976.40 TO NODE 1976.20 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1186.00  
DOWNSTREAM ELEVATION(FEET) = 1180.00  
ELEVATION DIFFERENCE(FEET) = 6.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.810  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.79  
TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 1.79

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1976.20 TO NODE 1976.00 IS CODE = 62

-----  
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1184.00 DOWNSTREAM ELEVATION(FEET) = 1115.00  
STREET LENGTH(FEET) = 780.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.37  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.33  
HALFSTREET FLOOD WIDTH(FEET) = 9.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.63  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.16  
STREET FLOW TRAVEL TIME(MIN.) = 1.96 Tc(MIN.) = 3.77  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222



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NOTE: RAINFALL INTENSITY IS BASED ON TC = 5-MINUTE.

\*USER-SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8900

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.889

SUBAREA AREA(ACRES) = 1.36 SUBAREA RUNOFF(CFS) = 11.16

TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 12.95

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.59

FLOW VELOCITY(FEET/SEC.) = 7.60 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.87

LONGEST FLOWPATH FROM NODE 1976.40 TO NODE 1976.00 = 860.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1976.00 TO NODE 1976.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 3.77

RAINFALL INTENSITY(INCH/HR) = 9.22

TOTAL STREAM AREA(ACRES) = 1.58

PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.95

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 88.73        | 10.70     | 5.645                 | 22.32       |
| 2             | 12.95        | 3.77      | 9.222                 | 1.58        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 44.22        | 3.77      | 9.222                 |
| 2             | 96.66        | 10.70     | 5.645                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 96.66 Tc(MIN.) = 10.70

TOTAL AREA(ACRES) = 23.9

LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1976.00 = 2925.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1976.00 TO NODE 1975.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1109.00 DOWNSTREAM(FEET) = 1070.00

FLOW LENGTH(FEET) = 625.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 24.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 22.57

ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 96.66

PIPE TRAVEL TIME(MIN.) = 0.46 Tc(MIN.) = 11.16

LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1975.00 = 3550.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1975.00 TO NODE 1906.50 IS CODE = 51

-----  
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1070.00 DOWNSTREAM(FEET) = 1054.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 165.00 CHANNEL SLOPE = 0.0970  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.430  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 99.43  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.63  
 AVERAGE FLOW DEPTH(FEET) = 1.30 TRAVEL TIME(MIN.) = 0.20  
 Tc(MIN.) = 11.36  
 SUBAREA AREA(ACRES) = 4.08 SUBAREA RUNOFF(CFS) = 5.54  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.613  
 TOTAL AREA(ACRES) = 28.0 PEAK FLOW RATE(CFS) = 96.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 1.28 FLOW VELOCITY(FEET/SEC.) = 13.51  
 LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1906.50 = 3715.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1906.50 TO NODE 1906.00 IS CODE = 31

-----  
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1048.00 DOWNSTREAM(FEET) = 1047.00  
 FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 26.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.24  
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 96.66  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 11.39  
 LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1906.00 = 3740.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1906.00 TO NODE 1906.00 IS CODE = 10

-----  
 >>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1968.00 TO NODE 1967.00 IS CODE = 21

-----  
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
 UPSTREAM ELEVATION(FEET) = 1320.00  
 DOWNSTREAM ELEVATION(FEET) = 1315.00  
 ELEVATION DIFFERENCE(FEET) = 5.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.196  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.705  
 SUBAREA RUNOFF(CFS) = 0.12  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.12

\*\*\*\*\*  
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FLOW PROCESS FROM NODE 1967.00 TO NODE 1964.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1315.00 DOWNSTREAM(FEET) = 1270.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 730.00 CHANNEL SLOPE = 0.0616
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.817
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2700
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.61
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.22
AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 5.49
Tc(MIN.) = 13.68
SUBAREA AREA(ACRES) = 0.74 SUBAREA RUNOFF(CFS) = 0.96
AREA-AVERAGE RUNOFF COEFFICIENT = 0.268
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 1.05

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 2.76
LONGEST FLOWPATH FROM NODE 1968.00 TO NODE 1964.00 = 820.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1964.00 TO NODE 1963.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1262.00
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.60
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.05
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 13.74
LONGEST FLOWPATH FROM NODE 1968.00 TO NODE 1963.00 = 845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1963.00 TO NODE 1963.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.74
RAINFALL INTENSITY(INCH/HR) = 4.81
TOTAL STREAM AREA(ACRES) = 0.81
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.05

\*\*\*\*\*

FLOW PROCESS FROM NODE 1974.00 TO NODE 1973.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00
UPSTREAM ELEVATION(FEET) = 1310.00

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DOWNSTREAM ELEVATION(FEET) = 1305.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.212  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.017  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1973.00 TO NODE 1972.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1305.00 DOWNSTREAM(FEET) = 1270.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 580.00 CHANNEL SLOPE = 0.0603  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.421  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.59  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.79  
AVERAGE FLOW DEPTH(FEET) = 0.20 TRAVEL TIME(MIN.) = 2.55  
Tc(MIN.) = 8.76  
SUBAREA AREA(ACRES) = 2.32 SUBAREA RUNOFF(CFS) = 4.02  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.276  
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 4.45

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.27 FLOW VELOCITY(FEET/SEC.) = 4.62  
LONGEST FLOWPATH FROM NODE 1974.00 TO NODE 1972.00 = 655.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1972.00 TO NODE 1963.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1262.00  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.51  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.45  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 8.88  
LONGEST FLOWPATH FROM NODE 1974.00 TO NODE 1963.00 = 715.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1963.00 TO NODE 1963.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.88  
RAINFALL INTENSITY(INCH/HR) = 6.37  
TOTAL STREAM AREA(ACRES) = 2.51  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.45

\*\* CONFLUENCE DATA \*\*

| P-19d.TXT     |              |           |                       |             |
|---------------|--------------|-----------|-----------------------|-------------|
| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
| 1             | 1.05         | 13.74     | 4.805                 | 0.81        |
| 2             | 4.45         | 8.88      | 6.366                 | 2.51        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 5.13         | 8.88      | 6.366                 |
| 2             | 4.41         | 13.74     | 4.805                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.13 Tc(MIN.) = 8.88  
 TOTAL AREA(ACRES) = 3.3  
 LONGEST FLOWPATH FROM NODE 1968.00 TO NODE 1963.00 = 845.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1963.00 TO NODE 1963.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1262.00 DOWNSTREAM(FEET) = 1261.50  
 FLOW LENGTH(FEET) = 26.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.24  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 5.13  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 8.94  
 LONGEST FLOWPATH FROM NODE 1968.00 TO NODE 1963.50 = 871.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1963.50 TO NODE 1963.50 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1971.00 TO NODE 1970.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1589.00  
 DOWNSTREAM ELEVATION(FEET) = 1558.00  
 ELEVATION DIFFERENCE(FEET) = 31.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
 SUBAREA RUNOFF(CFS) = 1.23  
 TOTAL AREA(ACRES) = 0.44 TOTAL RUNOFF(CFS) = 1.23

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1970.00 TO NODE 1969.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1558.00 DOWNSTREAM(FEET) = 1326.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1020.00 CHANNEL SLOPE = 0.2275  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.688  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.81  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.67  
AVERAGE FLOW DEPTH(FEET) = 0.26 TRAVEL TIME(MIN.) = 1.96  
Tc(MIN.) = 8.23  
SUBAREA AREA(ACRES) = 7.17 SUBAREA RUNOFF(CFS) = 12.95  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.275  
TOTAL AREA(ACRES) = 7.6 PEAK FLOW RATE(CFS) = 13.98

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 FLOW VELOCITY(FEET/SEC.) = 10.39  
LONGEST FLOWPATH FROM NODE 1971.00 TO NODE 1969.00 = 1120.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1969.00 TO NODE 1969.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.23  
RAINFALL INTENSITY(INCH/HR) = 6.69  
TOTAL STREAM AREA(ACRES) = 7.61  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1951.00 TO NODE 1950.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1600.00  
DOWNSTREAM ELEVATION(FEET) = 1529.00  
ELEVATION DIFFERENCE(FEET) = 71.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.39  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.39

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1950.00 TO NODE 1969.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1529.00 DOWNSTREAM(FEET) = 1272.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 900.00 CHANNEL SLOPE = 0.2856  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.803

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*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.19
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.59
AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 1.75
Tc(MIN.) = 8.01
SUBAREA AREA(ACRES) = 4.85 SUBAREA RUNOFF(CFS) = 11.55
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350
TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 11.88

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END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 FLOW VELOCITY(FEET/SEC.) = 10.67
LONGEST FLOWPATH FROM NODE 1951.00 TO NODE 1969.00 = 1000.00 FEET.

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FLOW PROCESS FROM NODE 1969.00 TO NODE 1969.00 IS CODE = 1

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>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.01
RAINFALL INTENSITY(INCH/HR) = 6.80
TOTAL STREAM AREA(ACRES) = 4.99
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.88

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FLOW PROCESS FROM NODE 1958.00 TO NODE 1957.00 IS CODE = 21

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>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1435.00
DOWNSTREAM ELEVATION(FEET) = 1405.00
ELEVATION DIFFERENCE(FEET) = 30.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972
SUBAREA RUNOFF(CFS) = 0.50
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.50

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*****
FLOW PROCESS FROM NODE 1957.00 TO NODE 1956.00 IS CODE = 51

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>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1405.00 DOWNSTREAM(FEET) = 1275.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1125.00 CHANNEL SLOPE = 0.1156
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.139
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.17
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.99
AVERAGE FLOW DEPTH(FEET) = 0.25 TRAVEL TIME(MIN.) = 3.13
Tc(MIN.) = 9.40

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 SUBAREA AREA(ACRES) = 4.29 SUBAREA RUNOFF(CFS) = 9.22  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
 TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 9.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.35 FLOW VELOCITY(FEET/SEC.) = 7.32  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1956.00 = 1225.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1956.00 TO NODE 1969.00 IS CODE = 31

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 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1269.00 DOWNSTREAM(FEET) = 1264.00  
 FLOW LENGTH(FEET) = 165.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.07  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 9.60  
 PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 9.67  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1969.00 = 1390.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1969.00 TO NODE 1969.00 IS CODE = 1

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 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.67  
 RAINFALL INTENSITY(INCH/HR) = 6.03  
 TOTAL STREAM AREA(ACRES) = 4.47  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.60

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 13.98        | 8.23      | 6.688                 | 7.61        |
| 2             | 11.88        | 8.01      | 6.803                 | 4.99        |
| 3             | 9.60         | 9.67      | 6.027                 | 4.47        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 33.45        | 8.01      | 6.803                 |
| 2             | 33.83        | 8.23      | 6.688                 |
| 3             | 32.72        | 9.67      | 6.027                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 33.83 Tc(MIN.) = 8.23  
 TOTAL AREA(ACRES) = 17.1  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1969.00 = 1390.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1969.00 TO NODE 1963.50 IS CODE = 31

-----  
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<



>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1261.50
FLOW LENGTH(FEET) = 155.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.63
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 33.83
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 8.47
LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1963.50 = 1545.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1963.50 TO NODE 1963.50 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 33.83 8.47 6.563 17.07
LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1963.50 = 1545.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 5.13 8.94 6.339 3.32
LONGEST FLOWPATH FROM NODE 1968.00 TO NODE 1963.50 = 871.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 38.69 8.47 6.563
2 37.80 8.94 6.339

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 38.69 Tc(MIN.) = 8.47
TOTAL AREA(ACRES) = 20.4

\*\*\*\*\*
FLOW PROCESS FROM NODE 1963.50 TO NODE 1963.50 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*
FLOW PROCESS FROM NODE 1963.00 TO NODE 1959.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1261.50 DOWNSTREAM(FEET) = 1179.00
FLOW LENGTH(FEET) = 829.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.98
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 38.69
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 9.10
LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1959.00 = 2374.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1959.00 TO NODE 1959.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.10
RAINFALL INTENSITY(INCH/HR) = 6.27
TOTAL STREAM AREA(ACRES) = 20.39
PEAK FLOW RATE(CFS) AT CONFLUENCE = 38.69

\*\*\*\*\*

FLOW PROCESS FROM NODE 1962.00 TO NODE 1961.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 1250.00
DOWNSTREAM ELEVATION(FEET) = 1240.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.166
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 1961.00 TO NODE 1960.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1240.00 DOWNSTREAM(FEET) = 1190.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 490.00 CHANNEL SLOPE = 0.1020
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6200
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.60
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.05
AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 1.62
Tc(MIN.) = 4.78
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 6.86
AREA-AVERAGE RUNOFF COEFFICIENT = 0.620
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 7.04

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 FLOW VELOCITY(FEET/SEC.) = 6.32
LONGEST FLOWPATH FROM NODE 1962.00 TO NODE 1960.00 = 555.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1960.00 TO NODE 1959.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1184.00 DOWNSTREAM(FEET) = 1179.00
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013

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ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.41  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.04  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 4.81  
LONGEST FLOWPATH FROM NODE 1962.00 TO NODE 1959.00 = 580.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1959.00 TO NODE 1959.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.81  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.23  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.04

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1959.60 TO NODE 1959.40 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1370.00  
DOWNSTREAM ELEVATION(FEET) = 1326.00  
ELEVATION DIFFERENCE(FEET) = 44.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.59  
TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1959.40 TO NODE 1959.20 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1326.00 DOWNSTREAM(FEET) = 1190.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1185.00 CHANNEL SLOPE = 0.1148  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.869  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.55  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.19  
AVERAGE FLOW DEPTH(FEET) = 0.20 TRAVEL TIME(MIN.) = 3.81  
Tc(MIN.) = 10.07  
SUBAREA AREA(ACRES) = 2.83 SUBAREA RUNOFF(CFS) = 5.81  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 6.24

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 FLOW VELOCITY(FEET/SEC.) = 6.33  
LONGEST FLOWPATH FROM NODE 1959.60 TO NODE 1959.20 = 1285.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1959.00 TO NODE 1959.00 IS CODE = 1

-----  
 >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.07  
 RAINFALL INTENSITY(INCH/HR) = 5.87  
 TOTAL STREAM AREA(ACRES) = 3.04  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.24

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 38.69        | 9.10      | 6.267                 | 20.39       |
| 2             | 7.04         | 4.81      | 9.222                 | 1.23        |
| 3             | 6.24         | 10.07     | 5.869                 | 3.04        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 30.45        | 4.81      | 9.222                 |
| 2             | 49.11        | 9.10      | 6.267                 |
| 3             | 46.95        | 10.07     | 5.869                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 49.11 Tc(MIN.) = 9.10  
 TOTAL AREA(ACRES) = 24.7  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1959.00 = 2374.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1959.00 TO NODE 1924.00 IS CODE = 31

-----  
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1179.00 DOWNSTREAM(FEET) = 1176.00  
 FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 17.55  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 49.11  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 9.16  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1924.00 = 2439.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1924.00 TO NODE 1924.00 IS CODE = 10

-----  
 >>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1993.00 TO NODE 1992.00 IS CODE = 21

-----  
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 194.00  
 UPSTREAM ELEVATION(FEET) = 1276.00  
 DOWNSTREAM ELEVATION(FEET) = 1273.00  
 ELEVATION DIFFERENCE(FEET) = 3.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.988  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
           THE MAXIMUM OVERLAND FLOW LENGTH = 73.20  
           (Reference: Table 3-1B of Hydrology Manual)  
           THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.902  
 SUBAREA RUNOFF(CFS) = 0.14  
 TOTAL AREA(ACRES) = 0.07      TOTAL RUNOFF(CFS) = 0.14

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1992.00 TO NODE 1933.00 IS CODE = 51

-----  
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1273.00    DOWNSTREAM(FEET) = 1267.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 255.00    CHANNEL SLOPE = 0.0235  
 CHANNEL BASE(FEET) = 3.00    "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030    MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.015

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.42  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.48  
 AVERAGE FLOW DEPTH(FEET) = 0.09    TRAVEL TIME(MIN.) = 2.87  
 Tc(MIN.) = 12.86  
 SUBAREA AREA(ACRES) = 0.31      SUBAREA RUNOFF(CFS) = 0.54  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
 TOTAL AREA(ACRES) = 0.4      PEAK FLOW RATE(CFS) = 0.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.12    FLOW VELOCITY(FEET/SEC.) = 1.73  
 LONGEST FLOWPATH FROM NODE 1993.00 TO NODE 1933.00 = 449.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1933.00 TO NODE 1933.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.86  
 RAINFALL INTENSITY(INCH/HR) = 5.01  
 TOTAL STREAM AREA(ACRES) = 0.38  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.67

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1935.00 TO NODE 1934.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
 UPSTREAM ELEVATION(FEET) = 1235.00

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DOWNSTREAM ELEVATION(FEET) = 1234.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.296  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.787  
SUBAREA RUNOFF(CFS) = 0.34  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1934.00 TO NODE 1933.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1234.00 DOWNSTREAM(FEET) = 1233.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 165.00 CHANNEL SLOPE = 0.0061  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.048  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3300  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.68  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.13  
AVERAGE FLOW DEPTH(FEET) = 0.18 TRAVEL TIME(MIN.) = 2.43  
Tc(MIN.) = 12.73  
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.67  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.330  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 0.97

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 1.29  
LONGEST FLOWPATH FROM NODE 1935.00 TO NODE 1933.00 = 235.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1933.00 TO NODE 1933.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.73  
RAINFALL INTENSITY(INCH/HR) = 5.05  
TOTAL STREAM AREA(ACRES) = 0.58  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.97

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 0.67         | 12.86     | 5.015                 | 0.38        |
| 2             | 0.97         | 12.73     | 5.048                 | 0.58        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 1.63         | 12.73     | 5.048                 |
| 2             | 1.63         | 12.86     | 5.015                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 1.63 Tc(MIN.) = 12.86

TOTAL AREA(ACRES) = 1.0  
LONGEST FLOWPATH FROM NODE 1993.00 TO NODE 1933.00 = 449.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1933.00 TO NODE 1932.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1227.00 DOWNSTREAM(FEET) = 1226.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.76  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.63  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 12.97  
LONGEST FLOWPATH FROM NODE 1993.00 TO NODE 1932.00 = 489.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1932.00 TO NODE 1925.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1226.00 DOWNSTREAM(FEET) = 1194.00  
FLOW LENGTH(FEET) = 490.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.07  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.63  
PIPE TRAVEL TIME(MIN.) = 1.01 Tc(MIN.) = 13.98  
LONGEST FLOWPATH FROM NODE 1993.00 TO NODE 1925.00 = 979.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1925.00 TO NODE 1925.00 IS CODE = 10

-----  
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1931.00 TO NODE 1930.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1280.00  
DOWNSTREAM ELEVATION(FEET) = 1258.00  
ELEVATION DIFFERENCE(FEET) = 22.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.73  
TOTAL AREA(ACRES) = 0.26 TOTAL RUNOFF(CFS) = 0.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1930.00 TO NODE 1929.00 IS CODE = 51

-----  
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1258.00 DOWNSTREAM(FEET) = 1214.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 200.00 CHANNEL SLOPE = 0.2200
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.611
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3100
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.73
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.14
AVERAGE FLOW DEPTH(FEET) = 0.20 TRAVEL TIME(MIN.) = 0.47
Tc(MIN.) = 6.73
SUBAREA AREA(ACRES) = 3.39 SUBAREA RUNOFF(CFS) = 8.00
AREA-AVERAGE RUNOFF COEFFICIENT = 0.313
TOTAL AREA(ACRES) = 3.7 PEAK FLOW RATE(CFS) = 8.69

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.28 FLOW VELOCITY(FEET/SEC.) = 8.81
LONGEST FLOWPATH FROM NODE 1931.00 TO NODE 1929.00 = 300.00 FEET.

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*****
FLOW PROCESS FROM NODE 1929.00 TO NODE 1926.00 IS CODE = 31

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```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1208.00 DOWNSTREAM(FEET) = 1207.00
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.39
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.69
PIPE TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 7.23
LONGEST FLOWPATH FROM NODE 1931.00 TO NODE 1926.00 = 460.00 FEET.

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*****
FLOW PROCESS FROM NODE 1926.00 TO NODE 1926.00 IS CODE = 1

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```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 7.23
RAINFALL INTENSITY(INCH/HR) = 7.27
TOTAL STREAM AREA(ACRES) = 3.65
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.69

```

```

*****
FLOW PROCESS FROM NODE 1928.00 TO NODE 1927.00 IS CODE = 21

```

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5800
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1223.00
DOWNSTREAM ELEVATION(FEET) = 1221.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.169
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.053

```



SUBAREA RUNOFF(CFS) = 0.51  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.51

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1927.00 TO NODE 1926.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1221.00 DOWNSTREAM(FEET) = 1216.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 260.00 CHANNEL SLOPE = 0.0192  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.062

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.42  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.11  
 AVERAGE FLOW DEPTH(FEET) = 0.38 TRAVEL TIME(MIN.) = 1.39  
 Tc(MIN.) = 7.56  
 SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 7.78  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.580  
 TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 8.23

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.54 FLOW VELOCITY(FEET/SEC.) = 3.76  
 LONGEST FLOWPATH FROM NODE 1928.00 TO NODE 1926.00 = 340.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1926.00 TO NODE 1926.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.56  
 RAINFALL INTENSITY(INCH/HR) = 7.06  
 TOTAL STREAM AREA(ACRES) = 2.01  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.23

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.69         | 7.23      | 7.271                 | 3.65        |
| 2             | 8.23         | 7.56      | 7.062                 | 2.01        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.56        | 7.23      | 7.271                 |
| 2             | 16.67        | 7.56      | 7.062                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 16.67 Tc(MIN.) = 7.56  
 TOTAL AREA(ACRES) = 5.7  
 LONGEST FLOWPATH FROM NODE 1931.00 TO NODE 1926.00 = 460.00 FEET.

FLOW PROCESS FROM NODE 1926.00 TO NODE 1925.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1210.00 DOWNSTREAM(FEET) = 1196.00
FLOW LENGTH(FEET) = 195.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.94
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 16.67
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 7.77
LONGEST FLOWPATH FROM NODE 1931.00 TO NODE 1925.00 = 655.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1925.00 TO NODE 1925.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 16.67 7.77 6.942 5.66
LONGEST FLOWPATH FROM NODE 1931.00 TO NODE 1925.00 = 655.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 1.63 13.98 4.750 0.96
LONGEST FLOWPATH FROM NODE 1993.00 TO NODE 1925.00 = 979.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 17.58 7.77 6.942
2 13.04 13.98 4.750

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 17.58 Tc(MIN.) = 7.77
TOTAL AREA(ACRES) = 6.6

\*\*\*\*\*

FLOW PROCESS FROM NODE 1925.00 TO NODE 1925.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1925.00 TO NODE 1924.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1196.00 DOWNSTREAM(FEET) = 1178.00
FLOW LENGTH(FEET) = 285.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.34
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 17.58
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 8.08
LONGEST FLOWPATH FROM NODE 1993.00 TO NODE 1924.00 = 1264.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1924.00 TO NODE 1924.00 IS CODE = 11

-----  
>>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 17.58        | 8.08      | 6.769                 | 6.62        |

LONGEST FLOWPATH FROM NODE 1993.00 TO NODE 1924.00 = 1264.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 49.11        | 9.16      | 6.240                 | 24.66       |

LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1924.00 = 2439.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 60.87        | 8.08      | 6.769                 |
| 2             | 65.31        | 9.16      | 6.240                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 65.31 Tc(MIN.) = 9.16  
TOTAL AREA(ACRES) = 31.3

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1924.00 TO NODE 1924.00 IS CODE = 12

-----  
>>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1924.00 TO NODE 1912.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1178.00 DOWNSTREAM(FEET) = 1087.40  
 FLOW LENGTH(FEET) = 690.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 27.73  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 65.31  
 PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 9.58  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1912.00 = 3129.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1912.00 TO NODE 1912.00 IS CODE = 10

-----  
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1921.50 TO NODE 1921.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1201.00  
DOWNSTREAM ELEVATION(FEET) = 1200.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.685  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.650  
SUBAREA RUNOFF(CFS) = 0.11  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1921.00 TO NODE 1920.00 IS CODE = 51

-----  
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1200.00 DOWNSTREAM(FEET) = 1195.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 475.00 CHANNEL SLOPE = 0.0105  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.185  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.55  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.25  
AVERAGE FLOW DEPTH(FEET) = 0.13 TRAVEL TIME(MIN.) = 6.33  
Tc(MIN.) = 17.02  
SUBAREA AREA(ACRES) = 0.82 SUBAREA RUNOFF(CFS) = 0.86  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 0.94

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.19 FLOW VELOCITY(FEET/SEC.) = 1.50  
LONGEST FLOWPATH FROM NODE 1921.50 TO NODE 1920.00 = 540.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1920.00 TO NODE 1917.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1189.00 DOWNSTREAM(FEET) = 1183.00  
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.81  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.94  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 17.06  
LONGEST FLOWPATH FROM NODE 1921.50 TO NODE 1917.00 = 565.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1917.00 TO NODE 1917.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.06  
RAINFALL INTENSITY(INCH/HR) = 4.18  
TOTAL STREAM AREA(ACRES) = 0.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.94

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1919.00 TO NODE 1918.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1200.00  
DOWNSTREAM ELEVATION(FEET) = 1198.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.169  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.053  
SUBAREA RUNOFF(CFS) = 0.51  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.51

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1918.00 TO NODE 1917.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1198.00 DOWNSTREAM ELEVATION(FEET) = 1189.00  
STREET LENGTH(FEET) = 545.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.37  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.24  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.77  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86  
STREET FLOW TRAVEL TIME(MIN.) = 3.28 Tc(MIN.) = 9.45  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.116

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.580  
SUBAREA AREA(ACRES) = 2.71 SUBAREA RUNOFF(CFS) = 9.61  
TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 10.00

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.03  
FLOW VELOCITY(FEET/SEC.) = 3.19 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.17  
LONGEST FLOWPATH FROM NODE 1919.00 TO NODE 1917.00 = 625.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1917.00 TO NODE 1917.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.45  
RAINFALL INTENSITY(INCH/HR) = 6.12  
TOTAL STREAM AREA(ACRES) = 2.82  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.00

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 0.94         | 17.06     | 4.179                 | 0.90        |
| 2             | 10.00        | 9.45      | 6.116                 | 2.82        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 10.52        | 9.45      | 6.116                 |
| 2             | 7.78         | 17.06     | 4.179                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.52 Tc(MIN.) = 9.45  
TOTAL AREA(ACRES) = 3.7  
LONGEST FLOWPATH FROM NODE 1919.00 TO NODE 1917.00 = 625.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1917.00 TO NODE 1914.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1189.00 DOWNSTREAM(FEET) = 1173.00  
FLOW LENGTH(FEET) = 215.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.40  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.52  
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 9.70  
LONGEST FLOWPATH FROM NODE 1919.00 TO NODE 1914.00 = 840.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1914.00 TO NODE 1914.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.70  
RAINFALL INTENSITY(INCH/HR) = 6.01  
TOTAL STREAM AREA(ACRES) = 3.72  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.52

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1916.00 TO NODE 1915.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

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UPSTREAM ELEVATION(FEET) = 1193.00  
DOWNSTREAM ELEVATION(FEET) = 1189.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.650  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.523  
SUBAREA RUNOFF(CFS) = 1.14  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 1.14

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1915.00 TO NODE 1914.00 IS CODE = 62

-----  
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1189.00 DOWNSTREAM ELEVATION(FEET) = 1179.00  
STREET LENGTH(FEET) = 780.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.58  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 10.66  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.62  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.89  
STREET FLOW TRAVEL TIME(MIN.) = 4.96 Tc(MIN.) = 10.61  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.677

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.580  
SUBAREA AREA(ACRES) = 3.23 SUBAREA RUNOFF(CFS) = 10.64  
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 11.39

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.34  
FLOW VELOCITY(FEET/SEC.) = 3.00 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.18  
LONGEST FLOWPATH FROM NODE 1916.00 TO NODE 1914.00 = 875.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1914.00 TO NODE 1914.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.61  
RAINFALL INTENSITY(INCH/HR) = 5.68  
TOTAL STREAM AREA(ACRES) = 3.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.39

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

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|---|-------|-------|-----------|------|
| 1 | 10.52 | 9.70  | 6.014     | 3.72 |
| 2 | 11.39 | 10.61 | 5.677     | 3.46 |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 20.94        | 9.70      | 6.014                 |
| 2             | 21.33        | 10.61     | 5.677                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 21.33 Tc(MIN.) = 10.61  
 TOTAL AREA(ACRES) = 7.2  
 LONGEST FLOWPATH FROM NODE 1916.00 TO NODE 1914.00 = 875.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1914.00 TO NODE 1913.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1173.00 DOWNSTREAM(FEET) = 1089.00  
 FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 38.35  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 21.33  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 10.66  
 LONGEST FLOWPATH FROM NODE 1916.00 TO NODE 1913.00 = 1005.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1913.00 TO NODE 1913.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.66  
 RAINFALL INTENSITY(INCH/HR) = 5.66  
 TOTAL STREAM AREA(ACRES) = 7.18  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.33

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1923.00 TO NODE 1922.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
 UPSTREAM ELEVATION(FEET) = 1180.00  
 DOWNSTREAM ELEVATION(FEET) = 1168.00  
 ELEVATION DIFFERENCE(FEET) = 12.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.738  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.608  
 SUBAREA RUNOFF(CFS) = 0.11  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.11



\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1922.00 TO NODE 1913.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1168.00 DOWNSTREAM(FEET) = 1095.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 675.00 CHANNEL SLOPE = 0.1081  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.539

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.59  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.63  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 4.28  
 Tc(MIN.) = 11.02  
 SUBAREA AREA(ACRES) = 0.67 SUBAREA RUNOFF(CFS) = 0.93  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
 TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 1.01

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 3.29  
 LONGEST FLOWPATH FROM NODE 1923.00 TO NODE 1913.00 = 765.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1913.00 TO NODE 1913.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.02  
 RAINFALL INTENSITY(INCH/HR) = 5.54  
 TOTAL STREAM AREA(ACRES) = 0.73  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.01

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 21.33        | 10.66     | 5.658                 | 7.18        |
| 2             | 1.01         | 11.02     | 5.539                 | 0.73        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 22.31        | 10.66     | 5.658                 |
| 2             | 21.89        | 11.02     | 5.539                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 22.31 Tc(MIN.) = 10.66  
 TOTAL AREA(ACRES) = 7.9  
 LONGEST FLOWPATH FROM NODE 1916.00 TO NODE 1913.00 = 1005.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1913.00 TO NODE 1912.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1089.00 DOWNSTREAM(FEET) = 1087.40
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.13
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 22.31
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 10.99
LONGEST FLOWPATH FROM NODE 1916.00 TO NODE 1912.00 = 1165.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1912.00 TO NODE 1912.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 22.31 10.99 5.548 7.91
LONGEST FLOWPATH FROM NODE 1916.00 TO NODE 1912.00 = 1165.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 65.31 9.58 6.064 31.28
LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1912.00 = 3129.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 84.75 9.58 6.064
2 82.06 10.99 5.548

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 84.75 Tc(MIN.) = 9.58
TOTAL AREA(ACRES) = 39.2

\*\*\*\*\*
FLOW PROCESS FROM NODE 1912.00 TO NODE 1912.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*
FLOW PROCESS FROM NODE 1912.00 TO NODE 1911.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1087.40 DOWNSTREAM(FEET) = 1079.00
FLOW LENGTH(FEET) = 220.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 33.0 INCH PIPE IS 23.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.58
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 84.75
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 9.77
LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1911.00 = 3349.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1911.00 TO NODE 1911.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.77
RAINFALL INTENSITY(INCH/HR) = 5.99
TOTAL STREAM AREA(ACRES) = 39.19
PEAK FLOW RATE(CFS) AT CONFLUENCE = 84.75

\*\*\*\*\*
FLOW PROCESS FROM NODE 1911.40 TO NODE 1911.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00
UPSTREAM ELEVATION(FEET) = 1150.00
DOWNSTREAM ELEVATION(FEET) = 1140.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.593
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.579
SUBAREA RUNOFF(CFS) = 0.21
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.21

\*\*\*\*\*
FLOW PROCESS FROM NODE 1911.20 TO NODE 1911.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1140.00 DOWNSTREAM(FEET) = 1085.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 250.00 CHANNEL SLOPE = 0.2200
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.591
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.71
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.57
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 1.17
Tc(MIN.) = 6.76
SUBAREA AREA(ACRES) = 0.53 SUBAREA RUNOFF(CFS) = 1.01
AREA-AVERAGE RUNOFF COEFFICIENT = 0.257
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.19

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 4.31
LONGEST FLOWPATH FROM NODE 1911.40 TO NODE 1911.00 = 320.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 1911.00 TO NODE 1911.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.76
RAINFALL INTENSITY(INCH/HR) = 7.59

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TOTAL STREAM AREA(ACRES) = 0.61  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.19

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 84.75        | 9.77      | 5.985                 | 39.19       |
| 2             | 1.19         | 6.76      | 7.591                 | 0.61        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 59.81        | 6.76      | 7.591                 |
| 2             | 85.68        | 9.77      | 5.985                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 85.68 Tc(MIN.) = 9.77  
TOTAL AREA(ACRES) = 39.8  
LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1911.00 = 3349.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1911.00 TO NODE 1907.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1079.00 DOWNSTREAM(FEET) = 1069.30  
FLOW LENGTH(FEET) = 585.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 27.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.65  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 85.68  
PIPE TRAVEL TIME(MIN.) = 0.71 Tc(MIN.) = 10.49  
LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1907.00 = 3934.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1907.00 TO NODE 1907.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.49  
RAINFALL INTENSITY(INCH/HR) = 5.72  
TOTAL STREAM AREA(ACRES) = 39.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 85.68

\*\*\*\*\*

FLOW PROCESS FROM NODE 1910.00 TO NODE 1909.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00  
UPSTREAM ELEVATION(FEET) = 1090.00  
DOWNSTREAM ELEVATION(FEET) = 1079.40  
ELEVATION DIFFERENCE(FEET) = 10.60  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.366

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.48

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 1909.00 TO NODE 1908.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1079.40 DOWNSTREAM(FEET) = 1075.80

CHANNEL LENGTH THRU SUBAREA(FEET) = 360.00 CHANNEL SLOPE = 0.0100

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6100

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.32

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.69

AVERAGE FLOW DEPTH(FEET) = 0.96 TRAVEL TIME(MIN.) = 1.63

Tc(MIN.) = 4.99

SUBAREA AREA(ACRES) = 6.00 SUBAREA RUNOFF(CFS) = 33.75

AREA-AVERAGE RUNOFF COEFFICIENT = 0.610

TOTAL AREA(ACRES) = 6.1 PEAK FLOW RATE(CFS) = 34.23

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.35 FLOW VELOCITY(FEET/SEC.) = 4.46

LONGEST FLOWPATH FROM NODE 1910.00 TO NODE 1908.00 = 420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1908.00 TO NODE 1907.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1070.00 DOWNSTREAM(FEET) = 1069.30

FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 8.94

ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 34.23

PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 5.12

LONGEST FLOWPATH FROM NODE 1910.00 TO NODE 1907.00 = 490.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1907.00 TO NODE 1907.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 5.12

RAINFALL INTENSITY(INCH/HR) = 9.08

TOTAL STREAM AREA(ACRES) = 6.09

PEAK FLOW RATE(CFS) AT CONFLUENCE = 34.23

\*\* CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 85.68 | 10.49  | 5.719       | 39.80  |
| 2      | 34.23 | 5.12   | 9.077       | 6.09   |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 88.21        | 5.12      | 9.077                 |
| 2             | 107.25       | 10.49     | 5.719                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 107.25 Tc(MIN.) = 10.49  
 TOTAL AREA(ACRES) = 45.9  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1907.00 = 3934.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1907.00 TO NODE 1906.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1069.30 DOWNSTREAM(FEET) = 1063.70  
 FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 26.45  
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 107.25  
 PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 10.53  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1906.00 = 3999.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1906.00 TO NODE 1906.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 107.25       | 10.53     | 5.704                 | 45.89       |

LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1906.00 = 3999.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 96.66        | 11.39     | 5.424                 | 27.98       |

LONGEST FLOWPATH FROM NODE 2025.00 TO NODE 1906.00 = 3740.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 196.64       | 10.53     | 5.704                 |
| 2             | 198.63       | 11.39     | 5.424                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 198.63 Tc(MIN.) = 11.39  
 TOTAL AREA(ACRES) = 73.9

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1906.00 TO NODE 1906.00 IS CODE = 12

=====  
 >>>>>CLEAR MEMORY BANK # 1 <<<<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1906.00 TO NODE 1907.00 IS CODE = 7  
 -----

>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<<  
 =====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
 TC(MIN) = 11.39 RAIN INTENSITY(INCH/HOUR) = 5.42  
 TOTAL AREA(ACRES) = 73.90 TOTAL RUNOFF(CFS) = 50.00

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1906.00 TO NODE 1905.00 IS CODE = 31  
 -----

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1063.70 DOWNSTREAM(FEET) = 1010.00  
 FLOW LENGTH(FEET) = 115.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 42.11  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 50.00  
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 11.44  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1905.00 = 4114.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1905.00 TO NODE 1901.00 IS CODE = 51  
 -----

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 1010.00 DOWNSTREAM(FEET) = 950.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 815.00 CHANNEL SLOPE = 0.0736  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.063  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 67.02  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.03  
 AVERAGE FLOW DEPTH(FEET) = 1.15 TRAVEL TIME(MIN.) = 1.23  
 Tc(MIN.) = 12.67  
 SUBAREA AREA(ACRES) = 21.06 SUBAREA RUNOFF(CFS) = 34.12  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.168  
 TOTAL AREA(ACRES) = 95.0 PEAK FLOW RATE(CFS) = 80.81

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 1.26 FLOW VELOCITY(FEET/SEC.) = 11.60  
 LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 1901.00 = 4929.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1901.00 TO NODE 1901.00 IS CODE = 7  
 -----

>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<<  
 =====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
 TC(MIN) = 12.66 RAIN INTENSITY(INCH/HOUR) = 5.06  
 TOTAL AREA(ACRES) = 95.00 TOTAL RUNOFF(CFS) = 74.00

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\*\*\*\*\*

FLOW PROCESS FROM NODE 1901.00 TO NODE 19.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

|  |               |                    |        |
|--|---------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 950.00        | DOWNSTREAM(FEET) = | 930.00 |
| FLOW LENGTH(FEET) =                                | 441.00        | MANNING'S N =      | 0.013  |
| DEPTH OF FLOW IN 60.0 INCH PIPE IS                 | 15.2 INCHES   |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 18.92         |                    |        |
| GIVEN PIPE DIAMETER(INCH) =                        | 60.00         | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 74.00         |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.39          | Tc(MIN.) =         | 13.05  |
| LONGEST FLOWPATH FROM NODE 1958.00 TO NODE 19.00 = | 5370.00 FEET. |                    |        |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 95.0 TC(MIN.) = 13.05  
PEAK FLOW RATE(CFS) = 74.00

-----  
END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* PROPOSED HYDROLOGY - NEULAND SIERRA \*
  - \* SUBBASIN 20 \*
  - \* POST DETENTION AT NODE 2003 WITH 24" OUTLET 12" ABOVE GROUND \*
- \*\*\*\*\*

FILE NAME: P-20D.DAT  
TIME/DATE OF STUDY: 16:35 01/12/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020                                       | 0.50                   | 1.50                                | 0.0313      | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2014.00 TO NODE 2013.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1110.00

DOWNSTREAM ELEVATION(FEET) = 1105.00

ELEVATION DIFFERENCE(FEET) = 5.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.158

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.96

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.96

\*\*\*\*\*

FLOW PROCESS FROM NODE 2013.00 TO NODE 2012.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1105.00 DOWNSTREAM ELEVATION(FEET) = 1077.00

STREET LENGTH(FEET) = 550.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.46

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.24

HALFSTREET FLOOD WIDTH(FEET) = 5.65

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.95

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.95

STREET FLOW TRAVEL TIME(MIN.) = 2.32 Tc(MIN.) = 5.48

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.696

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8100

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.808  
SUBAREA AREA(ACRES) = 0.71 SUBAREA RUNOFF(CFS) = 5.00  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 5.91

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.44  
FLOW VELOCITY(FEET/SEC.) = 4.39 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.21  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 2012.00 = 650.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2012.00 TO NODE 2005.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1071.00 DOWNSTREAM(FEET) = 1059.00  
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.83  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.91  
PIPE TRAVEL TIME(MIN.) = 0.51 Tc(MIN.) = 5.99  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 2005.00 = 950.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2005.00 TO NODE 2005.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2009.00 TO NODE 2008.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1090.00  
DOWNSTREAM ELEVATION(FEET) = 1088.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.834  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 80.00  
(Reference: Table 3-1B of Hydrology Manual)

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THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 3.02

TOTAL AREA(ACRES) = 0.41 TOTAL RUNOFF(CFS) = 3.02

\*\*\*\*\*

FLOW PROCESS FROM NODE 2008.00 TO NODE 2007.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1088.00 DOWNSTREAM(FEET) = 1082.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.0100  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.02  
FLOW VELOCITY(FEET/SEC) = 1.88 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.32 Tc(MIN.) = 9.15  
LONGEST FLOWPATH FROM NODE 2009.00 TO NODE 2007.00 = 700.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2008.00 TO NODE 2007.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.245  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8094  
SUBAREA AREA(ACRES) = 6.20 SUBAREA RUNOFF(CFS) = 31.36  
TOTAL AREA(ACRES) = 6.6 TOTAL RUNOFF(CFS) = 33.41  
TC(MIN.) = 9.15

\*\*\*\*\*

FLOW PROCESS FROM NODE 2007.00 TO NODE 2006.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1076.00 DOWNSTREAM(FEET) = 1051.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 39.35  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 33.41  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 9.17  
LONGEST FLOWPATH FROM NODE 2009.00 TO NODE 2006.00 = 750.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2006.00 TO NODE 2006.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.17  
RAINFALL INTENSITY(INCH/HR) = 6.24  
TOTAL STREAM AREA(ACRES) = 6.61  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 33.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2011.00 TO NODE 2010.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1078.00  
DOWNSTREAM ELEVATION(FEET) = 1077.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.063  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.51  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.51

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2010.00 TO NODE 2006.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1077.00 DOWNSTREAM ELEVATION(FEET) = 1057.00  
STREET LENGTH(FEET) = 350.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.98  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.92  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.26  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.04  
STREET FLOW TRAVEL TIME(MIN.) = 1.37 Tc(MIN.) = 5.43  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.740  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.820  
SUBAREA AREA(ACRES) = 0.69 SUBAREA RUNOFF(CFS) = 4.94  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 6.38

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.51  
FLOW VELOCITY(FEET/SEC.) = 4.68 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.29  
LONGEST FLOWPATH FROM NODE 2011.00 TO NODE 2006.00 = 450.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2006.00 TO NODE 2006.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.43  
RAINFALL INTENSITY(INCH/HR) = 8.74  
TOTAL STREAM AREA(ACRES) = 0.89  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.38

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 33.41        | 9.17      | 6.236                 | 6.61        |
| 2             | 6.38         | 5.43      | 8.740                 | 0.89        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

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\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 26.18        | 5.43      | 8.740                 |
| 2             | 37.96        | 9.17      | 6.236                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 37.96 Tc(MIN.) = 9.17  
TOTAL AREA(ACRES) = 7.5  
LONGEST FLOWPATH FROM NODE 2009.00 TO NODE 2006.00 = 750.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2006.00 TO NODE 2005.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1051.00 DOWNSTREAM(FEET) = 1049.00  
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.25  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 37.96  
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 9.35  
LONGEST FLOWPATH FROM NODE 2009.00 TO NODE 2005.00 = 870.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2005.00 TO NODE 2005.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 37.96        | 9.35      | 6.159                 | 7.50        |

LONGEST FLOWPATH FROM NODE 2009.00 TO NODE 2005.00 = 870.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 5.91         | 5.99      | 8.212                 | 0.84        |

LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 2005.00 = 950.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 30.21        | 5.99      | 8.212                 |



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6.159

2 42.39 9.35

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 42.39 Tc(MIN.) = 9.35  
TOTAL AREA(ACRES) = 8.3

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2005.00 TO NODE 2004.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1049.00 DOWNSTREAM(FEET) = 1045.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.57  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 42.39  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 9.46  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 2004.00 = 1050.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2004.00 TO NODE 2003.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1045.00 DOWNSTREAM(FEET) = 1042.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 150.00 CHANNEL SLOPE = 0.0200  
CHANNEL FLOW THRU SUBAREA(CFS) = 42.39  
FLOW VELOCITY(FEET/SEC) = 5.22 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 9.93  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 2003.00 = 1200.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2004.00 TO NODE 2003.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.922  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7394  
SUBAREA AREA(ACRES) = 1.52 SUBAREA RUNOFF(CFS) = 3.15  
TOTAL AREA(ACRES) = 9.9 TOTAL RUNOFF(CFS) = 43.18  
TC(MIN.) = 9.93

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2003.00 TO NODE 2003.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 9.93 RAIN INTENSITY(INCH/HOUR) = 5.92  
TOTAL AREA(ACRES) = 9.90 TOTAL RUNOFF(CFS) = 11.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2003.00 TO NODE 2000.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1042.00 DOWNSTREAM(FEET) = 1000.00  
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.58  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.00  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 10.04  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 2000.50 = 1350.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.50 TO NODE 2000.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1000.00 DOWNSTREAM(FEET) = 985.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 90.00 CHANNEL SLOPE = 0.1667  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1433 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 11.00  
FLOW VELOCITY(FEET/SEC) = 4.71 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 10.35  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 2000.00 = 1440.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.50 TO NODE 2000.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.766  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2211  
SUBAREA AREA(ACRES) = 2.58 SUBAREA RUNOFF(CFS) = 5.21  
TOTAL AREA(ACRES) = 12.5 TOTAL RUNOFF(CFS) = 15.91  
TC(MIN.) = 10.35

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.00 TO NODE 20.20 IS CODE = 41  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 986.50 DOWNSTREAM(FEET) = 969.10  
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 11.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.15  
GIVEN PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.91  
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 10.90  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 20.20 = 1740.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 20.20 TO NODE 20.10 IS CODE = 41  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 968.60 DOWNSTREAM(FEET) = 958.00  
FLOW LENGTH(FEET) = 532.00 MANNING'S N = 0.024  
DEPTH OF FLOW IN 42.0 INCH PIPE IS 13.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.07  
GIVEN PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.91  
PIPE TRAVEL TIME(MIN.) = 1.46 Tc(MIN.) = 12.36  
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 20.10 = 2272.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 20.10 TO NODE 20.10 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.36  
RAINFALL INTENSITY(INCH/HR) = 5.14  
TOTAL STREAM AREA(ACRES) = 12.48  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.91

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2002.40 TO NODE 2002.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00  
UPSTREAM ELEVATION(FEET) = 1035.00  
DOWNSTREAM ELEVATION(FEET) = 1025.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.431  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.16  
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2002.20 TO NODE 2002.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1025.00 DOWNSTREAM(FEET) = 973.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.1300  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1217 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.16  
FLOW VELOCITY(FEET/SEC) = 1.95 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.41 Tc(MIN.) = 7.84  
LONGEST FLOWPATH FROM NODE 2002.40 TO NODE 2002.00 = 450.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2002.20 TO NODE 2002.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.897  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.16 SUBAREA RUNOFF(CFS) = 2.80  
TOTAL AREA(ACRES) = 1.2 TOTAL RUNOFF(CFS) = 2.92  
TC(MIN.) = 7.84

\*\*\*\*\*

FLOW PROCESS FROM NODE 2002.00 TO NODE 20.10 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 966.90 DOWNSTREAM(FEET) = 958.80
FLOW LENGTH(FEET) = 198.00 MANNING'S N = 0.024
DEPTH OF FLOW IN 24.0 INCH PIPE IS 5.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.10
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.92
PIPE TRAVEL TIME(MIN.) = 0.65 Tc(MIN.) = 8.49
LONGEST FLOWPATH FROM NODE 2002.40 TO NODE 20.10 = 648.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 20.10 TO NODE 20.10 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.49
RAINFALL INTENSITY(INCH/HR) = 6.55
TOTAL STREAM AREA(ACRES) = 1.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.92

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 18.21 Tc(MIN.) = 12.36
TOTAL AREA(ACRES) = 13.7
LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 20.10 = 2272.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 20.10 TO NODE 20.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

|  |               |                    |        |
|--|---------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 957.00        | DOWNSTREAM(FEET) = | 944.80 |
| FLOW LENGTH(FEET) =                                | 200.00        | MANNING'S N =      | 0.024  |
| DEPTH OF FLOW IN 42.0 INCH PIPE IS                 | 10.7 INCHES   |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 9.41          |                    |        |
| GIVEN PIPE DIAMETER(INCH) =                        | 42.00         | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 18.21         |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.35          | Tc(MIN.) =         | 12.72  |
| LONGEST FLOWPATH FROM NODE 2014.00 TO NODE 20.00 = | 2472.00 FEET. |                    |        |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 13.7 TC(MIN.) = 12.72  
PEAK FLOW RATE(CFS) = 18.21

-----  
END OF RATIONAL METHOD ANALYSIS





| Node to Node |        | Code | Elev 1<br>(feet)                      | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|---------------------------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                                       |                  |                  |             |               |                | 1    | 2 | 3 |
| 2145         | 2144   | 2    | 1055                                  | 1050             | 90               | 0.35        | 0.12          |                |      |   |   |
| 2144         | 2143   | 5    | 1050                                  | 1045             | 250              |             |               |                |      |   |   |
| 2144         | 2143   | 8    |                                       |                  |                  | 0.3         | 0.79          |                |      |   |   |
| 2143         | 2126.9 | 3    | 1039                                  | 1017             | 775              |             |               |                |      |   |   |
| 2126.9       | 2126.9 | 1    |                                       |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2129         | 2128   | 2    | 1042                                  | 1040             | 80               | 0.81        | 0.17          |                |      |   |   |
| 2128         | 2127   | 5    | 1040                                  | 1027             | 575              |             |               |                |      |   |   |
| 2128         | 2127   | 8    |                                       |                  |                  | 0.81        | 5.35          |                |      |   |   |
| 2127         | 2127   | 7    | Tc=7.5 mins A = 5.5 acres Q = 1.8 cfs |                  |                  |             |               |                |      |   |   |
| 2127         | 2126.9 | 3    | 1021                                  | 1017             | 45               |             |               |                |      |   |   |
| 2126.9       | 2126.9 | 1    |                                       |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2126.9       | 2126.5 | 3    | 1017                                  | 1014             | 235              |             |               |                |      |   |   |
| 2126.5       | 2126.5 | 1    |                                       |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2126.8       | 2126.7 | 2    | 1030                                  | 1028             | 85               | 0.81        | 0.18          |                |      |   |   |
| 2126.7       | 2126.6 | 5    | 1028                                  | 1025             | 260              |             |               |                |      |   |   |
| 2126.7       | 2126.6 | 8    |                                       |                  |                  | 0.81        | 1.05          |                |      |   |   |
| 2126.6       | 2126.5 | 3    | 1019                                  | 1014             | 50               |             |               |                |      |   |   |
| 2126.5       | 2126.5 | 1    |                                       |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2126.5       | 2101   | 3    | 1014                                  | 979              | 1120             |             |               |                |      |   |   |
| 2101         | 2101   | 10   |                                       |                  |                  |             |               | save to bank 1 |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2134         | 2133   | 2    | 1055                                  | 1050             | 100              | 0.9         | 0.12          |                |      |   |   |
| 2133         | 2132   | 6    | 1050                                  | 1040             | 215              | 0.9         | 0.57          | 2 sides        |      |   |   |
| 2132         | 2149   | 3    | 1034                                  | 1017             | 735              |             |               |                |      |   |   |
| 2149         | 2149   | 1    |                                       |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2131         | 2130   | 2    | 1055                                  | 1050             | 80               | 0.9         | 0.15          |                |      |   |   |
| 2130         | 2149   | 6    | 1050                                  | 1023             | 510              | 0.47        | 2.65          | 2 sides        |      |   |   |
| 2149         | 2149   | 1    |                                       |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2149         | 2146   | 3    | 1017                                  | 1013             | 75               |             |               |                |      |   |   |
| 2146         | 2146   | 1    |                                       |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2147.4       | 2147.2 | 2    | 1035                                  | 1031             | 95               | 0.9         | 0.13          |                |      |   |   |
| 2147.2       | 2147   | 6    | 1031                                  | 1020             | 270              | 0.9         | 0.34          | 2 sides        |      |   |   |
| 2147         | 2146   | 3    | 1014                                  | 1013             | 40               |             |               |                |      |   |   |
| 2146         | 2146   | 1    |                                       |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                                       |                  |                  |             |               |                |      |   |   |
| 2146         | 2125   | 3    | 1013                                  | 1006             | 233              |             |               |                |      |   |   |
| 2125         | 2125   | 1    |                                       |                  |                  |             |               | 1 OF 2         |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet)                         | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments    | BANK |   |   |
|--------------|--------|------|--|------------------|------------------|-------------|---------------|-------------|------|---|---|
|              |        |      |  |                  |                  |             |               |             | 1    | 2 | 3 |
| 2151         | 2150   | 2    | 1023                                     | 1022             | 65               | 0.81        | 0.17          |             |      |   |   |
| 2150         | 2125   | 6    | 1022                                     | 1012             | 260              | 0.9         | 1.00          |             |      |   |   |
| 2125         | 2125   | 1    |  |                  |                  |             |               | 2 OF 2      |      |   |   |
| 2125         | 2123.6 | 3    | 1006                                     | 1004             | 460              |             |               |             |      |   |   |
| 2123.6       | 2123.6 | 1    |  |                  |                  |             |               | 1 of 3      |      |   |   |
| 2137.5       | 2137   | 2    | 1043                                     | 1040             | 95               | 0.9         | 0.22          |             |      |   |   |
| 2137         | 2123.6 | 6    | 1040                                     | 1010             | 680              | 0.9         | 1.74          | 2 Sides     |      |   |   |
| 2123.6       | 2123.6 | 1    |  |                  |                  |             |               | 2 of 3      |      |   |   |
| 2122         | 2121   | 2    | 1013                                     | 1012             | 68               | 0.81        | 0.13          |             |      |   |   |
| 2121         | 2123.6 | 5    | 1012                                     | 1010             | 311              | 0.81        | 2.14          |             |      |   |   |
| 2123.6       | 2123.6 | 1    |  |                  |                  |             |               | 3 of 3      |      |   |   |
| 2123.6       | 2118.6 | 3    | 1004                                     | 995              | 108              |             |               |             |      |   |   |
| 2118.6       | 2118.8 | 5    | 995                                      | 994.8            | 65               | 0.3         | 1.64          |             |      |   |   |
| 2118.8       | 2118.7 | 3    | 994.8                                    | 994.5            | 305              |             |               |             |      |   |   |
| 2118.7       | 2118.5 | 5    | 994.5                                    | 994              | 195              | 0.3         | 1.00          |             |      |   |   |
| 2118.6       | 2118.6 | 7    | Tc = 8.82 mins A = 12 acres Q = 12.7 Cfs |                  |                  |             |               |             |      |   |   |
| 2118.5       | 2118.4 | 3    | 994                                      | 989              | 37               |             |               |             |      |   |   |
| 2118.4       | 2118.4 | 10   |  |                  |                  |             |               | SAVE BANK 2 |      |   |   |
| 2142         | 2141   | 2    | 1110                                     | 1101             | 100              | 0.9         | 0.19          |             |      |   |   |
| 2141         | 2137   | 6    | 1101                                     | 1060             | 425              | 0.9         | 0.86          | one side    |      |   |   |
| 2137         | 2138   | 3    | 1054                                     | 1037             | 630              |             |               |             |      |   |   |
| 2138         | 2138   | 1    |  |                  |                  |             |               | 1 OF 2      |      |   |   |
| 2140         | 2139   | 2    | 1060                                     | 1055             | 100              | 0.9         | 0.21          |             |      |   |   |
| 2139         | 2138   | 6    | 1055                                     | 1043             | 550              | 0.9         | 0.67          | one side    |      |   |   |
| 2138         | 2138   | 1    |  |                  |                  |             |               | 2 OF 2      |      |   |   |
| 2138         | 2136   | 3    | 1037                                     | 1030             | 230              |             |               |             |      |   |   |
| 2136         | 2136   | 7    | Tc = 5.10 mins A = 1.93 acres Q = 2cfs   |                  |                  |             |               |             |      |   |   |
| 2136         | 2107.5 | 5    | 1030                                     | 1029.5           | 141              | 0.25        | *             |             |      |   |   |
| 2107.5       | 2107.5 | 1    |  |                  |                  |             |               | 1 of 2      |      |   |   |
| 2109         | 2108   | 2    | 1075                                     | 1071             | 80               | 0.25        | 0.11          |             |      |   |   |
| 2108         | 2107   | 5    | 1071                                     | 1055             | 108              | 0.25        | 0.43          |             |      |   |   |
| 2107         | 2107.5 | 3    | 1055                                     | 1029.5           | 170              |             |               |             |      |   |   |
| 2107.5       | 2107.5 | 1    |  |                  |                  |             |               | 2 of 2      |      |   |   |
| 2107.5       | 2106.5 | 3    | 1029.5                                   | 1029             | 88               |             |               |             |      |   |   |
| 2106.5       | 2106.5 | 10   |  |                  |                  |             |               | Save Bank 3 |      |   |   |





| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments     | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|--------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |              | 1    | 2 | 3 |
| 2116         | 2115   | 2    | 1175             | 1160             | 100              | 0.25        | 0.06          |              |      |   |   |
| 2115         | 2114   | 5    | 1160             | 1070             | 650              | 0.25        | 2.98          |              |      |   |   |
| 2114         | 2110   | 3    | 1064             | 1038             | 490              |             |               |              |      |   |   |
| 2110         | 2110   | 1    |                  |                  |                  |             |               | 1 of 2       |      |   |   |
| 2113         | 2112   | 2    | 1070             | 1060             | 100              | 0.25        | 0.10          |              |      |   |   |
| 2112         | 2111   | 5    | 1060             | 1045             | 370              | 0.25        | 2.81          |              |      |   |   |
| 2111         | 2110   | 3    | 1039             | 1038             | 40               |             |               |              |      |   |   |
| 2110         | 2110   | 1    |                  |                  |                  |             |               | 2 of 2       |      |   |   |
| 2110         | 2106.5 | 3    | 1038             | 1029             | 530              |             |               |              |      |   |   |
| 2106.5       | 2106.5 | 11   |                  |                  |                  |             |               | Add Bank 3   |      |   |   |
| 2106.5       | 2106.5 | 12   |                  |                  |                  |             |               | Clear Bank 3 |      |   |   |
| 2106.5       | 2104   | 3    | 1029             | 1020             | 170              |             |               |              |      |   |   |
| 2104         | 2104   | 1    |                  |                  |                  |             |               | 1 of 2       |      |   |   |
| 2106         | 2105   | 2    | 1037             | 1035             | 80               | 0.25        | 0.12          |              |      |   |   |
| 2105         | 2104   | 5    | 1035             | 1025             | 310              | 0.25        | 1.77          |              |      |   |   |
| 2104         | 2104   | 1    |                  |                  |                  |             |               | 2 of 2       |      |   |   |
| 2104         | 2103   | 3    | 1025             | 1015             | 27               |             |               |              |      |   |   |
| 2103         | 2103   | 1    |                  |                  |                  |             |               | 1 of 2       |      |   |   |
| 2103.4       | 2103.2 | 2    | 1240             | 1215             | 100              | 0.35        | 0.13          |              |      |   |   |
| 2103.2       | 2103   | 5    | 1215             | 1018             | 870              | 0.29        | 4.45          |              |      |   |   |
| 2103         | 2103   | 1    |                  |                  |                  |             |               | 2 of 2       |      |   |   |
| 2103         | 2118.4 | 3    | 1012             | 989              | 205              |             |               |              |      |   |   |
| 2118.4       | 2118.4 | 11   |                  |                  |                  |             |               | Add Bank 2   |      |   |   |
| 2118.4       | 2118.4 | 12   |                  |                  |                  |             |               | Clear Bank 2 |      |   |   |
| 2118.4       | 2102   | 3    | 989              | 984              | 50               |             |               |              |      |   |   |
| 2102         | 2102   | 1    |                  |                  |                  |             |               | 1 of 2       |      |   |   |
| 2101.9       | 2101.8 | 2    | 1020             | 1010             | 90               | 0.25        | 0.16          |              |      |   |   |
| 2101.8       | 2102   | 5    | 1010             | 990              | 477              | 0.25        | 1.04          |              |      |   |   |
| 2102         | 2102   | 1    |                  |                  |                  |             |               | 2 of 2       |      |   |   |
| 2102         | 2101   | 3    | 984              | 977              | 50               |             |               |              |      |   |   |
| 2101         | 2101   | 11   |                  |                  |                  |             |               | Add Bank 1   |      |   |   |
| 2101         | 2101   | 12   |                  |                  |                  |             |               | Clear Bank 1 |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* PROPOSED HYDROLOGY \*  
\* SUB BASIN 21 \*  
\* WITH DETENTION \*  
\*\*\*\*\*

FILE NAME: P-21D.DAT  
TIME/DATE OF STUDY: 15:06 01/26/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0312                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2145.00 TO NODE 2144.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1055.00  
DOWNSTREAM ELEVATION(FEET) = 1050.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.232  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.268  
SUBAREA RUNOFF(CFS) = 0.31  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.31

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2144.00 TO NODE 2143.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1050.00 DOWNSTREAM(FEET) = 1045.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 250.00 CHANNEL SLOPE = 0.0200  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0200 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.31  
FLOW VELOCITY(FEET/SEC) = 0.79 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.26 Tc(MIN.) = 12.49  
LONGEST FLOWPATH FROM NODE 2145.00 TO NODE 2143.00 = 340.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2144.00 TO NODE 2143.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.109  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3066  
SUBAREA AREA(ACRES) = 0.79 SUBAREA RUNOFF(CFS) = 1.21  
TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 1.43  
TC(MIN.) = 12.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2143.00 TO NODE 2126.90 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1039.00 DOWNSTREAM(FEET) = 1017.00  
FLOW LENGTH(FEET) = 775.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.79  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.43  
PIPE TRAVEL TIME(MIN.) = 2.23 Tc(MIN.) = 14.73  
LONGEST FLOWPATH FROM NODE 2145.00 TO NODE 2126.90 = 1115.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2126.90 TO NODE 2126.90 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.73  
RAINFALL INTENSITY(INCH/HR) = 4.59  
TOTAL STREAM AREA(ACRES) = 0.91  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.43

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2129.00 TO NODE 2128.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1042.00  
DOWNSTREAM ELEVATION(FEET) = 1040.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.440  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.27  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 1.27

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2128.00 TO NODE 2127.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |  |              |
|-------------------------------------|---------|--|--------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1040.00 | DOWNSTREAM(FEET) =                     | 1027.00      |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 575.00  | CHANNEL SLOPE =                        | 0.0226       |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 1.27    |  |              |
| FLOW VELOCITY(FEET/SEC) =           | 2.36    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |              |
| TRAVEL TIME(MIN.) =                 | 4.06    | Tc(MIN.) =                             | 7.50         |
| LONGEST FLOWPATH FROM NODE          | 2129.00 | TO NODE                                | 2127.00 =    |
|                                     |         |  | 655.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2128.00 TO NODE 2127.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |        |                       |       |
|--|--------|-----------------------|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 7.100  |                       |       |
| *USER SPECIFIED(SUBAREA):                |        |                       |       |
| USER-SPECIFIED RUNOFF COEFFICIENT =      | .8100  |                       |       |
| S.C.S. CURVE NUMBER (AMC II) =           | 0      |                       |       |
| AREA-AVERAGE RUNOFF COEFFICIENT =        | 0.8100 |                       |       |
| SUBAREA AREA(ACRES) =                    | 5.35   | SUBAREA RUNOFF(CFS) = | 30.77 |
| TOTAL AREA(ACRES) =                      | 5.5    | TOTAL RUNOFF(CFS) =   | 31.75 |
| TC(MIN.) =                               | 7.50   |                       |       |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2127.00 TO NODE 2127.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

|                                       |      |                             |      |
|---------------------------------------|------|-----------------------------|------|
| USER-SPECIFIED VALUES ARE AS FOLLOWS: |      |                             |      |
| TC(MIN) =                             | 7.50 | RAIN INTENSITY(INCH/HOUR) = | 7.10 |
| TOTAL AREA(ACRES) =                   | 5.50 | TOTAL RUNOFF(CFS) =         | 1.80 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2127.00 TO NODE 2126.90 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |         |                    |         |
|--|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =           | 1021.00 | DOWNSTREAM(FEET) = | 1017.00 |
| FLOW LENGTH(FEET) =                        | 45.00   | MANNING'S N =      | 0.013   |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO | 18.000  |                    |         |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS         | 3.0     | INCHES             |         |
| PIPE-FLOW VELOCITY(FEET/SEC.) =            | 9.29    |                    |         |
| ESTIMATED PIPE DIAMETER(INCH) =            | 18.00   | NUMBER OF PIPES =  | 1       |
| PIPE-FLOW(CFS) =                           | 1.80    |                    |         |
| PIPE TRAVEL TIME(MIN.) =                   | 0.08    | Tc(MIN.) =         | 7.58    |

LONGEST FLOWPATH FROM NODE 2129.00 TO NODE 2126.90 = 700.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2126.90 TO NODE 2126.90 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.58
RAINFALL INTENSITY(INCH/HR) = 7.05
TOTAL STREAM AREA(ACRES) = 5.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.80

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.60 Tc(MIN.) = 14.73
TOTAL AREA(ACRES) = 6.4
LONGEST FLOWPATH FROM NODE 2145.00 TO NODE 2126.90 = 1115.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2126.90 TO NODE 2126.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1017.00 DOWNSTREAM(FEET) = 1014.00
FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.18
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.60

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PIPE TRAVEL TIME(MIN.) = 0.76 Tc(MIN.) = 15.48  
LONGEST FLOWPATH FROM NODE 2145.00 TO NODE 2126.50 = 1350.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2126.50 TO NODE 2126.50 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.48  
RAINFALL INTENSITY(INCH/HR) = 4.45  
TOTAL STREAM AREA(ACRES) = 6.41  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.60

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2126.80 TO NODE 2126.70 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1030.00  
DOWNSTREAM ELEVATION(FEET) = 1028.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.618  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.34  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 1.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2126.70 TO NODE 2126.60 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1028.00 DOWNSTREAM(FEET) = 1025.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 260.00 CHANNEL SLOPE = 0.0115  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.34  
FLOW VELOCITY(FEET/SEC) = 1.71 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.54 Tc(MIN.) = 6.16  
LONGEST FLOWPATH FROM NODE 2126.80 TO NODE 2126.60 = 345.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2126.70 TO NODE 2126.60 IS CODE = 81



-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.061  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8100  
SUBAREA AREA(ACRES) = 1.05 SUBAREA RUNOFF(CFS) = 6.86  
TOTAL AREA(ACRES) = 1.2 TOTAL RUNOFF(CFS) = 8.03  
TC(MIN.) = 6.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2126.60 TO NODE 2126.50 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1019.00 DOWNSTREAM(FEET) = 1014.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.90  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.03  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.21  
LONGEST FLOWPATH FROM NODE 2126.80 TO NODE 2126.50 = 395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2126.50 TO NODE 2126.50 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.21  
RAINFALL INTENSITY(INCH/HR) = 8.01  
TOTAL STREAM AREA(ACRES) = 1.23  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.03

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 2.60         | 15.48     | 4.448                 | 6.41        |
| 2             | 8.03         | 6.21      | 8.014                 | 1.23        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 9.47         | 6.21      | 8.014                 |
| 2             | 7.06         | 15.48     | 4.448                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.47 Tc(MIN.) = 6.21  
 TOTAL AREA(ACRES) = 7.6  
 LONGEST FLOWPATH FROM NODE 2145.00 TO NODE 2126.50 = 1350.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2126.50 TO NODE 2101.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1014.00 DOWNSTREAM(FEET) = 979.00  
 FLOW LENGTH(FEET) = 1120.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.15  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 9.47  
 PIPE TRAVEL TIME(MIN.) = 1.84 Tc(MIN.) = 8.05  
 LONGEST FLOWPATH FROM NODE 2145.00 TO NODE 2101.00 = 2470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2101.00 TO NODE 2101.00 IS CODE = 10

-----  
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2134.00 TO NODE 2133.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1055.00  
 DOWNSTREAM ELEVATION(FEET) = 1050.00  
 ELEVATION DIFFERENCE(FEET) = 5.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.105

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.00  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 1.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2133.00 TO NODE 2132.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1050.00 DOWNSTREAM ELEVATION(FEET) = 1040.00  
STREET LENGTH(FEET) = 215.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.36  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.72  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.78  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.91  
STREET FLOW TRAVEL TIME(MIN.) = 0.95 Tc(MIN.) = 3.05  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.57 SUBAREA RUNOFF(CFS) = 4.73  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 5.73

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.51  
FLOW VELOCITY(FEET/SEC.) = 4.20 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.16  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2132.00 = 315.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2132.00 TO NODE 2149.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1034.00 DOWNSTREAM(FEET) = 1017.00  
FLOW LENGTH(FEET) = 735.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.98  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.73  
PIPE TRAVEL TIME(MIN.) = 1.54 Tc(MIN.) = 4.59  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2149.00 = 1050.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2149.00 TO NODE 2149.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.59  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.69  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2131.00 TO NODE 2130.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1055.00  
DOWNSTREAM ELEVATION(FEET) = 1050.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.748  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.24  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 1.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2130.00 TO NODE 2149.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1050.00 DOWNSTREAM ELEVATION(FEET) = 1023.00  
STREET LENGTH(FEET) = 510.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.99  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 7.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.63  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.32  
STREET FLOW TRAVEL TIME(MIN.) = 1.83 Tc(MIN.) = 3.58  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.493  
SUBAREA AREA(ACRES) = 2.65 SUBAREA RUNOFF(CFS) = 11.49  
TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 12.73

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.41  
FLOW VELOCITY(FEET/SEC.) = 5.30 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.77  
LONGEST FLOWPATH FROM NODE 2131.00 TO NODE 2149.00 = 590.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2149.00 TO NODE 2149.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

-----

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.58  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 2.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.73

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 5.73         | 4.59      | 9.222                 | 0.69        |
| 2             | 12.73        | 3.58      | 9.222                 | 2.80        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 17.20        | 3.58      | 9.222                 |
| 2             | 18.46        | 4.59      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 18.46 Tc(MIN.) = 4.59  
TOTAL AREA(ACRES) = 3.5  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2149.00 = 1050.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2149.00 TO NODE 2146.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1017.00 DOWNSTREAM(FEET) = 1013.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.48  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 18.46  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 4.68  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2146.00 = 1125.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2146.00 TO NODE 2146.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.68  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 3.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 2147.40 TO NODE 2147.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 1035.00
DOWNSTREAM ELEVATION(FEET) = 1031.00
ELEVATION DIFFERENCE(FEET) = 4.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.173
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.08
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 1.08

\*\*\*\*\*

FLOW PROCESS FROM NODE 2147.20 TO NODE 2147.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1031.00 DOWNSTREAM ELEVATION(FEET) = 1020.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.49
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.23
HALFSTREET FLOOD WIDTH(FEET) = 4.99
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.39
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.77
STREET FLOW TRAVEL TIME(MIN.) = 1.33 Tc(MIN.) = 3.50
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.34 SUBAREA RUNOFF(CFS) = 2.82  
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 3.90

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 6.45  
FLOW VELOCITY(FEET/SEC.) = 3.65 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.93  
LONGEST FLOWPATH FROM NODE 2147.40 TO NODE 2147.00 = 365.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2147.00 TO NODE 2146.00 IS CODE = 31

-----

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1014.00 DOWNSTREAM(FEET) = 1013.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.40  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.90  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 3.59  
LONGEST FLOWPATH FROM NODE 2147.40 TO NODE 2146.00 = 405.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2146.00 TO NODE 2146.00 IS CODE = 1

-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.59  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.47  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.90

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 18.46        | 4.68      | 9.222                 | 3.49        |
| 2             | 3.90         | 3.59      | 9.222                 | 0.47        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*



| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 22.36        | 3.59      | 9.222                 |
| 2             | 22.36        | 4.68      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 22.36 Tc(MIN.) = 4.68  
TOTAL AREA(ACRES) = 4.0  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2146.00 = 1125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2146.00 TO NODE 2125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1013.00 DOWNSTREAM(FEET) = 1006.00  
FLOW LENGTH(FEET) = 233.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.17  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 22.36  
PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 5.00  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2125.00 = 1358.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2125.00 TO NODE 2125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.00  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 3.96  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 22.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 2151.00 TO NODE 2150.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1023.00  
DOWNSTREAM ELEVATION(FEET) = 1022.00

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ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.646  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.27  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 1.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 2150.00 TO NODE 2125.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1022.00 DOWNSTREAM ELEVATION(FEET) = 1012.00  
STREET LENGTH(FEET) = 260.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.42  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.64  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.86  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.08  
STREET FLOW TRAVEL TIME(MIN.) = 1.12 Tc(MIN.) = 4.77  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.887  
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 8.30  
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 9.57

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.90  
FLOW VELOCITY(FEET/SEC.) = 4.36 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.41  
LONGEST FLOWPATH FROM NODE 2151.00 TO NODE 2125.00 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2125.00 TO NODE 2125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 4.77
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 1.17
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.57

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 31.93 Tc(MIN.) = 5.00
TOTAL AREA(ACRES) = 5.1
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2125.00 = 1358.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2125.00 TO NODE 2123.60 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1006.00 DOWNSTREAM(FEET) = 1004.00
FLOW LENGTH(FEET) = 460.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 33.0 INCH PIPE IS 26.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.34
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 31.93
PIPE TRAVEL TIME(MIN.) = 1.21 Tc(MIN.) = 6.20
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2123.60 = 1818.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2123.60 TO NODE 2123.60 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.20  
RAINFALL INTENSITY(INCH/HR) = 8.02  
TOTAL STREAM AREA(ACRES) = 5.13  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 31.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 2137.50 TO NODE 2137.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1043.00  
DOWNSTREAM ELEVATION(FEET) = 1040.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.392  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.83  
TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 1.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 2137.00 TO NODE 2123.60 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1040.00 DOWNSTREAM ELEVATION(FEET) = 1010.00  
STREET LENGTH(FEET) = 680.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.05  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.31  
 HALFSTREET FLOOD WIDTH(FEET) = 9.37  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.54  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.42  
 STREET FLOW TRAVEL TIME(MIN.) = 2.50 Tc(MIN.) = 4.89  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.74 SUBAREA RUNOFF(CFS) = 14.44  
 TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 16.27

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.03  
 FLOW VELOCITY(FEET/SEC.) = 5.19 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.91  
 LONGEST FLOWPATH FROM NODE 2137.50 TO NODE 2123.60 = 775.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2123.60 TO NODE 2123.60 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 4.89  
 RAINFALL INTENSITY(INCH/HR) = 9.22  
 TOTAL STREAM AREA(ACRES) = 1.96  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.27

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2122.00 TO NODE 2121.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .8100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 68.00  
 UPSTREAM ELEVATION(FEET) = 1013.00  
 DOWNSTREAM ELEVATION(FEET) = 1012.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.785  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.97  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.97

\*\*\*\*\*

FLOW PROCESS FROM NODE 2121.00 TO NODE 2123.60 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1012.00 DOWNSTREAM(FEET) = 1010.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 311.00 CHANNEL SLOPE = 0.0064  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.362

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8100  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.26  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.55  
AVERAGE FLOW DEPTH(FEET) = 0.73 TRAVEL TIME(MIN.) = 2.03  
Tc(MIN.) = 5.82  
SUBAREA AREA(ACRES) = 2.14 SUBAREA RUNOFF(CFS) = 14.49  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.810  
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 15.37

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.00 FLOW VELOCITY(FEET/SEC.) = 3.06  
LONGEST FLOWPATH FROM NODE 2122.00 TO NODE 2123.60 = 379.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2123.60 TO NODE 2123.60 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.82  
RAINFALL INTENSITY(INCH/HR) = 8.36  
TOTAL STREAM AREA(ACRES) = 2.27  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.37

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 31.93        | 6.20      | 8.024                 | 5.13        |
| 2             | 16.27        | 4.89      | 9.222                 | 1.96        |
| 3             | 15.37        | 5.82      | 8.362                 | 2.27        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 56.96        | 4.89      | 9.222                 |
| 2             | 60.76        | 5.82      | 8.362                 |
| 3             | 60.84        | 6.20      | 8.024                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 60.84 Tc(MIN.) = 6.20  
TOTAL AREA(ACRES) = 9.4  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2123.60 = 1818.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2123.60 TO NODE 2118.60 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1004.00 DOWNSTREAM(FEET) = 995.00  
FLOW LENGTH(FEET) = 108.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 22.48  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 60.84  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 6.28  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2118.60 = 1926.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2118.60 TO NODE 2118.80 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 995.00 DOWNSTREAM(FEET) = 994.80  
CHANNEL LENGTH THRU SUBAREA(FEET) = 65.00 CHANNEL SLOPE = 0.0031  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.706  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 62.73  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.37  
AVERAGE FLOW DEPTH(FEET) = 2.39 TRAVEL TIME(MIN.) = 0.32

Tc(MIN.) = 6.60  
SUBAREA AREA(ACRES) = 1.64 SUBAREA RUNOFF(CFS) = 3.79  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.687  
TOTAL AREA(ACRES) = 11.0 PEAK FLOW RATE(CFS) = 60.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 2.36 FLOW VELOCITY(FEET/SEC.) = 3.34  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2118.80 = 1991.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2118.80 TO NODE 2118.70 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 994.80 DOWNSTREAM(FEET) = 994.50  
FLOW LENGTH(FEET) = 305.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 57.0 INCH PIPE IS 42.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.32  
ESTIMATED PIPE DIAMETER(INCH) = 57.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 60.84  
PIPE TRAVEL TIME(MIN.) = 1.18 Tc(MIN.) = 7.78  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2118.70 = 2296.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2118.70 TO NODE 2118.50 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 994.50 DOWNSTREAM(FEET) = 994.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 195.00 CHANNEL SLOPE = 0.0026  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.395  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 61.80  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.14  
AVERAGE FLOW DEPTH(FEET) = 2.48 TRAVEL TIME(MIN.) = 1.04  
Tc(MIN.) = 8.82  
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 1.92  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.655  
TOTAL AREA(ACRES) = 12.0 PEAK FLOW RATE(CFS) = 60.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 2.46 FLOW VELOCITY(FEET/SEC.) = 3.12



LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2118.50 = 2491.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2118.60 TO NODE 2118.60 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 8.82 RAIN INTENSITY(INCH/HOUR) = 6.39
TOTAL AREA(ACRES) = 12.00 TOTAL RUNOFF(CFS) = 12.70

\*\*\*\*\*

FLOW PROCESS FROM NODE 2118.50 TO NODE 2118.40 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 994.00 DOWNSTREAM(FEET) = 989.00
FLOW LENGTH(FEET) = 37.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.85
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.70
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 8.85
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2118.40 = 2528.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2118.40 TO NODE 2118.40 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2142.00 TO NODE 2141.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====
\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1110.00
DOWNSTREAM ELEVATION(FEET) = 1101.00
ELEVATION DIFFERENCE(FEET) = 9.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.731
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.58  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 1.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 2141.00 TO NODE 2137.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1101.00 DOWNSTREAM ELEVATION(FEET) = 1060.00  
STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.15  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.31  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.37  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.86  
STREET FLOW TRAVEL TIME(MIN.) = 1.11 Tc(MIN.) = 2.84  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.86 SUBAREA RUNOFF(CFS) = 7.14  
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 8.71

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.47  
FLOW VELOCITY(FEET/SEC.) = 7.18 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.41  
LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2137.00 = 525.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2137.00 TO NODE 2138.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1054.00 DOWNSTREAM(FEET) = 1037.00  
FLOW LENGTH(FEET) = 630.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.41  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.71  
PIPE TRAVEL TIME(MIN.) = 1.12 Tc(MIN.) = 3.96  
LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2138.00 = 1155.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2138.00 TO NODE 2138.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.96  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.05  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 2140.00 TO NODE 2139.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1060.00  
DOWNSTREAM ELEVATION(FEET) = 1055.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.105  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.74  
TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 1.74

\*\*\*\*\*

FLOW PROCESS FROM NODE 2139.00 TO NODE 2138.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1055.00 DOWNSTREAM ELEVATION(FEET) = 1043.00

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STREET LENGTH(FEET) = 550.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.52  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 10.91  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.46  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.19  
STREET FLOW TRAVEL TIME(MIN.) = 2.65 Tc(MIN.) = 4.76  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.67 SUBAREA RUNOFF(CFS) = 5.56  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 7.30

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.28  
FLOW VELOCITY(FEET/SEC.) = 3.88 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.52  
LONGEST FLOWPATH FROM NODE 2140.00 TO NODE 2138.00 = 650.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2138.00 TO NODE 2138.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.76  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.88  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.30

\*\* CONFLUENCE DATA \*\*

| STREAM | RUNOFF | Tc | INTENSITY | AREA |
|--------|--------|----|-----------|------|
|--------|--------|----|-----------|------|

| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 8.71  | 3.96   | 9.222       | 1.05   |
| 2      | 7.30  | 4.76   | 9.222       | 0.88   |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 14.80        | 3.96      | 9.222                 |
| 2             | 16.02        | 4.76      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.02 Tc(MIN.) = 4.76  
TOTAL AREA(ACRES) = 1.9  
LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2138.00 = 1155.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2138.00 TO NODE 2136.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1037.00 DOWNSTREAM(FEET) = 1030.00  
FLOW LENGTH(FEET) = 230.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.16  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.02  
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 5.10  
LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2136.00 = 1385.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2136.00 TO NODE 2136.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 5.10 RAIN INTENSITY(INCH/HOUR) = 9.10  
TOTAL AREA(ACRES) = 1.93 TOTAL RUNOFF(CFS) = 2.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 2136.00 TO NODE 2107.50 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1030.00 DOWNSTREAM(FEET) = 1029.50  
CHANNEL LENGTH THRU SUBAREA(FEET) = 141.00 CHANNEL SLOPE = 0.0035  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.40  
FLOW VELOCITY(FEET/SEC) = 1.07 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.21 Tc(MIN.) = 7.31  
LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2107.50 = 1526.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2107.50 TO NODE 2107.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.31  
RAINFALL INTENSITY(INCH/HR) = 7.22  
TOTAL STREAM AREA(ACRES) = 1.93  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 2109.00 TO NODE 2108.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1075.00  
DOWNSTREAM ELEVATION(FEET) = 1071.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.003  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.808  
SUBAREA RUNOFF(CFS) = 0.19  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.19

\*\*\*\*\*

FLOW PROCESS FROM NODE 2108.00 TO NODE 2107.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1071.00 DOWNSTREAM(FEET) = 1055.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 108.00 CHANNEL SLOPE = 0.1481  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.493  
\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.54  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.95  
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 0.61  
Tc(MIN.) = 8.61  
SUBAREA AREA(ACRES) = 0.43 SUBAREA RUNOFF(CFS) = 0.70  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 0.88

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 3.42  
LONGEST FLOWPATH FROM NODE 2109.00 TO NODE 2107.00 = 188.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2107.00 TO NODE 2107.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1055.00 DOWNSTREAM(FEET) = 1029.50  
FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.00  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.88  
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 8.93  
LONGEST FLOWPATH FROM NODE 2109.00 TO NODE 2107.50 = 358.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2107.50 TO NODE 2107.50 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.93  
RAINFALL INTENSITY(INCH/HR) = 6.34  
TOTAL STREAM AREA(ACRES) = 0.54  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.88

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 2.40         | 7.31      | 7.220                 | 1.93        |
| 2             | 0.88         | 8.93      | 6.345                 | 0.54        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 3.12         | 7.31      | 7.220                 |
| 2             | 2.99         | 8.93      | 6.345                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.12 Tc(MIN.) = 7.31  
TOTAL AREA(ACRES) = 2.5  
LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2107.50 = 1526.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2107.50 TO NODE 2106.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1029.50 DOWNSTREAM(FEET) = 1029.00  
FLOW LENGTH(FEET) = 88.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.06  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.12  
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 7.67  
LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2106.50 = 1614.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2106.50 TO NODE 2106.50 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2116.00 TO NODE 2115.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1175.00  
DOWNSTREAM ELEVATION(FEET) = 1160.00



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ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.11  
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.11

\*\*\*\*\*

FLOW PROCESS FROM NODE 2115.00 TO NODE 2114.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1160.00 DOWNSTREAM(FEET) = 1070.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 650.00 CHANNEL SLOPE = 0.1385  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.178

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.43  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.92  
AVERAGE FLOW DEPTH(FEET) = 0.15 TRAVEL TIME(MIN.) = 2.20  
Tc(MIN.) = 9.30  
SUBAREA AREA(ACRES) = 2.98 SUBAREA RUNOFF(CFS) = 4.60  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 4.70

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 6.08  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2114.00 = 750.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2114.00 TO NODE 2110.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1064.00 DOWNSTREAM(FEET) = 1038.00  
FLOW LENGTH(FEET) = 490.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.21  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.70  
PIPE TRAVEL TIME(MIN.) = 0.80 Tc(MIN.) = 10.10  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2110.00 = 1240.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2110.00 TO NODE 2110.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.10  
RAINFALL INTENSITY(INCH/HR) = 5.86  
TOTAL STREAM AREA(ACRES) = 3.04  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2113.00 TO NODE 2112.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1070.00  
DOWNSTREAM ELEVATION(FEET) = 1060.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.18  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.18

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2112.00 TO NODE 2111.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1060.00 DOWNSTREAM(FEET) = 1045.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 370.00 CHANNEL SLOPE = 0.0405  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.312  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.42  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.25  
AVERAGE FLOW DEPTH(FEET) = 0.22 TRAVEL TIME(MIN.) = 1.90

Tc(MIN.) = 9.00  
SUBAREA AREA(ACRES) = 2.81 SUBAREA RUNOFF(CFS) = 4.43  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 2.9 PEAK FLOW RATE(CFS) = 4.59

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 FLOW VELOCITY(FEET/SEC.) = 4.01  
LONGEST FLOWPATH FROM NODE 2113.00 TO NODE 2111.00 = 470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2111.00 TO NODE 2110.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1039.00 DOWNSTREAM(FEET) = 1038.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.74  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.59  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 9.09  
LONGEST FLOWPATH FROM NODE 2113.00 TO NODE 2110.00 = 510.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2110.00 TO NODE 2110.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.09  
RAINFALL INTENSITY(INCH/HR) = 6.27  
TOTAL STREAM AREA(ACRES) = 2.91  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.59

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 4.70         | 10.10     | 5.858                 | 3.04        |
| 2             | 4.59         | 9.09      | 6.273                 | 2.91        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 8.81         | 9.09      | 6.273                 |
| 2             | 8.98         | 10.10     | 5.858                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.98 Tc(MIN.) = 10.10  
TOTAL AREA(ACRES) = 5.9  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2110.00 = 1240.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2110.00 TO NODE 2106.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1038.00 DOWNSTREAM(FEET) = 1029.00  
FLOW LENGTH(FEET) = 530.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.93  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.98  
PIPE TRAVEL TIME(MIN.) = 1.11 Tc(MIN.) = 11.22  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2106.50 = 1770.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2106.50 TO NODE 2106.50 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.98         | 11.22     | 5.476                 | 5.95        |

LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2106.50 = 1770.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.12         | 7.67      | 6.999                 | 2.47        |

LONGEST FLOWPATH FROM NODE 2142.00 TO NODE 2106.50 = 1614.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 9.26         | 7.67      | 6.999                 |
| 2             | 11.42        | 11.22     | 5.476                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.42 Tc(MIN.) = 11.22  
TOTAL AREA(ACRES) = 8.4

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2106.50 TO NODE 2106.50 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2106.50 TO NODE 2104.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1029.00 DOWNSTREAM(FEET) = 1020.00  
FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.97  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.42  
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 11.44  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2104.00 = 1940.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2104.00 TO NODE 2104.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.44  
RAINFALL INTENSITY(INCH/HR) = 5.41  
TOTAL STREAM AREA(ACRES) = 8.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2106.00 TO NODE 2105.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

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UPSTREAM ELEVATION(FEET) = 1037.00  
DOWNSTREAM ELEVATION(FEET) = 1035.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.083  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.866  
SUBAREA RUNOFF(CFS) = 0.18  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 2105.00 TO NODE 2104.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1035.00 DOWNSTREAM(FEET) = 1025.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 310.00 CHANNEL SLOPE = 0.0323  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.190

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.33  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.45  
AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 2.11  
Tc(MIN.) = 12.19  
SUBAREA AREA(ACRES) = 1.77 SUBAREA RUNOFF(CFS) = 2.30  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 2.45

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.23 FLOW VELOCITY(FEET/SEC.) = 3.03  
LONGEST FLOWPATH FROM NODE 2106.00 TO NODE 2104.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2104.00 TO NODE 2104.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.19  
RAINFALL INTENSITY(INCH/HR) = 5.19  
TOTAL STREAM AREA(ACRES) = 1.89  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.45

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.42        | 11.44     | 5.408                 | 8.42        |
| 2             | 2.45         | 12.19     | 5.190                 | 1.89        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 13.72        | 11.44     | 5.408                 |
| 2             | 13.41        | 12.19     | 5.190                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.72 Tc(MIN.) = 11.44  
TOTAL AREA(ACRES) = 10.3  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2104.00 = 1940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2104.00 TO NODE 2103.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1025.00 DOWNSTREAM(FEET) = 1015.00  
FLOW LENGTH(FEET) = 27.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 27.74  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 13.72  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 11.45  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2103.00 = 1967.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2103.00 TO NODE 2103.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.45  
RAINFALL INTENSITY(INCH/HR) = 5.40  
TOTAL STREAM AREA(ACRES) = 10.31  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 2103.40 TO NODE 2103.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1240.00
DOWNSTREAM ELEVATION(FEET) = 1215.00
ELEVATION DIFFERENCE(FEET) = 25.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972
SUBAREA RUNOFF(CFS) = 0.36
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.36

```

```

*****
FLOW PROCESS FROM NODE 2103.20 TO NODE 2103.00 IS CODE = 51

```

```

-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1215.00 DOWNSTREAM(FEET) = 1018.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 870.00 CHANNEL SLOPE = 0.2264
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.664
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2900
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.74
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.22
AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 2.01
Tc(MIN.) = 8.27
SUBAREA AREA(ACRES) = 4.45 SUBAREA RUNOFF(CFS) = 8.60
AREA-AVERAGE RUNOFF COEFFICIENT = 0.292
TOTAL AREA(ACRES) = 4.6 PEAK FLOW RATE(CFS) = 8.90

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.28 FLOW VELOCITY(FEET/SEC.) = 8.95
LONGEST FLOWPATH FROM NODE 2103.40 TO NODE 2103.00 = 970.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 2103.00 TO NODE 2103.00 IS CODE = 1

```

```

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```



=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.27  
RAINFALL INTENSITY(INCH/HR) = 6.66  
TOTAL STREAM AREA(ACRES) = 4.58  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.90

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 13.72        | 11.45     | 5.403                 | 10.31       |
| 2             | 8.90         | 8.27      | 6.664                 | 4.58        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 20.03        | 8.27      | 6.664                 |
| 2             | 20.94        | 11.45     | 5.403                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 20.94 Tc(MIN.) = 11.45  
TOTAL AREA(ACRES) = 14.9  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2103.00 = 1967.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2103.00 TO NODE 2118.40 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1012.00 DOWNSTREAM(FEET) = 989.00  
FLOW LENGTH(FEET) = 205.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.95  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.94  
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 11.62  
LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2118.40 = 2172.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2118.40 TO NODE 2118.40 IS CODE = 11

-----

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.94        | 11.62     | 5.352                 | 14.89       |

LONGEST FLOWPATH FROM NODE 2116.00 TO NODE 2118.40 = 2172.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.70        | 8.85      | 6.379                 | 12.00       |

LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2118.40 = 2528.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 28.65        | 8.85      | 6.379                 |
| 2             | 31.59        | 11.62     | 5.352                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 31.59 Tc(MIN.) = 11.62  
TOTAL AREA(ACRES) = 26.9

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2118.40 TO NODE 2118.40 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2118.40 TO NODE 2102.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 989.00 DOWNSTREAM(FEET) = 984.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.15  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 31.59  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 11.66  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2102.00 = 2578.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2102.00 TO NODE 2102.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.66
RAINFALL INTENSITY(INCH/HR) = 5.34
TOTAL STREAM AREA(ACRES) = 26.89
PEAK FLOW RATE(CFS) AT CONFLUENCE = 31.59
```

```
*****
FLOW PROCESS FROM NODE 2101.90 TO NODE 2101.90 IS CODE = 21
```

```
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
```

```
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 1020.00
DOWNSTREAM ELEVATION(FEET) = 1010.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.738
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.608
SUBAREA RUNOFF(CFS) = 0.30
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.30
```

```
*****
FLOW PROCESS FROM NODE 2101.80 TO NODE 2102.00 IS CODE = 51
```

```
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1010.00 DOWNSTREAM(FEET) = 990.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 477.00 CHANNEL SLOPE = 0.0419
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.912
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.08
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.47
AVERAGE FLOW DEPTH(FEET) = 0.13 TRAVEL TIME(MIN.) = 3.22
Tc(MIN.) = 9.96
SUBAREA AREA(ACRES) = 1.04 SUBAREA RUNOFF(CFS) = 1.54
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 1.77
```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.18 FLOW VELOCITY(FEET/SEC.) = 2.96

LONGEST FLOWPATH FROM NODE 2101.90 TO NODE 2102.00 = 567.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2102.00 TO NODE 2102.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.96

RAINFALL INTENSITY(INCH/HR) = 5.91

TOTAL STREAM AREA(ACRES) = 1.20

PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.77

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 31.59        | 11.66     | 5.340                 | 26.89       |
| 2             | 1.77         | 9.96      | 5.912                 | 1.20        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 28.75        | 9.96      | 5.912                 |
| 2             | 33.20        | 11.66     | 5.340                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 33.20 Tc(MIN.) = 11.66

TOTAL AREA(ACRES) = 28.1

LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2102.00 = 2578.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2102.00 TO NODE 2101.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 984.00 DOWNSTREAM(FEET) = 977.00

FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.2 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 23.84

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

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PIPE-FLOW(CFS) = 33.20  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 11.70  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2101.00 = 2628.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2101.00 TO NODE 2101.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 33.20        | 11.70     | 5.330                 | 28.09       |

LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2101.00 = 2628.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.47         | 8.05      | 6.780                 | 7.64        |

LONGEST FLOWPATH FROM NODE 2145.00 TO NODE 2101.00 = 2470.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 32.33        | 8.05      | 6.780                 |
| 2             | 40.64        | 11.70     | 5.330                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 40.64 Tc(MIN.) = 11.70  
TOTAL AREA(ACRES) = 35.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 2101.00 TO NODE 2101.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2101.00 TO NODE 2100.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 977.00 DOWNSTREAM(FEET) = 975.00  
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.17

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ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 40.64  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 11.80  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 2100.00 = 2708.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2100.00 TO NODE 21.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 975.00 DOWNSTREAM(FEET) = 950.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 450.00 CHANNEL SLOPE = 0.0556  
CHANNEL FLOW THRU SUBAREA(CFS) = 40.64  
FLOW VELOCITY(FEET/SEC) = 8.60 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.87 Tc(MIN.) = 12.67  
LONGEST FLOWPATH FROM NODE 2134.00 TO NODE 21.00 = 3158.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 35.7 TC(MIN.) = 12.67  
PEAK FLOW RATE(CFS) = 40.64

=====

END OF RATIONAL METHOD ANALYSIS

↑

# APPENDIX A

AES  
Rational Method Hydrology

Proposed Condition

BASIN B



| Node to Node |     | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments | BANK |   |   |
|--------------|-----|------|------------------|------------------|------------------|-------------|---------------|----------|------|---|---|
|              |     |      |                  |                  |                  |             |               |          | 1    | 2 | 3 |
| 298          | 297 | 2    | 1003.2           | 1001             | 75               | 0.9         | 0.11          |          |      |   |   |
| 297          | 296 | 6    | 1001             | 982.5            | 440              | 0.9         | 0.38          | 1 SIDE   |      |   |   |
| 296          | 292 | 3    | 976.5            | 976              | 35               |             |               |          |      |   |   |
| 292          | 292 | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 295          | 294 | 2    | 1003.2           | 1001             | 75               | 0.9         | 0.10          |          |      |   |   |
| 294          | 293 | 6    | 1001             | 978              | 430              | 0.9         | 0.55          | 1 SIDE   |      |   |   |
| 293          | 292 | 3    | 972              | 971.5            | 40               |             |               |          |      |   |   |
| 292          | 292 | 1    |                  |                  |                  |             |               | 2 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 292          | 288 | 3    | 971.5            | 929              | 595              |             |               |          |      |   |   |
| 288          | 288 | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 291          | 290 | 2    | 994              | 987              | 100              | 0.9         | 0.09          |          |      |   |   |
| 290          | 289 | 6    | 987              | 936              | 680              | 0.9         | 1.36          | 1 SIDE   |      |   |   |
| 289          | 288 | 3    | 930              | 929              | 28               |             |               |          |      |   |   |
| 288          | 288 | 1    |                  |                  |                  |             |               | 2 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 288          | 285 | 3    | 929              | 890              | 595              |             |               |          |      |   |   |
| 285          | 285 | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 287          | 286 | 2    | 947              | 937              | 100              | 0.9         | 0.11          |          |      |   |   |
| 286          | 285 | 6    | 937              | 896              | 585              | 0.9         | 1.26          | 2 SIDES  |      |   |   |
| 285          | 285 | 1    |                  |                  |                  |             |               | 2 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 285          | 281 | 3    | 890              | 851              | 595              |             |               |          |      |   |   |
| 281          | 281 | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 284          | 283 | 2    | 898              | 891              | 90               | 0.9         | 0.16          |          |      |   |   |
| 283          | 282 | 6    | 891              | 857              | 530              | 0.9         | 1.04          | 2 SIDES  |      |   |   |
| 282          | 281 | 3    | 851.5            | 851              | 25               |             |               |          |      |   |   |
| 281          | 281 | 1    |                  |                  |                  |             |               | 2 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 281          | 277 | 3    | 851              | 840              | 250              |             |               |          |      |   |   |
| 277          | 277 | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |
|              |     |      |                  |                  |                  |             |               |          |      |   |   |
| 280          | 279 | 2    | 858              | 853              | 100              | 0.9         | 0.09          |          |      |   |   |
| 279          | 278 | 6    | 853              | 846.6            | 185              | 0.9         | 0.21          | 1 SIDE   |      |   |   |
| 278          | 277 | 3    | 840.5            | 840              | 38               |             |               |          |      |   |   |
| 277          | 277 | 1    |                  |                  |                  |             |               | 2 OF 2   |      |   |   |
| 277          | 275 | 3    | 840              | 837              | 237              |             |               |          |      |   |   |
| 275          | 275 | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |





| Node to Node |      | Code | Elev 1<br>(feet)  | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|-------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                   |                  |                  |             |               |                | 1    | 2 | 3 |
| 280          | 276  | 2    | 858               | 853              | 100              | 0.9         | 0.09          |                |      |   |   |
| 276          | 275  | 6    | 853               | 840.1            | 390              | 0.9         | 0.40          | 1 SIDE         |      |   |   |
| 275          | 275  | 1    |                   |                  |                  |             |               | 2 OF 2         |      |   |   |
| 275          | 274  | 3    | 837               | 836.5            | 20               |             |               |                |      |   |   |
| 274          | 273  | 5    | 836.5             | 835              | 150              |             |               | VALLEY         |      |   |   |
| 274          | 273  | 8    |                   |                  |                  | 0.3         | 0.40          |                |      |   |   |
| 273          | 273  | 7    | Tc=7.4 A=6.4 Q=18 |                  |                  |             |               |                |      |   |   |
| 273          | 272  | 3    | 835               | 834              | 65               |             |               |                |      |   |   |
| 272          | 272  | 10   |                   |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2203         | 2202 | 2    | 1445              | 1405             | 100              | 0.35        | 0.08          |                |      |   |   |
| 2202         | 2201 | 5    | 1405              | 890              | 1382             |             |               | MTN            |      |   |   |
| 2202         | 2201 | 8    |                   |                  |                  | 0.45        | 18.06         |                |      |   |   |
| 2201         | 2200 | 5    | 890               | 835              | 428              |             |               | MTN            |      |   |   |
| 2201         | 2200 | 8    |                   |                  |                  | 0.43        | 2.14          |                |      |   |   |
| 2200         | 2200 | 1    |                   |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2207         | 2206 | 2    | 1295              | 1270             | 100              | 0.35        | 0.15          |                |      |   |   |
| 2206         | 2205 | 5    | 1270              | 1070             | 475              |             |               | MTN            |      |   |   |
| 2206         | 2205 | 8    |                   |                  |                  | 0.46        | 4.44          |                |      |   |   |
| 2205         | 2200 | 5    | 1070              | 840.1            | 930              |             |               | MTN            |      |   |   |
| 2205         | 2200 | 8    |                   |                  |                  | 0.45        | 10.76         |                |      |   |   |
| 2200         | 2200 | 1    |                   |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2200         | 272  | 3    | 840.1             | 834              | 13               |             |               |                |      |   |   |
| 272          | 272  | 11   |                   |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 272          | 22   | 3    | 834               | 820              | 100              |             |               |                |      |   |   |
|              |      |      |                   |                  |                  |             | 41.98         |                |      |   |   |

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* WITH DETENTION AT NODE 273 \*
  - \* SUB-BASIN 22 \*
- \*\*\*\*\*

FILE NAME: P-22D.DAT  
TIME/DATE OF STUDY: 15:13 01/26/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | PARK-<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|-------------------------|--|--------------|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020                                       | 0.50                    | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 298.00 TO NODE 297.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 1003.20

DOWNSTREAM ELEVATION(FEET) = 1001.00

ELEVATION DIFFERENCE(FEET) = 2.20

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.178

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.91

TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 297.00 TO NODE 296.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1001.00 DOWNSTREAM ELEVATION(FEET) = 982.50

STREET LENGTH(FEET) = 440.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.49

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.27

HALFSTREET FLOOD WIDTH(FEET) = 7.21

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.90

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.06

STREET FLOW TRAVEL TIME(MIN.) = 1.88 Tc(MIN.) = 4.06

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.38 SUBAREA RUNOFF(CFS) = 3.15  
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 4.07

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.05  
FLOW VELOCITY(FEET/SEC.) = 4.34 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.33  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 296.00 = 515.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 296.00 TO NODE 292.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 976.50 DOWNSTREAM(FEET) = 976.00  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.10  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.07  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 4.15  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 292.00 = 550.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 292.00 TO NODE 292.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.15  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 295.00 TO NODE 294.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

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UPSTREAM ELEVATION(FEET) = 1003.20  
DOWNSTREAM ELEVATION(FEET) = 1001.00  
ELEVATION DIFFERENCE(FEET) = 2.20  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.178  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.00 TO NODE 293.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1001.00 DOWNSTREAM ELEVATION(FEET) = 978.00  
STREET LENGTH(FEET) = 430.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.11  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.55  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.52  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.25  
STREET FLOW TRAVEL TIME(MIN.) = 1.58 Tc(MIN.) = 3.76  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.55 SUBAREA RUNOFF(CFS) = 4.56  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 5.39

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.67  
FLOW VELOCITY(FEET/SEC.) = 5.12 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.64  
LONGEST FLOWPATH FROM NODE 295.00 TO NODE 293.00 = 505.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 293.00 TO NODE 292.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 972.00 DOWNSTREAM(FEET) = 971.50
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.25
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.39
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 3.87
LONGEST FLOWPATH FROM NODE 295.00 TO NODE 292.00 = 545.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 292.00 TO NODE 292.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.87
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.65
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.39

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 9.46 Tc(MIN.) = 4.15
TOTAL AREA(ACRES) = 1.1

LONGEST FLOWPATH FROM NODE 298.00 TO NODE 292.00 = 550.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 292.00 TO NODE 288.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 971.50 DOWNSTREAM(FEET) = 929.00
FLOW LENGTH(FEET) = 595.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.79
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.46
PIPE TRAVEL TIME(MIN.) = 0.72 Tc(MIN.) = 4.87
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 288.00 = 1145.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 288.00 TO NODE 288.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.87
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 1.14
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 291.00 TO NODE 290.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 994.00
DOWNSTREAM ELEVATION(FEET) = 987.00
ELEVATION DIFFERENCE(FEET) = 7.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.882
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.75
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 290.00 TO NODE 289.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 987.00 DOWNSTREAM ELEVATION(FEET) = 936.00
STREET LENGTH(FEET) = 680.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.39
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 9.67
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.07
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.94
STREET FLOW TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 3.75
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 1.36 SUBAREA RUNOFF(CFS) = 11.29
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 12.03

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.61
FLOW VELOCITY(FEET/SEC.) = 7.05 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.67
LONGEST FLOWPATH FROM NODE 291.00 TO NODE 289.00 = 780.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 289.00 TO NODE 288.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 930.00 DOWNSTREAM(FEET) = 929.00
FLOW LENGTH(FEET) = 28.00 MANNING'S N = 0.013



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DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.30  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.03  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 3.79  
LONGEST FLOWPATH FROM NODE 291.00 TO NODE 288.00 = 808.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 288.00 TO NODE 288.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.79  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.45  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.03

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.46         | 4.87      | 9.222                 | 1.14        |
| 2             | 12.03        | 3.79      | 9.222                 | 1.45        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 21.50        | 3.79      | 9.222                 |
| 2             | 21.50        | 4.87      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 21.50 Tc(MIN.) = 4.87  
TOTAL AREA(ACRES) = 2.6  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 288.00 = 1145.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 288.00 TO NODE 285.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 929.00 DOWNSTREAM(FEET) = 890.00  
FLOW LENGTH(FEET) = 595.00 MANNING'S N = 0.013

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DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.18  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 21.50  
PIPE TRAVEL TIME(MIN.) = 0.61 Tc(MIN.) = 5.48  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 285.00 = 1740.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 285.00 TO NODE 285.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.48  
RAINFALL INTENSITY(INCH/HR) = 8.69  
TOTAL STREAM AREA(ACRES) = 2.59  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 287.00 TO NODE 286.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 947.00  
DOWNSTREAM ELEVATION(FEET) = 937.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.671  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.91  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 286.00 TO NODE 285.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 937.00 DOWNSTREAM ELEVATION(FEET) = 896.00  
STREET LENGTH(FEET) = 585.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.14  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.00  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.05  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.34  
STREET FLOW TRAVEL TIME(MIN.) = 1.93 Tc(MIN.) = 3.60  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.26 SUBAREA RUNOFF(CFS) = 10.46  
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 11.37

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.33  
FLOW VELOCITY(FEET/SEC.) = 5.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.80  
LONGEST FLOWPATH FROM NODE 287.00 TO NODE 285.00 = 685.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 285.00 TO NODE 285.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.60  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.37  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.37

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 21.50        | 5.48      | 8.688                 | 2.59        |
| 2             | 11.37        | 3.60      | 9.222                 | 1.37        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 31.62        | 3.60      | 9.222                 |
| 2             | 32.21        | 5.48      | 8.688                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 32.21 Tc(MIN.) = 5.48  
TOTAL AREA(ACRES) = 4.0  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 285.00 = 1740.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 285.00 TO NODE 281.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 890.00 DOWNSTREAM(FEET) = 851.00  
FLOW LENGTH(FEET) = 595.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.92  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 32.21  
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 6.04  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 281.00 = 2335.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 281.00 TO NODE 281.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.04  
RAINFALL INTENSITY(INCH/HR) = 8.17  
TOTAL STREAM AREA(ACRES) = 3.96  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 32.21

\*\*\*\*\*  
FLOW PROCESS FROM NODE 284.00 TO NODE 283.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
 UPSTREAM ELEVATION(FEET) = 898.00  
 DOWNSTREAM ELEVATION(FEET) = 891.00  
 ELEVATION DIFFERENCE(FEET) = 7.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.724  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.33  
 TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 1.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 283.00 TO NODE 282.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 891.00 DOWNSTREAM ELEVATION(FEET) = 857.00  
 STREET LENGTH(FEET) = 530.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.64  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.26  
 HALFSTREET FLOOD WIDTH(FEET) = 6.87  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.79  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.26  
 STREET FLOW TRAVEL TIME(MIN.) = 1.85 Tc(MIN.) = 3.57  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.04 SUBAREA RUNOFF(CFS) = 8.63  
 TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 9.96

END OF SUBAREA STREET FLOW HYDRAULICS:

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DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.99  
FLOW VELOCITY(FEET/SEC.) = 5.38 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.65  
LONGEST FLOWPATH FROM NODE 284.00 TO NODE 282.00 = 620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 282.00 TO NODE 281.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 851.50 DOWNSTREAM(FEET) = 851.00  
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.64  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.96  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 3.62  
LONGEST FLOWPATH FROM NODE 284.00 TO NODE 281.00 = 645.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 281.00 TO NODE 281.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.62  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.20  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.96

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 32.21        | 6.04      | 8.166                 | 3.96        |
| 2             | 9.96         | 3.62      | 9.222                 | 1.20        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 38.48        | 3.62      | 9.222                 |
| 2             | 41.03        | 6.04      | 8.166                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

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PEAK FLOW RATE(CFS) = 41.03 Tc(MIN.) = 6.04  
TOTAL AREA(ACRES) = 5.2  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 281.00 = 2335.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 281.00 TO NODE 277.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 851.00 DOWNSTREAM(FEET) = 840.00  
FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.24  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 41.03  
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 6.29  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 277.00 = 2585.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 277.00 TO NODE 277.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.29  
RAINFALL INTENSITY(INCH/HR) = 7.95  
TOTAL STREAM AREA(ACRES) = 5.16  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.03

\*\*\*\*\*

FLOW PROCESS FROM NODE 280.00 TO NODE 279.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 858.00  
DOWNSTREAM ELEVATION(FEET) = 853.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.105  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 279.00 TO NODE 278.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

|                            |        |                              |        |
|----------------------------|--------|------------------------------|--------|
| UPSTREAM ELEVATION(FEET) = | 853.00 | DOWNSTREAM ELEVATION(FEET) = | 846.60 |
| STREET LENGTH(FEET) =      | 185.00 | CURB HEIGHT(INCHES) =        | 6.0    |
| STREET HALFWIDTH(FEET) =   | 39.00  |                              |        |

|   |       |
|---|-------|
| DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = | 20.00 |
| INSIDE STREET CROSSFALL(DECIMAL) =                  | 0.020 |
| OUTSIDE STREET CROSSFALL(DECIMAL) =                 | 0.020 |

|  |        |
|--|--------|
| SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =                  | 1      |
| STREET PARKWAY CROSSFALL(DECIMAL) =                                | 0.020  |
| Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = | 0.0150 |
| Manning's FRICTION FACTOR for Back-of-Walk Flow Section =          | 0.0150 |

|   |       |            |      |
|---|-------|------------|------|
| **TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =  | 1.62  |            |      |
| STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:      |       |            |      |
| STREET FLOW DEPTH(FEET) =                           | 0.25  |            |      |
| HALFSTREET FLOOD WIDTH(FEET) =                      | 6.05  |            |      |
| AVERAGE FLOW VELOCITY(FEET/SEC.) =                  | 3.35  |            |      |
| PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =             | 0.83  |            |      |
| STREET FLOW TRAVEL TIME(MIN.) =                     | 0.92  | Tc(MIN.) = | 3.03 |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =            | 9.222 |            |      |
| NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE. |       |            |      |

\*USER SPECIFIED(SUBAREA):

|                                     |       |                       |      |
|-------------------------------------|-------|-----------------------|------|
| USER-SPECIFIED RUNOFF COEFFICIENT = | .9000 |                       |      |
| S.C.S. CURVE NUMBER (AMC II) =      | 0     |                       |      |
| AREA-AVERAGE RUNOFF COEFFICIENT =   | 0.900 |                       |      |
| SUBAREA AREA(ACRES) =               | 0.21  | SUBAREA RUNOFF(CFS) = | 1.74 |
| TOTAL AREA(ACRES) =                 | 0.3   | PEAK FLOW RATE(CFS) = | 2.49 |

END OF SUBAREA STREET FLOW HYDRAULICS:

|                            |        |                                |          |              |
|----------------------------|--------|--------------------------------|----------|--------------|
| DEPTH(FEET) =              | 0.28   | HALFSTREET FLOOD WIDTH(FEET) = | 7.55     |              |
| FLOW VELOCITY(FEET/SEC.) = | 3.62   | DEPTH*VELOCITY(FT*FT/SEC.) =   | 1.00     |              |
| LONGEST FLOWPATH FROM NODE | 280.00 | TO NODE                        | 278.00 = | 285.00 FEET. |

\*\*\*\*\*

FLOW PROCESS FROM NODE 278.00 TO NODE 277.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|                                  |        |                    |        |
|----------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) = | 840.50 | DOWNSTREAM(FEET) = | 840.00 |
|----------------------------------|--------|--------------------|--------|



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FLOW LENGTH(FEET) = 38.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.17  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.49  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 3.15  
LONGEST FLOWPATH FROM NODE 280.00 TO NODE 277.00 = 323.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 277.00 TO NODE 277.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.15  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.49

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 41.03        | 6.29      | 7.950                 | 5.16        |
| 2             | 2.49         | 3.15      | 9.222                 | 0.30        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 37.86        | 3.15      | 9.222                 |
| 2             | 43.17        | 6.29      | 7.950                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 43.17 Tc(MIN.) = 6.29  
TOTAL AREA(ACRES) = 5.5  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 277.00 = 2585.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 277.00 TO NODE 275.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

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ELEVATION DATA: UPSTREAM(FEET) = 840.00 DOWNSTREAM(FEET) = 837.00  
FLOW LENGTH(FEET) = 237.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 24.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.17  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 43.17  
PIPE TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 6.68  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 275.00 = 2822.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 275.00 TO NODE 275.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.68  
RAINFALL INTENSITY(INCH/HR) = 7.65  
TOTAL STREAM AREA(ACRES) = 5.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 280.00 TO NODE 276.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 858.00  
DOWNSTREAM ELEVATION(FEET) = 853.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.105  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 276.00 TO NODE 275.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 853.00 DOWNSTREAM ELEVATION(FEET) = 840.10  
STREET LENGTH(FEET) = 390.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.41  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.48  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.55  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.98  
STREET FLOW TRAVEL TIME(MIN.) = 1.83 Tc(MIN.) = 3.94  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 3.32  
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 4.07

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.53  
FLOW VELOCITY(FEET/SEC.) = 3.96 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.26  
LONGEST FLOWPATH FROM NODE 280.00 TO NODE 275.00 = 490.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 275.00 TO NODE 275.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.94  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.07

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 43.17        | 6.68      | 7.648                 | 5.46        |

2          4.07          3.94          P-22d.TXT  
    9.222          0.49

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 39.87        | 3.94      | 9.222                 |
| 2             | 46.55        | 6.68      | 7.648                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 46.55 Tc(MIN.) = 6.68  
 TOTAL AREA(ACRES) = 5.9  
 LONGEST FLOWPATH FROM NODE 298.00 TO NODE 275.00 = 2822.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 275.00 TO NODE 274.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 837.00 DOWNSTREAM(FEET) = 836.50  
 FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.78  
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 46.55  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 6.71  
 LONGEST FLOWPATH FROM NODE 298.00 TO NODE 274.00 = 2842.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 274.00 TO NODE 273.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 836.50 DOWNSTREAM(FEET) = 835.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 150.00 CHANNEL SLOPE = 0.0100  
 CHANNEL FLOW THRU SUBAREA(CFS) = 46.55  
 FLOW VELOCITY(FEET/SEC) = 3.79 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 7.37  
 LONGEST FLOWPATH FROM NODE 298.00 TO NODE 273.00 = 2992.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 274.00 TO NODE 273.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.183  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8622  
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.86  
TOTAL AREA(ACRES) = 6.3 TOTAL RUNOFF(CFS) = 46.55  
TC(MIN.) = 7.37  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*  
FLOW PROCESS FROM NODE 273.00 TO NODE 273.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 7.40 RAIN INTENSITY(INCH/HOUR) = 7.16  
TOTAL AREA(ACRES) = 6.40 TOTAL RUNOFF(CFS) = 18.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 273.00 TO NODE 272.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 835.00 DOWNSTREAM(FEET) = 834.00  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.83  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 18.00  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 7.52  
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 272.00 = 3057.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 272.00 TO NODE 272.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2203.00 TO NODE 2202.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500

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S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1445.00  
DOWNSTREAM ELEVATION(FEET) = 1405.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.22  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.22

\*\*\*\*\*

FLOW PROCESS FROM NODE 2202.00 TO NODE 2201.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1405.00 DOWNSTREAM(FEET) = 890.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1382.00 CHANNEL SLOPE = 0.3726  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2092 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.22  
FLOW VELOCITY(FEET/SEC) = 2.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 8.99 Tc(MIN.) = 15.26  
LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2201.00 = 1482.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2202.00 TO NODE 2201.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.490  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4496  
SUBAREA AREA(ACRES) = 18.06 SUBAREA RUNOFF(CFS) = 36.49  
TOTAL AREA(ACRES) = 18.1 TOTAL RUNOFF(CFS) = 36.62  
TC(MIN.) = 15.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 2201.00 TO NODE 2200.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 890.00 DOWNSTREAM(FEET) = 835.00

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CHANNEL LENGTH THRU SUBAREA(FEET) = 428.00 CHANNEL SLOPE = 0.1285  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1207 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 36.62  
FLOW VELOCITY(FEET/SEC) = 6.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.11 Tc(MIN.) = 16.36  
LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2200.00 = 1910.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2201.00 TO NODE 2200.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.292  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4475  
SUBAREA AREA(ACRES) = 2.14 SUBAREA RUNOFF(CFS) = 3.95  
TOTAL AREA(ACRES) = 20.3 TOTAL RUNOFF(CFS) = 38.95  
TC(MIN.) = 16.36

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2200.00 TO NODE 2200.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.36  
RAINFALL INTENSITY(INCH/HR) = 4.29  
TOTAL STREAM AREA(ACRES) = 20.28  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 38.95

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2207.00 TO NODE 2206.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1295.00  
DOWNSTREAM ELEVATION(FEET) = 1270.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.42  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*

FLOW PROCESS FROM NODE 2206.00 TO NODE 2205.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1270.00 DOWNSTREAM(FEET) = 1070.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 475.00 CHANNEL SLOPE = 0.4211  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2165 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.42  
FLOW VELOCITY(FEET/SEC) = 2.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.04 Tc(MIN.) = 9.30  
LONGEST FLOWPATH FROM NODE 2207.00 TO NODE 2205.00 = 575.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2206.00 TO NODE 2205.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.178  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4564  
SUBAREA AREA(ACRES) = 4.44 SUBAREA RUNOFF(CFS) = 12.62  
TOTAL AREA(ACRES) = 4.6 TOTAL RUNOFF(CFS) = 12.94  
TC(MIN.) = 9.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2205.00 TO NODE 2200.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1070.00 DOWNSTREAM(FEET) = 840.10  
CHANNEL LENGTH THRU SUBAREA(FEET) = 930.00 CHANNEL SLOPE = 0.2472  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1791 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 12.94  
FLOW VELOCITY(FEET/SEC) = 5.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.79 Tc(MIN.) = 12.09  
LONGEST FLOWPATH FROM NODE 2207.00 TO NODE 2200.00 = 1505.00 FEET.



\*\*\*\*\*

FLOW PROCESS FROM NODE 2205.00 TO NODE 2200.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.217  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4519  
SUBAREA AREA(ACRES) = 10.76 SUBAREA RUNOFF(CFS) = 25.26  
TOTAL AREA(ACRES) = 15.4 TOTAL RUNOFF(CFS) = 36.19  
TC(MIN.) = 12.09

\*\*\*\*\*

FLOW PROCESS FROM NODE 2200.00 TO NODE 2200.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.09  
RAINFALL INTENSITY(INCH/HR) = 5.22  
TOTAL STREAM AREA(ACRES) = 15.35  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.19

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 38.95        | 16.36     | 4.292                 | 20.28       |
| 2             | 36.19        | 12.09     | 5.217                 | 15.35       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 64.97        | 12.09     | 5.217                 |
| 2             | 68.73        | 16.36     | 4.292                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 68.73 Tc(MIN.) = 16.36  
TOTAL AREA(ACRES) = 35.6  
LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2200.00 = 1910.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2200.00 TO NODE 272.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 840.10            | DOWNSTREAM(FEET) = | 834.00        |
| FLOW LENGTH(FEET) =              | 13.00             | MANNING'S N =      | 0.013         |
| DEPTH OF FLOW IN                 | 21.0 INCH PIPE IS | 12.5 INCHES        |               |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 45.84             |                    |               |
| ESTIMATED PIPE DIAMETER(INCH) =  | 21.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 68.73             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.00              | Tc(MIN.) =         | 16.37         |
| LONGEST FLOWPATH FROM NODE       | 2203.00 TO NODE   | 272.00 =           | 1923.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 272.00 TO NODE 272.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 68.73        | 16.37     | 4.291                 | 35.63       |

LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 272.00 = 1923.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 18.00        | 7.52      | 7.086                 | 6.40        |

LONGEST FLOWPATH FROM NODE 298.00 TO NODE 272.00 = 3057.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 49.58        | 7.52      | 7.086                 |
| 2             | 79.63        | 16.37     | 4.291                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 79.63 Tc(MIN.) = 16.37  
TOTAL AREA(ACRES) = 42.0

\*\*\*\*\*  
FLOW PROCESS FROM NODE 272.00 TO NODE 22.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 834.00 DOWNSTREAM(FEET) = 820.00
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 29.14
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 79.63
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 16.43
LONGEST FLOWPATH FROM NODE 298.00 TO NODE 22.00 = 3157.00 FEET.
=====
```

END OF STUDY SUMMARY:

```
=====
TOTAL AREA(ACRES) = 42.0 TC(MIN.) = 16.43
PEAK FLOW RATE(CFS) = 79.63
=====
```

```
=====
END OF RATIONAL METHOD ANALYSIS
=====
```





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 22.1 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-22-1.DAT  
TIME/DATE OF STUDY: 14:50 11/17/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2213.00 TO NODE 2212.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1260.00  
DOWNSTREAM ELEVATION(FEET) = 1230.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 1.09  
TOTAL AREA(ACRES) = 0.39 TOTAL RUNOFF(CFS) = 1.09

\*\*\*\*\*

FLOW PROCESS FROM NODE 2212.00 TO NODE 2211.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1230.00 DOWNSTREAM(FEET) = 1095.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 655.00 CHANNEL SLOPE = 0.2061  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1631 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.09  
FLOW VELOCITY(FEET/SEC) = 2.33 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.69 Tc(MIN.) = 10.96  
LONGEST FLOWPATH FROM NODE 2213.00 TO NODE 2211.00 = 755.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2212.00 TO NODE 2211.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.558  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4470  
SUBAREA AREA(ACRES) = 2.91 SUBAREA RUNOFF(CFS) = 7.44  
TOTAL AREA(ACRES) = 3.3 TOTAL RUNOFF(CFS) = 8.20  
TC(MIN.) = 10.96

P-22-1.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2211.00 TO NODE 2210.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1095.00 DOWNSTREAM(FEET) = 850.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 835.00 CHANNEL SLOPE = 0.2934  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1934 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.20  
FLOW VELOCITY(FEET/SEC) = 4.96 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.80 Tc(MIN.) = 13.77  
LONGEST FLOWPATH FROM NODE 2213.00 TO NODE 2210.00 = 1590.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2211.00 TO NODE 2210.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.799  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4400  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4420  
SUBAREA AREA(ACRES) = 8.02 SUBAREA RUNOFF(CFS) = 16.93  
TOTAL AREA(ACRES) = 11.3 TOTAL RUNOFF(CFS) = 24.01  
TC(MIN.) = 13.77

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2210.00 TO NODE 22.10 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 850.00 DOWNSTREAM(FEET) = 837.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.78  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 24.01  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 13.84  
LONGEST FLOWPATH FROM NODE 2213.00 TO NODE 22.10 = 1690.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 11.3 TC(MIN.) = 13.84  
PEAK FLOW RATE(CFS) = 24.01

=====

=====  
END OF RATIONAL METHOD ANALYSIS







\*\*\*\*\*

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2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 22.2 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-22-2.DAT  
TIME/DATE OF STUDY: 15:31 11/17/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2223.00 TO NODE 2222.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1235.00

DOWNSTREAM ELEVATION(FEET) = 1234.00

ELEVATION DIFFERENCE(FEET) = 1.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.884

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 65.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.584

SUBAREA RUNOFF(CFS) = 0.57

TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2222.00 TO NODE 2221.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1234.00 DOWNSTREAM(FEET) = 1115.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 530.00 CHANNEL SLOPE = 0.2245

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1715 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION

CHANNEL FLOW THRU SUBAREA(CFS) = 0.57

FLOW VELOCITY(FEET/SEC) = 2.32 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 3.81 Tc(MIN.) = 14.69

LONGEST FLOWPATH FROM NODE 2223.00 TO NODE 2221.00 = 630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2222.00 TO NODE 2221.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.601

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.4456

P-22-2.TXT

SUBAREA AREA(ACRES) = 6.34 SUBAREA RUNOFF(CFS) = 13.13  
TOTAL AREA(ACRES) = 6.6 TOTAL RUNOFF(CFS) = 13.59  
TC(MIN.) = 14.69

\*\*\*\*\*

FLOW PROCESS FROM NODE 2221.00 TO NODE 2220.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1115.00 DOWNSTREAM(FEET) = 885.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 735.00 CHANNEL SLOPE = 0.3129  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1982 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 13.59  
FLOW VELOCITY(FEET/SEC) = 5.95 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 16.75  
LONGEST FLOWPATH FROM NODE 2223.00 TO NODE 2220.00 = 1365.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2221.00 TO NODE 2220.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.228  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4478  
SUBAREA AREA(ACRES) = 6.71 SUBAREA RUNOFF(CFS) = 12.77  
TOTAL AREA(ACRES) = 13.3 TOTAL RUNOFF(CFS) = 25.26  
TC(MIN.) = 16.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 2220.00 TO NODE 22.20 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 885.00 DOWNSTREAM(FEET) = 865.00  
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 25.07  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 25.26  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 16.83  
LONGEST FLOWPATH FROM NODE 2223.00 TO NODE 22.20 = 1475.00 FEET.

=====  
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 13.3 TC(MIN.) = 16.83

PEAK FLOW RATE(CFS) = 25.26  
=====

=====  
END OF RATIONAL METHOD ANALYSIS





\*\*\*\*\*

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Analysis prepared by:

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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 22.3 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-22-3.DAT  
TIME/DATE OF STUDY: 15:35 11/17/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2232.00 TO NODE 2231.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1240.00  
DOWNSTREAM ELEVATION(FEET) = 1195.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.73  
TOTAL AREA(ACRES) = 0.26 TOTAL RUNOFF(CFS) = 0.73

\*\*\*\*\*

FLOW PROCESS FROM NODE 2231.00 TO NODE 2230.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1195.00 DOWNSTREAM(FEET) = 930.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 490.00 CHANNEL SLOPE = 0.5408  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2270 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.73  
FLOW VELOCITY(FEET/SEC) = 2.67 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.06 Tc(MIN.) = 9.33  
LONGEST FLOWPATH FROM NODE 2232.00 TO NODE 2230.00 = 590.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2231.00 TO NODE 2230.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.168  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4443  
SUBAREA AREA(ACRES) = 4.32 SUBAREA RUNOFF(CFS) = 11.99  
TOTAL AREA(ACRES) = 4.6 TOTAL RUNOFF(CFS) = 12.55  
TC(MIN.) = 9.33



\*\*\*\*\*

FLOW PROCESS FROM NODE 2230.00 TO NODE 22.30 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |        |                    |        |
|--|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 930.00 | DOWNSTREAM(FEET) = | 882.00 |
| FLOW LENGTH(FEET) =                                | 180.00 | MANNING'S N =      | 0.013  |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO         | 18.000 |                    |        |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS                 | 6.1    | INCHES             |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 24.04  |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =                    | 18.00  | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 12.55  |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.12   | Tc(MIN.) =         | 9.45   |
| LONGEST FLOWPATH FROM NODE 2232.00 TO NODE 22.30 = | 770.00 | FEET.              |        |

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 4.6 TC(MIN.) = 9.45

PEAK FLOW RATE(CFS) = 12.55

-----  
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

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6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 22.4 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-22-4.DAT  
TIME/DATE OF STUDY: 15:38 11/17/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2242.00 TO NODE 2241.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1205.00  
DOWNSTREAM ELEVATION(FEET) = 1135.00  
ELEVATION DIFFERENCE(FEET) = 70.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.42  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2241.00 TO NODE 2240.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 920.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 830.00 CHANNEL SLOPE = 0.2590  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1830 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.42  
FLOW VELOCITY(FEET/SEC) = 2.40 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.77 Tc(MIN.) = 12.04  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2240.00 = 930.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2241.00 TO NODE 2240.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.231  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 4.00 SUBAREA RUNOFF(CFS) = 7.32  
TOTAL AREA(ACRES) = 4.2 TOTAL RUNOFF(CFS) = 7.60  
TC(MIN.) = 12.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 2240.00 TO NODE 22.40 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |               |                    |        |
|--|---------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 920.00        | DOWNSTREAM(FEET) = | 900.00 |
| FLOW LENGTH(FEET) =                                | 115.00        | MANNING'S N =      | 0.013  |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO         | 18.000        |                    |        |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS                 | 5.2 INCHES    |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 17.89         |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =                    | 18.00         | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 7.60          |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.11          | Tc(MIN.) =         | 12.15  |
| LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 22.40 = | 1045.00 FEET. |                    |        |

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 4.2 TC(MIN.) = 12.15

PEAK FLOW RATE(CFS) = 7.60

-----  
END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* WITH DETENTION AT NODE 23.02 \*
  - \* SUB-BASIN 23 \*
- \*\*\*\*\*

FILE NAME: P-23D.DAT  
TIME/DATE OF STUDY: 16:11 01/27/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0312 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2304.00 TO NODE 2303.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1325.00

DOWNSTREAM ELEVATION(FEET) = 1268.00

ELEVATION DIFFERENCE(FEET) = 57.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972

SUBAREA RUNOFF(CFS) = 2.90

TOTAL AREA(ACRES) = 1.04 TOTAL RUNOFF(CFS) = 2.90

\*\*\*\*\*

FLOW PROCESS FROM NODE 2303.00 TO NODE 2301.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1268.00 DOWNSTREAM(FEET) = 863.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1070.00 CHANNEL SLOPE = 0.3785

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .2102 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 2.90

FLOW VELOCITY(FEET/SEC) = 3.66 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 4.87 Tc(MIN.) = 11.14

LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 2301.00 = 1170.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2303.00 TO NODE 2301.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.501

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500

SUBAREA AREA(ACRES) = 7.47 SUBAREA RUNOFF(CFS) = 14.38

TOTAL AREA(ACRES) = 8.5 TOTAL RUNOFF(CFS) = 16.39

TC(MIN.) = 11.14



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2301.00 TO NODE 2300.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 863.00 DOWNSTREAM(FEET) = 803.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 480.00 CHANNEL SLOPE = 0.1250  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1183 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 16.39  
FLOW VELOCITY(FEET/SEC) = 4.89 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.64 Tc(MIN.) = 12.77  
LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 2300.00 = 1650.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2301.00 TO NODE 2300.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.036  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4146  
SUBAREA AREA(ACRES) = 15.54 SUBAREA RUNOFF(CFS) = 35.21  
TOTAL AREA(ACRES) = 24.0 TOTAL RUNOFF(CFS) = 50.21  
TC(MIN.) = 12.77

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2300.00 TO NODE 23.01 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 803.00 DOWNSTREAM(FEET) = 797.50  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.26  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 50.21  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 12.87  
LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 23.01 = 1750.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.01 TO NODE 23.01 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.90 TO NODE 23.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 826.60  
DOWNSTREAM ELEVATION(FEET) = 823.20  
ELEVATION DIFFERENCE(FEET) = 3.40  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.988  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.80 TO NODE 23.04 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

\*\*\*\*\*  
UPSTREAM ELEVATION(FEET) = 823.20 DOWNSTREAM ELEVATION(FEET) = 809.50  
STREET LENGTH(FEET) = 650.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.53  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.36  
HALFSTREET FLOOD WIDTH(FEET) = 11.65  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.57  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.28  
STREET FLOW TRAVEL TIME(MIN.) = 3.04 Tc(MIN.) = 5.02  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.192  
\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 2.35 SUBAREA RUNOFF(CFS) = 19.44  
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 20.27

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 15.21  
FLOW VELOCITY(FEET/SEC.) = 4.17 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.79  
LONGEST FLOWPATH FROM NODE 23.90 TO NODE 23.04 = 730.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.04 TO NODE 23.04 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.02  
RAINFALL INTENSITY(INCH/HR) = 9.19  
TOTAL STREAM AREA(ACRES) = 2.45  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.70 TO NODE 23.60 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 814.70  
DOWNSTREAM ELEVATION(FEET) = 814.00  
ELEVATION DIFFERENCE(FEET) = 0.70  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.968  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 59.71  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.41  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 1.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.60 TO NODE 23.50 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 814.00 DOWNSTREAM ELEVATION(FEET) = 812.90
STREET LENGTH(FEET) = 355.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.01
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.65
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.36
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.49
STREET FLOW TRAVEL TIME(MIN.) = 4.35 Tc(MIN.) = 7.32
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.213

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 0.79 SUBAREA RUNOFF(CFS) = 5.13
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 6.23

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 13.98
FLOW VELOCITY(FEET/SEC.) = 1.50 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.61
LONGEST FLOWPATH FROM NODE 23.70 TO NODE 23.50 = 440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.50 TO NODE 23.04 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 807.00 DOWNSTREAM(FEET) = 803.00
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.95
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.23

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PIPE TRAVEL TIME(MIN.) = 1.12      Tc(MIN.) = 8.44  
 LONGEST FLOWPATH FROM NODE 23.70 TO NODE 23.04 = 840.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.04 TO NODE 23.04 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.44  
 RAINFALL INTENSITY(INCH/HR) = 6.58  
 TOTAL STREAM AREA(ACRES) = 0.96  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.23

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.27        | 5.02      | 9.192                 | 2.45        |
| 2             | 6.23         | 8.44      | 6.580                 | 0.96        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 23.98        | 5.02      | 9.192                 |
| 2             | 20.74        | 8.44      | 6.580                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 23.98      Tc(MIN.) = 5.02  
 TOTAL AREA(ACRES) = 3.4  
 LONGEST FLOWPATH FROM NODE 23.70 TO NODE 23.04 = 840.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.04 TO NODE 23.03 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 803.00      DOWNSTREAM(FEET) = 800.00  
 FLOW LENGTH(FEET) = 75.00      MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.88  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00      NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 23.98

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PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.11  
LONGEST FLOWPATH FROM NODE 23.70 TO NODE 23.03 = 915.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.03 TO NODE 23.02 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |  |                      |
|-------------------------------------|--------|--|----------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 800.00 | DOWNSTREAM(FEET) =                     | 799.50               |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 35.00  | CHANNEL SLOPE =                        | 0.0143               |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 23.98  |  |                      |
| FLOW VELOCITY(FEET/SEC) =           | 3.76   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                      |
| TRAVEL TIME(MIN.) =                 | 0.16   | Tc(MIN.) =                             | 5.27                 |
| LONGEST FLOWPATH FROM NODE          | 23.70  | TO NODE                                | 23.02 = 950.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.03 TO NODE 23.02 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |        |                       |       |
|--|--------|-----------------------|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 8.914  |                       |       |
| *USER SPECIFIED(SUBAREA):                |        |                       |       |
| USER-SPECIFIED RUNOFF COEFFICIENT =      | .3000  |                       |       |
| S.C.S. CURVE NUMBER (AMC II) =           | 0      |                       |       |
| AREA-AVERAGE RUNOFF COEFFICIENT =        | 0.8090 |                       |       |
| SUBAREA AREA(ACRES) =                    | 0.61   | SUBAREA RUNOFF(CFS) = | 1.63  |
| TOTAL AREA(ACRES) =                      | 4.0    | TOTAL RUNOFF(CFS) =   | 28.99 |
| TC(MIN.) =                               | 5.27   |                       |       |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.02 TO NODE 23.02 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

|                                       |      |                             |      |
|---------------------------------------|------|-----------------------------|------|
| USER-SPECIFIED VALUES ARE AS FOLLOWS: |      |                             |      |
| TC(MIN) =                             | 5.30 | RAIN INTENSITY(INCH/HOUR) = | 8.88 |
| TOTAL AREA(ACRES) =                   | 4.10 | TOTAL RUNOFF(CFS) =         | 5.00 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 23.02 TO NODE 23.01 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |        |                    |        |
|--|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =           | 799.50 | DOWNSTREAM(FEET) = | 797.50 |
| FLOW LENGTH(FEET) =                        | 190.00 | MANNING'S N =      | 0.013  |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO | 18.000 |                    |        |

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DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.75  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.00  
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 5.85  
LONGEST FLOWPATH FROM NODE 23.70 TO NODE 23.01 = 1140.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.01 TO NODE 23.01 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 5.00 5.85 8.333 4.10  
LONGEST FLOWPATH FROM NODE 23.70 TO NODE 23.01 = 1140.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 50.21 12.87 5.013 24.05  
LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 23.01 = 1750.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY  
NUMBER (CFS) (MIN.) (INCH/HOUR)  
1 27.83 5.85 8.333  
2 53.22 12.87 5.013

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 53.22 Tc(MIN.) = 12.87  
TOTAL AREA(ACRES) = 28.1

\*\*\*\*\*

FLOW PROCESS FROM NODE 23.01 TO NODE 23.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 797.50 DOWNSTREAM(FEET) = 790.00  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 31.87  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 53.22  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 12.88

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LONGEST FLOWPATH FROM NODE 2304.00 TO NODE 23.00 = 1785.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 28.1 TC(MIN.) = 12.88

PEAK FLOW RATE(CFS) = 53.22

=====

=====

END OF RATIONAL METHOD ANALYSIS

↑





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* NO DETENTION \*
  - \* SUB-BASIN 23.1 \*
- \*\*\*\*\*

FILE NAME: P-23-1.DAT  
TIME/DATE OF STUDY: 14:35 11/17/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2312.00 TO NODE 2311.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1150.00  
DOWNSTREAM ELEVATION(FEET) = 1080.00  
ELEVATION DIFFERENCE(FEET) = 70.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.348  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.830  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2311.00 TO NODE 2310.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1080.00 DOWNSTREAM(FEET) = 818.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 880.00 CHANNEL SLOPE = 0.2977  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1944 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.53  
FLOW VELOCITY(FEET/SEC) = 2.47 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.94 Tc(MIN.) = 11.29  
LONGEST FLOWPATH FROM NODE 2312.00 TO NODE 2310.00 = 980.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2311.00 TO NODE 2310.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.454  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4309  
SUBAREA AREA(ACRES) = 4.09 SUBAREA RUNOFF(CFS) = 9.59  
TOTAL AREA(ACRES) = 4.2 TOTAL RUNOFF(CFS) = 9.92  
TC(MIN.) = 11.29

P-23-1.TXT

\*\*\*\*\*

FLOW PROCESS FROM NODE 2310.00 TO NODE 23.10 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |               |                    |        |
|--|---------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 818.00        | DOWNSTREAM(FEET) = | 803.00 |
| FLOW LENGTH(FEET) =                                | 125.00        | MANNING'S N =      | 0.013  |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO         | 18.000        |                    |        |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS                 | 6.6 INCHES    |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 16.88         |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =                    | 18.00         | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 9.92          |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.12          | Tc(MIN.) =         | 11.41  |
| LONGEST FLOWPATH FROM NODE 2312.00 TO NODE 23.10 = | 1105.00 FEET. |                    |        |

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 4.2 TC(MIN.) = 11.41

PEAK FLOW RATE(CFS) = 9.92

=====

END OF RATIONAL METHOD ANALYSIS

↑



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* NO DETENTION \*
  - \* SUB-BASIN 23.2 \*
- \*\*\*\*\*

FILE NAME: P-23-2.DAT  
TIME/DATE OF STUDY: 14:08 11/17/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2323.00 TO NODE 2322.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1350.00  
DOWNSTREAM ELEVATION(FEET) = 1300.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.348  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.830  
SUBAREA RUNOFF(CFS) = 1.18  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 1.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 2322.00 TO NODE 2321.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1300.00 DOWNSTREAM(FEET) = 950.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 715.00 CHANNEL SLOPE = 0.4895  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2240 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.18  
FLOW VELOCITY(FEET/SEC) = 2.80 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.26 Tc(MIN.) = 9.61  
LONGEST FLOWPATH FROM NODE 2323.00 TO NODE 2321.00 = 815.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2322.00 TO NODE 2321.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.052  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4600  
SUBAREA AREA(ACRES) = 2.78 SUBAREA RUNOFF(CFS) = 7.74  
TOTAL AREA(ACRES) = 3.1 TOTAL RUNOFF(CFS) = 8.55  
TC(MIN.) = 9.61

P-23-2.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2321.00 TO NODE 2320.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 950.00 DOWNSTREAM(FEET) = 813.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 660.00 CHANNEL SLOPE = 0.2076  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1638 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.55  
FLOW VELOCITY(FEET/SEC) = 4.63 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.38 Tc(MIN.) = 11.98  
LONGEST FLOWPATH FROM NODE 2323.00 TO NODE 2320.00 = 1475.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2321.00 TO NODE 2320.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.248  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4371  
SUBAREA AREA(ACRES) = 4.13 SUBAREA RUNOFF(CFS) = 9.10  
TOTAL AREA(ACRES) = 7.2 TOTAL RUNOFF(CFS) = 16.52  
TC(MIN.) = 11.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2320.00 TO NODE 23.20 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 813.00 DOWNSTREAM(FEET) = 795.00  
FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.83  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.52  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 12.10  
LONGEST FLOWPATH FROM NODE 2323.00 TO NODE 23.20 = 1615.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 7.2 TC(MIN.) = 12.10  
PEAK FLOW RATE(CFS) = 16.52



=====  
=====

END OF RATIONAL METHOD ANALYSIS





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 23.3 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-23-3.DAT  
TIME/DATE OF STUDY: 11:17 11/18/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020  | 0.67                   | 2.00 0.0313 0.167                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2333.00 TO NODE 2332.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1270.00  
DOWNSTREAM ELEVATION(FEET) = 1195.00  
ELEVATION DIFFERENCE(FEET) = 75.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.348  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.830  
SUBAREA RUNOFF(CFS) = 1.26  
TOTAL AREA(ACRES) = 0.31 TOTAL RUNOFF(CFS) = 1.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 2332.00 TO NODE 2331.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1195.00 DOWNSTREAM(FEET) = 925.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 515.00 CHANNEL SLOPE = 0.5243  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2262 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.26  
FLOW VELOCITY(FEET/SEC) = 2.88 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.98 Tc(MIN.) = 8.33  
LONGEST FLOWPATH FROM NODE 2333.00 TO NODE 2331.00 = 615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2332.00 TO NODE 2331.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.634  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4600  
SUBAREA AREA(ACRES) = 2.23 SUBAREA RUNOFF(CFS) = 6.80  
TOTAL AREA(ACRES) = 2.5 TOTAL RUNOFF(CFS) = 7.75  
TC(MIN.) = 8.33

P-23-3.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2331.00 TO NODE 2330.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 925.00 DOWNSTREAM(FEET) = 823.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 500.00 CHANNEL SLOPE = 0.2040  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1620 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.75  
FLOW VELOCITY(FEET/SEC) = 4.46 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 10.20  
LONGEST FLOWPATH FROM NODE 2333.00 TO NODE 2330.00 = 1115.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2331.00 TO NODE 2330.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.822  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4411  
SUBAREA AREA(ACRES) = 4.32 SUBAREA RUNOFF(CFS) = 10.81  
TOTAL AREA(ACRES) = 6.9 TOTAL RUNOFF(CFS) = 17.62  
TC(MIN.) = 10.20

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2330.00 TO NODE 23.30 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 823.00 DOWNSTREAM(FEET) = 798.00  
FLOW LENGTH(FEET) = 470.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.33  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 17.62  
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 10.75  
LONGEST FLOWPATH FROM NODE 2333.00 TO NODE 23.30 = 1585.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 6.9 TC(MIN.) = 10.75  
PEAK FLOW RATE(CFS) = 17.62

=====

=====  
END OF RATIONAL METHOD ANALYSIS





| Node to Node |      | Code | Elev 1<br>(feet)   | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments | BANK |   |   |
|--------------|------|------|--------------------|------------------|------------------|-------------|---------------|----------|------|---|---|
|              |      |      |                    |                  |                  |             |               |          | 1    | 2 | 3 |
| 2343         | 2342 | 2    | 1360               | 1305             | 100              | 0.34        | 0.12          |          |      |   |   |
| 2342         | 2341 | 5    | 1305               | 890              | 900              |             |               |          |      |   |   |
| 2342         | 2341 | 8    |                    |                  |                  | 0.45        | 3.46          |          |      |   |   |
| 2341         | 2340 | 5    | 890                | 820              | 520              |             |               |          |      |   |   |
| 2341         | 2340 | 8    |                    |                  |                  | 0.42        | 5.96          |          |      |   |   |
| 2340         | 260  | 3    | 820                | 809              | 100              |             |               |          |      |   |   |
| 260          | 260  | 1    |                    |                  |                  |             |               | 1 OF 2   |      |   |   |
| 270          | 268  | 2    | 846.6              | 844.1            | 80               | 0.9         | 0.08          |          |      |   |   |
| 268          | 266  | 6    | 844.1              | 826.6            | 570              | 0.9         | 1.13          | 2 SIDES  |      |   |   |
| 266          | 264  | 3    | 820                | 818              | 200              |             |               |          |      |   |   |
| 264          | 262  | 5    | 818                | 817.8            | 20               |             |               | VALLEY   |      |   |   |
| 264          | 262  | 8    |                    |                  |                  | 0.3         | 0.16          |          |      |   |   |
| 262          | 262  | 7    | Tc=5.5 A=1.4 Q=1.2 |                  |                  |             |               |          |      |   |   |
| 262          | 260  | 3    | 812                | 809              | 245              |             |               |          |      |   |   |
| 260          | 260  | 1    |                    |                  |                  |             |               | 2 OF 2   |      |   |   |
| 260          | 23.4 | 3    | 809                | 795              | 35               |             |               |          |      |   |   |
|              |      |      |                    |                  |                  |             | 10.91         |          |      |   |   |

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* WITH DETENTION AT NODE 262 \*  
\* SUB-BASIN 23.4 \*  
\*\*\*\*\*

FILE NAME: P-23-4D.DAT  
TIME/DATE OF STUDY: 15:49 12/09/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2343.00 TO NODE 2342.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3400  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1360.00  
DOWNSTREAM ELEVATION(FEET) = 1305.00  
ELEVATION DIFFERENCE(FEET) = 55.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.350  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.904  
SUBAREA RUNOFF(CFS) = 0.32  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.32

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2342.00 TO NODE 2341.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1305.00 DOWNSTREAM(FEET) = 890.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 900.00 CHANNEL SLOPE = 0.4611  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2211 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.32  
FLOW VELOCITY(FEET/SEC) = 2.63 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.70 Tc(MIN.) = 12.05  
LONGEST FLOWPATH FROM NODE 2343.00 TO NODE 2341.00 = 1000.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2342.00 TO NODE 2341.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.230  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4463  
SUBAREA AREA(ACRES) = 3.46 SUBAREA RUNOFF(CFS) = 8.14  
TOTAL AREA(ACRES) = 3.6 TOTAL RUNOFF(CFS) = 8.36  
TC(MIN.) = 12.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2341.00 TO NODE 2340.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |        |                    |        |
|-------------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 890.00 | DOWNSTREAM(FEET) = | 820.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 520.00 | CHANNEL SLOPE =    | 0.1346 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1247 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.36  
FLOW VELOCITY(FEET/SEC) = 4.01 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.16 Tc(MIN.) = 14.21  
LONGEST FLOWPATH FROM NODE 2343.00 TO NODE 2340.00 = 1520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2341.00 TO NODE 2340.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.702 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4299  
SUBAREA AREA(ACRES) = 5.96 SUBAREA RUNOFF(CFS) = 11.77  
TOTAL AREA(ACRES) = 9.5 TOTAL RUNOFF(CFS) = 19.28  
TC(MIN.) = 14.21

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2340.00 TO NODE 260.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|                                  |        |                    |        |
|----------------------------------|--------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) = | 820.00 | DOWNSTREAM(FEET) = | 809.00 |
| FLOW LENGTH(FEET) =              | 100.00 | MANNING'S N =      | 0.013  |

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.28  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 14.29  
LONGEST FLOWPATH FROM NODE 2343.00 TO NODE 260.00 = 1620.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 260.00 TO NODE 260.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.29  
RAINFALL INTENSITY(INCH/HR) = 4.68  
TOTAL STREAM AREA(ACRES) = 9.54  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 270.00 TO NODE 268.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 846.60  
DOWNSTREAM ELEVATION(FEET) = 844.10  
ELEVATION DIFFERENCE(FEET) = 2.50  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.202  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.66  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 268.00 TO NODE 266.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 844.10 DOWNSTREAM ELEVATION(FEET) = 826.60  
STREET LENGTH(FEET) = 570.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.35

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 8.03
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.51
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.01
STREET FLOW TRAVEL TIME(MIN.) = 2.71 Tc(MIN.) = 4.91
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 1.13 SUBAREA RUNOFF(CFS) = 9.38
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 10.04

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.56
FLOW VELOCITY(FEET/SEC.) = 4.07 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.37
LONGEST FLOWPATH FROM NODE 270.00 TO NODE 266.00 = 650.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 266.00 TO NODE 264.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 820.00 DOWNSTREAM(FEET) = 818.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.69
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.04
PIPE TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 5.41
LONGEST FLOWPATH FROM NODE 270.00 TO NODE 264.00 = 850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 264.00 TO NODE 262.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 818.00 DOWNSTREAM(FEET) = 817.80
CHANNEL LENGTH THRU SUBAREA(FEET) = 20.00 CHANNEL SLOPE = 0.0100
CHANNEL FLOW THRU SUBAREA(CFS) = 10.04
FLOW VELOCITY(FEET/SEC) = 2.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 5.54
LONGEST FLOWPATH FROM NODE 270.00 TO NODE 262.00 = 870.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 264.00 TO NODE 262.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.631  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8299  
SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.41  
TOTAL AREA(ACRES) = 1.4 TOTAL RUNOFF(CFS) = 10.04  
TC(MIN.) = 5.54  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*  
FLOW PROCESS FROM NODE 262.00 TO NODE 262.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 5.50 RAIN INTENSITY(INCH/HOUR) = 8.67  
TOTAL AREA(ACRES) = 1.40 TOTAL RUNOFF(CFS) = 1.20

\*\*\*\*\*  
FLOW PROCESS FROM NODE 262.00 TO NODE 260.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 812.00 DOWNSTREAM(FEET) = 809.00  
FLOW LENGTH(FEET) = 245.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.08  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.20  
PIPE TRAVEL TIME(MIN.) = 1.00 Tc(MIN.) = 6.50  
LONGEST FLOWPATH FROM NODE 270.00 TO NODE 260.00 = 1115.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 260.00 TO NODE 260.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

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TIME OF CONCENTRATION(MIN.) = 6.50  
RAINFALL INTENSITY(INCH/HR) = 7.79  
TOTAL STREAM AREA(ACRES) = 1.40  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.20

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 19.28        | 14.29     | 4.684                 | 9.54        |
| 2             | 1.20         | 6.50      | 7.785                 | 1.40        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 9.97         | 6.50      | 7.785                 |
| 2             | 20.00        | 14.29     | 4.684                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 20.00 Tc(MIN.) = 14.29  
TOTAL AREA(ACRES) = 10.9  
LONGEST FLOWPATH FROM NODE 2343.00 TO NODE 260.00 = 1620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.00 TO NODE 23.40 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 809.00 DOWNSTREAM(FEET) = 795.00  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 31.66  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.00  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 14.31  
LONGEST FLOWPATH FROM NODE 2343.00 TO NODE 23.40 = 1655.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 10.9 TC(MIN.) = 14.31  
PEAK FLOW RATE(CFS) = 20.00

=====

END OF RATIONAL METHOD ANALYSIS

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| Node to Node |      | Code | Elev 1<br>(feet)   | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments | BANK |   |   |
|--------------|------|------|--------------------|------------------|------------------|-------------|---------------|----------|------|---|---|
|              |      |      |                    |                  |                  |             |               |          | 1    | 2 | 3 |
| 258          | 257  | 2    | 814.7              | 814              | 70               | 0.9         | 0.17          |          |      |   |   |
| 257          | 256  | 6    | 814                | 808.4            | 175              | 0.9         | 0.36          |          |      |   |   |
| 256          | 253  | 3    | 802                | 798              | 400              |             |               |          |      |   |   |
| 253          | 253  | 1    |                    |                  |                  |             |               | 1 OF 2   |      |   |   |
| 255          | 254  | 2    | 809.9              | 807.7            | 80               | 0.9         | 0.13          |          |      |   |   |
| 254          | 253  | 6    | 807.7              | 804.1            | 360              | 0.9         | 1.40          | 2 SIDES  |      |   |   |
| 253          | 253  | 1    |                    |                  |                  |             |               | 2 OF 2   |      |   |   |
| 253          | 252  | 3    | 798                | 795.5            | 70               |             |               |          |      |   |   |
| 252          | 251  | 5    | 795.5              | 795              | 50               |             |               |          |      |   |   |
| 252          | 251  | 8    |                    |                  |                  | 0.3         | 0.90          |          |      |   |   |
| 251          | 251  | 7    | Tc=5.7 A=3.0 Q=4.5 |                  |                  |             |               |          |      |   |   |
| 251          | 245  | 3    | 795                | 793              | 180              |             |               |          |      |   |   |
| 245          | 245  | 1    |                    |                  |                  |             |               | 1 OF 3   |      |   |   |
| 2403         | 2402 | 2    | 1360               | 1310             | 95               | 0.46        | 0.33          |          |      |   |   |
| 2402         | 2401 | 5    | 1310               | 1130             | 305              |             |               |          |      |   |   |
| 2402         | 2401 | 8    |                    |                  |                  | 0.46        | 1.82          |          |      |   |   |
| 2401         | 2400 | 5    | 1130               | 805              | 1315             |             |               |          |      |   |   |
| 2401         | 2400 | 8    |                    |                  |                  | 0.44        | 29.06         |          |      |   |   |
| 2400         | 245  | 3    | 805                | 793              | 55               |             |               |          |      |   |   |
| 245          | 245  | 1    |                    |                  |                  |             |               | 2 OF 3   |      |   |   |
| 250          | 249  | 2    | 812.2              | 812              | 80               | 0.9         | 0.09          |          |      |   |   |
| 249          | 248  | 6    | 812                | 808.2            | 230              | 0.9         | 0.23          |          |      |   |   |
| 248          | 247  | 3    | 802                | 800              | 100              |             |               |          |      |   |   |
| 247          | 246  | 5    | 800                | 799              | 85               |             |               |          |      |   |   |
| 247          | 246  | 8    |                    |                  |                  | 0.3         | 0.41          |          |      |   |   |
| 246          | 245  | 3    | 799                | 793              | 125              |             |               |          |      |   |   |
| 245          | 245  | 1    |                    |                  |                  |             |               | 3 OF 3   |      |   |   |
|              |      |      |                    |                  |                  |             | <b>34.90</b>  |          |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* WITH DETENTION AT NODE 251 \*
  - \* SUB-BASIN 24 \*
- \*\*\*\*\*

FILE NAME: P-24D.DAT  
TIME/DATE OF STUDY: 16:20 12/09/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 258.00 TO NODE 257.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00

UPSTREAM ELEVATION(FEET) = 814.70

DOWNSTREAM ELEVATION(FEET) = 814.00

ELEVATION DIFFERENCE(FEET) = 0.70

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.902

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 65.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.41

TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 1.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 257.00 TO NODE 256.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 814.00 DOWNSTREAM ELEVATION(FEET) = 808.40

STREET LENGTH(FEET) = 175.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.90

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.24

HALFSTREET FLOOD WIDTH(FEET) = 5.84

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.16

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.77

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STREET FLOW TRAVEL TIME(MIN.) = 0.92 Tc(MIN.) = 3.82

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.36 SUBAREA RUNOFF(CFS) = 2.99

TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 4.40

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.21

FLOW VELOCITY(FEET/SEC.) = 3.45 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.93

LONGEST FLOWPATH FROM NODE 258.00 TO NODE 256.00 = 245.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 256.00 TO NODE 253.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 802.00 DOWNSTREAM(FEET) = 798.00

FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.46

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 4.40

PIPE TRAVEL TIME(MIN.) = 1.22 Tc(MIN.) = 5.05

LONGEST FLOWPATH FROM NODE 258.00 TO NODE 253.00 = 645.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 253.00 TO NODE 253.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 5.05

RAINFALL INTENSITY(INCH/HR) = 9.17

TOTAL STREAM AREA(ACRES) = 0.53

PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 255.00 TO NODE 254.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 809.90  
 DOWNSTREAM ELEVATION(FEET) = 807.70  
 ELEVATION DIFFERENCE(FEET) = 2.20  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.298  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.08  
 TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 1.08

\*\*\*\*\*

FLOW PROCESS FROM NODE 254.00 TO NODE 253.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 807.70 DOWNSTREAM ELEVATION(FEET) = 804.10  
 STREET LENGTH(FEET) = 360.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.89

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.36  
 HALFSTREET FLOOD WIDTH(FEET) = 11.45  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.41  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86  
 STREET FLOW TRAVEL TIME(MIN.) = 2.49 Tc(MIN.) = 4.79  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 11.62  
 TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 12.70

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.66  
FLOW VELOCITY(FEET/SEC.) = 2.80 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.17  
LONGEST FLOWPATH FROM NODE 255.00 TO NODE 253.00 = 440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 253.00 TO NODE 253.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.79  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.53  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.70

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 4.40         | 5.05      | 9.167                 | 0.53        |
| 2             | 12.70        | 4.79      | 9.222                 | 1.53        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.87        | 4.79      | 9.222                 |
| 2             | 17.02        | 5.05      | 9.167                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 17.02 Tc(MIN.) = 5.05  
TOTAL AREA(ACRES) = 2.1  
LONGEST FLOWPATH FROM NODE 258.00 TO NODE 253.00 = 645.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 253.00 TO NODE 252.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 798.00 DOWNSTREAM(FEET) = 795.50  
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.07

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ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 17.02  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 5.14  
LONGEST FLOWPATH FROM NODE 258.00 TO NODE 252.00 = 715.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 252.00 TO NODE 251.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 795.50 DOWNSTREAM(FEET) = 795.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 50.00 CHANNEL SLOPE = 0.0100  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0100 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 17.02  
FLOW VELOCITY(FEET/SEC) = 1.44 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.58 Tc(MIN.) = 5.72  
LONGEST FLOWPATH FROM NODE 258.00 TO NODE 251.00 = 765.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 252.00 TO NODE 251.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.454  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7176  
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.28  
TOTAL AREA(ACRES) = 3.0 TOTAL RUNOFF(CFS) = 17.96  
TC(MIN.) = 5.72

\*\*\*\*\*  
FLOW PROCESS FROM NODE 251.00 TO NODE 251.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 5.70 RAIN INTENSITY(INCH/HOUR) = 8.47  
TOTAL AREA(ACRES) = 3.00 TOTAL RUNOFF(CFS) = 4.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 251.00 TO NODE 245.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 795.00 DOWNSTREAM(FEET) = 793.00  
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.72  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.50  
PIPE TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 6.22  
LONGEST FLOWPATH FROM NODE 258.00 TO NODE 245.00 = 945.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 245.00 TO NODE 245.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.22  
RAINFALL INTENSITY(INCH/HR) = 8.01  
TOTAL STREAM AREA(ACRES) = 3.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 2403.00 TO NODE 2402.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1360.00  
DOWNSTREAM ELEVATION(FEET) = 1310.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.212  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.978  
SUBAREA RUNOFF(CFS) = 1.36  
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 1.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 2402.00 TO NODE 2401.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1310.00 DOWNSTREAM(FEET) = 1130.00

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CHANNEL LENGTH THRU SUBAREA(FEET) = 305.00 CHANNEL SLOPE = 0.5902  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2295 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.36  
FLOW VELOCITY(FEET/SEC) = 2.97 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.71 Tc(MIN.) = 6.92  
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 2401.00 = 400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2402.00 TO NODE 2401.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.477  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4600  
SUBAREA AREA(ACRES) = 1.82 SUBAREA RUNOFF(CFS) = 6.26  
TOTAL AREA(ACRES) = 2.2 TOTAL RUNOFF(CFS) = 7.39  
TC(MIN.) = 6.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 2401.00 TO NODE 2400.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1130.00 DOWNSTREAM(FEET) = 805.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1315.00 CHANNEL SLOPE = 0.2471  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1790 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.39  
FLOW VELOCITY(FEET/SEC) = 4.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.75 Tc(MIN.) = 11.67  
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 2400.00 = 1715.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2401.00 TO NODE 2400.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.337  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4400  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4414  
SUBAREA AREA(ACRES) = 29.06 SUBAREA RUNOFF(CFS) = 68.25



TOTAL AREA(ACRES) = 31.2 TOTAL RUNOFF(CFS) = 73.53  
TC(MIN.) = 11.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 2400.00 TO NODE 245.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 805.00 DOWNSTREAM(FEET) = 793.00  
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.86  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 73.53  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 11.70  
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 245.00 = 1770.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 245.00 TO NODE 245.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.70  
RAINFALL INTENSITY(INCH/HR) = 5.33  
TOTAL STREAM AREA(ACRES) = 31.21  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 73.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 250.00 TO NODE 249.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 812.20  
DOWNSTREAM ELEVATION(FEET) = 812.00  
ELEVATION DIFFERENCE(FEET) = 0.20  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.207  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 50.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.75

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 249.00 TO NODE 248.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 812.00 DOWNSTREAM ELEVATION(FEET) = 808.20

STREET LENGTH(FEET) = 230.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.70

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.28

HALFSTREET FLOOD WIDTH(FEET) = 7.48

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.51

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.69

STREET FLOW TRAVEL TIME(MIN.) = 1.53 Tc(MIN.) = 4.73

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.23 SUBAREA RUNOFF(CFS) = 1.91

TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 2.66

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.19

FLOW VELOCITY(FEET/SEC.) = 2.76 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.86

LONGEST FLOWPATH FROM NODE 250.00 TO NODE 248.00 = 310.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 248.00 TO NODE 247.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 802.00 DOWNSTREAM(FEET) = 800.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.66  
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 5.01  
LONGEST FLOWPATH FROM NODE 250.00 TO NODE 247.00 = 410.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 247.00 TO NODE 246.00 IS CODE = 52

-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 800.00 DOWNSTREAM(FEET) = 799.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 85.00 CHANNEL SLOPE = 0.0118  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.66  
FLOW VELOCITY(FEET/SEC) = 1.98 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.71 Tc(MIN.) = 5.72  
LONGEST FLOWPATH FROM NODE 250.00 TO NODE 246.00 = 495.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 247.00 TO NODE 246.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.454  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5630  
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 1.04  
TOTAL AREA(ACRES) = 0.7 TOTAL RUNOFF(CFS) = 3.47  
TC(MIN.) = 5.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 246.00 TO NODE 245.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 799.00 DOWNSTREAM(FEET) = 793.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

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DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.03  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.47  
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 5.95  
LONGEST FLOWPATH FROM NODE 250.00 TO NODE 245.00 = 620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 245.00 TO NODE 245.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.95  
RAINFALL INTENSITY(INCH/HR) = 8.24  
TOTAL STREAM AREA(ACRES) = 0.73  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.47

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 4.50         | 6.22      | 8.006                 | 3.00        |
| 2             | 73.53        | 11.70     | 5.330                 | 31.21       |
| 3             | 3.47         | 5.95      | 8.241                 | 0.73        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 45.18        | 5.95      | 8.241                 |
| 2             | 47.00        | 6.22      | 8.006                 |
| 3             | 78.77        | 11.70     | 5.330                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 78.77 Tc(MIN.) = 11.70  
TOTAL AREA(ACRES) = 34.9  
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 245.00 = 1770.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 34.9 TC(MIN.) = 11.70  
PEAK FLOW RATE(CFS) = 78.77

=====

=====

END OF RATIONAL METHOD ANALYSIS

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\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* NO DETENTION \*
  - \* SUB-BASIN 24.2 \*
- \*\*\*\*\*

FILE NAME: P-24-2.DAT  
TIME/DATE OF STUDY: 14:26 11/17/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.00 TO NODE 2421.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1080.00  
DOWNSTREAM ELEVATION(FEET) = 990.00  
ELEVATION DIFFERENCE(FEET) = 90.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.682  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.492  
SUBAREA RUNOFF(CFS) = 1.18  
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 1.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 2421.00 TO NODE 2420.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 990.00 DOWNSTREAM(FEET) = 815.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1025.00 CHANNEL SLOPE = 0.1707  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1454 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 1.18  
FLOW VELOCITY(FEET/SEC) = 2.25 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 7.58 Tc(MIN.) = 13.26  
LONGEST FLOWPATH FROM NODE 2422.00 TO NODE 2420.00 = 1125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2421.00 TO NODE 2420.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.916  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4296  
SUBAREA AREA(ACRES) = 7.96 SUBAREA RUNOFF(CFS) = 16.83  
TOTAL AREA(ACRES) = 8.3 TOTAL RUNOFF(CFS) = 17.51  
TC(MIN.) = 13.26



P-24-2.TXT

\*\*\*\*\*

FLOW PROCESS FROM NODE 2420.00 TO NODE 24.20 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |               |                    |        |
|--|---------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 815.00        | DOWNSTREAM(FEET) = | 802.00 |
| FLOW LENGTH(FEET) =                                | 140.00        | MANNING'S N =      | 0.013  |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO         | 18.000        |                    |        |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS                 | 9.8 INCHES    |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 17.80         |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =                    | 18.00         | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 17.51         |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.13          | Tc(MIN.) =         | 13.39  |
| LONGEST FLOWPATH FROM NODE 2422.00 TO NODE 24.20 = | 1265.00 FEET. |                    |        |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 8.3 TC(MIN.) = 13.39  
PEAK FLOW RATE(CFS) = 17.51

=====

END OF RATIONAL METHOD ANALYSIS





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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------|------|---|---|
|              |        |      |                  |                  |                  |             |               |          | 1    | 2 | 3 |
| 1372         | 1371   | 2    | 1315             | 1313             | 80               | 0.52        | 0.24          |          |      |   |   |
| 1371         | 1368   | 5    | 1313             | 1296             | 570              | 0.51        | 1.71          |          |      |   |   |
| 1368         | 1364   | 3    | 1290             | 1287             | 100              |             |               |          |      |   |   |
| 1364         | 1364   | 1    |                  |                  |                  |             |               | 1 of 2   |      |   |   |
| 1367         | 1366   | 2    | 1312             | 1310             | 80               | 0.51        | 0.12          |          |      |   |   |
| 1366         | 1365   | 6    | 1310             | 1294             | 495              | 0.51        | 1.08          | 1 side   |      |   |   |
| 1365         | 1364   | 3    | 1288             | 1287             | 30               |             |               |          |      |   |   |
| 1364         | 1364   | 1    |                  |                  |                  |             |               | 2 of 2   |      |   |   |
| 1364         | 1360   | 3    | 1287             | 1279             | 240              |             |               |          |      |   |   |
| 1360         | 1360   | 1    |                  |                  |                  |             |               | 1 of 2   |      |   |   |
| 1363         | 1362   | 2    | 1311             | 1309             | 80               | 0.51        | 0.10          |          |      |   |   |
| 1362         | 1361   | 6    | 1309             | 1289             | 425              | 0.51        | 2.02          | 2 sides  |      |   |   |
| 1361         | 1360   | 3    | 1283             | 1279             | 30               |             |               |          |      |   |   |
| 1360         | 1360   | 1    |                  |                  |                  |             |               | 2 of 2   |      |   |   |
| 1360         | 1356   | 3    | 1279             | 1276             | 240              |             |               |          |      |   |   |
| 1356         | 1356   | 1    |                  |                  |                  |             |               | 1 of 3   |      |   |   |
| 1370         | 1369   | 2    | 1308             | 1306             | 50               | 0.51        | 0.09          |          |      |   |   |
| 1369         | 1359   | 6    | 1306             | 1282             | 1070             | 0.51        | 2.59          | 1 side   |      |   |   |
| 1359         | 1356   | 3    | 1276.5           | 1276             | 25               |             |               |          |      |   |   |
| 1356         | 1356   | 1    |                  |                  |                  |             |               | 2 of 3   |      |   |   |
| 1358         | 1357   | 2    | 1290             | 1288             | 70               | 0.51        | 0.04          |          |      |   |   |
| 1357         | 1356   | 5    | 1288             | 1281             | 400              | 0.53        | 0.81          |          |      |   |   |
| 1356         | 1356   | 1    |                  |                  |                  |             |               | 3 of 3   |      |   |   |
| 1356         | 1353.5 | 3    | 1275             | 1270             | 55               |             |               |          |      |   |   |
| 1353.5       | 1353.5 | 1    |                  |                  |                  |             |               | 1 of 2   |      |   |   |
| 1355         | 1354   | 2    | 1290             | 1288             | 70               | 0.51        | 0.07          |          |      |   |   |
| 1354         | 1353.5 | 5    | 1288             | 1278             | 400              | 0.52        | 1.08          |          |      |   |   |
| 1353.5       | 1353.5 | 1    |                  |                  |                  |             |               | 2 of 2   |      |   |   |
| 1353.5       | 2296.5 | 3    | 1270             | 1260             | 1050             |             |               |          |      |   |   |
| 2296.5       | 2296.5 | 1    |                  |                  |                  |             |               | 1 of 2   |      |   |   |
| 2299         | 2298   | 2    | 1273             | 1271             | 80               | 0.51        | 0.12          |          |      |   |   |
| 2298         | 2297   | 6    | 1271             | 1269             | 215              | 0.51        | 0.44          | 1 SIDE   |      |   |   |
| 2297         | 2296.5 | 3    | 1263             | 1260             | 50               |             |               |          |      |   |   |
| 2296.5       | 2296.5 | 1    |                  |                  |                  |             |               | 2 of 2   |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments             | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                      | 1    | 2 | 3 |
| 2296.5       | 2296   | 3    | 1260             | 1258             | 75               |             |               |                      |      |   |   |
| 2296         | 2296   | 1    |                  |                  |                  |             |               | 1 of 2               |      |   |   |
| 2295         | 2294   | 2    | 1272             | 1270             | 80               | 0.51        | 0.10          |                      |      |   |   |
| 2294         | 2293   | 6    | 1270             | 1265             | 225              | 0.51        | 0.53          | 1 SIDE               |      |   |   |
| 2293         | 2296   | 3    | 1259             | 1258             | 40               |             |               |                      |      |   |   |
| 2296         | 2296   | 1    |                  |                  |                  |             |               | 2 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2296         | 2292   | 3    | 1258             | 1257             | 90               |             |               |                      |      |   |   |
| 2292         | 2292   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1- 2292 |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2498         | 2497   | 2    | 1295             | 1292             | 95               | 0.57        | 0.15          |                      |      |   |   |
| 2497         | 2496   | 5    | 1292             | 1291             | 175              | 0.57        | 1.51          |                      |      |   |   |
| 2496         | 2495   | 3    | 1285             | 1279             | 230              |             |               |                      |      |   |   |
| 2495         | 2495   | 1    |                  |                  |                  |             |               | 1 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2491         | 2490   | 2    | 1288             | 1286             | 80               | 0.54        | 0.11          |                      |      |   |   |
| 2490         | 2495   | 6    | 1286             | 1285             | 80               | 0.51        | 0.33          | 1 SIDE               |      |   |   |
| 2495         | 2495   | 1    |                  |                  |                  |             |               | 2 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2495         | 2495.8 | 3    | 1279             | 1265             | 535              |             |               |                      |      |   |   |
| 2495.8       | 2495.8 | 1    |                  |                  |                  |             |               | 1 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2291         | 2290   | 2    | 1277             | 1276             | 65.00            | 0.51        | 0.11          |                      |      |   |   |
| 2290         | 2289   | 6    | 1276             | 1268             | 220              | 0.51        | 0.58          | 1 SIDE               |      |   |   |
| 2289         | 2495.8 | 3    | 1268             | 1265             | 110              |             |               |                      |      |   |   |
| 2495.8       | 2495.8 | 1    |                  |                  |                  |             |               | 2 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2495.8       | 2288   | 3    | 1265             | 1263             | 110              |             |               |                      |      |   |   |
| 2288         | 2288   | 1    |                  |                  |                  |             |               | 1 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2287         | 2286   | 2    | 1277             | 1276             | 66.67            | 0.51        | 0.08          |                      |      |   |   |
| 2286         | 2285   | 6    | 1276             | 1269             | 230              | 0.51        | 0.58          | 1 SIDE               |      |   |   |
| 2285         | 2288   | 3    | 1263             | 1260             | 40               |             |               |                      |      |   |   |
| 2288         | 2288   | 1    |                  |                  |                  |             |               | 2 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2288         | 2292   | 3    | 1260             | 1257             | 150              |             |               |                      |      |   |   |
| 2292         | 2292   | 11   |                  |                  |                  |             |               | ADD BANK 1 - 2292    |      |   |   |
| 2292         | 2292   | 12   |                  |                  |                  |             |               | CLEAR BANK 1         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2292         | 2284   | 3    | 1257             | 1252             | 325              |             |               |                      |      |   |   |
| 2284         | 2284   | 1    |                  |                  |                  |             |               | 1 OF 2               |      |   |   |
|              |        |      |                  |                  |                  |             |               |                      |      |   |   |
| 2283         | 2282   | 2    | 1375             | 1350             | 100              | 0.25        | 0.32          |                      |      |   |   |
| 2282         | 2284   | 5    | 1350             | 1348             | 420              | 0.25        | 4.16          |                      |      |   |   |
| 2284         | 2284   | 1    |                  |                  |                  |             |               | 2 OF 2               |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor           | Area<br>(ac.) | Comments              | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-----------------------|---------------|-----------------------|------|---|---|
|              |        |      |                  |                  |                  |                       |               |                       | 1    | 2 | 3 |
| 2284         | 2281   | 3    | 1252             | 1234             | 205              |                       |               |                       |      |   |   |
| 2281         | 2281   | 1    |                  |                  |                  |                       |               | 1 OF 2                |      |   |   |
| 2281         | 2281   | 7    | Q=55.70          |                  | A=21.0           | T <sub>c</sub> =15.35 |               | ADD RUN 25.2          |      |   |   |
| 2281         | 2281   | 1    |                  |                  |                  |                       |               | 2 OF 2                |      |   |   |
| 2281         | 2222   | 3    | 1234             | 1115             | 400              |                       |               |                       |      |   |   |
| 2222         | 2222   | 10   |                  |                  |                  |                       |               | SAVE TO BANK 1 - 2222 |      |   |   |
| 2221         | 2220   | 2    | 1430             | 1403             | 100              | 0.35                  | 0.87          |                       |      |   |   |
| 2220         | 2219   | 5    | 1403             | 1225             | 770              | 0.35                  | 16.08         |                       |      |   |   |
| 2219         | 2219   | 10   |                  |                  |                  |                       |               | SAVE TO BANK 2 - 2219 |      |   |   |
| 2231         | 2230   | 2    | 1314             | 1310             | 95.00            | 0.57                  | 0.17          |                       |      |   |   |
| 2230         | 2229   | 6    | 1310             | 1300             | 385              | 0.57                  | 2.33          | 1 Side                |      |   |   |
| 2229         | 2229.8 | 3    | 1294             | 1293             | 105              |                       |               |                       |      |   |   |
| 2229         | 2229.8 | 8    |                  |                  |                  | 0.57                  | 0.47          |                       |      |   |   |
| 2229.8       | 2215   | 3    | 1293             | 1291             | 235              |                       |               |                       |      |   |   |
| 2215         | 2215   | 1    |                  |                  |                  |                       |               | 1 of 3                |      |   |   |
| 2218         | 2217   | 2    | 1344             | 1342             | 80               | 0.88                  | 0.15          |                       |      |   |   |
| 2217         | 2216   | 6    | 1342             | 1321             | 410              | 0.55                  | 0.82          | 1 SIDE                |      |   |   |
| 2216         | 2215   | 3    | 1315             | 1291             | 340              |                       |               |                       |      |   |   |
| 2215         | 2215   | 1    |                  |                  |                  |                       |               | 2 of 3                |      |   |   |
| 2214         | 2213   | 2    | 1321             | 1315             | 97.50            | 0.57                  | 0.26          |                       |      |   |   |
| 2213         | 2215   | 6    | 1315             | 1305             | 225              | 0.57                  | 0.54          | 1 SIDE                |      |   |   |
| 2215         | 2215   | 1    |                  |                  |                  |                       |               | 3 of 3                |      |   |   |
| 2215         | 2212   | 3    | 1291             | 1287             | 50               |                       |               |                       |      |   |   |
| 2212         | 2219   | 5    | 1287             | 1225             | 270              |                       | *             |                       |      |   |   |
| 2219         | 2219   | 11   |                  |                  |                  |                       |               | ADD BANK 2 - 2219     |      |   |   |
| 2219         | 2219   | 12   |                  |                  |                  |                       |               | CLEAR BANK 2          |      |   |   |
| 2219         | 2222   | 5    | 1225             | 1115             | 500              | 0.35                  | 6.26          |                       |      |   |   |
| 2222         | 2222   | 11   |                  |                  |                  |                       |               | ADD BANK 1 - 2222     |      |   |   |
| 2222         | 2222   | 12   |                  |                  |                  |                       |               | CLEAR BANK 1          |      |   |   |
| 2222         | 2209   | 5    | 1115             | 960              | 1140             | 0.35                  | 30.46         |                       |      |   |   |
| 2209         | 2208.8 | 3    | 954              | 942              | 140              |                       |               |                       |      |   |   |
| 2208.8       | 2208.8 | 1    |                  |                  |                  |                       |               | 1 of 2                |      |   |   |
| 2203         | 2202   | 2    | 1210             | 1165             | 100              | 0.25                  | 0.27          |                       |      |   |   |
| 2202         | 2201   | 5    | 1165             | 945              | 665              | 0.25                  | 6.32          |                       |      |   |   |
| 2201         | 2208.8 | 3    | 945              | 942              | 225              |                       |               |                       |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* NEWLAND SIERRA - BASIN 25 - SUBBASIN 25.1 \*  
\* RESULTS TO BE INSERTED AS CODE 7 INTO RUN 25 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-25-1.DAT  
TIME/DATE OF STUDY: 10:27 02/15/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1372.00 TO NODE 1371.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1315.00  
DOWNSTREAM ELEVATION(FEET) = 1313.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.880  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.506  
SUBAREA RUNOFF(CFS) = 0.94  
TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.94

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1371.00 TO NODE 1368.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1313.00 DOWNSTREAM(FEET) = 1296.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 570.00 CHANNEL SLOPE = 0.0298  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.020  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.58  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.39  
AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 2.81  
Tc(MIN.) = 9.69  
SUBAREA AREA(ACRES) = 1.71 SUBAREA RUNOFF(CFS) = 5.25  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.511  
TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 6.00

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.40 FLOW VELOCITY(FEET/SEC.) = 3.95  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1368.00 = 650.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1368.00 TO NODE 1364.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1290.00  DOWNSTREAM(FEET) = 1287.00
FLOW LENGTH(FEET) = 100.00  MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.89
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.00
PIPE TRAVEL TIME(MIN.) = 0.19  Tc(MIN.) = 9.87
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1364.00 = 750.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 1364.00 TO NODE 1364.00 IS CODE = 1
-----

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.87
RAINFALL INTENSITY(INCH/HR) = 5.95
TOTAL STREAM AREA(ACRES) = 1.95
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.00

```

```

*****
FLOW PROCESS FROM NODE 1367.00 TO NODE 1366.00 IS CODE = 21
-----

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1312.00
DOWNSTREAM ELEVATION(FEET) = 1310.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423
SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 0.12  TOTAL RUNOFF(CFS) = 0.45

```

```

*****
FLOW PROCESS FROM NODE 1366.00 TO NODE 1365.00 IS CODE = 62
-----

```

```

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

```

```

=====
UPSTREAM ELEVATION(FEET) = 1310.00  DOWNSTREAM ELEVATION(FEET) = 1294.00

```



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STREET LENGTH(FEET) = 495.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.15  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.18  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.40  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.92  
STREET FLOW TRAVEL TIME(MIN.) = 2.43 Tc(MIN.) = 9.42  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.127  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 1.08 SUBAREA RUNOFF(CFS) = 3.37  
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 3.75

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.24  
FLOW VELOCITY(FEET/SEC.) = 3.86 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.20  
LONGEST FLOWPATH FROM NODE 1367.00 TO NODE 1365.00 = 575.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1365.00 TO NODE 1364.00 IS CODE = 31

-----

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1288.00 DOWNSTREAM(FEET) = 1287.00  
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.11  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.75  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 9.49  
LONGEST FLOWPATH FROM NODE 1367.00 TO NODE 1364.00 = 605.00 FEET.

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\*\*\*\*\*

FLOW PROCESS FROM NODE 1364.00 TO NODE 1364.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.49
RAINFALL INTENSITY(INCH/HR) = 6.10
TOTAL STREAM AREA(ACRES) = 1.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.75

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 9.66 Tc(MIN.) = 9.87
TOTAL AREA(ACRES) = 3.2
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1364.00 = 750.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1364.00 TO NODE 1360.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1287.00 DOWNSTREAM(FEET) = 1279.00
FLOW LENGTH(FEET) = 240.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.45
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.66
PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 10.26
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1360.00 = 990.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1360.00 TO NODE 1360.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.26  
RAINFALL INTENSITY(INCH/HR) = 5.80  
TOTAL STREAM AREA(ACRES) = 3.15  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1363.00 TO NODE 1362.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1311.00  
DOWNSTREAM ELEVATION(FEET) = 1309.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.38  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1362.00 TO NODE 1361.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1309.00 DOWNSTREAM ELEVATION(FEET) = 1289.00  
STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.68  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 5.98  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.86  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.95  
STREET FLOW TRAVEL TIME(MIN.) = 1.83 Tc(MIN.) = 8.83  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.389  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 2.02 SUBAREA RUNOFF(CFS) = 6.58  
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 6.91

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.17  
FLOW VELOCITY(FEET/SEC.) = 4.39 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.27  
LONGEST FLOWPATH FROM NODE 1363.00 TO NODE 1361.00 = 505.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1361.00 TO NODE 1360.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1283.00 DOWNSTREAM(FEET) = 1279.00  
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.84  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.91  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 8.86  
LONGEST FLOWPATH FROM NODE 1363.00 TO NODE 1360.00 = 535.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1360.00 TO NODE 1360.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.86  
RAINFALL INTENSITY(INCH/HR) = 6.37  
TOTAL STREAM AREA(ACRES) = 2.12

PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.91

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.66         | 10.26     | 5.802                 | 3.15        |
| 2             | 6.91         | 8.86      | 6.374                 | 2.12        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 15.70        | 8.86      | 6.374                 |
| 2             | 15.94        | 10.26     | 5.802                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.94 Tc(MIN.) = 10.26  
TOTAL AREA(ACRES) = 5.3  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1360.00 = 990.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1360.00 TO NODE 1356.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1279.00 DOWNSTREAM(FEET) = 1276.00  
FLOW LENGTH(FEET) = 240.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.95  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.94  
PIPE TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 10.76  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1356.00 = 1230.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1356.00 TO NODE 1356.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.76  
RAINFALL INTENSITY(INCH/HR) = 5.63  
TOTAL STREAM AREA(ACRES) = 5.27  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.94

\*\*\*\*\*

FLOW PROCESS FROM NODE 1370.00 TO NODE 1369.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00

UPSTREAM ELEVATION(FEET) = 1308.00

DOWNSTREAM ELEVATION(FEET) = 1306.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.731

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.42

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*

FLOW PROCESS FROM NODE 1369.00 TO NODE 1359.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1306.00 DOWNSTREAM ELEVATION(FEET) = 1282.00

STREET LENGTH(FEET) = 1070.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.48

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.34

HALFSTREET FLOOD WIDTH(FEET) = 10.78

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.50

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.20

STREET FLOW TRAVEL TIME(MIN.) = 5.10 Tc(MIN.) = 9.83

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.962

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 2.59 SUBAREA RUNOFF(CFS) = 7.88  
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 8.15

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.78  
FLOW VELOCITY(FEET/SEC.) = 4.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.62  
LONGEST FLOWPATH FROM NODE 1370.00 TO NODE 1359.00 = 1120.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1359.00 TO NODE 1356.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1276.50 DOWNSTREAM(FEET) = 1276.00  
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.26  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.15  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 9.88  
LONGEST FLOWPATH FROM NODE 1370.00 TO NODE 1356.00 = 1145.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1356.00 TO NODE 1356.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.88  
RAINFALL INTENSITY(INCH/HR) = 5.94  
TOTAL STREAM AREA(ACRES) = 2.68  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.15

\*\*\*\*\*

FLOW PROCESS FROM NODE 1358.00 TO NODE 1357.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 1290.00

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DOWNSTREAM ELEVATION(FEET) = 1288.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.262
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.976
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.16

\*\*\*\*\*

FLOW PROCESS FROM NODE 1357.00 TO NODE 1356.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1288.00 DOWNSTREAM(FEET) = 1281.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.0175
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.118

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.49
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.09
AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 3.18
Tc(MIN.) = 9.45
SUBAREA AREA(ACRES) = 0.81 SUBAREA RUNOFF(CFS) = 2.63
AREA-AVERAGE RUNOFF COEFFICIENT = 0.529
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.75

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 2.60
LONGEST FLOWPATH FROM NODE 1358.00 TO NODE 1356.00 = 470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1356.00 TO NODE 1356.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 9.45
RAINFALL INTENSITY(INCH/HR) = 6.12
TOTAL STREAM AREA(ACRES) = 0.85
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.75

\*\* CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA



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|------------|-------|--------|-------------|--------|
| NUMBER     | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
| 1          | 15.94 | 10.76  | 5.625       | 5.27   |
| 2          | 8.15  | 9.88   | 5.943       | 2.68   |
| 3          | 2.75  | 9.45   | 6.118       | 0.85   |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 25.20        | 9.45      | 6.118                 |
| 2             | 25.91        | 9.88      | 5.943                 |
| 3             | 26.19        | 10.76     | 5.625                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.19 Tc(MIN.) = 10.76  
 TOTAL AREA(ACRES) = 8.8  
 LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1356.00 = 1230.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1356.00 TO NODE 1353.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1275.00 DOWNSTREAM(FEET) = 1270.00  
 FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.16  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 26.19  
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 10.81  
 LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1353.50 = 1285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1353.50 TO NODE 1353.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.81  
 RAINFALL INTENSITY(INCH/HR) = 5.61  
 TOTAL STREAM AREA(ACRES) = 8.80  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 26.19

\*\*\*\*\*

FLOW PROCESS FROM NODE 1355.00 TO NODE 1354.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00
UPSTREAM ELEVATION(FEET) = 1290.00
DOWNSTREAM ELEVATION(FEET) = 1288.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.262
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.976
SUBAREA RUNOFF(CFS) = 0.28
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 1354.00 TO NODE 1353.50 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1288.00 DOWNSTREAM(FEET) = 1278.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.0250
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.400

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.10
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.62
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 2.55
Tc(MIN.) = 8.81
SUBAREA AREA(ACRES) = 1.08 SUBAREA RUNOFF(CFS) = 3.59
AREA-AVERAGE RUNOFF COEFFICIENT = 0.519
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 3.82

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 FLOW VELOCITY(FEET/SEC.) = 3.24
LONGEST FLOWPATH FROM NODE 1355.00 TO NODE 1353.50 = 470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1353.50 TO NODE 1353.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.81  
RAINFALL INTENSITY(INCH/HR) = 6.40  
TOTAL STREAM AREA(ACRES) = 1.15  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.82

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 26.19        | 10.81     | 5.609                 | 8.80        |
| 2             | 3.82         | 8.81      | 6.400                 | 1.15        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 26.77        | 8.81      | 6.400                 |
| 2             | 29.54        | 10.81     | 5.609                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 29.54 Tc(MIN.) = 10.81  
TOTAL AREA(ACRES) = 10.0  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 1353.50 = 1285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1353.50 TO NODE 2296.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1270.00 DOWNSTREAM(FEET) = 1260.00  
FLOW LENGTH(FEET) = 1050.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.55  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 29.54  
PIPE TRAVEL TIME(MIN.) = 2.05 Tc(MIN.) = 12.85  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2296.50 = 2335.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2296.50 TO NODE 2296.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

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CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.85  
RAINFALL INTENSITY(INCH/HR) = 5.02  
TOTAL STREAM AREA(ACRES) = 9.95  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 29.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 2299.00 TO NODE 2298.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1273.00  
DOWNSTREAM ELEVATION(FEET) = 1271.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.45  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 2298.00 TO NODE 2297.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1271.00 DOWNSTREAM ELEVATION(FEET) = 1269.00  
STREET LENGTH(FEET) = 215.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.17

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.27

HALFSTREET FLOOD WIDTH(FEET) = 7.18

AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.84

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.50

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STREET FLOW TRAVEL TIME(MIN.) = 1.94 Tc(MIN.) = 8.94  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.338

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.44 SUBAREA RUNOFF(CFS) = 1.42  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 1.81

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.77  
FLOW VELOCITY(FEET/SEC.) = 2.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.62  
LONGEST FLOWPATH FROM NODE 2299.00 TO NODE 2297.00 = 295.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2297.00 TO NODE 2296.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1260.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.08  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.81  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.05  
LONGEST FLOWPATH FROM NODE 2299.00 TO NODE 2296.50 = 345.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2296.50 TO NODE 2296.50 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.05  
RAINFALL INTENSITY(INCH/HR) = 6.29  
TOTAL STREAM AREA(ACRES) = 0.56  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.81

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 29.54        | 12.85     | 5.015                 | 9.95        |
| 2             | 1.81         | 9.05      | 6.291                 | 0.56        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 25.36        | 9.05      | 6.291                 |
| 2             | 30.98        | 12.85     | 5.015                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 30.98 Tc(MIN.) = 12.85  
TOTAL AREA(ACRES) = 10.5  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2296.50 = 2335.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2296.50 TO NODE 2296.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1260.00 DOWNSTREAM(FEET) = 1258.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.59  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 30.98  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 12.95  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2296.00 = 2410.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2296.00 TO NODE 2296.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.95  
RAINFALL INTENSITY(INCH/HR) = 4.99  
TOTAL STREAM AREA(ACRES) = 10.51  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2295.00 TO NODE 2294.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 1272.00  
 DOWNSTREAM ELEVATION(FEET) = 1270.00  
 ELEVATION DIFFERENCE(FEET) = 2.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
 SUBAREA RUNOFF(CFS) = 0.38  
 TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 2294.00 TO NODE 2293.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====  
 UPSTREAM ELEVATION(FEET) = 1270.00 DOWNSTREAM ELEVATION(FEET) = 1265.00  
 STREET LENGTH(FEET) = 225.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.27  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.25  
 HALFSTREET FLOOD WIDTH(FEET) = 5.98  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.67  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.66  
 STREET FLOW TRAVEL TIME(MIN.) = 1.40 Tc(MIN.) = 8.40  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.598

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
 SUBAREA AREA(ACRES) = 0.53 SUBAREA RUNOFF(CFS) = 1.78  
 TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.12

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.78  
 FLOW VELOCITY(FEET/SEC.) = 2.93 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.83

LONGEST FLOWPATH FROM NODE 2295.00 TO NODE 2293.00 = 305.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2293.00 TO NODE 2296.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1259.00 DOWNSTREAM(FEET) = 1258.00
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.22
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.12
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 8.51
LONGEST FLOWPATH FROM NODE 2295.00 TO NODE 2296.00 = 345.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2296.00 TO NODE 2296.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.51
RAINFALL INTENSITY(INCH/HR) = 6.54
TOTAL STREAM AREA(ACRES) = 0.63
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.12

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 32.60 Tc(MIN.) = 12.95



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TOTAL AREA(ACRES) = 11.1  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2296.00 = 2410.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2296.00 TO NODE 2292.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1258.00 DOWNSTREAM(FEET) = 1257.00  
FLOW LENGTH(FEET) = 90.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.27  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 32.60  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 13.12  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2292.00 = 2500.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2292.00 TO NODE 2292.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2498.00 TO NODE 2497.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1295.00  
DOWNSTREAM ELEVATION(FEET) = 1292.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914  
SUBAREA RUNOFF(CFS) = 0.68  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.68

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2497.00 TO NODE 2496.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1292.00 DOWNSTREAM(FEET) = 1291.00

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CHANNEL LENGTH THRU SUBAREA(FEET) = 175.00 CHANNEL SLOPE = 0.0057  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.896  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.66  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.93  
AVERAGE FLOW DEPTH(FEET) = 0.48 TRAVEL TIME(MIN.) = 1.51  
Tc(MIN.) = 7.85  
SUBAREA AREA(ACRES) = 1.51 SUBAREA RUNOFF(CFS) = 5.94  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 6.53

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.66 FLOW VELOCITY(FEET/SEC.) = 2.29  
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2496.00 = 270.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2496.00 TO NODE 2495.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1285.00 DOWNSTREAM(FEET) = 1279.00  
FLOW LENGTH(FEET) = 230.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.63  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.53  
PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 8.29  
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2495.00 = 500.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2495.00 TO NODE 2495.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.29  
RAINFALL INTENSITY(INCH/HR) = 6.66  
TOTAL STREAM AREA(ACRES) = 1.66  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2491.00 TO NODE 2490.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5400
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1288.00
DOWNSTREAM ELEVATION(FEET) = 1286.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.643
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.677
SUBAREA RUNOFF(CFS) = 0.46
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 2490.00 TO NODE 2495.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1286.00 DOWNSTREAM ELEVATION(FEET) = 1285.00
STREET LENGTH(FEET) = 80.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.06
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.25
HALFSTREET FLOOD WIDTH(FEET) = 6.38
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.03
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.51
STREET FLOW TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 7.30
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.224

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.518
SUBAREA AREA(ACRES) = 0.33 SUBAREA RUNOFF(CFS) = 1.22

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TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.64

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.91
FLOW VELOCITY(FEET/SEC.) = 2.21 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.63
LONGEST FLOWPATH FROM NODE 2491.00 TO NODE 2495.00 = 160.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2495.00 TO NODE 2495.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.30
RAINFALL INTENSITY(INCH/HR) = 7.22
TOTAL STREAM AREA(ACRES) = 0.44
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.64

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.04 Tc(MIN.) = 8.29
TOTAL AREA(ACRES) = 2.1
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2495.00 = 500.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2495.00 TO NODE 2495.80 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1279.00 DOWNSTREAM(FEET) = 1265.00
FLOW LENGTH(FEET) = 535.00 MANNING'S N = 0.013

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ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.04  
PIPE TRAVEL TIME(MIN.) = 0.98 Tc(MIN.) = 9.27  
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2495.80 = 1035.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2495.80 TO NODE 2495.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.27  
RAINFALL INTENSITY(INCH/HR) = 6.19  
TOTAL STREAM AREA(ACRES) = 2.10  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.04

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2291.00 TO NODE 2290.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1277.00  
DOWNSTREAM ELEVATION(FEET) = 1276.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 0.40  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.40

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2290.00 TO NODE 2289.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1276.00 DOWNSTREAM ELEVATION(FEET) = 1268.00  
STREET LENGTH(FEET) = 220.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

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INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.37  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.45  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.30  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.78  
STREET FLOW TRAVEL TIME(MIN.) = 1.11 Tc(MIN.) = 8.53  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.534  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.58 SUBAREA RUNOFF(CFS) = 1.93  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.30

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.18  
FLOW VELOCITY(FEET/SEC.) = 3.63 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.98  
LONGEST FLOWPATH FROM NODE 2291.00 TO NODE 2289.00 = 285.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2289.00 TO NODE 2495.80 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1268.00 DOWNSTREAM(FEET) = 1265.00  
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.57  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.30  
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 8.81  
LONGEST FLOWPATH FROM NODE 2291.00 TO NODE 2495.80 = 395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2495.80 TO NODE 2495.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.81
RAINFALL INTENSITY(INCH/HR) = 6.40
TOTAL STREAM AREA(ACRES) = 0.69
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.30

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.04         | 9.27      | 6.193                 | 2.10        |
| 2             | 2.30         | 8.81      | 6.400                 | 0.69        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 10.08        | 8.81      | 6.400                 |
| 2             | 10.27        | 9.27      | 6.193                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 10.27 Tc(MIN.) = 9.27
TOTAL AREA(ACRES) = 2.8
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2495.80 = 1035.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2495.80 TO NODE 2288.00 IS CODE = 31

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1265.00 DOWNSTREAM(FEET) = 1263.00
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.37
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.27
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 9.49
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2288.00 = 1145.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2288.00 TO NODE 2288.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.49  
RAINFALL INTENSITY(INCH/HR) = 6.10  
TOTAL STREAM AREA(ACRES) = 2.79  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.27

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2287.00 TO NODE 2286.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 66.67  
UPSTREAM ELEVATION(FEET) = 1277.00  
DOWNSTREAM ELEVATION(FEET) = 1276.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.575  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.054  
SUBAREA RUNOFF(CFS) = 0.29  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2286.00 TO NODE 2285.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1276.00 DOWNSTREAM ELEVATION(FEET) = 1269.00  
STREET LENGTH(FEET) = 230.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.23  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.23  
HALFSTREET FLOOD WIDTH(FEET) = 5.38



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AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.02  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.71  
STREET FLOW TRAVEL TIME(MIN.) = 1.27 Tc(MIN.) = 8.84  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.383

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.58 SUBAREA RUNOFF(CFS) = 1.89  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.15

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.24  
FLOW VELOCITY(FEET/SEC.) = 3.34 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.91  
LONGEST FLOWPATH FROM NODE 2287.00 TO NODE 2285.00 = 296.67 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2285.00 TO NODE 2288.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1260.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.22  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.15  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 8.92  
LONGEST FLOWPATH FROM NODE 2287.00 TO NODE 2288.00 = 336.67 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2288.00 TO NODE 2288.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.92  
RAINFALL INTENSITY(INCH/HR) = 6.35  
TOTAL STREAM AREA(ACRES) = 0.66  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.15

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

|   |       |      |            |      |
|---|-------|------|------------|------|
|   |       |      | P-25-1.TXT |      |
| 1 | 10.27 | 9.49 | 6.101      | 2.79 |
| 2 | 2.15  | 8.92 | 6.350      | 0.66 |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.01        | 8.92      | 6.350                 |
| 2             | 12.33        | 9.49      | 6.101                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.33 Tc(MIN.) = 9.49  
TOTAL AREA(ACRES) = 3.4  
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2288.00 = 1145.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2288.00 TO NODE 2292.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1260.00 DOWNSTREAM(FEET) = 1257.00  
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.99  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.33  
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 9.77  
LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2292.00 = 1295.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2292.00 TO NODE 2292.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK #1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.33        | 9.77      | 5.988                 | 3.45        |

LONGEST FLOWPATH FROM NODE 2498.00 TO NODE 2292.00 = 1295.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 32.60        | 13.12     | 4.951                 | 11.14       |

LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2292.00 = 2500.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 36.60        | 9.77      | 5.988                 |
| 2             | 42.79        | 13.12     | 4.951                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 42.79 Tc(MIN.) = 13.12  
 TOTAL AREA(ACRES) = 14.6

\*\*\*\*\*

FLOW PROCESS FROM NODE 2292.00 TO NODE 2292.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 2292.00 TO NODE 2284.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1257.00 DOWNSTREAM(FEET) = 1252.00  
 FLOW LENGTH(FEET) = 325.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 22.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.11  
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 42.79  
 PIPE TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 13.60  
 LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2284.00 = 2825.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2284.00 TO NODE 2284.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 13.60  
 RAINFALL INTENSITY(INCH/HR) = 4.84  
 TOTAL STREAM AREA(ACRES) = 14.59  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 42.79

\*\*\*\*\*

FLOW PROCESS FROM NODE 2283.00 TO NODE 2282.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1375.00  
DOWNSTREAM ELEVATION(FEET) = 1350.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.59  
TOTAL AREA(ACRES) = 0.32 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2282.00 TO NODE 2284.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1350.00 DOWNSTREAM(FEET) = 1348.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 420.00 CHANNEL SLOPE = 0.0048  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.104

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.79  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.94  
AVERAGE FLOW DEPTH(FEET) = 0.35 TRAVEL TIME(MIN.) = 2.38  
Tc(MIN.) = 9.48  
SUBAREA AREA(ACRES) = 4.16 SUBAREA RUNOFF(CFS) = 6.35  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 6.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.49 FLOW VELOCITY(FEET/SEC.) = 3.55  
LONGEST FLOWPATH FROM NODE 2283.00 TO NODE 2284.00 = 520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2284.00 TO NODE 2284.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

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CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.48  
RAINFALL INTENSITY(INCH/HR) = 6.10  
TOTAL STREAM AREA(ACRES) = 4.48  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.84

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 42.79        | 13.60     | 4.836                 | 14.59       |
| 2             | 6.84         | 9.48      | 6.104                 | 4.48        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 36.65        | 9.48      | 6.104                 |
| 2             | 48.21        | 13.60     | 4.836                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 48.21 Tc(MIN.) = 13.60  
TOTAL AREA(ACRES) = 19.1  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2284.00 = 2825.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2284.00 TO NODE 2281.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1252.00 DOWNSTREAM(FEET) = 1234.00  
FLOW LENGTH(FEET) = 205.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 22.26  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 48.21  
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 13.76  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2281.00 = 3030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2281.00 TO NODE 2281.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

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TIME OF CONCENTRATION(MIN.) = 13.76  
RAINFALL INTENSITY(INCH/HR) = 4.80  
TOTAL STREAM AREA(ACRES) = 19.07  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 48.21

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2281.00 TO NODE 2281.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 15.35 RAIN INTENSITY(INCH/HOUR) = 4.47  
TOTAL AREA(ACRES) = 21.00 TOTAL RUNOFF(CFS) = 55.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2281.00 TO NODE 2281.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.35  
RAINFALL INTENSITY(INCH/HR) = 4.47  
TOTAL STREAM AREA(ACRES) = 21.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 55.70

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 48.21        | 13.76     | 4.801                 | 19.07       |
| 2             | 55.70        | 15.35     | 4.473                 | 21.00       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 98.12        | 13.76     | 4.801                 |
| 2             | 100.62       | 15.35     | 4.473                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 100.62 Tc(MIN.) = 15.35  
TOTAL AREA(ACRES) = 40.1  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2281.00 = 3030.00 FEET.

\*\*\*\*\*

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FLOW PROCESS FROM NODE 2281.00 TO NODE 2222.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1234.00 DOWNSTREAM(FEET) = 1115.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 41.90  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 100.62  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 15.51  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2222.00 = 3430.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2222.00 TO NODE 2222.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2221.00 TO NODE 2220.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1430.00  
DOWNSTREAM ELEVATION(FEET) = 1403.00  
ELEVATION DIFFERENCE(FEET) = 27.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 2.43  
TOTAL AREA(ACRES) = 0.87 TOTAL RUNOFF(CFS) = 2.43

\*\*\*\*\*

FLOW PROCESS FROM NODE 2220.00 TO NODE 2219.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1403.00 DOWNSTREAM(FEET) = 1225.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 770.00 CHANNEL SLOPE = 0.2312  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 10.00

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.481  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 23.49  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 19.79  
AVERAGE FLOW DEPTH(FEET) = 0.33 TRAVEL TIME(MIN.) = 0.65  
Tc(MIN.) = 6.92  
SUBAREA AREA(ACRES) = 16.08 SUBAREA RUNOFF(CFS) = 42.10  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 17.0 PEAK FLOW RATE(CFS) = 44.38

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.47 FLOW VELOCITY(FEET/SEC.) = 24.08  
LONGEST FLOWPATH FROM NODE 2221.00 TO NODE 2219.00 = 870.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2219.00 TO NODE 2219.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2231.00 TO NODE 2230.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1314.00  
DOWNSTREAM ELEVATION(FEET) = 1310.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.759  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.419  
SUBAREA RUNOFF(CFS) = 0.82  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.82

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2230.00 TO NODE 2229.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

-----  
UPSTREAM ELEVATION(FEET) = 1310.00 DOWNSTREAM ELEVATION(FEET) = 1300.00  
STREET LENGTH(FEET) = 385.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00



DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.59  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.36  
HALFSTREET FLOOD WIDTH(FEET) = 11.47  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.90  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.39  
STREET FLOW TRAVEL TIME(MIN.) = 1.65 Tc(MIN.) = 7.40  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.158

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 2.33 SUBAREA RUNOFF(CFS) = 9.51  
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 10.20

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.66  
FLOW VELOCITY(FEET/SEC.) = 4.50 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.89  
LONGEST FLOWPATH FROM NODE 2231.00 TO NODE 2229.00 = 480.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2229.00 TO NODE 2229.80 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1294.00 DOWNSTREAM(FEET) = 1293.00  
FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.59  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.20  
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 7.67  
LONGEST FLOWPATH FROM NODE 2231.00 TO NODE 2229.80 = 585.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2229.00 TO NODE 2229.80 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.998  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5700  
SUBAREA AREA(ACRES) = 0.47 SUBAREA RUNOFF(CFS) = 1.87  
TOTAL AREA(ACRES) = 3.0 TOTAL RUNOFF(CFS) = 11.85  
TC(MIN.) = 7.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 2229.80 TO NODE 2215.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1293.00 DOWNSTREAM(FEET) = 1291.00  
FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.48  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.85  
PIPE TRAVEL TIME(MIN.) = 0.60 Tc(MIN.) = 8.27  
LONGEST FLOWPATH FROM NODE 2231.00 TO NODE 2215.00 = 820.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2215.00 TO NODE 2215.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.27  
RAINFALL INTENSITY(INCH/HR) = 6.66  
TOTAL STREAM AREA(ACRES) = 2.97  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.85

\*\*\*\*\*

FLOW PROCESS FROM NODE 2218.00 TO NODE 2217.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1344.00

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DOWNSTREAM ELEVATION(FEET) = 1342.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.610  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.22  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 1.22

\*\*\*\*\*

FLOW PROCESS FROM NODE 2217.00 TO NODE 2216.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1342.00 DOWNSTREAM ELEVATION(FEET) = 1321.00  
STREET LENGTH(FEET) = 410.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.30  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.84  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.50  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.27  
STREET FLOW TRAVEL TIME(MIN.) = 1.52 Tc(MIN.) = 4.13

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.601  
SUBAREA AREA(ACRES) = 0.82 SUBAREA RUNOFF(CFS) = 4.16  
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 5.38

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.77  
FLOW VELOCITY(FEET/SEC.) = 5.01 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.61  
LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2216.00 = 490.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2216.00 TO NODE 2215.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1315.00 DOWNSTREAM(FEET) = 1291.00  
FLOW LENGTH(FEET) = 340.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.75  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.38  
PIPE TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 4.61  
LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2215.00 = 830.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2215.00 TO NODE 2215.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.61  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.97  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2214.00 TO NODE 2213.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.50  
UPSTREAM ELEVATION(FEET) = 1321.00  
DOWNSTREAM ELEVATION(FEET) = 1315.00  
ELEVATION DIFFERENCE(FEET) = 6.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.141  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.058  
SUBAREA RUNOFF(CFS) = 1.34  
TOTAL AREA(ACRES) = 0.26 TOTAL RUNOFF(CFS) = 1.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2213.00 TO NODE 2215.00 IS CODE = 62

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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1315.00 DOWNSTREAM ELEVATION(FEET) = 1305.00  
STREET LENGTH(FEET) = 225.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.60  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.24  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.04  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.09  
STREET FLOW TRAVEL TIME(MIN.) = 0.93 Tc(MIN.) = 6.07  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.138

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.54 SUBAREA RUNOFF(CFS) = 2.50  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 3.71

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.57  
FLOW VELOCITY(FEET/SEC.) = 4.35 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.30  
LONGEST FLOWPATH FROM NODE 2214.00 TO NODE 2215.00 = 322.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2215.00 TO NODE 2215.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.07  
RAINFALL INTENSITY(INCH/HR) = 8.14  
TOTAL STREAM AREA(ACRES) = 0.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.71

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.85        | 8.27      | 6.663                 | 2.97        |
| 2             | 5.38         | 4.61      | 9.222                 | 0.97        |
| 3             | 3.71         | 6.07      | 8.138                 | 0.80        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 14.80        | 4.61      | 9.222                 |
| 2             | 17.14        | 6.07      | 8.138                 |
| 3             | 18.77        | 8.27      | 6.663                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 18.77 Tc(MIN.) = 8.27  
 TOTAL AREA(ACRES) = 4.7  
 LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2215.00 = 830.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2215.00 TO NODE 2212.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1291.00 DOWNSTREAM(FEET) = 1287.00  
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 17.07  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 18.77  
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 8.32  
 LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2212.00 = 880.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2212.00 TO NODE 2219.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1287.00 DOWNSTREAM(FEET) = 1225.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 270.00 CHANNEL SLOPE = 0.2296  
 NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION  
 CHANNEL FLOW THRU SUBAREA(CFS) = 18.77

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FLOW VELOCITY(FEET/SEC) = 9.32 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 8.81  
LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2219.00 = 1150.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2219.00 TO NODE 2219.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 18.77        | 8.81      | 6.401                 | 4.74        |

LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2219.00 = 1150.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 44.38        | 6.92      | 7.481                 | 16.95       |

LONGEST FLOWPATH FROM NODE 2221.00 TO NODE 2219.00 = 870.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 59.12        | 6.92      | 7.481                 |
| 2             | 56.74        | 8.81      | 6.401                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 59.12 Tc(MIN.) = 6.92  
TOTAL AREA(ACRES) = 21.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 2219.00 TO NODE 2219.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2219.00 TO NODE 2222.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1225.00 DOWNSTREAM(FEET) = 1115.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 500.00 CHANNEL SLOPE = 0.2200  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 10.00

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.271  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 67.09  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 26.74  
 AVERAGE FLOW DEPTH(FEET) = 0.60 TRAVEL TIME(MIN.) = 0.31  
 Tc(MIN.) = 7.23  
 SUBAREA AREA(ACRES) = 6.26 SUBAREA RUNOFF(CFS) = 15.93  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.388  
 TOTAL AREA(ACRES) = 28.0 PEAK FLOW RATE(CFS) = 78.93

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.65 FLOW VELOCITY(FEET/SEC.) = 28.16  
 LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2222.00 = 1650.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2222.00 TO NODE 2222.00 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
 \*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 78.93        | 7.23      | 7.271                 | 27.95       |

LONGEST FLOWPATH FROM NODE 2218.00 TO NODE 2222.00 = 1650.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 100.62       | 15.51     | 4.443                 | 40.07       |

LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2222.00 = 3430.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 125.82       | 7.23      | 7.271                 |
| 2             | 148.85       | 15.51     | 4.443                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 148.85 Tc(MIN.) = 15.51  
 TOTAL AREA(ACRES) = 68.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 2222.00 TO NODE 2222.00 IS CODE = 12

-----  
 >>>>CLEAR MEMORY BANK # 1 <<<<<



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2222.00 TO NODE 2209.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1115.00 DOWNSTREAM(FEET) = 960.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1140.00 CHANNEL SLOPE = 0.1360  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.257

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 171.56  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 17.82  
AVERAGE FLOW DEPTH(FEET) = 1.57 TRAVEL TIME(MIN.) = 1.07  
Tc(MIN.) = 16.58  
SUBAREA AREA(ACRES) = 30.46 SUBAREA RUNOFF(CFS) = 45.38  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.433  
TOTAL AREA(ACRES) = 98.5 PEAK FLOW RATE(CFS) = 181.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.61 FLOW VELOCITY(FEET/SEC.) = 18.06  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2209.00 = 4570.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2209.00 TO NODE 2208.80 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 954.00 DOWNSTREAM(FEET) = 942.00  
FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 28.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 29.87  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 181.60  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 16.65  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2208.80 = 4710.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2208.80 TO NODE 2208.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.65  
RAINFALL INTENSITY(INCH/HR) = 4.24  
TOTAL STREAM AREA(ACRES) = 98.48  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 181.60

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2203.00 TO NODE 2202.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1210.00  
DOWNSTREAM ELEVATION(FEET) = 1165.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2202.00 TO NODE 2201.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1165.00 DOWNSTREAM(FEET) = 945.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 665.00 CHANNEL SLOPE = 0.3308  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.615  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.74  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.76  
AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 1.27  
Tc(MIN.) = 8.37  
SUBAREA AREA(ACRES) = 6.32 SUBAREA RUNOFF(CFS) = 10.45  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 6.6 PEAK FLOW RATE(CFS) = 10.90

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

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DEPTH(FEET) = 0.28 FLOW VELOCITY(FEET/SEC.) = 10.96  
LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2201.00 = 765.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2201.00 TO NODE 2208.80 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 945.00 DOWNSTREAM(FEET) = 942.00  
FLOW LENGTH(FEET) = 225.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.41  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.90  
PIPE TRAVEL TIME(MIN.) = 0.51 Tc(MIN.) = 8.87  
LONGEST FLOWPATH FROM NODE 2203.00 TO NODE 2208.80 = 990.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2208.80 TO NODE 2208.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.87  
RAINFALL INTENSITY(INCH/HR) = 6.37  
TOTAL STREAM AREA(ACRES) = 6.59  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.90

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 181.60       | 16.65     | 4.244                 | 98.48       |
| 2             | 10.90        | 8.87      | 6.369                 | 6.59        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 107.67       | 8.87      | 6.369                 |
| 2             | 188.87       | 16.65     | 4.244                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 188.87 Tc(MIN.) = 16.65

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TOTAL AREA(ACRES) = 105.1  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2208.80 = 4710.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2208.80 TO NODE 2208.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |                   |                    |        |
|--|-------------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                     | 942.00            | DOWNSTREAM(FEET) = | 924.00 |
| FLOW LENGTH(FEET) =                                  | 110.00            | MANNING'S N =      | 0.013  |
| DEPTH OF FLOW IN                                     | 33.0 INCH PIPE IS | 25.2 INCHES        |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                      | 38.81             |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =                      | 33.00             | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                     | 188.87            |                    |        |
| PIPE TRAVEL TIME(MIN.) =                             | 0.05              | Tc(MIN.) =         | 16.70  |
| LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2208.00 = | 4820.00 FEET.     |                    |        |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2208.00 TO NODE 2208.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

|  |        |
|--|--------|
| TOTAL NUMBER OF STREAMS =                            | 2      |
| CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE: |        |
| TIME OF CONCENTRATION(MIN.) =                        | 16.70  |
| RAINFALL INTENSITY(INCH/HR) =                        | 4.24   |
| TOTAL STREAM AREA(ACRES) =                           | 105.07 |
| PEAK FLOW RATE(CFS) AT CONFLUENCE =                  | 188.87 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2207.00 TO NODE 2206.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

|  |         |                     |      |
|--|---------|---------------------|------|
| USER-SPECIFIED RUNOFF COEFFICIENT =  | .3500   |                     |      |
| S.C.S. CURVE NUMBER (AMC II) =   | 0       |                     |      |
| INITIAL SUBAREA FLOW-LENGTH(FEET) =  | 100.00  |                     |      |
| UPSTREAM ELEVATION(FEET) =   | 1420.00 |                     |      |
| DOWNSTREAM ELEVATION(FEET) =   | 1385.00 |                     |      |
| ELEVATION DIFFERENCE(FEET) =   | 35.00   |                     |      |
| SUBAREA OVERLAND TIME OF FLOW(MIN.) =                                      | 6.267   |                     |      |
| WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION! |         |                     |      |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =                                   | 7.972   |                     |      |
| SUBAREA RUNOFF(CFS) =  | 1.23    |                     |      |
| TOTAL AREA(ACRES) =  | 0.44    | TOTAL RUNOFF(CFS) = | 1.23 |

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2206.00 TO NODE 2205.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1385.00 DOWNSTREAM(FEET) = 945.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1065.00 CHANNEL SLOPE = 0.4131  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.836

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.90  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.52  
AVERAGE FLOW DEPTH(FEET) = 0.22 TRAVEL TIME(MIN.) = 1.69  
Tc(MIN.) = 7.95  
SUBAREA AREA(ACRES) = 5.54 SUBAREA RUNOFF(CFS) = 13.25  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 6.0 PEAK FLOW RATE(CFS) = 14.31

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 FLOW VELOCITY(FEET/SEC.) = 12.84  
LONGEST FLOWPATH FROM NODE 2207.00 TO NODE 2205.00 = 1165.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2205.00 TO NODE 2208.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 939.00 DOWNSTREAM(FEET) = 924.00  
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 25.13  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.31  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 7.99  
LONGEST FLOWPATH FROM NODE 2207.00 TO NODE 2208.00 = 1220.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2208.00 TO NODE 2208.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.99  
RAINFALL INTENSITY(INCH/HR) = 6.82  
TOTAL STREAM AREA(ACRES) = 5.98  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.31

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 188.87       | 16.70     | 4.236                 | 105.07      |
| 2             | 14.31        | 7.99      | 6.816                 | 5.98        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 131.69       | 7.99      | 6.816                 |
| 2             | 197.76       | 16.70     | 4.236                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 197.76 Tc(MIN.) = 16.70  
TOTAL AREA(ACRES) = 111.1  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2208.00 = 4820.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2208.00 TO NODE 2201.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 924.00 DOWNSTREAM(FEET) = 910.00  
FLOW LENGTH(FEET) = 520.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.09  
ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 197.76  
PIPE TRAVEL TIME(MIN.) = 0.43 Tc(MIN.) = 17.13  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2201.10 = 5340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2201.10 TO NODE 2201.10 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

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CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 17.13  
RAINFALL INTENSITY(INCH/HR) = 4.17  
TOTAL STREAM AREA(ACRES) = 111.05  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 197.76

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2201.20 TO NODE 2201.30 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1200.00  
DOWNSTREAM ELEVATION(FEET) = 1160.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.108  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.105  
SUBAREA RUNOFF(CFS) = 0.54  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2201.30 TO NODE 2201.40 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1160.00 DOWNSTREAM(FEET) = 943.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.3617  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.422

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.78  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.20  
AVERAGE FLOW DEPTH(FEET) = 0.27 TRAVEL TIME(MIN.) = 0.89  
Tc(MIN.) = 7.00  
SUBAREA AREA(ACRES) = 7.87 SUBAREA RUNOFF(CFS) = 20.44  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 8.1 PEAK FLOW RATE(CFS) = 20.94

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.40 FLOW VELOCITY(FEET/SEC.) = 13.79

LONGEST FLOWPATH FROM NODE 2201.20 TO NODE 2201.40 = 695.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2201.40 TO NODE 2201.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 937.00 DOWNSTREAM(FEET) = 910.00
FLOW LENGTH(FEET) = 165.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.03
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.94
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 7.12
LONGEST FLOWPATH FROM NODE 2201.20 TO NODE 2201.10 = 860.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2201.10 TO NODE 2201.10 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.12
RAINFALL INTENSITY(INCH/HR) = 7.34
TOTAL STREAM AREA(ACRES) = 8.06
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.94

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 209.64 Tc(MIN.) = 17.13



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TOTAL AREA(ACRES) = 119.1  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2201.10 = 5340.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2201.10 TO NODE 2200.90 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 910.00 DOWNSTREAM(FEET) = 908.00  
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 57.0 INCH PIPE IS 43.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.55  
ESTIMATED PIPE DIAMETER(INCH) = 57.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 209.64  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 17.34  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2200.90 = 5520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2200.90 TO NODE 2200.90 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.34  
RAINFALL INTENSITY(INCH/HR) = 4.14  
TOTAL STREAM AREA(ACRES) = 119.11  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 209.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2199.60 TO NODE 2199.50 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1600.00  
DOWNSTREAM ELEVATION(FEET) = 1584.00  
ELEVATION DIFFERENCE(FEET) = 16.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.39  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.39

\*\*\*\*\*

FLOW PROCESS FROM NODE 2199.50 TO NODE 2199.80 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1584.00 DOWNSTREAM(FEET) = 1118.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1000.00 CHANNEL SLOPE = 0.4660
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.228

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 26.34
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 16.21
AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 1.03
Tc(MIN.) = 7.29
SUBAREA AREA(ACRES) = 20.46 SUBAREA RUNOFF(CFS) = 51.76
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350
TOTAL AREA(ACRES) = 20.6 PEAK FLOW RATE(CFS) = 52.11

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.62 FLOW VELOCITY(FEET/SEC.) = 20.03
LONGEST FLOWPATH FROM NODE 2199.60 TO NODE 2199.80 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2199.80 TO NODE 2199.70 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1118.00 DOWNSTREAM(FEET) = 918.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1355.00 CHANNEL SLOPE = 0.1476
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.457

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3200
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 107.33
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 16.21
AVERAGE FLOW DEPTH(FEET) = 1.22 TRAVEL TIME(MIN.) = 1.39
Tc(MIN.) = 8.69
SUBAREA AREA(ACRES) = 53.29 SUBAREA RUNOFF(CFS) = 110.12
AREA-AVERAGE RUNOFF COEFFICIENT = 0.328
TOTAL AREA(ACRES) = 73.9 PEAK FLOW RATE(CFS) = 156.67

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END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.47 FLOW VELOCITY(FEET/SEC.) = 17.95

LONGEST FLOWPATH FROM NODE 2199.60 TO NODE 2199.70 = 2455.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2199.70 TO NODE 2200.90 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 912.00 DOWNSTREAM(FEET) = 908.00

FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 42.0 INCH PIPE IS 29.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 21.70

ESTIMATED PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 156.67

PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 8.77

LONGEST FLOWPATH FROM NODE 2199.60 TO NODE 2200.90 = 2560.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2200.90 TO NODE 2200.90 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 8.77

RAINFALL INTENSITY(INCH/HR) = 6.42

TOTAL STREAM AREA(ACRES) = 73.89

PEAK FLOW RATE(CFS) AT CONFLUENCE = 156.67

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 209.64       | 17.34     | 4.135                 | 119.11      |
| 2             | 156.67       | 8.77      | 6.419                 | 73.89       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 291.72       | 8.77      | 6.419                 |
| 2             | 310.57       | 17.34     | 4.135                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

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PEAK FLOW RATE(CFS) = 310.57 Tc(MIN.) = 17.34  
TOTAL AREA(ACRES) = 193.0  
LONGEST FLOWPATH FROM NODE 1372.00 TO NODE 2200.90 = 5520.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 193.0 TC(MIN.) = 17.34  
PEAK FLOW RATE(CFS) = 310.57

=====

END OF RATIONAL METHOD ANALYSIS





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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2494         | 2493   | 2    | 1294             | 1292             | 80               | 0.57        | 0.13          |                |      |   |   |
| 2493         | 2272   | 6    | 1294             | 1284.5           | 245              | 0.57        | 0.93          | 1 side         |      |   |   |
| 2272         | 2272   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2280         | 2279   | 2    | 1287             | 1286             | 65               | 0.51        | 0.11          |                |      |   |   |
| 2279         | 2278   | 6    | 1286             | 1285             | 145              | 0.51        | 0.62          | 2 SIDES        |      |   |   |
| 2278         | 2272   | 3    | 1279             | 1278.5           | 55               |             |               |                |      |   |   |
| 2272         | 2272   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2272         | 2277   | 3    | 1278.5           | 1269             | 280              |             |               |                |      |   |   |
| 2277         | 2277   | 1    |                  |                  |                  |             |               | 1 of 3         |      |   |   |
| 2272.8       | 2272.6 | 2    | 1286             | 1284             | 81               | 0.51        | 0.12          |                |      |   |   |
| 2272.6       | 2277   | 6    | 1284             | 1275             | 225              | 0.51        | 1.11          | 1 side         |      |   |   |
| 2277         | 2277   | 1    |                  |                  |                  |             |               | 2 of 3         |      |   |   |
| 2276         | 2275   | 2    | 1284             | 1282             | 85               | 0.51        | 0.05          |                |      |   |   |
| 2275         | 2274   | 6    | 1282             | 1278             | 180              | 0.51        | 0.98          |                |      |   |   |
| 2274         | 2277   | 3    | 1272             | 1269             | 100              |             |               |                |      |   |   |
| 2277         | 2277   | 1    |                  |                  |                  |             |               | 3 of 3         |      |   |   |
| 2277         | 2271   | 3    | 1269             | 1259             | 440              |             |               |                |      |   |   |
| 2271         | 2271   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2271.2       | 2271.3 | 2    | 1272             | 1271             | 65               | 0.51        | 0.12          |                |      |   |   |
| 2271.3       | 2271.4 | 6    | 1271             | 1265             | 210              | 0.51        | 0.65          | 2 SIDES        |      |   |   |
| 2271.4       | 2271   | 3    | 1259             | 1258             | 50               |             |               |                |      |   |   |
| 2271         | 2271   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2271         | 2271   | 10   |                  |                  |                  |             |               | Save to Bank 1 |      |   |   |
| 2250.2       | 2241   | 2    | 1300             | 1295             | 90               | 0.57        | 0.10          |                |      |   |   |
| 2241         | 2240   | 6    | 1295             | 1284             | 525              | 0.54        | 1.78          | 2 sides        |      |   |   |
| 2240         | 2236   | 3    | 1278             | 1277             | 690              |             |               |                |      |   |   |
| 2236         | 2236   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2238         | 2237   | 2    | 1295             | 1292             | 95               | 0.51        | 0.15          |                |      |   |   |
| 2237         | 2236   | 6    | 1292             | 1283             | 295              | 0.51        | 1.09          | 2 sides        |      |   |   |
| 2236         | 2236   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2236         | 2235   | 3    | 1277             | 1276             | 240              |             |               |                |      |   |   |
| 2235         | 2235   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2234         | 2233   | 2    | 1284             | 1283             | 65               | 0.51        | 0.11          |                |      |   |   |
| 2233         | 2235   | 6    | 1283             | 1282             | 95               | 0.51        | 0.55          | 2 SIDES        |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments     | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|--------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |              | 1    | 2 | 3 |
| 2235         | 2235   | 1    |                  |                  |                  |             |               | 2 of 2       |      |   |   |
| 2235         | 2232   | 3    | 1276             | 1274             | 55               |             |               |              |      |   |   |
| 2232         | 2232   | 1    |                  |                  |                  |             |               | 1 of 2       |      |   |   |
| 2227         | 2226   | 2    | 1296             | 1295             | 65               | 0.57        | 0.11          |              |      |   |   |
| 2226         | 2232   | 6    | 1295             | 1274             | 495              | 0.57        | 2.70          | 1 side       |      |   |   |
| 2232         | 2232   | 1    |                  |                  |                  |             |               | 2 of 2       |      |   |   |
| 2232         | 2268.8 | 3    | 1274             | 1267             | 245              |             |               |              |      |   |   |
| 2268.8       | 2268.8 | 1    |                  |                  |                  |             |               | 1 of 2       |      |   |   |
| 2270         | 2269   | 2    | 1278             | 1276             | 83.33            | 0.51        | 0.10          |              |      |   |   |
| 2269         | 2268   | 6    | 1276             | 1275             | 110              | 0.51        | 0.77          | 2 SIDES      |      |   |   |
| 2268         | 2268.8 | 3    | 1269             | 1267             | 105              |             |               |              |      |   |   |
| 2268.8       | 2268.8 | 1    |                  |                  |                  |             |               | 2 of 2       |      |   |   |
| 2268.8       | 2267   | 3    | 1267             | 1262             | 165              |             |               |              |      |   |   |
| 2267         | 2267   | 1    |                  |                  |                  |             |               | 1 of 3       |      |   |   |
| 2266         | 2265   | 2    | 1280             | 1275             | 85               | 0.51        | 0.13          |              |      |   |   |
| 2265         | 2267   | 6    | 1275             | 1270             | 350              | 0.51        | 1.26          | 1 side       |      |   |   |
| 2267         | 2267   | 1    |                  |                  |                  |             |               | 2 of 3       |      |   |   |
| 2264         | 2263   | 2    | 1274             | 1272             | 81.58            | 0.51        | 0.10          |              |      |   |   |
| 2263         | 2262   | 6    | 1272             | 1271             | 125              | 0.51        | 0.35          | 1 SIDE       |      |   |   |
| 2262         | 2267   | 3    | 1265             | 1264             | 65               |             |               |              |      |   |   |
| 2267         | 2267   | 1    |                  |                  |                  |             |               | 3 of 3       |      |   |   |
| 2267         | 2271   | 3    | 1264             | 1258             | 280              |             |               |              |      |   |   |
| 2271         | 2271   | 11   |                  |                  |                  |             |               | Add Bank 1   |      |   |   |
| 2271         | 2271   | 12   |                  |                  |                  |             |               | Clear Bank 1 |      |   |   |
| 2271         | 2261   | 3    | 1258             | 1257.5           | 10               |             |               |              |      |   |   |
| 2261         | 2261   | 1    |                  |                  |                  |             |               | 1 of 3       |      |   |   |
| 2260         | 2259   | 2    | 1278             | 1276             | 80               | 0.51        | 0.13          |              |      |   |   |
| 2259         | 2261   | 6    | 1276             | 1263.5           | 370              | 0.51        | 1.67          | 1 side       |      |   |   |
| 2261         | 2261   | 1    |                  |                  |                  |             |               | 2 of 3       |      |   |   |
| 2258         | 2257   | 2    | 1271             | 1269             | 80               | 0.51        | 0.14          |              |      |   |   |
| 2257         | 2261   | 6    | 1269             | 1263.5           | 250              | 0.51        | 0.89          | 1 side       |      |   |   |
| 2261         | 2261   | 1    |                  |                  |                  |             |               | 3 of 3       |      |   |   |
| 2261         | 2256   | 3    | 1257.5           | 1244             | 170              |             |               |              |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2256         | 2256   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2255         | 2254   | 2    | 1275             | 1274             | 65               | 0.51        | 0.20          |                |      |   |   |
| 2254         | 2253   | 6    | 1274             | 1267             | 295              | 0.51        | 0.54          | 1 SIDE         |      |   |   |
| 2253         | 2256   | 3    | 1261             | 1244             | 340              |             |               |                |      |   |   |
| 2256         | 2256   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2256         | 2252   | 3    | 1244             | 1243             | 125              |             |               |                |      |   |   |
| 2252         | 2252   | 1    |                  |                  |                  |             |               | 1 OF 3         |      |   |   |
| 2251         | 2250   | 2    | 1266             | 1261             | 95               | 0.51        | 0.18          |                |      |   |   |
| 2250         | 2252   | 6    | 1261             | 1249             | 350              | 0.51        | 0.70          | 1 SIDE         |      |   |   |
| 2252         | 2252   | 1    |                  |                  |                  |             |               | 2 OF 3         |      |   |   |
| 2250.2       | 2250.4 | 2    | 1270             | 1265             | 75               | 0.57        | 0.19          |                |      |   |   |
| 2250.4       | 2252   | 6    | 1265             | 1249             | 455              | 0.57        | 1.01          | 1 SIDE         |      |   |   |
| 2252         | 2252   | 1    |                  |                  |                  |             |               | 3 OF 3         |      |   |   |
| 2252         | 2252   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2249         | 2248   | 2    | 1320             | 1314             | 100              | 0.57        | 0.22          |                |      |   |   |
| 2248         | 2247   | 6    | 1314             | 1306             | 100              | 0.57        | 0.20          | 1 SIDE         |      |   |   |
| 2247         | 2246   | 3    | 1300             | 1264             | 440              |             |               |                |      |   |   |
| 2246         | 2246   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2245         | 2244   | 2    | 1294             | 1289             | 100              | 0.57        | 0.19          |                |      |   |   |
| 2244         | 2246   | 6    | 1289             | 1270             | 330              | 0.57        | 0.57          | 1 SIDE         |      |   |   |
| 2246         | 2246   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2246         | 2252   | 3    | 1264             | 1243             | 525              |             |               |                |      |   |   |
| 2252         | 2252   | 11   |                  |                  |                  |             |               | Add Bank 1     |      |   |   |
| 2252         | 2252   | 12   |                  |                  |                  |             |               | Clear Bank 1   |      |   |   |
| 2252         | 2223   | 3    | 1243             | 1242             | 35               |             |               |                |      |   |   |
| 2223         | 2281   | 5    | 1242             | 1240             | 205              |             | *             |                |      |   |   |
|              |        |      |                  |                  |                  |             | 20.95         |                |      |   |   |

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* NEWLAND SIERRA - PROPOSED HYDROLOGY - SUBBASIN 25 \*  
\* RESULTS ARE TO BE ENTERED INTO RUN 25.1 AS A CODE 7 AT NODE 2281 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-25-2.DAT  
TIME/DATE OF STUDY: 10:05 02/15/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0312 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*



\*\*\*\*\*

FLOW PROCESS FROM NODE 2494.00 TO NODE 2493.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 1294.00

DOWNSTREAM ELEVATION(FEET) = 1292.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.287

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.955

SUBAREA RUNOFF(CFS) = 0.59

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 2493.00 TO NODE 2272.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1292.00 DOWNSTREAM ELEVATION(FEET) = 1284.50

STREET LENGTH(FEET) = 245.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.48

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.28

HALFSTREET FLOOD WIDTH(FEET) = 7.78

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.43

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.97

STREET FLOW TRAVEL TIME(MIN.) = 1.19 Tc(MIN.) = 7.48

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.93 SUBAREA RUNOFF(CFS) = 3.77  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 4.30

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.90  
FLOW VELOCITY(FEET/SEC.) = 3.91 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.27  
LONGEST FLOWPATH FROM NODE 2494.00 TO NODE 2272.00 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2272.00 TO NODE 2272.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.48  
RAINFALL INTENSITY(INCH/HR) = 7.11  
TOTAL STREAM AREA(ACRES) = 1.06  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2280.00 TO NODE 2279.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1287.00  
DOWNSTREAM ELEVATION(FEET) = 1286.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 0.40  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 2279.00 TO NODE 2278.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1286.00 DOWNSTREAM ELEVATION(FEET) = 1285.00  
STREET LENGTH(FEET) = 145.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.40  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 5.98  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.47  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.36  
STREET FLOW TRAVEL TIME(MIN.) = 1.65 Tc(MIN.) = 9.06  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.283

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.62 SUBAREA RUNOFF(CFS) = 1.99  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.34

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.71  
FLOW VELOCITY(FEET/SEC.) = 1.64 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.46  
LONGEST FLOWPATH FROM NODE 2280.00 TO NODE 2278.00 = 210.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2278.00 TO NODE 2272.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
-----

ELEVATION DATA: UPSTREAM(FEET) = 1279.00 DOWNSTREAM(FEET) = 1278.50  
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.45  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.34  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 9.27  
LONGEST FLOWPATH FROM NODE 2280.00 TO NODE 2272.00 = 265.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2272.00 TO NODE 2272.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.27
RAINFALL INTENSITY(INCH/HR) = 6.19
TOTAL STREAM AREA(ACRES) = 0.73
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.34

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.19 Tc(MIN.) = 7.48
TOTAL AREA(ACRES) = 1.8
LONGEST FLOWPATH FROM NODE 2494.00 TO NODE 2272.00 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2272.00 TO NODE 2277.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1278.50 DOWNSTREAM(FEET) = 1269.00
FLOW LENGTH(FEET) = 280.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.37
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.19
PIPE TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 7.98
LONGEST FLOWPATH FROM NODE 2494.00 TO NODE 2277.00 = 605.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2277.00 TO NODE 2277.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.98  
RAINFALL INTENSITY(INCH/HR) = 6.82  
TOTAL STREAM AREA(ACRES) = 1.79  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2272.80 TO NODE 2272.60 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 81.00  
UPSTREAM ELEVATION(FEET) = 1286.00  
DOWNSTREAM ELEVATION(FEET) = 1284.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.072  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.374  
SUBAREA RUNOFF(CFS) = 0.45  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2272.60 TO NODE 2277.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1284.00 DOWNSTREAM ELEVATION(FEET) = 1275.00  
STREET LENGTH(FEET) = 225.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.37  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

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STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.11  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.80  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.02  
STREET FLOW TRAVEL TIME(MIN.) = 0.99 Tc(MIN.) = 8.06  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.778

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 1.11 SUBAREA RUNOFF(CFS) = 3.84  
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 4.25

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.30  
FLOW VELOCITY(FEET/SEC.) = 4.32 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.35  
LONGEST FLOWPATH FROM NODE 2272.80 TO NODE 2277.00 = 306.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2277.00 TO NODE 2277.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.06  
RAINFALL INTENSITY(INCH/HR) = 6.78  
TOTAL STREAM AREA(ACRES) = 1.23  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.25

\*\*\*\*\*

FLOW PROCESS FROM NODE 2276.00 TO NODE 2275.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1284.00  
DOWNSTREAM ELEVATION(FEET) = 1282.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.362  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.185  
SUBAREA RUNOFF(CFS) = 0.18  
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 2275.00 TO NODE 2274.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1282.00 DOWNSTREAM ELEVATION(FEET) = 1278.00
STREET LENGTH(FEET) = 180.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.83
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 7.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.85
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.77
STREET FLOW TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 8.41
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.592

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510
SUBAREA AREA(ACRES) = 0.98 SUBAREA RUNOFF(CFS) = 3.29
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 3.46

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.70
FLOW VELOCITY(FEET/SEC.) = 3.27 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.05
LONGEST FLOWPATH FROM NODE 2276.00 TO NODE 2274.00 = 265.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2274.00 TO NODE 2277.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1272.00 DOWNSTREAM(FEET) = 1269.00
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.5 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 7.63  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.46  
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 8.63  
LONGEST FLOWPATH FROM NODE 2276.00 TO NODE 2277.00 = 365.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2277.00 TO NODE 2277.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.63  
RAINFALL INTENSITY(INCH/HR) = 6.48  
TOTAL STREAM AREA(ACRES) = 1.03  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.46

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.19         | 7.98      | 6.824                 | 1.79        |
| 2             | 4.25         | 8.06      | 6.778                 | 1.23        |
| 3             | 3.46         | 8.63      | 6.484                 | 1.03        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 13.59        | 7.98      | 6.824                 |
| 2             | 13.63        | 8.06      | 6.778                 |
| 3             | 13.41        | 8.63      | 6.484                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 13.63 Tc(MIN.) = 8.06  
TOTAL AREA(ACRES) = 4.1  
LONGEST FLOWPATH FROM NODE 2494.00 TO NODE 2277.00 = 605.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2277.00 TO NODE 2271.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1269.00 DOWNSTREAM(FEET) = 1259.00



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FLOW LENGTH(FEET) = 440.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.63  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 13.63  
PIPE TRAVEL TIME(MIN.) = 0.76 Tc(MIN.) = 8.82  
LONGEST FLOWPATH FROM NODE 2494.00 TO NODE 2271.00 = 1045.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2271.00 TO NODE 2271.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.82  
RAINFALL INTENSITY(INCH/HR) = 6.39  
TOTAL STREAM AREA(ACRES) = 4.05  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.63

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2271.20 TO NODE 2271.30 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1272.00  
DOWNSTREAM ELEVATION(FEET) = 1271.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 0.44  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.44

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2271.30 TO NODE 2271.40 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1271.00 DOWNSTREAM ELEVATION(FEET) = 1265.00  
STREET LENGTH(FEET) = 210.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

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INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.51  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.21  
HALFSTREET FLOOD WIDTH(FEET) = 3.99  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.72  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.56  
STREET FLOW TRAVEL TIME(MIN.) = 1.29 Tc(MIN.) = 8.70  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.449  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.65 SUBAREA RUNOFF(CFS) = 2.14  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.53

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.58  
FLOW VELOCITY(FEET/SEC.) = 2.95 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.70  
LONGEST FLOWPATH FROM NODE 2271.20 TO NODE 2271.40 = 275.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2271.40 TO NODE 2271.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1259.00 DOWNSTREAM(FEET) = 1258.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.04  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.53  
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 8.84  
LONGEST FLOWPATH FROM NODE 2271.20 TO NODE 2271.00 = 325.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2271.00 TO NODE 2271.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.84
RAINFALL INTENSITY(INCH/HR) = 6.38
TOTAL STREAM AREA(ACRES) = 0.77
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.53

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 13.63        | 8.82      | 6.395                 | 4.05        |
| 2             | 2.53         | 8.84      | 6.384                 | 0.77        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.15        | 8.82      | 6.395                 |
| 2             | 16.14        | 8.84      | 6.384                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 16.15 Tc(MIN.) = 8.82
TOTAL AREA(ACRES) = 4.8
LONGEST FLOWPATH FROM NODE 2494.00 TO NODE 2271.00 = 1045.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2271.00 TO NODE 2271.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2242.00 TO NODE 2241.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 1300.00
DOWNSTREAM ELEVATION(FEET) = 1295.00
ELEVATION DIFFERENCE(FEET) = 5.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.110

```

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.093  
SUBAREA RUNOFF(CFS) = 0.52  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 2241.00 TO NODE 2240.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1295.00 DOWNSTREAM ELEVATION(FEET) = 1284.00  
STREET LENGTH(FEET) = 525.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.79  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.44  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.82  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.77  
STREET FLOW TRAVEL TIME(MIN.) = 3.11 Tc(MIN.) = 8.22  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.693

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5400  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.542  
SUBAREA AREA(ACRES) = 1.78 SUBAREA RUNOFF(CFS) = 6.43  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 6.82

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.70  
FLOW VELOCITY(FEET/SEC.) = 3.22 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.03  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2240.00 = 615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2240.00 TO NODE 2236.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1278.00 DOWNSTREAM(FEET) = 1277.00  
FLOW LENGTH(FEET) = 690.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.91  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.82  
PIPE TRAVEL TIME(MIN.) = 3.95 Tc(MIN.) = 12.17  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2236.00 = 1305.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2236.00 TO NODE 2236.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.17  
RAINFALL INTENSITY(INCH/HR) = 5.20  
TOTAL STREAM AREA(ACRES) = 1.88  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 2238.00 TO NODE 2237.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1295.00  
DOWNSTREAM ELEVATION(FEET) = 1292.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.056  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.385  
SUBAREA RUNOFF(CFS) = 0.56  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 2237.00 TO NODE 2236.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1292.00 DOWNSTREAM ELEVATION(FEET) = 1283.00  
STREET LENGTH(FEET) = 295.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.36  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.23  
HALFSTREET FLOOD WIDTH(FEET) = 5.25  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.00  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.69  
STREET FLOW TRAVEL TIME(MIN.) = 1.64 Tc(MIN.) = 8.70  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.453

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 1.09 SUBAREA RUNOFF(CFS) = 3.59  
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 4.08

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.04  
FLOW VELOCITY(FEET/SEC.) = 3.32 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.89  
LONGEST FLOWPATH FROM NODE 2238.00 TO NODE 2236.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2236.00 TO NODE 2236.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====  
TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.70  
RAINFALL INTENSITY(INCH/HR) = 6.45  
TOTAL STREAM AREA(ACRES) = 1.24  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.08

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.82         | 12.17     | 5.196                 | 1.88        |
| 2             | 4.08         | 8.70      | 6.453                 | 1.24        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 8.95         | 8.70      | 6.453                 |
| 2             | 10.10        | 12.17     | 5.196                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.10 Tc(MIN.) = 12.17  
TOTAL AREA(ACRES) = 3.1  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2236.00 = 1305.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2236.00 TO NODE 2235.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1277.00 DOWNSTREAM(FEET) = 1276.00  
FLOW LENGTH(FEET) = 240.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.81  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.10  
PIPE TRAVEL TIME(MIN.) = 0.83 Tc(MIN.) = 13.00  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2235.00 = 1545.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2235.00 TO NODE 2235.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.00  
RAINFALL INTENSITY(INCH/HR) = 4.98  
TOTAL STREAM AREA(ACRES) = 3.12  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2234.00 TO NODE 2233.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 1284.00  
 DOWNSTREAM ELEVATION(FEET) = 1283.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
 SUBAREA RUNOFF(CFS) = 0.40  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 2233.00 TO NODE 2235.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1283.00 DOWNSTREAM ELEVATION(FEET) = 1282.00  
 STREET LENGTH(FEET) = 95.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.33  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.23  
 HALFSTREET FLOOD WIDTH(FEET) = 5.12  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.75  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.40  
 STREET FLOW TRAVEL TIME(MIN.) = 0.90 Tc(MIN.) = 8.32  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.640

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
 SUBAREA AREA(ACRES) = 0.55 SUBAREA RUNOFF(CFS) = 1.86  
 TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.23

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 6.85  
 FLOW VELOCITY(FEET/SEC.) = 1.90 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.50



LONGEST FLOWPATH FROM NODE 2234.00 TO NODE 2235.00 = 160.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2235.00 TO NODE 2235.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.32
RAINFALL INTENSITY(INCH/HR) = 6.64
TOTAL STREAM AREA(ACRES) = 0.66
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.23

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 11.78 Tc(MIN.) = 13.00
TOTAL AREA(ACRES) = 3.8
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2235.00 = 1545.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2235.00 TO NODE 2232.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1276.00 DOWNSTREAM(FEET) = 1274.00
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.33
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.78
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 13.08

LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2232.00 = 1600.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2232.00 TO NODE 2232.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.08
RAINFALL INTENSITY(INCH/HR) = 4.96
TOTAL STREAM AREA(ACRES) = 3.78
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 2227.00 TO NODE 2226.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 1296.00
DOWNSTREAM ELEVATION(FEET) = 1295.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.663
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.663
SUBAREA RUNOFF(CFS) = 0.48
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 2226.00 TO NODE 2232.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1295.00 DOWNSTREAM ELEVATION(FEET) = 1274.00
STREET LENGTH(FEET) = 495.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.58

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.33

HALFSTREET FLOOD WIDTH(FEET) = 10.34

AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.69

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.56

STREET FLOW TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 8.42

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.589

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.570

SUBAREA AREA(ACRES) = 2.70 SUBAREA RUNOFF(CFS) = 10.14

TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 10.55

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.47

FLOW VELOCITY(FEET/SEC.) = 5.46 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.16

LONGEST FLOWPATH FROM NODE 2227.00 TO NODE 2232.00 = 560.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2232.00 TO NODE 2232.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 8.42

RAINFALL INTENSITY(INCH/HR) = 6.59

TOTAL STREAM AREA(ACRES) = 2.81

PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.55

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.78        | 13.08     | 4.959                 | 3.78        |
| 2             | 10.55        | 8.42      | 6.589                 | 2.81        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.42        | 8.42      | 6.589                 |

2 19.72 13.08 P-25-2.TXT  
4.959

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.72 Tc(MIN.) = 13.08  
TOTAL AREA(ACRES) = 6.6  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2232.00 = 1600.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2232.00 TO NODE 2268.80 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1274.00 DOWNSTREAM(FEET) = 1267.00  
FLOW LENGTH(FEET) = 245.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.67  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.72  
PIPE TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 13.43  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2268.80 = 1845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2268.80 TO NODE 2268.80 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.43  
RAINFALL INTENSITY(INCH/HR) = 4.88  
TOTAL STREAM AREA(ACRES) = 6.59  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 2270.00 TO NODE 2269.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 83.33  
UPSTREAM ELEVATION(FEET) = 1278.00  
DOWNSTREAM ELEVATION(FEET) = 1276.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.241  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.262

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SUBAREA RUNOFF(CFS) = 0.37  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*

FLOW PROCESS FROM NODE 2269.00 TO NODE 2268.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1276.00 DOWNSTREAM ELEVATION(FEET) = 1275.00  
STREET LENGTH(FEET) = 110.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.68  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 6.12  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.70  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.42  
STREET FLOW TRAVEL TIME(MIN.) = 1.08 Tc(MIN.) = 8.32  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.641

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.77 SUBAREA RUNOFF(CFS) = 2.61  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.95

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.04  
FLOW VELOCITY(FEET/SEC.) = 1.93 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.55  
LONGEST FLOWPATH FROM NODE 2270.00 TO NODE 2268.00 = 193.33 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2268.00 TO NODE 2268.80 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1269.00 DOWNSTREAM(FEET) = 1267.00  
FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.19  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.95  
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 8.60  
LONGEST FLOWPATH FROM NODE 2270.00 TO NODE 2268.80 = 298.33 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2268.80 TO NODE 2268.80 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.60  
RAINFALL INTENSITY(INCH/HR) = 6.50  
TOTAL STREAM AREA(ACRES) = 0.87  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.95

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 19.72        | 13.43     | 4.875                 | 6.59        |
| 2             | 2.95         | 8.60      | 6.500                 | 0.87        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 17.74        | 8.60      | 6.500                 |
| 2             | 21.93        | 13.43     | 4.875                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 21.93 Tc(MIN.) = 13.43  
TOTAL AREA(ACRES) = 7.5  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2268.80 = 1845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2268.80 TO NODE 2267.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1267.00 DOWNSTREAM(FEET) = 1262.00  
FLOW LENGTH(FEET) = 165.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.18  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 21.93  
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 13.66  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2267.00 = 2010.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2267.00 TO NODE 2267.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.66  
RAINFALL INTENSITY(INCH/HR) = 4.82  
TOTAL STREAM AREA(ACRES) = 7.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 1280.00 TO NODE 1275.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1280.00  
DOWNSTREAM ELEVATION(FEET) = 1275.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.424  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.750  
SUBAREA RUNOFF(CFS) = 0.58  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 2265.00 TO NODE 2267.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1275.00 DOWNSTREAM ELEVATION(FEET) = 1270.00  
STREET LENGTH(FEET) = 350.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.85  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.32  
HALFSTREET FLOOD WIDTH(FEET) = 9.77  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.66  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86  
STREET FLOW TRAVEL TIME(MIN.) = 2.19 Tc(MIN.) = 7.62  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.030

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 1.26 SUBAREA RUNOFF(CFS) = 4.52  
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 4.98

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.34  
FLOW VELOCITY(FEET/SEC.) = 3.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.13  
LONGEST FLOWPATH FROM NODE 1280.00 TO NODE 2267.00 = 435.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2267.00 TO NODE 2267.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.62  
RAINFALL INTENSITY(INCH/HR) = 7.03  
TOTAL STREAM AREA(ACRES) = 1.39  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2264.00 TO NODE 2263.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):



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USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 81.58  
UPSTREAM ELEVATION(FEET) = 1274.00  
DOWNSTREAM ELEVATION(FEET) = 1272.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.114  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.346  
SUBAREA RUNOFF(CFS) = 0.37  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*

FLOW PROCESS FROM NODE 2263.00 TO NODE 2262.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1272.00 DOWNSTREAM ELEVATION(FEET) = 1271.00  
STREET LENGTH(FEET) = 125.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.97  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.67  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.44  
STREET FLOW TRAVEL TIME(MIN.) = 1.25 Tc(MIN.) = 8.36  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.620

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.35 SUBAREA RUNOFF(CFS) = 1.18  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.52

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.44  
FLOW VELOCITY(FEET/SEC.) = 1.83 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.54

LONGEST FLOWPATH FROM NODE 2264.00 TO NODE 2262.00 = 206.58 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2262.00 TO NODE 2267.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1265.00 DOWNSTREAM(FEET) = 1264.00
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.74
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.52
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 8.59
LONGEST FLOWPATH FROM NODE 2264.00 TO NODE 2267.00 = 271.58 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2267.00 TO NODE 2267.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 8.59
RAINFALL INTENSITY(INCH/HR) = 6.51
TOTAL STREAM AREA(ACRES) = 0.45
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.52

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1-3.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows 1-3.

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COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.48 Tc(MIN.) = 13.66  
TOTAL AREA(ACRES) = 9.3  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2267.00 = 2010.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2267.00 TO NODE 2271.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1258.00  
FLOW LENGTH(FEET) = 280.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.21  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.48  
PIPE TRAVEL TIME(MIN.) = 0.42 Tc(MIN.) = 14.07  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2271.00 = 2290.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2271.00 TO NODE 2271.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 26.48        | 14.07     | 4.731                 | 9.30        |

LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2271.00 = 2290.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.15        | 8.82      | 6.395                 | 4.82        |

LONGEST FLOWPATH FROM NODE 2494.00 TO NODE 2271.00 = 1045.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 32.75        | 8.82      | 6.395                 |
| 2             | 38.43        | 14.07     | 4.731                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 38.43 Tc(MIN.) = 14.07  
TOTAL AREA(ACRES) = 14.1

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2271.00 TO NODE 2271.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2271.00 TO NODE 2261.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1258.00 DOWNSTREAM(FEET) = 1257.50  
FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.97  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 38.43  
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 14.08  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2261.00 = 2300.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2261.00 TO NODE 2261.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.08  
RAINFALL INTENSITY(INCH/HR) = 4.73  
TOTAL STREAM AREA(ACRES) = 14.12  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 38.43

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2260.00 TO NODE 2259.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1278.00  
DOWNSTREAM ELEVATION(FEET) = 1276.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.49

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 2259.00 TO NODE 2261.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1276.00 DOWNSTREAM ELEVATION(FEET) = 1263.50
STREET LENGTH(FEET) = 370.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.26
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 8.57
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.83
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.14
STREET FLOW TRAVEL TIME(MIN.) = 1.61 Tc(MIN.) = 8.61
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.495

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510
SUBAREA AREA(ACRES) = 1.67 SUBAREA RUNOFF(CFS) = 5.53
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 5.96

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.16
FLOW VELOCITY(FEET/SEC.) = 4.38 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.53
LONGEST FLOWPATH FROM NODE 2260.00 TO NODE 2261.00 = 450.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2261.00 TO NODE 2261.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

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TIME OF CONCENTRATION(MIN.) = 8.61  
RAINFALL INTENSITY(INCH/HR) = 6.49  
TOTAL STREAM AREA(ACRES) = 1.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.96

\*\*\*\*\*

FLOW PROCESS FROM NODE 2258.00 TO NODE 2257.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1271.00  
DOWNSTREAM ELEVATION(FEET) = 1269.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2257.00 TO NODE 2261.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1269.00 DOWNSTREAM ELEVATION(FEET) = 1263.50  
STREET LENGTH(FEET) = 250.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.03  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.64  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.89  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.81  
STREET FLOW TRAVEL TIME(MIN.) = 1.44 Tc(MIN.) = 8.44

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.578  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
 SUBAREA AREA(ACRES) = 0.89 SUBAREA RUNOFF(CFS) = 2.99  
 TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 3.46

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.70  
 FLOW VELOCITY(FEET/SEC.) = 3.26 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.04  
 LONGEST FLOWPATH FROM NODE 2258.00 TO NODE 2261.00 = 330.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2261.00 TO NODE 2261.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.44  
 RAINFALL INTENSITY(INCH/HR) = 6.58  
 TOTAL STREAM AREA(ACRES) = 1.03  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.46

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 38.43        | 14.08     | 4.729                 | 14.12       |
| 2             | 5.96         | 8.61      | 6.495                 | 1.80        |
| 3             | 3.46         | 8.44      | 6.578                 | 1.03        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 32.34        | 8.44      | 6.578                 |
| 2             | 32.87        | 8.61      | 6.495                 |
| 3             | 45.25        | 14.08     | 4.729                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 45.25 Tc(MIN.) = 14.08  
 TOTAL AREA(ACRES) = 17.0  
 LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2261.00 = 2300.00 FEET.

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2261.00 TO NODE 2256.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1257.50 DOWNSTREAM(FEET) = 1244.00  
FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.12  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 45.25  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 14.22  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2256.00 = 2470.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2256.00 TO NODE 2256.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.22  
RAINFALL INTENSITY(INCH/HR) = 4.70  
TOTAL STREAM AREA(ACRES) = 16.95  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 45.25

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2255.00 TO NODE 2254.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1275.00  
DOWNSTREAM ELEVATION(FEET) = 1274.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 0.73  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2254.00 TO NODE 2253.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<



>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1274.00 DOWNSTREAM ELEVATION(FEET) = 1267.00  
STREET LENGTH(FEET) = 295.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.59  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.65  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.84  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.74  
STREET FLOW TRAVEL TIME(MIN.) = 1.73 Tc(MIN.) = 9.15  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.246

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.54 SUBAREA RUNOFF(CFS) = 1.72  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.36

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.04  
FLOW VELOCITY(FEET/SEC.) = 3.08 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.88  
LONGEST FLOWPATH FROM NODE 2255.00 TO NODE 2253.00 = 360.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2253.00 TO NODE 2256.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1261.00 DOWNSTREAM(FEET) = 1244.00  
FLOW LENGTH(FEET) = 340.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.20  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.36

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PIPE TRAVEL TIME(MIN.) = 0.69      Tc(MIN.) = 9.84  
 LONGEST FLOWPATH FROM NODE 2255.00 TO NODE 2256.00 = 700.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2256.00 TO NODE 2256.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.84  
 RAINFALL INTENSITY(INCH/HR) = 5.96  
 TOTAL STREAM AREA(ACRES) = 0.74  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.36

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 45.25        | 14.22     | 4.700                 | 16.95       |
| 2             | 2.36         | 9.84      | 5.960                 | 0.74        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 38.04        | 9.84      | 5.960                 |
| 2             | 47.11        | 14.22     | 4.700                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 47.11      Tc(MIN.) = 14.22  
 TOTAL AREA(ACRES) = 17.7  
 LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2256.00 = 2470.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2256.00 TO NODE 2252.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1244.00      DOWNSTREAM(FEET) = 1243.00  
 FLOW LENGTH(FEET) = 125.00      MANNING'S N = 0.013  
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.96  
 ESTIMATED PIPE DIAMETER(INCH) = 36.00      NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 47.11

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PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 14.45  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2252.00 = 2595.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2252.00 TO NODE 2252.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.45  
RAINFALL INTENSITY(INCH/HR) = 4.65  
TOTAL STREAM AREA(ACRES) = 17.69  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 47.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2251.00 TO NODE 2250.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1266.00  
DOWNSTREAM ELEVATION(FEET) = 1261.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.951  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.242  
SUBAREA RUNOFF(CFS) = 0.76  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.76

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2250.00 TO NODE 2252.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1261.00 DOWNSTREAM ELEVATION(FEET) = 1249.00  
STREET LENGTH(FEET) = 350.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

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Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.01  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.48  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.91  
STREET FLOW TRAVEL TIME(MIN.) = 1.67 Tc(MIN.) = 7.63  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.024

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.70 SUBAREA RUNOFF(CFS) = 2.51  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 3.15

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.44  
FLOW VELOCITY(FEET/SEC.) = 3.80 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.12  
LONGEST FLOWPATH FROM NODE 2251.00 TO NODE 2252.00 = 445.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2252.00 TO NODE 2252.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.63  
RAINFALL INTENSITY(INCH/HR) = 7.02  
TOTAL STREAM AREA(ACRES) = 0.88  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.15

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2250.20 TO NODE 2250.40 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1270.00  
DOWNSTREAM ELEVATION(FEET) = 1265.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.390

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.00  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 1.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 2250.40 TO NODE 2252.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1265.00 DOWNSTREAM ELEVATION(FEET) = 1249.00  
STREET LENGTH(FEET) = 455.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.28  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.51  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.90  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.16  
STREET FLOW TRAVEL TIME(MIN.) = 1.94 Tc(MIN.) = 6.33  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.917

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.01 SUBAREA RUNOFF(CFS) = 4.56  
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 5.42

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.59  
FLOW VELOCITY(FEET/SEC.) = 4.37 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.48  
LONGEST FLOWPATH FROM NODE 2250.20 TO NODE 2252.00 = 530.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2252.00 TO NODE 2252.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 6.33
RAINFALL INTENSITY(INCH/HR) = 7.92
TOTAL STREAM AREA(ACRES) = 1.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.42

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 47.11        | 14.45     | 4.651                 | 17.69       |
| 2             | 3.15         | 7.63      | 7.024                 | 0.88        |
| 3             | 5.42         | 6.33      | 7.917                 | 1.20        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 35.71        | 6.33      | 7.917                 |
| 2             | 39.15        | 7.63      | 7.024                 |
| 3             | 52.38        | 14.45     | 4.651                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 52.38 Tc(MIN.) = 14.45
TOTAL AREA(ACRES) = 19.8
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2252.00 = 2595.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 2252.00 TO NODE 2252.00 IS CODE = 10

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

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*****
FLOW PROCESS FROM NODE 2249.00 TO NODE 2248.00 IS CODE = 21

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1320.00
DOWNSTREAM ELEVATION(FEET) = 1314.00

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ELEVATION DIFFERENCE(FEET) = 6.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.250  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.935  
SUBAREA RUNOFF(CFS) = 1.12  
TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 1.12

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2248.00 TO NODE 2247.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1314.00 DOWNSTREAM ELEVATION(FEET) = 1306.00  
STREET LENGTH(FEET) = 100.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.61  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.22  
HALFSTREET FLOOD WIDTH(FEET) = 4.72  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.72  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.04  
STREET FLOW TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 5.60  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.568

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 0.98  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 2.05

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.52  
FLOW VELOCITY(FEET/SEC.) = 4.85 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.15  
LONGEST FLOWPATH FROM NODE 2249.00 TO NODE 2247.00 = 200.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2247.00 TO NODE 2246.00 IS CODE = 31  
-----

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1300.00 DOWNSTREAM(FEET) = 1264.00  
FLOW LENGTH(FEET) = 440.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.37  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.05  
PIPE TRAVEL TIME(MIN.) = 0.78 Tc(MIN.) = 6.39  
LONGEST FLOWPATH FROM NODE 2249.00 TO NODE 2246.00 = 640.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2246.00 TO NODE 2246.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.39  
RAINFALL INTENSITY(INCH/HR) = 7.88  
TOTAL STREAM AREA(ACRES) = 0.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2245.00 TO NODE 2244.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1294.00  
DOWNSTREAM ELEVATION(FEET) = 128.00  
ELEVATION DIFFERENCE(FEET) = 1166.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.428  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.00  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 1.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2244.00 TO NODE 2246.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<



>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1289.00 DOWNSTREAM ELEVATION(FEET) = 1270.00  
STREET LENGTH(FEET) = 330.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.38  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.51  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.39  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.13  
STREET FLOW TRAVEL TIME(MIN.) = 1.25 Tc(MIN.) = 5.68  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.492

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.57 SUBAREA RUNOFF(CFS) = 2.76  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 3.68

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.04  
FLOW VELOCITY(FEET/SEC.) = 4.81 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.38  
LONGEST FLOWPATH FROM NODE 2245.00 TO NODE 2246.00 = 430.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2246.00 TO NODE 2246.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.68  
RAINFALL INTENSITY(INCH/HR) = 8.49  
TOTAL STREAM AREA(ACRES) = 0.76  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.68

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 2.05         | 6.39      | 7.875                 | 0.42        |
| 2             | 3.68         | 5.68      | 8.492                 | 0.76        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 5.50         | 5.68      | 8.492                 |
| 2             | 5.46         | 6.39      | 7.875                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.50 Tc(MIN.) = 5.68  
 TOTAL AREA(ACRES) = 1.2  
 LONGEST FLOWPATH FROM NODE 2249.00 TO NODE 2246.00 = 640.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2246.00 TO NODE 2252.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1243.00  
 FLOW LENGTH(FEET) = 525.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.64  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 5.50  
 PIPE TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 6.59  
 LONGEST FLOWPATH FROM NODE 2249.00 TO NODE 2252.00 = 1165.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2252.00 TO NODE 2252.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER  | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|--|--------------|-----------|-----------------------|-------------|
| 1  | 5.50         | 6.59      | 7.718                 | 1.18        |
| LONGEST FLOWPATH FROM NODE 2249.00 TO NODE 2252.00 = 1165.00 FEET. |              |           |                       |             |

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\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 52.38        | 14.45     | 4.651                 | 19.77       |

LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2252.00 = 2595.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 29.39        | 6.59      | 7.718                 |
| 2             | 55.70        | 14.45     | 4.651                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 55.70 Tc(MIN.) = 14.45  
TOTAL AREA(ACRES) = 21.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 2252.00 TO NODE 2252.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2252.00 TO NODE 2223.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1243.00 DOWNSTREAM(FEET) = 1242.00  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.03  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 55.70  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 14.49  
LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2223.00 = 2630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2223.00 TO NODE 2281.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1242.00 DOWNSTREAM(FEET) = 1240.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 205.00 CHANNEL SLOPE = 0.0098  
CHANNEL FLOW THRU SUBAREA(CFS) = 55.70  
FLOW VELOCITY(FEET/SEC) = 3.94 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.87 Tc(MIN.) = 15.35

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LONGEST FLOWPATH FROM NODE 2242.00 TO NODE 2281.00 = 2835.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 21.0 TC(MIN.) = 15.35

PEAK FLOW RATE(CFS) = 55.70

=====

=====

END OF RATIONAL METHOD ANALYSIS

↑



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\*AREA ALREADY ACCOUNTED FOR

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| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2599         | 2598 | 2    | 1290             | 1288             | 80               | 0.51        | 0.17          |                |      |   |   |
| 2598         | 2597 | 6    | 1288             | 1280             | 800              | 0.51        | 3.15          | 1 SIDE         |      |   |   |
| 2597         | 2593 | 3    | 1274             | 1267             | 195              |             |               |                |      |   |   |
| 2593         | 2593 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2596         | 2595 | 2    | 1290             | 1288             | 83.33            | 0.51        | 0.09          |                |      |   |   |
| 2595         | 2594 | 6    | 1288             | 1274             | 435              | 0.51        | 1.93          | 2 SIDES        |      |   |   |
| 2594         | 2593 | 3    | 1268             | 1267.8           | 30               |             |               |                |      |   |   |
| 2593         | 2593 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2593         | 2589 | 3    | 1267.8           | 1267             | 175              |             |               |                |      |   |   |
| 2589         | 2589 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2592         | 2591 | 2    | 1288             | 1286             | 83.33            | 0.51        | 0.08          |                |      |   |   |
| 2591         | 2590 | 6    | 1286             | 1274             | 440              | 0.51        | 0.93          | 2 SIDES        |      |   |   |
| 2590         | 2589 | 3    | 1268             | 1267.6           | 40               |             |               |                |      |   |   |
| 2589         | 2589 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2589         | 2584 | 3    | 1267.6           | 1259             | 385              |             |               |                |      |   |   |
| 2584         | 2584 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2588         | 2587 | 2    | 1282             | 1281             | 67.65            | 0.51        | 0.10          |                |      |   |   |
| 2587         | 2584 | 6    | 1281             | 1265             | 745              | 0.51        | 3.35          | 2 SIDES        |      |   |   |
| 2584         | 2584 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2584         | 2568 | 3    | 1259             | 1257             | 65               |             |               |                |      |   |   |
| 2568         | 2568 | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2580         | 2579 | 2    | 1291.5           | 1289             | 87.50            | 0.57        | 0.23          |                |      |   |   |
| 2579         | 2578 | 6    | 1289             | 1282             | 785              | 0.51        | 2.78          | 1 SIDE         |      |   |   |
| 2578         | 2575 | 3    | 1276             | 1267             | 320              |             |               |                |      |   |   |
| 2575         | 2575 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2583         | 2582 | 2    | 1286             | 1285             | 70               | 0.51        | 0.05          |                |      |   |   |
| 2582         | 2581 | 6    | 1285             | 1274             | 315              | 0.51        | 1.06          | 2 SIDES        |      |   |   |
| 2581         | 2575 | 3    | 1268             | 1267             | 60               |             |               |                |      |   |   |
| 2575         | 2575 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2575         | 2573 | 3    | 1267             | 1263.8           | 105              |             |               |                |      |   |   |
| 2573         | 2573 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2577         | 2576 | 2    | 1286             | 1284             | 80               | 0.51        | 0.08          |                |      |   |   |
| 2576         | 2574 | 6    | 1284             | 1270             | 455              | 0.51        | 2.24          | 1 SIDE         |      |   |   |
| 2574         | 2573 | 3    | 1264             | 1263.8           | 10               |             |               |                |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2573         | 2573   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2573         | 2569   | 3    | 1263.8           | 1263.3           | 65               |             |               |                |      |   |   |
| 2569         | 2569   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2572         | 2571   | 2    | 1284             | 1283             | 70               | 0.51        | 0.04          |                |      |   |   |
| 2571         | 2570   | 6    | 1283             | 1270             | 365              | 0.51        | 1.22          | 2 SIDES        |      |   |   |
| 2570         | 2569   | 3    | 1264             | 1263             | 60               |             |               |                |      |   |   |
| 2569         | 2569   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2569         | 2568   | 3    | 1263             | 1257             | 230              |             |               |                |      |   |   |
| 2568         | 2568   | 11   |                  |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 2568         | 2568   | 12   |                  |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 2568         | 2565   | 3    | 1257             | 1251             | 205              |             |               |                |      |   |   |
| 2565         | 2565   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2568.2       | 2567   | 2    | 1271             | 1269             | 81.58            | 0.51        | 0.07          |                |      |   |   |
| 2567         | 2566   | 6    | 1269             | 1257             | 460              | 0.51        | 2.15          | 1 SIDE         |      |   |   |
| 2566         | 2565   | 3    | 1257             | 1256.8           | 10               |             |               |                |      |   |   |
| 2565         | 2565   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2565         | 2544   | 3    | 1256.8           | 1256             | 45               |             |               |                |      |   |   |
| 2544         | 2544   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2553         | 2553.2 | 2    | 1265             | 1263             | 80               | 0.51        | 0.11          |                |      |   |   |
| 2553.2       | 2551.2 | 6    | 1263             | 1261             | 170              | 0.51        | 0.58          | 1 SIDE         |      |   |   |
| 2551.2       | 2552   | 3    | 1255             | 1254             | 30               |             |               |                |      |   |   |
| 2552         | 2552   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2552         | 2545   | 3    | 1254             | 1250             | 325              |             |               |                |      |   |   |
| 2545         | 2545   | 1    |                  |                  |                  |             |               | 1 OF 3         |      |   |   |
| 2551         | 2550   | 2    | 1262             | 1261             | 65               | 0.51        | 0.13          |                |      |   |   |
| 2550         | 2549   | 6    | 1261             | 1257             | 330              | 0.51        | 1.84          | 1 SIDE         |      |   |   |
| 2549         | 2545   | 3    | 1251             | 1250             | 10               |             |               |                |      |   |   |
| 2545         | 2545   | 1    |                  |                  |                  |             |               | 2 OF 3         |      |   |   |
| 2548         | 2547   | 2    | 1265             | 1264             | 68.75            | 0.51        | 0.19          |                |      |   |   |
| 2547         | 2546   | 5    | 1264             | 1258             | 410              | 0.51        | 3.15          |                |      |   |   |
| 2546         | 2545   | 3    | 1252             | 1250             | 45               |             |               |                |      |   |   |
| 2545         | 2545   | 1    |                  |                  |                  |             |               | 3 OF 3         |      |   |   |
| 2545         | 2544   | 3    | 1250             | 1249             | 60               |             |               |                |      |   |   |



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| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2544         | 2544 | 11   |                  |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 2544         | 2544 | 12   |                  |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 2544         | 2542 | 3    | 1249             | 1248             | 125              |             |               |                |      |   |   |
| 2542         | 2542 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2543         | 2542 | 2    | 1255             | 1254             | 65               | 0.51        | 0.39          | 2 SIDES        |      |   |   |
| 2542         | 2542 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2542         | 2515 | 3    | 1254             | 1246.7           | 60               |             |               |                |      |   |   |
| 2515         | 2515 | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2541         | 2540 | 2    | 1315             | 1310             | 100              | 0.9         | 0.20          |                |      |   |   |
| 2540         | 2539 | 6    | 1310             | 1285             | 335              | 0.9         | 0.50          | 1 SIDE         |      |   |   |
| 2539         | 2538 | 3    | 1279             | 1270             | 310              |             |               |                |      |   |   |
| 2538         | 2538 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2537         | 2536 | 2    | 1285             | 1282             | 95               | 0.9         | 0.15          |                |      |   |   |
| 2536         | 2538 | 6    | 1282             | 1270             | 210              | 0.89        | 0.32          | 1 SIDE         |      |   |   |
| 2538         | 2538 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2538         | 2534 | 3    | 1264             | 1250             | 480              |             |               |                |      |   |   |
| 2534         | 2534 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2533         | 2532 | 2    | 1270             | 1265             | 70               | 0.88        | 0.37          |                |      |   |   |
| 2532         | 2534 | 6    | 1265             | 1256             | 375              | 0.88        | 1.06          | 1 SIDE         |      |   |   |
| 2534         | 2534 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2534         | 2527 | 3    | 1250             | 1247.2           | 460              |             |               |                |      |   |   |
| 2527         | 2527 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2526         | 2525 | 2    | 1256             | 1255             | 65               | 0.51        | 0.29          |                |      |   |   |
| 2525         | 2527 | 6    | 1255             | 1253.2           | 355              | 0.51        | 0.79          | 2 SIDES        |      |   |   |
| 2527         | 2527 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2527         | 2515 | 3    | 1247.2           | 1246.7           | 45               |             |               |                |      |   |   |
| 2515         | 2515 | 10   |                  |                  |                  |             |               | SAVE TO BANK 2 |      |   |   |
| 2523         | 2522 | 2    | 1275             | 1274             | 65               | 0.88        | 0.19          |                |      |   |   |
| 2522         | 2520 | 6    | 1274             | 1260             | 820              | 0.88        | 1.30          | 2 SIDES        |      |   |   |
| 2520         | 2519 | 3    | 1248             | 1247.2           | 515              |             |               |                |      |   |   |
| 2519         | 2519 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2518         | 2517 | 2    | 1260             | 1259             | 66.67            | 0.88        | 0.13          |                |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments     | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|--------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |              | 1    | 2 | 3 |
| 2517         | 2519   | 6    | 1259             | 1253.2           | 510              | 0.88        | 1.01          | 2 SIDES      |      |   |   |
| 2519         | 2519   | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2519         | 2515   | 3    | 1247.2           | 1246.7           | 60               |             |               |              |      |   |   |
| 2515         | 2515   | 11   |                  |                  |                  |             |               | ADD BANK 2   |      |   |   |
| 2515         | 2515   | 12   |                  |                  |                  |             |               | CLEAR BANK 2 |      |   |   |
| 2515         | 2515   | 11   |                  |                  |                  |             |               | ADD BANK 1   |      |   |   |
| 2515         | 2515   | 12   |                  |                  |                  |             |               | CLEAR BANK 1 |      |   |   |
| 2515         | 2514   | 3    | 1247             | 1139             | 1060             |             |               |              |      |   |   |
| 2514         | 2514   | 1    |                  |                  |                  |             |               | 1 of 2       |      |   |   |
| 2513         | 2512   | 2    | 1253             | 1250             | 95               | 0.88        | 0.16          |              |      |   |   |
| 2512         | 2514   | 6    | 1250             | 1145             | 945              | 0.88        | 1.43          | 2 SIDES      |      |   |   |
| 2514         | 2514   | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2514         | 2510   | 3    | 1139             | 1104             | 290              |             |               |              |      |   |   |
| 2510         | 2510   | 1    |                  |                  |                  |             |               | 1 OF 2       |      |   |   |
| 2509         | 2508   | 2    | 1142             | 1133             | 95               | 0.88        | 0.13          |              |      |   |   |
| 2508         | 2510   | 6    | 1133             | 1110             | 185              | 0.88        | 0.29          | 2 SIDES      |      |   |   |
| 2510         | 2510   | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2510         | 2506   | 3    | 1104             | 1075             | 300              |             |               |              |      |   |   |
| 2506         | 2506   | 1    |                  |                  |                  |             |               | 1 OF 2       |      |   |   |
| 2505         | 2504   | 2    | 1110             | 1095             | 100              | 0.88        | 0.16          |              |      |   |   |
| 2504         | 2506   | 6    | 1095             | 1075             | 160              | 0.88        | 0.24          | 2 SIDES      |      |   |   |
| 2506         | 2506   | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2506         | 2502   | 3    | 1069             | 1034             | 190              |             |               |              |      |   |   |
| 2502         | 2502   | 1    |                  |                  |                  |             |               | 1 OF 2       |      |   |   |
| 2501         | 2500   | 2    | 1075             | 1062             | 80               | 0.88        | 0.13          |              |      |   |   |
| 2500         | 2502   | 6    | 1062             | 1040             | 190              | 0.89        | 0.29          | 2 SIDES      |      |   |   |
| 2502         | 2502   | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2502         | 2499.2 | 3    | 1034             | 994              | 305              |             |               |              |      |   |   |
| 2499.2       | 2499.2 | 1    |                  |                  |                  |             |               | 1 OF 2       |      |   |   |
| 2499.6       | 2499.8 | 2    | 1040             | 1022             | 100              | 0.89        | 0.20          |              |      |   |   |
| 2499.8       | 2499.2 | 6    | 1022             | 1000             | 185              | 0.89        | 0.27          | 2 SIDES      |      |   |   |
| 2499.2       | 2499.2 | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |





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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2499.2       | 2472   | 3    | 994              | 970              | 350              |             |               |                |      |   |   |
| 2472         | 2472   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2487         | 2486   | 2    | 1405             | 1375             | 100              | 0.25        | 0.27          |                |      |   |   |
| 2486         | 2485   | 5    | 1375             | 1294             | 400              | 0.25        | 3.38          |                |      |   |   |
| 2485         | 2485   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2484         | 2483   | 2    | 1325             | 1320             | 95               | 0.25        | 0.25          |                |      |   |   |
| 2483         | 2485   | 5    | 1320             | 1294             | 205              | 0.25        | *             |                |      |   |   |
| 2485         | 2485   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2485         | 2482   | 3    | 1288             | 1251             | 95               |             |               |                |      |   |   |
| 2482         | 2482   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2481         | 2480   | 2    | 1270             | 1268             | 80               | 0.25        | 0.12          |                |      |   |   |
| 2480         | 2482   | 5    | 1268             | 1257             | 425              | 0.25        | 1.46          |                |      |   |   |
| 2482         | 2482   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2482         | 2478   | 3    | 1251             | 1247             | 430              |             |               |                |      |   |   |
| 2478         | 2478   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2477         | 2476   | 2    | 1300             | 1298             | 80               | 0.25        | 0.10          |                |      |   |   |
| 2476         | 2475   | 5    | 1298             | 1268             | 410              | 0.25        | 0.48          |                |      |   |   |
| 2475         | 2478   | 3    | 1262             | 1247             | 995              |             |               |                |      |   |   |
| 2478         | 2478   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2478         | 2515.6 | 3    | 1247             | 1246             | 130              |             |               |                |      |   |   |
| 2515.6       | 2515.6 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2515.8       | 2515.7 | 2    | 1254             | 1253             | 65               | 0.25        | 0.24          |                |      |   |   |
| 2515.7       | 2515.6 | 5    | 1253             | 1252             | 510              | 0.25        | 3.25          |                |      |   |   |
| 2515.6       | 2515.6 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2515.6       | 2474   | 3    | 1246             | 1244             | 50               |             |               |                |      |   |   |
| 2474         | 2473.5 | 5    | 1244             | 978.5            | 955              | 0.25        | 10.53         |                |      |   |   |
| 2473.5       | 2473.5 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2488         | 2473   | 2    | 1250             | 1200             | 100              | 0.25        | 0.50          |                |      |   |   |
| 2473         | 2473.5 | 5    | 1200             | 978.5            | 930              | 0.27        | 12.02         |                |      |   |   |
| 2473.5       | 2473.5 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2473.5       | 2472   | 5    | 978.5            | 976              | 410              | 0.29        | 13.37         |                |      |   |   |
| 2472         | 2472   | 11   |                  |                  |                  |             |               | ADD BANK 1     |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet)                      | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|---------------------------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                                       |                  |                  |             |               |                | 1    | 2 | 3 |
| 2472         | 2472   | 12   |                                       |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 2472         | 2472   | 7    | Q=20.1 cfs Tc = 15.71 min A = 81.7 ac |                  |                  |             |               | CANYON DET.    |      |   |   |
| 2472         | 2471   | 3    | 970                                   | 920              | 385              |             |               |                |      |   |   |
| 2471         | 2471   | 1    |                                       |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2470         | 2469   | 2    | 1030                                  | 1024             | 100              | 0.25        | 0.59          |                |      |   |   |
| 2469         | 2471   | 5    | 1024                                  | 934              | 925              | 0.25        | 1.30          |                |      |   |   |
| 2471         | 2471   | 1    |                                       |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2471         | 2459   | 3    | 928                                   | 914              | 200              |             |               |                |      |   |   |
| 2459         | 2459   | 10   |                                       |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2468         | 2467   | 2    | 1255                                  | 1197             | 100              | 0.25        | 0.36          |                |      |   |   |
| 2467         | 2460   | 5    | 1197                                  | 923              | 1265             | 0.25        | 5.11          |                |      |   |   |
| 2460         | 2460   | 10   |                                       |                  |                  |             |               | SAVE TO BANK 2 |      |   |   |
| 2465         | 2464   | 2    | 1225                                  | 1215             | 100              | 0.25        | 0.45          |                |      |   |   |
| 2464         | 2463   | 5    | 1215                                  | 912              | 2135             | 0.25        | 7.44          |                |      |   |   |
| 2463         | 2463   | 1    |                                       |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2462         | 2461   | 2    | 925                                   | 923              | 80               | 0.57        | 0.11          |                |      |   |   |
| 2461         | 2463   | 6    | 923                                   | 916              | 590              | 0.57        | 3.38          | 2 SIDES        |      |   |   |
| 2463         | 2463   | 1    |                                       |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2463         | 2460   | 3    | 913                                   | 912              | 225              |             |               |                |      |   |   |
| 2460         | 2460   | 11   |                                       |                  |                  |             |               | ADD BANK 2     |      |   |   |
| 2460         | 2460   | 12   |                                       |                  |                  |             |               | CLEAR BANK 2   |      |   |   |
| 2460         | 2459   | 3    | 912                                   | 911              | 145              |             |               |                |      |   |   |
| 2459         | 2459   | 11   |                                       |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 2459         | 2459   | 12   |                                       |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 2459         | 2458   | 3    | 911                                   | 905              | 635              |             |               |                |      |   |   |
| 2458         | 2458   | 10   |                                       |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2457         | 2456   | 2    | 920                                   | 917              | 95               | 0.57        | 0.19          |                |      |   |   |
| 2456         | 2456.1 | 6    | 917                                   | 910              | 355              | 0.57        | 2.02          | 1 SIDE         |      |   |   |
| 2456.1       | 2455   | 3    | 904                                   | 897              | 300              |             |               |                |      |   |   |
| 2455         | 2455   | 1    |                                       |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2456.2       | 2456.3 | 2    | 912                                   | 909              | 90               | 0.57        | 0.09          |                |      |   |   |
| 2456.3       | 2455   | 6    | 909                                   | 903              | 245              | 0.57        | 4.61          | 2 SIDES        |      |   |   |
| 2455         | 2455   | 1    |                                       |                  |                  |             |               | 2 OF 2         |      |   |   |





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| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments    | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|-------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |             | 1    | 2 | 3 |
| 2437         | 2436 | 2    | 897              | 895              | 80               | 0.57        | 0.13          |             |      |   |   |
| 2436         | 2435 | 6    | 895              | 894              | 300              | 0.57        | 0.86          | 2 SIDES     |      |   |   |
| 2435         | 2438 | 3    | 888              | 887              | 110              |             |               |             |      |   |   |
| 2438         | 2438 | 1    |                  |                  |                  |             |               | 2 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2438         | 2434 | 3    | 889              | 887              | 355              |             |               |             |      |   |   |
| 2434         | 2434 | 1    |                  |                  |                  |             |               | 1 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2433         | 2432 | 2    | 903              | 899              | 95               | 0.57        | 0.15          |             |      |   |   |
| 2432         | 2431 | 5    | 899              | 896              | 510              | 0.57        | 2.93          |             |      |   |   |
| 2431         | 2434 | 3    | 890              | 889              | 65               |             |               |             |      |   |   |
| 2434         | 2434 | 1    |                  |                  |                  |             |               | 2 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2434         | 2430 | 3    | 889              | 888              | 45               |             |               |             |      |   |   |
| 2430         | 2430 | 1    |                  |                  |                  |             |               | 1 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2429         | 2428 | 2    | 1290             | 1235             | 100              | 0.25        | 0.29          |             |      |   |   |
| 2428         | 2427 | 5    | 1235             | 910              | 710              | 0.26        | 23.50         |             |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2427         | 2430 | 3    | 904              | 888              | 395              |             |               |             |      |   |   |
| 2430         | 2430 | 1    |                  |                  |                  |             |               | 2 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2430         | 2391 | 3    | 888              | 877              | 400              |             |               |             |      |   |   |
| 2391         | 2391 | 10   |                  |                  |                  |             |               | SAVE BANK 1 |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2417         | 2416 | 2    | 906              | 905              | 65               | 0.57        | 0.06          |             |      |   |   |
| 2416         | 2415 | 6    | 905              | 895              | 325              | 0.57        | 1.88          |             |      |   |   |
| 2415         | 2414 | 3    | 889              | 888              | 160              |             |               |             |      |   |   |
| 2414         | 2414 | 10   |                  |                  |                  |             |               | SAVE BANK 2 |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2400         | 2399 | 2    | 1000             | 987              | 100              | 0.89        | 0.15          |             |      |   |   |
| 2399         | 2398 | 6    | 987              | 940              | 445              | 0.89        | 0.68          | 2 SIDES     |      |   |   |
| 2398         | 2397 | 3    | 934              | 908              | 400              |             |               |             |      |   |   |
| 2397         | 2397 | 1    |                  |                  |                  |             |               | 1 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2396         | 2395 | 2    | 940              | 930              | 100              | 0.57        | 0.18          |             |      |   |   |
| 2395         | 2397 | 6    | 930              | 916              | 285              | 0.57        | 0.42          | 2 SIDES     |      |   |   |
| 2397         | 2397 | 1    |                  |                  |                  |             |               | 2 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2397         | 2394 | 3    | 910              | 894              | 455              |             |               |             |      |   |   |
| 2394         | 2394 | 1    |                  |                  |                  |             |               | 1 OF 2      |      |   |   |
|              |      |      |                  |                  |                  |             |               |             |      |   |   |
| 2393         | 2392 | 2    | 916              | 912              | 97.50            | 0.57        | 0.19          |             |      |   |   |
| 2392         | 2394 | 6    | 912              | 900              | 365              | 0.57        | 0.56          | 2 SIDES     |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2394         | 2394   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2394         | 2414   | 3    | 894              | 888              | 105              |             |               |                |      |   |   |
| 2414         | 2414   | 11   |                  |                  |                  |             |               | ADD BANK 2     |      |   |   |
| 2414         | 2414   | 12   |                  |                  |                  |             |               | CLEAR BANK 2   |      |   |   |
| 2414         | 2391   | 5    | 894              | 883              | 320              |             | *             |                |      |   |   |
| 2391         | 2391   | 11   |                  |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 2391         | 2391   | 12   |                  |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 2391         | 2418   | 3    | 877              | 869              | 267              |             |               |                |      |   |   |
| 2418         | 2418   | 10   |                  |                  |                  |             |               | SAVE BANK 1    |      |   |   |
| 2425         | 2424   | 2    | 1198             | 1135             | 100              | 0.25        | 0.52          |                |      |   |   |
| 2424         | 2423   | 5    | 1135             | 926              | 715              | 0.25        | 6.25          |                |      |   |   |
| 2423         | 2422.5 | 3    | 920              | 891              | 75               |             |               |                |      |   |   |
| 2422.5       | 2422.5 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2422.7       | 2422.6 | 2    | 914              | 912              | 80               | 0.25        | 0.11          |                |      |   |   |
| 2422.6       | 2422.5 | 5    | 912              | 897              | 550              | 0.3         | 0.53          |                |      |   |   |
| 2422.5       | 2422.5 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2422.5       | 2422   | 3    | 891              | 881              | 350              |             |               |                |      |   |   |
| 2422         | 2422   | 10   |                  |                  |                  |             |               | SAVE TO BANK 2 |      |   |   |
| 2421         | 2420   | 2    | 1185             | 1143             | 100              | 0.25        | 0.56          |                |      |   |   |
| 2420         | 2419   | 5    | 1143             | 918              | 765              | 0.25        | 4.46          |                |      |   |   |
| 2419         | 2422.2 | 3    | 912              | 885              | 80               |             |               |                |      |   |   |
| 2422.2       | 2422.2 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2422.6       | 2422.4 | 2    | 897              | 895              | 80               | 0.3         | 0.14          |                |      |   |   |
| 2422.4       | 2422.2 | 5    | 895              | 891              | 145              | 0.3         | 0.31          |                |      |   |   |
| 2422.2       | 2422.2 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2422.2       | 2422   | 3    | 885              | 881              | 400              |             |               |                |      |   |   |
| 2422         | 2422   | 11   |                  |                  |                  |             |               | Add bank 2     |      |   |   |
| 2422         | 2422   | 12   |                  |                  |                  |             |               | Clear bank 2   |      |   |   |
| 2422         | 2418   | 3    | 881              | 869              | 690              |             |               |                |      |   |   |
| 2418         | 2418   | 11   |                  |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 2418         | 2418   | 12   |                  |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 2418         | 2418   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2418.9       | 2418.8 | 2    | 922              | 920              | 80               | 0.51        | 0.24          |                |      |   |   |



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| Node to Node |         | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor           | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|---------|------|------------------|------------------|------------------|-----------------------|---------------|----------------|------|---|---|
|              |         |      |                  |                  |                  |                       |               |                | 1    | 2 | 3 |
| 2418.8       | 2418.2  | 6    | 920              | 907              | 660              | 0.51                  | 2.71          | 2 sides        |      |   |   |
| 2418.2       | 2418.2  | 1    |                  |                  |                  |                       |               | 1 of 2         |      |   |   |
| 2417.84      | 2417.85 | 2    | 919              | 918              | 70               | 0.57                  | 0.08          |                |      |   |   |
| 2417.85      | 2418.2  | 6    | 918              | 907              | 1005             | 0.57                  | 3.99          | 2 sides        |      |   |   |
| 2418.2       | 2418.2  | 1    |                  |                  |                  |                       |               | 2 of 2         |      |   |   |
| 2418.2       | 2418.7  | 5    | 907              | 902              | 425              | 0.57                  | 0.69          |                |      |   |   |
| 2418.7       | 2418.6  | 3    | 896              | 890              | 145              |                       |               |                |      |   |   |
| 2418.6       | 2418.6  | 10   |                  |                  |                  |                       |               | save to Bank 2 |      |   |   |
| 2418.5       | 2418.4  | 2    | 1105             | 1055             | 100              | 0.25                  | 0.25          |                |      |   |   |
| 2418.4       | 2418.3  | 5    | 1055             | 909              | 410              | 0.25                  | 4.91          |                |      |   |   |
| 2418.3       | 2418.32 | 3    | 903              | 900              | 340              |                       |               |                |      |   |   |
| 2418.32      | 2418.32 | 1    |                  |                  |                  |                       |               | 1 of 2         |      |   |   |
| 2418.1       | 2417.9  | 2    | 925              | 918              | 75               | 0.55                  | 0.08          |                |      |   |   |
| 2417.9       | 2417.91 | 6    | 918              | 912              | 115              | 0.57                  | 0.51          | 2 sides        |      |   |   |
| 2417.91      | 2417.8  | 5    | 912              | 908              | 530              | 0.57                  | 2.18          |                |      |   |   |
| 2417.8       | 2417.32 | 3    | 902              | 900              | 50               |                       |               |                |      |   |   |
| 2417.32      | 2417.32 | 1    |                  |                  |                  |                       |               | 2 of 2         |      |   |   |
| 2418.32      | 2417.7  | 3    | 900              | 899              | 115              |                       |               |                |      |   |   |
| 2417.7       | 2417.7  | 10   |                  |                  |                  |                       |               | save to bank 3 |      |   |   |
| 2417.6       | 2417.5  | 2    | 1185             | 1145             | 100              | 0.3                   | 0.34          |                |      |   |   |
| 2417.5       | 2417.4  | 5    | 1145             | 908              | 580              | 0.3                   | 3.81          |                |      |   |   |
| 2417.4       | 2417.3  | 3    | 902              | 899              | 110              |                       |               |                |      |   |   |
| 2417.3       | 2417.3  | 1    |                  |                  |                  |                       |               | 1 of 2         |      |   |   |
| 2417.2       | 2417.1  | 2    | 1190             | 1136             | 100              | 0.3                   | 0.21          |                |      |   |   |
| 2417.1       | 2417.3  | 5    | 1136             | 910              | 1085             | 0.3                   | 6.18          |                |      |   |   |
| 2417.3       | 2417.3  | 1    |                  |                  |                  |                       |               | 2 of 2         |      |   |   |
| 2417.3       | 2417.7  | 3    | 904              | 899              | 85               |                       |               |                |      |   |   |
| 2417.7       | 2417.7  | 1    |                  |                  |                  |                       |               | 1 OF 2         |      |   |   |
| 2417.7       | 2417.7  | 7    | Q=308.19         |                  | A=192.1          | T <sub>c</sub> =17.37 |               | ADD RUN 25.1   |      |   |   |
| 2417.7       | 2417.7  | 1    |                  |                  |                  |                       |               | 2 OF 2         |      |   |   |
| 2417.7       | 2417.7  | 11   |                  |                  |                  |                       |               | ADD BANK 3     |      |   |   |
| 2417.7       | 2417.7  | 12   |                  |                  |                  |                       |               | CLEAR BANK 3   |      |   |   |
| 2417.7       | 2418.6  | 3    | 899              | 891              | 515              |                       |               |                |      |   |   |
| 2418.6       | 2418.6  | 11   |                  |                  |                  |                       |               | ADD BANK 2     |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet)                      | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments         | BANK |   |   |
|--------------|--------|------|---------------------------------------|------------------|------------------|-------------|---------------|------------------|------|---|---|
|              |        |      |                                       |                  |                  |             |               |                  | 1    | 2 | 3 |
| 2418.6       | 2418.6 | 12   |                                       |                  |                  |             |               | CLEAR BANK 2     |      |   |   |
| 2418.6       | 2418   | 3    | 891                                   | 869              | 745              |             |               |                  |      |   |   |
| 2418         | 2418   | 11   |                                       |                  |                  |             |               | ADD BANK 1       |      |   |   |
| 2418         | 2418   | 12   |                                       |                  |                  |             |               | CLEAR BANK 1     |      |   |   |
| 2418         | 2380.2 | 3    | 869                                   | 858              | 325              |             |               |                  |      |   |   |
| 2380.2       | 2380.2 | 10   |                                       |                  |                  |             |               | SAVE TO BANK 1   |      |   |   |
| 2415.9       | 2415.8 | 2    | 915                                   | 907              | 85               | 0.57        | 0.10          |                  |      |   |   |
| 2415.8       | 2415.7 | 6    | 907                                   | 902              | 395              | 0.57        | 2.43          | 2 SIDES          |      |   |   |
| 2415.7       | 2415.6 | 3    | 896                                   | 895              | 245              |             |               |                  |      |   |   |
| 2415.6       | 2415.6 | 1    |                                       |                  |                  |             |               | 1 OF 2           |      |   |   |
| 2415.5       | 2415.4 | 2    | 905                                   | 904              | 68.75            | 0.57        | 0.07          |                  |      |   |   |
| 2415.4       | 2415.3 | 6    | 904                                   | 898              | 420              | 0.57        | 1.93          | 2 SIDES          |      |   |   |
| 2415.3       | 2415.6 | 3    | 892                                   | 891              | 40               |             |               |                  |      |   |   |
| 2415.6       | 2415.6 | 1    |                                       |                  |                  |             |               | 2 OF 2           |      |   |   |
| 2415.6       | 2415.2 | 3    | 891                                   | 874              | 600              |             |               |                  |      |   |   |
| 2415.2       | 2415.2 | 1    |                                       |                  |                  |             |               | 1 OF 2           |      |   |   |
| 2415.1       | 2414.9 | 2    | 902                                   | 900              | 81.58            | 0.57        | 0.12          |                  |      |   |   |
| 2414.9       | 2415.2 | 6    | 900                                   | 880              | 725              | 0.57        | 3.27          | 2 SIDES          |      |   |   |
| 2415.2       | 2415.2 | 1    |                                       |                  |                  |             |               | 2 OF 2           |      |   |   |
| 2415.2       | 2414.8 | 3    | 874                                   | 849              | 55               |             |               |                  |      |   |   |
| 2414.8       | 2414.7 | 5    | 855                                   | 854              | 135              | 0.57        | 8.65          |                  |      |   |   |
| 2414.7       | 2414.7 | 7    | Q = 3.7 cfs Tc = 10.44 mins A=16.6 ac |                  |                  |             |               | EAST VALLEY DET. |      |   |   |
| 2414.7       | 2380.2 | 3    | 848                                   | 847              | 105              |             |               |                  |      |   |   |
| 2380.2       | 2380.2 | 11   |                                       |                  |                  |             |               | ADD BANK 1       |      |   |   |
| 2380.2       | 2380.2 | 12   |                                       |                  |                  |             |               | CLEAR BANK 1     |      |   |   |
| 2380.2       | 2380   | 3    | 847                                   | 831              | 65               |             |               |                  |      |   |   |
| 2380         | 2380   | 10   |                                       |                  |                  |             |               | SAVE TO BANK 1   |      |   |   |
| 2413         | 2412   | 2    | 891                                   | 888              | 95               | 0.57        | 0.10          |                  |      |   |   |
| 2412         | 2412.5 | 6    | 888                                   | 882              | 358              | 0.57        | 1.84          | 1 SIDE           |      |   |   |
| 2412.5       | 2412.5 | 1    |                                       |                  |                  |             |               | 2 OF 2           |      |   |   |
| 2412.5       | 2411   | 3    | 876                                   | 874              | 360              |             |               |                  |      |   |   |
| 2411         | 2411   | 1    |                                       |                  |                  |             |               | 1 OF 2           |      |   |   |
| 2410         | 2409   | 2    | 895                                   | 894              | 68.75            | 0.57        | 0.07          |                  |      |   |   |
| 2409         | 2411   | 6    | 894                                   | 880              | 495              | 0.57        | 3.81          | 2 SIDES          |      |   |   |
| 2411         | 2411   | 1    |                                       |                  |                  |             |               | 2 OF 2           |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet)                    | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK             |   |   |  |
|--------------|--------|------|-------------------------------------|------------------|------------------|-------------|---------------|----------------|------------------|---|---|--|
|              |        |      |                                     |                  |                  |             |               |                | 1                | 2 | 3 |  |
| 2411         | 2408   | 3    | 874                                 | 873              | 65               |             |               |                |                  |   |   |  |
| 2408         | 2408   | 1    |                                     |                  |                  |             |               | 1 OF 2         |                  |   |   |  |
| 2407         | 2406   | 2    | 885                                 | 883              | 85               | 0.57        | 0.10          |                |                  |   |   |  |
| 2406         | 2405   | 6    | 883                                 | 880              | 285              | 0.57        | 1.61          | 2 SIDES        |                  |   |   |  |
| 2405         | 2408   | 3    | 874                                 | 873              | 330              |             |               |                |                  |   |   |  |
| 2408         | 2408   | 1    |                                     |                  |                  |             |               | 2 OF 2         |                  |   |   |  |
| 2408         | 2404   | 3    | 873                                 | 867              | 395              |             |               |                |                  |   |   |  |
| 2404         | 2404   | 1    |                                     |                  |                  |             |               | 1 OF 2         |                  |   |   |  |
| 2403         | 2402   | 2    | 885                                 | 884              | 66.67            | 0.57        | 0.13          |                |                  |   |   |  |
| 2402         | 2404   | 6    | 884                                 | 873              | 425              | 0.57        | 1.93          | 2 SIDES        |                  |   |   |  |
| 2404         | 2404   | 1    |                                     |                  |                  |             |               | 2 OF 2         |                  |   |   |  |
| 2404         | 2401   | 3    | 867                                 | 830              | 160              |             |               |                |                  |   |   |  |
| 2401         | 2380   | 5    | 830                                 | 829              | 95               | 0.57        | 1.66          |                |                  |   |   |  |
| 2380         | 2380   | 10   |                                     |                  |                  |             |               | SAVE TO BANK 2 |                  |   |   |  |
| 2390         | 2389   | 2    | 900                                 | 895              | 100              | 0.57        | 0.20          |                |                  |   |   |  |
| 2389         | 2389.5 | 6    | 895                                 | 876              | 565              | 0.57        | 0.91          | 2 SIDES        |                  |   |   |  |
| 2389.5       | 2388   | 3    | 870                                 | 867              | 75               |             |               |                |                  |   |   |  |
| 2388         | 2388   | 1    |                                     |                  |                  |             |               | 1 OF 2         |                  |   |   |  |
| 2387         | 2386   | 2    | 881                                 | 878              | 95               | 0.57        | 0.11          |                |                  |   |   |  |
| 2386         | 2385   | 6    | 878                                 | 874              | 170              | 0.57        | 0.95          | 2 SIDES        | #                |   |   |  |
| 2385         | 2388   | 3    | 868                                 | 867              | 35               |             |               |                |                  |   |   |  |
| 2388         | 2388   | 1    |                                     |                  |                  |             |               | 2 OF 2         |                  |   |   |  |
| 2388         | 2384   | 3    | 867                                 | 859              | 200              |             |               |                |                  |   |   |  |
| 2384         | 2384   | 1    |                                     |                  |                  |             |               | 1 OF 2         |                  |   |   |  |
| 2383         | 2382   | 2    | 876                                 | 872              | 97.50            | 0.57        | 0.20          |                |                  |   |   |  |
| 2382         | 2384   | 6    | 872                                 | 865              | 150              | 0.57        | 0.20          | 2 SIDES        |                  |   |   |  |
| 2384         | 2384   | 1    |                                     |                  |                  |             |               | 2 OF 2         |                  |   |   |  |
| 2384         | 2381   | 3    | 859                                 | 832              | 90               |             |               |                |                  |   |   |  |
| 2381         | 2380   | 5    | 832                                 | 830              | 80               |             |               |                |                  |   |   |  |
| 2380         | 2380   | 11   |                                     |                  |                  |             |               | ADD BANK 2     |                  |   |   |  |
| 2380         | 2380   | 12   |                                     |                  |                  |             |               | CLEAR BANK 2   |                  |   |   |  |
| 2380         | 2380   | 7    | Q =7.4 cf Tc = 10.46 min A =13.8 ac |                  |                  |             |               |                | WEST VALLEY DET. |   |   |  |
| 2380         | 2380   | 11   |                                     |                  |                  |             |               | ADD BANK 1     |                  |   |   |  |
| 2380         | 2380   | 12   |                                     |                  |                  |             |               | CLEAR BANK 1   |                  |   |   |  |





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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2380         | 2379   | 5    | 837              | 825              | 170              |             |               |                |      |   |   |
| 2379         | 2379   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2378         | 2377   | 2    | 1175             | 1155             | 85               | 0.25        | 0.10          |                |      |   |   |
| 2377         | 2376   | 5    | 1155             | 1070             | 300              | 0.25        | 1.84          |                |      |   |   |
| 2376         | 2375   | 5    | 1070             | 955              | 605              | 0.25        | 10.41         |                |      |   |   |
| 2375         | 2374   | 5    | 955              | 885              | 455              | 0.26        | 16.11         |                |      |   |   |
| 2374         | 2379.2 | 5    | 885              | 855              | 420              | 0.3         | 4.23          |                |      |   |   |
| 2379.2       | 2379.2 | 10   |                  |                  |                  |             |               | SAVE TO BANK 2 |      |   |   |
| 2373         | 2372   | 2    | 925              | 924              | 65               | 0.57        | 0.09          |                |      |   |   |
| 2372         | 2371   | 6    | 924              | 914              | 290              | 0.57        | 1.30          | 2 SIDES        |      |   |   |
| 2371         | 2370   | 3    | 908              | 906              | 310              |             |               |                |      |   |   |
| 2370         | 2370   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2369         | 2368   | 2    | 920              | 917              | 95               | 0.57        | 0.11          |                |      |   |   |
| 2368         | 2370   | 6    | 917              | 912              | 360              | 0.57        | 2.01          | 2 SIDES        |      |   |   |
| 2370         | 2370   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2370         | 2367   | 3    | 906              | 894              | 300              |             |               |                |      |   |   |
| 2367         | 2367   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2366         | 2365   | 2    | 911              | 909              | 81.58            | 0.57        | 0.06          |                |      |   |   |
| 2365         | 2367   | 6    | 909              | 900              | 405              | 0.57        | 1.80          | 1 SIDE         |      |   |   |
| 2367         | 2367   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2367         | 2364   | 3    | 894              | 887              | 205              |             |               |                |      |   |   |
| 2364         | 2364   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2363         | 2362   | 2    | 905              | 903              | 83.33            | 0.57        | 0.10          |                |      |   |   |
| 2362         | 2364   | 6    | 903              | 894              | 230              | 0.57        | 1.02          | 1 SIDE         |      |   |   |
| 2364         | 2364   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2364         | 2361   | 3    | 888              | 884              | 100              |             |               |                |      |   |   |
| 2361         | 2361   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2360         | 2359   | 2    | 898              | 895              | 95               | 0.57        | 0.14          |                |      |   |   |
| 2359         | 2361   | 6    | 895              | 890              | 195              | 0.57        | 0.88          | 1SIDE          |      |   |   |
| 2361         | 2361   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2361         | 2358   | 3    | 884              | 879              | 145              |             |               |                |      |   |   |
| 2358         | 2358   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2357         | 2356   | 2    | 895              | 892.4            | 85               | 0.57        | 0.10          |                |      |   |   |
| 2356         | 2358   | 6    | 892.4            | 885              | 370              | 0.57        | 1.77          | 2 SIDES        |      |   |   |



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| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments     | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|--------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |              | 1    | 2 | 3 |
| 2358         | 2358   | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2358         | 2555   | 3    | 879              | 865              | 205              |             |               |              |      |   |   |
| 2555         | 2554.8 | 5    | 865              | 864              | 50               | 0.3         | 0.78          |              |      |   |   |
| 2554.8       | 2379.2 | 5    | 864              | 855              | 300              | 0.28        | 4.94          |              |      |   |   |
| 2379.2       | 2379.2 | 11   |                  |                  |                  |             |               | ADD BANK 2   |      |   |   |
| 2379.2       | 2379.2 | 12   |                  |                  |                  |             |               | CLEAR BANK 2 |      |   |   |
| 2379.2       | 2379   | 5    | 855              | 825              | 610              | 0.3         | 5.40          |              |      |   |   |
| 2379         | 2379   | 11   |                  |                  |                  |             |               | ADD BANK 1   |      |   |   |
| 2379         | 2379   | 12   |                  |                  |                  |             |               | CLEAR BANK 1 |      |   |   |
| 2379         | 2379   | 1    |                  |                  |                  |             |               | 1 OF 2       |      |   |   |
| 2370         | 2369   | 2    | 1065             | 1020             | 95               | 0.42        | 0.11          |              |      |   |   |
| 2369         | 2368   | 5    | 1020             | 860              | 360              |             |               |              |      |   |   |
| 2369         | 2368   | 8    |                  |                  |                  | 0.42        | 0.93          |              |      |   |   |
| 2368         | 2367   | 3    | 865              | 830              | 115              |             |               |              |      |   |   |
| 2367         | 2379   | 5    | 830              | 825              | 110              |             |               |              |      |   |   |
| 2379         | 2379   | 1    |                  |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2379         | 2378   | 5    | 825              | 815              | 655              |             |               |              |      |   |   |
| 2379         | 2378   | 8    |                  |                  |                  | 0.42        | 13.91         |              |      |   |   |
| 2378         | 2378   | 1    |                  |                  |                  |             |               | 1 OF 3       |      |   |   |
| 2366         | 2365   | 2    | 1180             | 1175             | 80.00            | 0.42        | 0.13          |              |      |   |   |
| 2365         | 2364   | 5    | 1175             | 860              | 665              |             |               |              |      |   |   |
| 2365         | 2364   | 8    |                  |                  |                  | 0.42        | 3.34          |              |      |   |   |
| 2364         | 2363   | 3    | 860              | 842              | 100              |             |               |              |      |   |   |
| 2363         | 2378   | 5    | 842              | 815              | 450              |             |               |              |      |   |   |
| 2378         | 2378   | 1    |                  |                  |                  |             |               | 2 OF 3       |      |   |   |
| 2362         | 2361   | 2    | 1175             | 1165             | 80               | 0.42        | 0.10          |              |      |   |   |
| 2361         | 2360   | 5    | 1165             | 865              | 580.00           |             |               |              |      |   |   |
| 2361         | 2360   | 8    |                  |                  |                  | 0.42        | 2.99          |              |      |   |   |
| 2360         | 2359   | 3    | 865              | 839              | 100              |             |               |              |      |   |   |
| 2359         | 2378   | 5    | 839              | 815              | 310              |             |               |              |      |   |   |
| 2378         | 2378   | 1    |                  |                  |                  |             |               | 3 OF 3       |      |   |   |
| 2378         | 25     | 5    | 815              | 795              | 935              |             |               |              |      |   |   |
| 2378         | 25     | 8    |                  |                  |                  | 0.42        | 4.80          |              |      |   |   |
| 25           | 25     | 1    |                  |                  |                  |             |               | 1 OF 2       |      |   |   |
| 25.3         | 25.2   | 2    | 1175             | 1150             | 90               | 0.38        | 0.29          |              |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* PROPOSED HYDROLOGY \*
  - \* SUB BASIN 25 - POST DETENTION \*
  - \* JANUARY 2017 \*
- \*\*\*\*\*

FILE NAME: P-25D.DAT  
TIME/DATE OF STUDY: 11:20 02/16/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0312                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2599.00 TO NODE 2598.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 1290.00

DOWNSTREAM ELEVATION(FEET) = 1288.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423

SUBAREA RUNOFF(CFS) = 0.64

TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 2598.00 TO NODE 2597.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1288.00 DOWNSTREAM ELEVATION(FEET) = 1280.00

STREET LENGTH(FEET) = 800.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.92

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.39

HALFSTREET FLOOD WIDTH(FEET) = 13.22

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.64

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.03

STREET FLOW TRAVEL TIME(MIN.) = 5.06 Tc(MIN.) = 12.06

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.227

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 3.15 SUBAREA RUNOFF(CFS) = 8.40  
TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 8.85

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.46 HALFSTREET FLOOD WIDTH(FEET) = 16.72  
FLOW VELOCITY(FEET/SEC.) = 3.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.40  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2597.00 = 880.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2597.00 TO NODE 2593.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1274.00 DOWNSTREAM(FEET) = 1267.00  
FLOW LENGTH(FEET) = 195.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.52  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.85  
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 12.36  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2593.00 = 1075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2593.00 TO NODE 2593.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.36  
RAINFALL INTENSITY(INCH/HR) = 5.14  
TOTAL STREAM AREA(ACRES) = 3.32  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.85

\*\*\*\*\*

FLOW PROCESS FROM NODE 2596.00 TO NODE 2595.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 83.33  
UPSTREAM ELEVATION(FEET) = 1290.00  
DOWNSTREAM ELEVATION(FEET) = 1288.00

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ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.241  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.262  
SUBAREA RUNOFF(CFS) = 0.33  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.33

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2595.00 TO NODE 2594.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1288.00 DOWNSTREAM ELEVATION(FEET) = 1274.00  
STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.35  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 6.31  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.24  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.82  
STREET FLOW TRAVEL TIME(MIN.) = 2.24 Tc(MIN.) = 9.48  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.105

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 1.93 SUBAREA RUNOFF(CFS) = 6.01  
TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 6.29

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.51  
FLOW VELOCITY(FEET/SEC.) = 3.74 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.11  
LONGEST FLOWPATH FROM NODE 2596.00 TO NODE 2594.00 = 518.33 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2594.00 TO NODE 2593.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1268.00 DOWNSTREAM(FEET) = 1267.80
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.08
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.29
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.58
LONGEST FLOWPATH FROM NODE 2596.00 TO NODE 2593.00 = 548.33 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2593.00 TO NODE 2593.00 IS CODE = 1
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.58
RAINFALL INTENSITY(INCH/HR) = 6.06
TOTAL STREAM AREA(ACRES) = 2.02
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.29

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 14.18 Tc(MIN.) = 12.36
TOTAL AREA(ACRES) = 5.3
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2593.00 = 1075.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2593.00 TO NODE 2589.00 IS CODE = 31
-----



>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1267.80 DOWNSTREAM(FEET) = 1267.00  
FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.26  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.18  
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 12.92  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2589.00 = 1250.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2589.00 TO NODE 2589.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.92  
RAINFALL INTENSITY(INCH/HR) = 5.00  
TOTAL STREAM AREA(ACRES) = 5.34  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.18

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2592.00 TO NODE 2591.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 83.33  
UPSTREAM ELEVATION(FEET) = 1288.00  
DOWNSTREAM ELEVATION(FEET) = 1286.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.241  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.262  
SUBAREA RUNOFF(CFS) = 0.30  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2591.00 TO NODE 2590.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1286.00 DOWNSTREAM ELEVATION(FEET) = 1274.00

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STREET LENGTH(FEET) = 440.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.70  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.22  
HALFSTREET FLOOD WIDTH(FEET) = 4.46  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.69  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.58  
STREET FLOW TRAVEL TIME(MIN.) = 2.73 Tc(MIN.) = 9.97  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.910  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.93 SUBAREA RUNOFF(CFS) = 2.80  
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 3.04

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.25  
FLOW VELOCITY(FEET/SEC.) = 2.99 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.75  
LONGEST FLOWPATH FROM NODE 2592.00 TO NODE 2590.00 = 523.33 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2590.00 TO NODE 2589.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1268.00 DOWNSTREAM(FEET) = 1267.60  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.95  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.04  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 10.10  
LONGEST FLOWPATH FROM NODE 2592.00 TO NODE 2589.00 = 563.33 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2589.00 TO NODE 2589.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.10
RAINFALL INTENSITY(INCH/HR) = 5.86
TOTAL STREAM AREA(ACRES) = 1.01
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.04

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 16.78 Tc(MIN.) = 12.92
TOTAL AREA(ACRES) = 6.4
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2589.00 = 1250.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2589.00 TO NODE 2584.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1267.60 DOWNSTREAM(FEET) = 1259.00
FLOW LENGTH(FEET) = 385.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.24
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 16.78
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 13.55
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2584.00 = 1635.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2584.00 TO NODE 2584.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.55  
RAINFALL INTENSITY(INCH/HR) = 4.85  
TOTAL STREAM AREA(ACRES) = 6.35  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.78

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2588.00 TO NODE 2587.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 67.65  
UPSTREAM ELEVATION(FEET) = 1282.00  
DOWNSTREAM ELEVATION(FEET) = 1281.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.668  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.999  
SUBAREA RUNOFF(CFS) = 0.36  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.36

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2587.00 TO NODE 2584.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1281.00 DOWNSTREAM ELEVATION(FEET) = 1265.00  
STREET LENGTH(FEET) = 745.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

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\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.94

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.29

HALFSTREET FLOOD WIDTH(FEET) = 8.37

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.02

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.89

STREET FLOW TRAVEL TIME(MIN.) = 4.12 Tc(MIN.) = 11.78

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.304

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.510

SUBAREA AREA(ACRES) = 3.35 SUBAREA RUNOFF(CFS) = 9.06

TOTAL AREA(ACRES) = 3.4 PEAK FLOW RATE(CFS) = 9.33

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.09

FLOW VELOCITY(FEET/SEC.) = 3.46 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.20

LONGEST FLOWPATH FROM NODE 2588.00 TO NODE 2584.00 = 812.65 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2584.00 TO NODE 2584.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 11.78

RAINFALL INTENSITY(INCH/HR) = 5.30

TOTAL STREAM AREA(ACRES) = 3.45

PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.33

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.78        | 13.55     | 4.849                 | 6.35        |
| 2             | 9.33         | 11.78     | 5.304                 | 3.45        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 24.67        | 11.78     | 5.304                 |
| 2             | 25.31        | 13.55     | 4.849                 |

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COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 25.31 Tc(MIN.) = 13.55  
TOTAL AREA(ACRES) = 9.8  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2584.00 = 1635.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2584.00 TO NODE 2568.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1259.00 DOWNSTREAM(FEET) = 1257.00  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.48  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 25.31  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 13.63  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2568.00 = 1700.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2568.00 TO NODE 2568.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2580.00 TO NODE 2579.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 87.50  
UPSTREAM ELEVATION(FEET) = 1291.50  
DOWNSTREAM ELEVATION(FEET) = 1289.00  
ELEVATION DIFFERENCE(FEET) = 2.50  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.289  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.953  
SUBAREA RUNOFF(CFS) = 1.04  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 1.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 2579.00 TO NODE 2578.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1289.00 DOWNSTREAM ELEVATION(FEET) = 1282.00  
STREET LENGTH(FEET) = 785.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.97  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.40  
HALFSTREET FLOOD WIDTH(FEET) = 13.59  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.53  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.01  
STREET FLOW TRAVEL TIME(MIN.) = 5.17 Tc(MIN.) = 11.46  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.400

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.515  
SUBAREA AREA(ACRES) = 2.78 SUBAREA RUNOFF(CFS) = 7.66  
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 8.36

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.46 HALFSTREET FLOOD WIDTH(FEET) = 16.72  
FLOW VELOCITY(FEET/SEC.) = 2.87 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.32  
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2578.00 = 872.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2578.00 TO NODE 2575.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1276.00 DOWNSTREAM(FEET) = 1267.00  
FLOW LENGTH(FEET) = 320.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.46  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.36  
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 12.03

LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2575.00 = 1192.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2575.00 TO NODE 2575.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.03
RAINFALL INTENSITY(INCH/HR) = 5.24
TOTAL STREAM AREA(ACRES) = 3.01
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 2583.00 TO NODE 2582.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00
UPSTREAM ELEVATION(FEET) = 1286.00
DOWNSTREAM ELEVATION(FEET) = 1285.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.889
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.871
SUBAREA RUNOFF(CFS) = 0.18
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 2582.00 TO NODE 2581.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1285.00 DOWNSTREAM ELEVATION(FEET) = 1274.00
STREET LENGTH(FEET) = 315.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150



Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.81  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.21  
 HALFSTREET FLOOD WIDTH(FEET) = 4.26  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.03  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.64  
 STREET FLOW TRAVEL TIME(MIN.) = 1.73 Tc(MIN.) = 9.62  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.045  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
 SUBAREA AREA(ACRES) = 1.06 SUBAREA RUNOFF(CFS) = 3.27  
 TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 3.42

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.25  
 FLOW VELOCITY(FEET/SEC.) = 3.36 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.85  
 LONGEST FLOWPATH FROM NODE 2583.00 TO NODE 2581.00 = 385.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2581.00 TO NODE 2575.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1268.00 DOWNSTREAM(FEET) = 1267.00  
 FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.16  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.42  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 9.78  
 LONGEST FLOWPATH FROM NODE 2583.00 TO NODE 2575.00 = 445.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2575.00 TO NODE 2575.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.78  
 RAINFALL INTENSITY(INCH/HR) = 5.98

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TOTAL STREAM AREA(ACRES) = 1.11  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.42

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.36         | 12.03     | 5.236                 | 3.01        |
| 2             | 3.42         | 9.78      | 5.981                 | 1.11        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 10.23        | 9.78      | 5.981                 |
| 2             | 11.36        | 12.03     | 5.236                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.36 Tc(MIN.) = 12.03  
TOTAL AREA(ACRES) = 4.1  
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2575.00 = 1192.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2575.00 TO NODE 2573.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1267.00 DOWNSTREAM(FEET) = 1263.80  
FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.49  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.36  
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 12.19  
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2573.00 = 1297.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2573.00 TO NODE 2573.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.19  
RAINFALL INTENSITY(INCH/HR) = 5.19  
TOTAL STREAM AREA(ACRES) = 4.12

PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 2577.00 TO NODE 2576.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 1286.00

DOWNSTREAM ELEVATION(FEET) = 1284.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423

SUBAREA RUNOFF(CFS) = 0.30

TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2576.00 TO NODE 2574.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1284.00 DOWNSTREAM ELEVATION(FEET) = 1270.00

STREET LENGTH(FEET) = 455.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.93

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.32

HALFSTREET FLOOD WIDTH(FEET) = 9.50

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.85

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.22

STREET FLOW TRAVEL TIME(MIN.) = 1.97 Tc(MIN.) = 8.97

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.326

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 2.24 SUBAREA RUNOFF(CFS) = 7.23  
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 7.48

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.47  
FLOW VELOCITY(FEET/SEC.) = 4.47 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.68  
LONGEST FLOWPATH FROM NODE 2577.00 TO NODE 2574.00 = 535.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2574.00 TO NODE 2573.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1263.80  
FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.09  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.48  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 8.99  
LONGEST FLOWPATH FROM NODE 2577.00 TO NODE 2573.00 = 545.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2573.00 TO NODE 2573.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.99  
RAINFALL INTENSITY(INCH/HR) = 6.32  
TOTAL STREAM AREA(ACRES) = 2.32  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.48

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.36        | 12.19     | 5.189                 | 4.12        |
| 2             | 7.48         | 8.99      | 6.316                 | 2.32        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.82        | 8.99      | 6.316                 |
| 2             | 17.51        | 12.19     | 5.189                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 17.51 Tc(MIN.) = 12.19  
TOTAL AREA(ACRES) = 6.4  
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2573.00 = 1297.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2573.00 TO NODE 2569.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1263.80 DOWNSTREAM(FEET) = 1263.30  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.81  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 17.51  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 12.35  
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2569.00 = 1362.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2569.00 TO NODE 2569.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.35  
RAINFALL INTENSITY(INCH/HR) = 5.15  
TOTAL STREAM AREA(ACRES) = 6.44  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.51

\*\*\*\*\*

FLOW PROCESS FROM NODE 2572.00 TO NODE 2571.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 1284.00

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DOWNSTREAM ELEVATION(FEET) = 1283.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.889  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.871  
SUBAREA RUNOFF(CFS) = 0.14  
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.14

\*\*\*\*\*

FLOW PROCESS FROM NODE 2571.00 TO NODE 2570.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1283.00 DOWNSTREAM ELEVATION(FEET) = 1270.00  
STREET LENGTH(FEET) = 365.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.00  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.22  
HALFSTREET FLOOD WIDTH(FEET) = 4.52  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.10  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.67  
STREET FLOW TRAVEL TIME(MIN.) = 1.97 Tc(MIN.) = 9.85  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.953

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 1.22 SUBAREA RUNOFF(CFS) = 3.70  
TOTAL AREA(ACRES) = 1.3 PEAK FLOW RATE(CFS) = 3.83

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 6.58  
FLOW VELOCITY(FEET/SEC.) = 3.47 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.89  
LONGEST FLOWPATH FROM NODE 2572.00 TO NODE 2570.00 = 435.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2570.00 TO NODE 2569.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1263.00  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.35  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.83  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 10.01  
LONGEST FLOWPATH FROM NODE 2572.00 TO NODE 2569.00 = 495.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2569.00 TO NODE 2569.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.01  
RAINFALL INTENSITY(INCH/HR) = 5.89  
TOTAL STREAM AREA(ACRES) = 1.26  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.83

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 17.51        | 12.35     | 5.146                 | 6.44        |
| 2             | 3.83         | 10.01     | 5.893                 | 1.26        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.12        | 10.01     | 5.893                 |
| 2             | 20.85        | 12.35     | 5.146                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 20.85 Tc(MIN.) = 12.35  
TOTAL AREA(ACRES) = 7.7  
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2569.00 = 1362.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2569.00 TO NODE 2568.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1263.00 DOWNSTREAM(FEET) = 1257.00
FLOW LENGTH(FEET) = 230.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.35
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.85
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 12.69
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2568.00 = 1592.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2568.00 TO NODE 2568.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 20.85 12.69 5.057 7.70
LONGEST FLOWPATH FROM NODE 2580.00 TO NODE 2568.00 = 1592.50 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 25.31 13.63 4.829 9.80
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2568.00 = 1700.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 44.41 12.69 5.057
2 45.22 13.63 4.829

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 45.22 Tc(MIN.) = 13.63
TOTAL AREA(ACRES) = 17.5

\*\*\*\*\*

FLOW PROCESS FROM NODE 2568.00 TO NODE 2568.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2568.00 TO NODE 2565.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1257.00 DOWNSTREAM(FEET) = 1251.00  
FLOW LENGTH(FEET) = 205.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.31  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 45.22  
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 13.87  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2565.00 = 1905.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2565.00 TO NODE 2565.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.87  
RAINFALL INTENSITY(INCH/HR) = 4.78  
TOTAL STREAM AREA(ACRES) = 17.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 45.22

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2568.20 TO NODE 2567.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 81.58  
UPSTREAM ELEVATION(FEET) = 1271.00  
DOWNSTREAM ELEVATION(FEET) = 1269.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.114  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.346  
SUBAREA RUNOFF(CFS) = 0.26  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.26

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2567.00 TO NODE 2566.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1269.00 DOWNSTREAM ELEVATION(FEET) = 1257.00  
STREET LENGTH(FEET) = 460.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.68  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.32  
HALFSTREET FLOOD WIDTH(FEET) = 9.57  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.56  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.13  
STREET FLOW TRAVEL TIME(MIN.) = 2.16 Tc(MIN.) = 9.27  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.193

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 2.15 SUBAREA RUNOFF(CFS) = 6.79  
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 7.01

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.59  
FLOW VELOCITY(FEET/SEC.) = 4.11 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.56  
LONGEST FLOWPATH FROM NODE 2568.20 TO NODE 2566.00 = 541.58 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2566.00 TO NODE 2565.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1257.00 DOWNSTREAM(FEET) = 1256.80  
FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.97  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.01

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PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 9.29  
LONGEST FLOWPATH FROM NODE 2568.20 TO NODE 2565.00 = 551.58 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2565.00 TO NODE 2565.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.29  
RAINFALL INTENSITY(INCH/HR) = 6.18  
TOTAL STREAM AREA(ACRES) = 2.22  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.01

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 45.22        | 13.87     | 4.775                 | 17.50       |
| 2             | 7.01         | 9.29      | 6.184                 | 2.22        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 37.30        | 9.29      | 6.184                 |
| 2             | 50.64        | 13.87     | 4.775                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 50.64 Tc(MIN.) = 13.87  
TOTAL AREA(ACRES) = 19.7  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2565.00 = 1905.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2565.00 TO NODE 2544.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1256.80 DOWNSTREAM(FEET) = 1256.00  
FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 24.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.05  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 50.64

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PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 13.93  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2544.00 = 1950.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2544.00 TO NODE 2544.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2553.00 TO NODE 2553.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1265.00  
DOWNSTREAM ELEVATION(FEET) = 1263.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.42  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2553.20 TO NODE 2551.20 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 1263.00 DOWNSTREAM ELEVATION(FEET) = 1261.00  
STREET LENGTH(FEET) = 170.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.40  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27

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HALFSTREET FLOOD WIDTH(FEET) = 7.38  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.11  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.58  
 STREET FLOW TRAVEL TIME(MIN.) = 1.34 Tc(MIN.) = 8.34  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.629  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
 SUBAREA AREA(ACRES) = 0.58 SUBAREA RUNOFF(CFS) = 1.96  
 TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.33

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.37  
 FLOW VELOCITY(FEET/SEC.) = 2.34 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.73  
 LONGEST FLOWPATH FROM NODE 2553.00 TO NODE 2551.20 = 250.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2551.20 TO NODE 2552.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1255.00 DOWNSTREAM(FEET) = 1254.00  
 FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.08  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.33  
 PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 8.41  
 LONGEST FLOWPATH FROM NODE 2553.00 TO NODE 2552.00 = 280.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2552.00 TO NODE 2545.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1254.00 DOWNSTREAM(FEET) = 1250.00  
 FLOW LENGTH(FEET) = 325.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.96  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.33  
 PIPE TRAVEL TIME(MIN.) = 1.09 Tc(MIN.) = 9.51  
 LONGEST FLOWPATH FROM NODE 2553.00 TO NODE 2545.00 = 605.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2545.00 TO NODE 2545.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.51  
RAINFALL INTENSITY(INCH/HR) = 6.09  
TOTAL STREAM AREA(ACRES) = 0.69  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.33

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2551.00 TO NODE 2550.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1262.00  
DOWNSTREAM ELEVATION(FEET) = 1261.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 0.47  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2550.00 TO NODE 2549.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1261.00 DOWNSTREAM ELEVATION(FEET) = 1257.00  
STREET LENGTH(FEET) = 330.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.34  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 10.84  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.58  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.89  
STREET FLOW TRAVEL TIME(MIN.) = 2.13 Tc(MIN.) = 9.55  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.075  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 1.84 SUBAREA RUNOFF(CFS) = 5.70  
TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 6.10

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.91  
FLOW VELOCITY(FEET/SEC.) = 2.97 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.20  
LONGEST FLOWPATH FROM NODE 2551.00 TO NODE 2549.00 = 395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2549.00 TO NODE 2545.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1251.00 DOWNSTREAM(FEET) = 1250.00  
FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.80  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.10  
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 9.56  
LONGEST FLOWPATH FROM NODE 2551.00 TO NODE 2545.00 = 405.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2545.00 TO NODE 2545.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.56  
RAINFALL INTENSITY(INCH/HR) = 6.07  
TOTAL STREAM AREA(ACRES) = 1.97  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2548.00 TO NODE 2547.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 68.75  
UPSTREAM ELEVATION(FEET) = 1265.00  
DOWNSTREAM ELEVATION(FEET) = 1264.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.772  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.938  
SUBAREA RUNOFF(CFS) = 0.67  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.67

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2547.00 TO NODE 2546.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1258.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 410.00 CHANNEL SLOPE = 0.0146  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.879  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.42  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.00  
AVERAGE FLOW DEPTH(FEET) = 0.46 TRAVEL TIME(MIN.) = 2.28  
Tc(MIN.) = 10.05  
SUBAREA AREA(ACRES) = 3.15 SUBAREA RUNOFF(CFS) = 9.44  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 10.01

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.64 FLOW VELOCITY(FEET/SEC.) = 3.63  
LONGEST FLOWPATH FROM NODE 2548.00 TO NODE 2546.00 = 478.75 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2546.00 TO NODE 2545.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<



>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1252.00  DOWNSTREAM(FEET) = 1250.00
FLOW LENGTH(FEET) = 45.00  MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.74
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.01
PIPE TRAVEL TIME(MIN.) = 0.06  Tc(MIN.) = 10.11
LONGEST FLOWPATH FROM NODE 2548.00 TO NODE 2545.00 = 523.75 FEET.

```

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*****
FLOW PROCESS FROM NODE 2545.00 TO NODE 2545.00 IS CODE = 1
-----

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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 10.11
RAINFALL INTENSITY(INCH/HR) = 5.86
TOTAL STREAM AREA(ACRES) = 3.34
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.01

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 2.33         | 9.51      | 6.093                 | 0.69        |
| 2             | 6.10         | 9.56      | 6.071                 | 1.97        |
| 3             | 10.01        | 10.11     | 5.855                 | 3.34        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 17.82        | 9.51      | 6.093                 |
| 2             | 17.90        | 9.56      | 6.071                 |
| 3             | 18.14        | 10.11     | 5.855                 |

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 18.14  Tc(MIN.) = 10.11
TOTAL AREA(ACRES) = 6.0
LONGEST FLOWPATH FROM NODE 2553.00 TO NODE 2545.00 = 605.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2545.00 TO NODE 2544.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1250.00 DOWNSTREAM(FEET) = 1249.00
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.17
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 18.14
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 10.22
LONGEST FLOWPATH FROM NODE 2553.00 TO NODE 2544.00 = 665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2544.00 TO NODE 2544.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 18.14 10.22 5.815 6.00
LONGEST FLOWPATH FROM NODE 2553.00 TO NODE 2544.00 = 665.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 50.64 13.93 4.761 19.72
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2544.00 = 1950.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 55.29 10.22 5.815
2 65.49 13.93 4.761

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 65.49 Tc(MIN.) = 13.93
TOTAL AREA(ACRES) = 25.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 2544.00 TO NODE 2544.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2544.00 TO NODE 2542.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1249.00 DOWNSTREAM(FEET) = 1248.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 29.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.60  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 65.49  
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 14.15  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2542.00 = 2075.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2542.00 TO NODE 2542.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.15  
RAINFALL INTENSITY(INCH/HR) = 4.71  
TOTAL STREAM AREA(ACRES) = 25.72  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 65.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2543.00 TO NODE 2542.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1255.00  
DOWNSTREAM ELEVATION(FEET) = 1254.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 1.42  
TOTAL AREA(ACRES) = 0.39 TOTAL RUNOFF(CFS) = 1.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2542.00 TO NODE 2542.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.42
RAINFALL INTENSITY(INCH/HR) = 7.15
TOTAL STREAM AREA(ACRES) = 0.39
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.42

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 65.49        | 14.15     | 4.714                 | 25.72       |
| 2             | 1.42         | 7.42      | 7.151                 | 0.39        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 35.75        | 7.42      | 7.151                 |
| 2             | 66.43        | 14.15     | 4.714                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 66.43 Tc(MIN.) = 14.15
TOTAL AREA(ACRES) = 26.1
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2542.00 = 2075.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2542.00 TO NODE 2515.00 IS CODE = 31

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1254.00 DOWNSTREAM(FEET) = 1246.70
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 26.92
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 66.43
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 14.19
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2515.00 = 2135.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.00 TO NODE 2515.00 IS CODE = 10

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-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

```

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2541.00 TO NODE 2540.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1315.00  
DOWNSTREAM ELEVATION(FEET) = 1310.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.105  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.66  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2540.00 TO NODE 2539.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

\*\*\*\*\*  
UPSTREAM ELEVATION(FEET) = 1310.00 DOWNSTREAM ELEVATION(FEET) = 1285.00  
STREET LENGTH(FEET) = 335.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.73  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.64  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.32  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.48  
STREET FLOW TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 3.16  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 4.15
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 5.81

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.30
FLOW VELOCITY(FEET/SEC.) = 5.91 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.84
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2539.00 = 435.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2539.00 TO NODE 2538.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1279.00 DOWNSTREAM(FEET) = 1270.00
FLOW LENGTH(FEET) = 310.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.70
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.81
PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 3.75
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2538.00 = 745.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2538.00 TO NODE 2538.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 3.75
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.81

\*\*\*\*\*

FLOW PROCESS FROM NODE 2537.00 TO NODE 2536.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1285.00  
DOWNSTREAM ELEVATION(FEET) = 1282.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.392  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.24  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 1.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 2536.00 TO NODE 2538.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1282.00 DOWNSTREAM ELEVATION(FEET) = 1270.00  
STREET LENGTH(FEET) = 210.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.56  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.43  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.16  
STREET FLOW TRAVEL TIME(MIN.) = 0.79 Tc(MIN.) = 3.18  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.893  
SUBAREA AREA(ACRES) = 0.32 SUBAREA RUNOFF(CFS) = 2.63  
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 3.87

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.24  
FLOW VELOCITY(FEET/SEC.) = 4.86 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.41

LONGEST FLOWPATH FROM NODE 2537.00 TO NODE 2538.00 = 305.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2538.00 TO NODE 2538.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.18
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.47
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.87

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.68 Tc(MIN.) = 3.75
TOTAL AREA(ACRES) = 1.2
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2538.00 = 745.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2538.00 TO NODE 2534.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1264.00 DOWNSTREAM(FEET) = 1250.00
FLOW LENGTH(FEET) = 480.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.94
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.68



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PIPE TRAVEL TIME(MIN.) = 0.80 Tc(MIN.) = 4.55  
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2534.00 = 1225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2534.00 TO NODE 2534.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.55  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.17  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.68

\*\*\*\*\*

FLOW PROCESS FROM NODE 2533.00 TO NODE 2532.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 1270.00  
DOWNSTREAM ELEVATION(FEET) = 1265.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.720  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 3.00  
TOTAL AREA(ACRES) = 0.37 TOTAL RUNOFF(CFS) = 3.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 2532.00 TO NODE 2534.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1265.00 DOWNSTREAM ELEVATION(FEET) = 1256.00  
STREET LENGTH(FEET) = 375.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

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STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.30  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.39  
HALFSTREET FLOOD WIDTH(FEET) = 13.03  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.02  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.56  
STREET FLOW TRAVEL TIME(MIN.) = 1.55 Tc(MIN.) = 3.27  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
SUBAREA AREA(ACRES) = 1.06 SUBAREA RUNOFF(CFS) = 8.60  
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 11.60

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.66  
FLOW VELOCITY(FEET/SEC.) = 4.52 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.98  
LONGEST FLOWPATH FROM NODE 2533.00 TO NODE 2534.00 = 445.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2534.00 TO NODE 2534.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.27  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.43  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.60

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.68         | 4.55      | 9.222                 | 1.17        |
| 2             | 11.60        | 3.27      | 9.222                 | 1.43        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

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| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 21.29        | 3.27      | 9.222                 |
| 2             | 21.29        | 4.55      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 21.29 Tc(MIN.) = 4.55  
TOTAL AREA(ACRES) = 2.6  
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2534.00 = 1225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2534.00 TO NODE 2527.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1250.00 DOWNSTREAM(FEET) = 1247.20  
FLOW LENGTH(FEET) = 460.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.55  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 21.29  
PIPE TRAVEL TIME(MIN.) = 1.17 Tc(MIN.) = 5.72  
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2527.00 = 1685.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2527.00 TO NODE 2527.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.72  
RAINFALL INTENSITY(INCH/HR) = 8.45  
TOTAL STREAM AREA(ACRES) = 2.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.29

\*\*\*\*\*

FLOW PROCESS FROM NODE 2526.00 TO NODE 2525.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1256.00  
DOWNSTREAM ELEVATION(FEET) = 1255.00

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ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.417  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.151  
SUBAREA RUNOFF(CFS) = 1.06  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 1.06

\*\*\*\*\*

FLOW PROCESS FROM NODE 2525.00 TO NODE 2527.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1255.00 DOWNSTREAM ELEVATION(FEET) = 1253.20  
STREET LENGTH(FEET) = 355.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.15  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 7.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.42  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.41  
STREET FLOW TRAVEL TIME(MIN.) = 4.16 Tc(MIN.) = 11.58  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.366

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 0.79 SUBAREA RUNOFF(CFS) = 2.16  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 2.96

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.24  
FLOW VELOCITY(FEET/SEC.) = 1.52 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.47  
LONGEST FLOWPATH FROM NODE 2526.00 TO NODE 2527.00 = 420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2527.00 TO NODE 2527.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 11.58
RAINFALL INTENSITY(INCH/HR) = 5.37
TOTAL STREAM AREA(ACRES) = 1.08
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.96

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 22.75 Tc(MIN.) = 5.72
TOTAL AREA(ACRES) = 3.7
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2527.00 = 1685.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2527.00 TO NODE 2515.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1247.20 DOWNSTREAM(FEET) = 1246.70
FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.51
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 22.75
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.81
LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2515.00 = 1730.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.00 TO NODE 2515.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2523.00 TO NODE 2522.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1275.00  
DOWNSTREAM ELEVATION(FEET) = 1274.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.766  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.54  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 1.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2522.00 TO NODE 2520.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1274.00 DOWNSTREAM ELEVATION(FEET) = 1260.00  
STREET LENGTH(FEET) = 820.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.65  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.37  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.83  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.89  
STREET FLOW TRAVEL TIME(MIN.) = 4.82 Tc(MIN.) = 7.59  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.047

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 8.06  
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 9.24

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.53  
FLOW VELOCITY(FEET/SEC.) = 3.19 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.14  
LONGEST FLOWPATH FROM NODE 2523.00 TO NODE 2520.00 = 885.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2520.00 TO NODE 2519.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1248.00 DOWNSTREAM(FEET) = 1247.20  
FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.23  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.24  
PIPE TRAVEL TIME(MIN.) = 2.65 Tc(MIN.) = 10.24  
LONGEST FLOWPATH FROM NODE 2523.00 TO NODE 2519.00 = 1400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2519.00 TO NODE 2519.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.24  
RAINFALL INTENSITY(INCH/HR) = 5.81  
TOTAL STREAM AREA(ACRES) = 1.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 2518.00 TO NODE 2517.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 66.67

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UPSTREAM ELEVATION(FEET) = 1260.00  
DOWNSTREAM ELEVATION(FEET) = 1259.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.825  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.05  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 1.05

\*\*\*\*\*

FLOW PROCESS FROM NODE 2517.00 TO NODE 2519.00 IS CODE = 62

-----  
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1259.00 DOWNSTREAM ELEVATION(FEET) = 1253.20  
STREET LENGTH(FEET) = 510.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.55  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.30  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.31  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.72  
STREET FLOW TRAVEL TIME(MIN.) = 3.68 Tc(MIN.) = 6.50  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.785

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
SUBAREA AREA(ACRES) = 1.01 SUBAREA RUNOFF(CFS) = 6.92  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 7.81

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.72  
FLOW VELOCITY(FEET/SEC.) = 2.62 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.94  
LONGEST FLOWPATH FROM NODE 2518.00 TO NODE 2519.00 = 576.67 FEET.



\*\*\*\*\*

FLOW PROCESS FROM NODE 2519.00 TO NODE 2519.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.50
RAINFALL INTENSITY(INCH/HR) = 7.79
TOTAL STREAM AREA(ACRES) = 1.14
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.81

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 15.07 Tc(MIN.) = 10.24
TOTAL AREA(ACRES) = 2.6
LONGEST FLOWPATH FROM NODE 2523.00 TO NODE 2519.00 = 1400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2519.00 TO NODE 2515.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1247.20 DOWNSTREAM(FEET) = 1246.70
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.88
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.07
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 10.39
LONGEST FLOWPATH FROM NODE 2523.00 TO NODE 2515.00 = 1460.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2515.00 TO NODE 2515.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 15.07        | 10.39     | 5.755                 | 2.63        |

LONGEST FLOWPATH FROM NODE 2523.00 TO NODE 2515.00 = 1460.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 22.75        | 5.81      | 8.368                 | 3.68        |

LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2515.00 = 1730.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 31.18        | 5.81      | 8.368                 |
| 2             | 30.71        | 10.39     | 5.755                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 31.18 Tc(MIN.) = 5.81  
TOTAL AREA(ACRES) = 6.3

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2515.00 TO NODE 2515.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2515.00 TO NODE 2515.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 31.18        | 5.81      | 8.368                 | 6.31        |

LONGEST FLOWPATH FROM NODE 2541.00 TO NODE 2515.00 = 1730.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM | RUNOFF | Tc | INTENSITY | AREA |
|--------|--------|----|-----------|------|
|--------|--------|----|-----------|------|

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 66.43 | 14.19  | 4.706       | 26.11  |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2515.00 = 2135.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 58.40        | 5.81      | 8.368                 |
| 2             | 83.97        | 14.19     | 4.706                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 83.97 Tc(MIN.) = 14.19  
TOTAL AREA(ACRES) = 32.4

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.00 TO NODE 2515.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.00 TO NODE 2514.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1247.00 DOWNSTREAM(FEET) = 1139.00  
FLOW LENGTH(FEET) = 1060.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 26.67  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 83.97  
PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 14.85  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2514.00 = 3195.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2514.00 TO NODE 2514.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.85  
RAINFALL INTENSITY(INCH/HR) = 4.57  
TOTAL STREAM AREA(ACRES) = 32.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 83.97

\*\*\*\*\*

FLOW PROCESS FROM NODE 2513.00 TO NODE 2512.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8800
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 1253.00
DOWNSTREAM ELEVATION(FEET) = 1250.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.631
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.30
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 1.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2512.00 TO NODE 2514.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1250.00 DOWNSTREAM ELEVATION(FEET) = 1145.00
STREET LENGTH(FEET) = 945.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.99
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.26
HALFSTREET FLOOD WIDTH(FEET) = 6.71
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.14
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.60
STREET FLOW TRAVEL TIME(MIN.) = 2.56 Tc(MIN.) = 5.19
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.997

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8800
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880

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SUBAREA AREA(ACRES) = 1.43 SUBAREA RUNOFF(CFS) = 11.32  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 12.59

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.84  
FLOW VELOCITY(FEET/SEC.) = 7.00 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.12  
LONGEST FLOWPATH FROM NODE 2513.00 TO NODE 2514.00 = 1040.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2514.00 TO NODE 2514.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.19  
RAINFALL INTENSITY(INCH/HR) = 9.00  
TOTAL STREAM AREA(ACRES) = 1.59  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.59

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 83.97        | 14.85     | 4.570                 | 32.42       |
| 2             | 12.59        | 5.19      | 8.997                 | 1.59        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 41.96        | 5.19      | 8.997                 |
| 2             | 90.36        | 14.85     | 4.570                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 90.36 Tc(MIN.) = 14.85  
TOTAL AREA(ACRES) = 34.0  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2514.00 = 3195.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2514.00 TO NODE 2510.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1139.00 DOWNSTREAM(FEET) = 1104.00

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FLOW LENGTH(FEET) = 290.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.99  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 90.36  
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 15.02  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2510.00 = 3485.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.00 TO NODE 2510.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.02  
RAINFALL INTENSITY(INCH/HR) = 4.54  
TOTAL STREAM AREA(ACRES) = 34.01  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 90.36

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2509.00 TO NODE 2508.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1142.00  
DOWNSTREAM ELEVATION(FEET) = 1133.00  
ELEVATION DIFFERENCE(FEET) = 9.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.824  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.05  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 1.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2508.00 TO NODE 2510.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1133.00 DOWNSTREAM ELEVATION(FEET) = 1110.00  
STREET LENGTH(FEET) = 185.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.23  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.18  
HALFSTREET FLOOD WIDTH(FEET) = 2.79  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.69  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.04  
STREET FLOW TRAVEL TIME(MIN.) = 0.54 Tc(MIN.) = 2.37  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
SUBAREA AREA(ACRES) = 0.29 SUBAREA RUNOFF(CFS) = 2.35  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.41

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 4.26  
FLOW VELOCITY(FEET/SEC.) = 5.69 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.20  
LONGEST FLOWPATH FROM NODE 2509.00 TO NODE 2510.00 = 280.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2510.00 TO NODE 2510.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.37  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.41

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 90.36        | 15.02     | 4.537                 | 34.01       |
| 2             | 3.41         | 2.37      | 9.222                 | 0.42        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 47.86        | 2.37      | 9.222                 |
| 2             | 92.04        | 15.02     | 4.537                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 92.04 Tc(MIN.) = 15.02  
TOTAL AREA(ACRES) = 34.4  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2510.00 = 3485.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2510.00 TO NODE 2506.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1104.00 DOWNSTREAM(FEET) = 1075.00  
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 27.12  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 92.04  
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 15.20  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2506.00 = 3785.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2506.00 TO NODE 2506.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.20  
RAINFALL INTENSITY(INCH/HR) = 4.50  
TOTAL STREAM AREA(ACRES) = 34.43  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 92.04

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2505.00 TO NODE 2504.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):



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USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1110.00  
 DOWNSTREAM ELEVATION(FEET) = 1095.00  
 ELEVATION DIFFERENCE(FEET) = 15.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.838  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.30  
 TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 1.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2504.00 TO NODE 2506.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1095.00 DOWNSTREAM ELEVATION(FEET) = 1075.00  
 STREET LENGTH(FEET) = 160.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.27

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.18  
 HALFSTREET FLOOD WIDTH(FEET) = 2.86  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.68  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.04  
 STREET FLOW TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 2.31  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
 SUBAREA AREA(ACRES) = 0.24 SUBAREA RUNOFF(CFS) = 1.95  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.25

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 4.06  
FLOW VELOCITY(FEET/SEC.) = 5.74 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.19  
LONGEST FLOWPATH FROM NODE 2505.00 TO NODE 2506.00 = 260.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2506.00 TO NODE 2506.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.31  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.40  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.25

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 92.04        | 15.20     | 4.501                 | 34.43       |
| 2             | 3.25         | 2.31      | 9.222                 | 0.40        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 48.17        | 2.31      | 9.222                 |
| 2             | 93.62        | 15.20     | 4.501                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 93.62 Tc(MIN.) = 15.20  
TOTAL AREA(ACRES) = 34.8  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2506.00 = 3785.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2506.00 TO NODE 2502.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1069.00 DOWNSTREAM(FEET) = 1034.00  
FLOW LENGTH(FEET) = 190.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.74

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ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 93.62  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 15.29  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2502.00 = 3975.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2502.00 TO NODE 2502.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.29  
RAINFALL INTENSITY(INCH/HR) = 4.48  
TOTAL STREAM AREA(ACRES) = 34.83  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 93.62

\*\*\*\*\*

FLOW PROCESS FROM NODE 2501.00 TO NODE 2500.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1075.00  
DOWNSTREAM ELEVATION(FEET) = 1062.00  
ELEVATION DIFFERENCE(FEET) = 13.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.644  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.05  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 1.05

\*\*\*\*\*

FLOW PROCESS FROM NODE 2500.00 TO NODE 2502.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1062.00 DOWNSTREAM ELEVATION(FEET) = 1040.00  
STREET LENGTH(FEET) = 190.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.24

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.19

HALFSTREET FLOOD WIDTH(FEET) = 2.99

AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.40

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.01

STREET FLOW TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 2.23

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8900

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.887

SUBAREA AREA(ACRES) = 0.29 SUBAREA RUNOFF(CFS) = 2.38

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.44

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 4.39

FLOW VELOCITY(FEET/SEC.) = 5.53 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.18

LONGEST FLOWPATH FROM NODE 2501.00 TO NODE 2502.00 = 270.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2502.00 TO NODE 2502.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 2.23

RAINFALL INTENSITY(INCH/HR) = 9.22

TOTAL STREAM AREA(ACRES) = 0.42

PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.44

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 93.62        | 15.29     | 4.484                 | 34.83       |
| 2             | 3.44         | 2.23      | 9.222                 | 0.42        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 48.96        | 2.23      | 9.222                 |
| 2             | 95.29        | 15.29     | 4.484                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 95.29 Tc(MIN.) = 15.29  
 TOTAL AREA(ACRES) = 35.2  
 LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2502.00 = 3975.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2502.00 TO NODE 2499.20 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1034.00 DOWNSTREAM(FEET) = 994.00  
 FLOW LENGTH(FEET) = 305.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 30.26  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 95.29  
 PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 15.46  
 LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2499.20 = 4280.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2499.20 TO NODE 2499.20 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 15.46  
 RAINFALL INTENSITY(INCH/HR) = 4.45  
 TOTAL STREAM AREA(ACRES) = 35.25  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 95.29

\*\*\*\*\*

FLOW PROCESS FROM NODE 2499.60 TO NODE 2499.80 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .8900  
 S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1040.00  
 DOWNSTREAM ELEVATION(FEET) = 1022.00  
 ELEVATION DIFFERENCE(FEET) = 18.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.755  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.64  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 2499.80 TO NODE 2499.20 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1022.00 DOWNSTREAM ELEVATION(FEET) = 1000.00  
 STREET LENGTH(FEET) = 185.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.75  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.20  
 HALFSTREET FLOOD WIDTH(FEET) = 3.66  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.46  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.09  
 STREET FLOW TRAVEL TIME(MIN.) = 0.57 Tc(MIN.) = 2.32

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8900  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.890  
 SUBAREA AREA(ACRES) = 0.27 SUBAREA RUNOFF(CFS) = 2.22  
 TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 3.86

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.22 HALFSTREET FLOOD WIDTH(FEET) = 4.65

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FLOW VELOCITY(FEET/SEC.) = 5.76 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.26  
LONGEST FLOWPATH FROM NODE 2499.60 TO NODE 2499.20 = 285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2499.20 TO NODE 2499.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.32  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.47  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.86

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 95.29        | 15.46     | 4.453                 | 35.25       |
| 2             | 3.86         | 2.32      | 9.222                 | 0.47        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 49.87        | 2.32      | 9.222                 |
| 2             | 97.15        | 15.46     | 4.453                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 97.15 Tc(MIN.) = 15.46  
TOTAL AREA(ACRES) = 35.7  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2499.20 = 4280.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2499.20 TO NODE 2472.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 994.00 DOWNSTREAM(FEET) = 970.00  
FLOW LENGTH(FEET) = 350.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.63  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 97.15

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PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 15.71  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2472.00 = 4630.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2472.00 TO NODE 2472.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2487.00 TO NODE 2486.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1405.00  
DOWNSTREAM ELEVATION(FEET) = 1375.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2486.00 TO NODE 2485.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1375.00 DOWNSTREAM(FEET) = 1294.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.2025  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.710  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.34  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.15  
AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 1.08  
Tc(MIN.) = 8.19  
SUBAREA AREA(ACRES) = 3.38 SUBAREA RUNOFF(CFS) = 5.67  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 3.7 PEAK FLOW RATE(CFS) = 6.12



END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 FLOW VELOCITY(FEET/SEC.) = 7.63  
LONGEST FLOWPATH FROM NODE 2487.00 TO NODE 2485.00 = 500.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2485.00 TO NODE 2485.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.19  
RAINFALL INTENSITY(INCH/HR) = 6.71  
TOTAL STREAM AREA(ACRES) = 3.65  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.12

\*\*\*\*\*

FLOW PROCESS FROM NODE 2484.00 TO NODE 2483.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1325.00  
DOWNSTREAM ELEVATION(FEET) = 1320.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.574  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.513  
SUBAREA RUNOFF(CFS) = 0.41  
TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 0.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 2483.00 TO NODE 2485.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1320.00 DOWNSTREAM(FEET) = 1294.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 205.00 CHANNEL SLOPE = 0.1268  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.41  
FLOW VELOCITY(FEET/SEC) = 4.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.72 Tc(MIN.) = 9.29  
LONGEST FLOWPATH FROM NODE 2484.00 TO NODE 2485.00 = 300.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2485.00 TO NODE 2485.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.29  
RAINFALL INTENSITY(INCH/HR) = 6.18  
TOTAL STREAM AREA(ACRES) = 0.25  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.41

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.12         | 8.19      | 6.710                 | 3.65        |
| 2             | 0.41         | 9.29      | 6.182                 | 0.25        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 6.48         | 8.19      | 6.710                 |
| 2             | 6.05         | 9.29      | 6.182                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.48 Tc(MIN.) = 8.19  
TOTAL AREA(ACRES) = 3.9  
LONGEST FLOWPATH FROM NODE 2487.00 TO NODE 2485.00 = 500.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2485.00 TO NODE 2482.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1288.00 DOWNSTREAM(FEET) = 1251.00  
FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 22.78  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.48  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 8.26

LONGEST FLOWPATH FROM NODE 2487.00 TO NODE 2482.00 = 595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2482.00 TO NODE 2482.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.26
RAINFALL INTENSITY(INCH/HR) = 6.67
TOTAL STREAM AREA(ACRES) = 3.90
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 2481.00 TO NODE 2480.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1270.00
DOWNSTREAM ELEVATION(FEET) = 1268.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.083
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.866
SUBAREA RUNOFF(CFS) = 0.18
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.18

\*\*\*\*\*

FLOW PROCESS FROM NODE 2480.00 TO NODE 2482.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1268.00 DOWNSTREAM(FEET) = 1257.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 425.00 CHANNEL SLOPE = 0.0259
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.866
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.08
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.09
AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 3.39

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Tc(MIN.) = 13.47  
SUBAREA AREA(ACRES) = 1.46 SUBAREA RUNOFF(CFS) = 1.78  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 1.92

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 2.59  
LONGEST FLOWPATH FROM NODE 2481.00 TO NODE 2482.00 = 505.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2482.00 TO NODE 2482.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.47  
RAINFALL INTENSITY(INCH/HR) = 4.87  
TOTAL STREAM AREA(ACRES) = 1.58  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.92

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.48         | 8.26      | 6.674                 | 3.90        |
| 2             | 1.92         | 13.47     | 4.866                 | 1.58        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 7.66         | 8.26      | 6.674                 |
| 2             | 6.65         | 13.47     | 4.866                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 7.66 Tc(MIN.) = 8.26  
TOTAL AREA(ACRES) = 5.5  
LONGEST FLOWPATH FROM NODE 2487.00 TO NODE 2482.00 = 595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2482.00 TO NODE 2478.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

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ELEVATION DATA: UPSTREAM(FEET) = 1251.00 DOWNSTREAM(FEET) = 1247.00  
FLOW LENGTH(FEET) = 430.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.04  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.66  
PIPE TRAVEL TIME(MIN.) = 1.19 Tc(MIN.) = 9.44  
LONGEST FLOWPATH FROM NODE 2487.00 TO NODE 2478.00 = 1025.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2478.00 TO NODE 2478.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.44  
RAINFALL INTENSITY(INCH/HR) = 6.12  
TOTAL STREAM AREA(ACRES) = 5.48  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 2477.00 TO NODE 2476.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1300.00  
DOWNSTREAM ELEVATION(FEET) = 1298.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.083  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.866  
SUBAREA RUNOFF(CFS) = 0.15  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.15

\*\*\*\*\*

FLOW PROCESS FROM NODE 2476.00 TO NODE 2475.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1298.00 DOWNSTREAM(FEET) = 1268.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 410.00 CHANNEL SLOPE = 0.0732  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.915  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.44  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.15  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 3.18  
 Tc(MIN.) = 13.26  
 SUBAREA AREA(ACRES) = 0.48 SUBAREA RUNOFF(CFS) = 0.59  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
 TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 0.71

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 2.53  
 LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2475.00 = 490.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2475.00 TO NODE 2478.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1262.00 DOWNSTREAM(FEET) = 1247.00  
 FLOW LENGTH(FEET) = 995.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.77  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.71  
 PIPE TRAVEL TIME(MIN.) = 4.40 Tc(MIN.) = 17.66  
 LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2478.00 = 1485.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2478.00 TO NODE 2478.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 17.66  
 RAINFALL INTENSITY(INCH/HR) = 4.09  
 TOTAL STREAM AREA(ACRES) = 0.58  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.71

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

|   |      |       | P-25d.TXT |      |
|---|------|-------|-----------|------|
| 1 | 7.66 | 9.44  | 6.119     | 5.48 |
| 2 | 0.71 | 17.66 | 4.086     | 0.58 |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | RUNOFF<br>(CFS) | Tc<br>(MIN.) | INTENSITY<br>(INCH/HOUR) |
|------------------|-----------------|--------------|--------------------------|
| 1                | 8.04            | 9.44         | 6.119                    |
| 2                | 5.83            | 17.66        | 4.086                    |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.04 Tc(MIN.) = 9.44  
TOTAL AREA(ACRES) = 6.1  
LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2478.00 = 1485.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2478.00 TO NODE 2515.60 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1247.00 DOWNSTREAM(FEET) = 1246.00  
FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.61  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.04  
PIPE TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 9.83  
LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2515.60 = 1615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.60 TO NODE 2515.60 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.83  
RAINFALL INTENSITY(INCH/HR) = 5.96  
TOTAL STREAM AREA(ACRES) = 6.06  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.80 TO NODE 2515.70 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1254.00  
DOWNSTREAM ELEVATION(FEET) = 1253.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.685  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.650  
SUBAREA RUNOFF(CFS) = 0.34  
TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.70 TO NODE 2515.60 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1253.00 DOWNSTREAM(FEET) = 1252.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 510.00 CHANNEL SLOPE = 0.0020  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.982

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.99  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.10  
AVERAGE FLOW DEPTH(FEET) = 0.46 TRAVEL TIME(MIN.) = 7.70  
Tc(MIN.) = 18.38  
SUBAREA AREA(ACRES) = 3.25 SUBAREA RUNOFF(CFS) = 3.24  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 3.47

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.63 FLOW VELOCITY(FEET/SEC.) = 1.30  
LONGEST FLOWPATH FROM NODE 2515.80 TO NODE 2515.60 = 575.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.60 TO NODE 2515.60 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.38



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RAINFALL INTENSITY(INCH/HR) = 3.98  
TOTAL STREAM AREA(ACRES) = 3.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.47

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.04         | 9.83      | 5.963                 | 6.06        |
| 2             | 3.47         | 18.38     | 3.982                 | 3.49        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 9.90         | 9.83      | 5.963                 |
| 2             | 8.84         | 18.38     | 3.982                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.90 Tc(MIN.) = 9.83  
TOTAL AREA(ACRES) = 9.6  
LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2515.60 = 1615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2515.60 TO NODE 2474.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1246.00 DOWNSTREAM(FEET) = 1244.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.26  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.90  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 9.90  
LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2474.00 = 1665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2474.00 TO NODE 2473.50 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1244.00 DOWNSTREAM(FEET) = 978.50  
CHANNEL LENGTH THRU SUBAREA(FEET) = 955.00 CHANNEL SLOPE = 0.2780

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CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.465  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.07  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.79  
AVERAGE FLOW DEPTH(FEET) = 0.38 TRAVEL TIME(MIN.) = 1.35  
Tc(MIN.) = 11.25  
SUBAREA AREA(ACRES) = 10.53 SUBAREA RUNOFF(CFS) = 14.39  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 20.1 PEAK FLOW RATE(CFS) = 27.43

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.50 FLOW VELOCITY(FEET/SEC.) = 13.76  
LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2473.50 = 2620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2473.50 TO NODE 2473.50 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.25  
RAINFALL INTENSITY(INCH/HR) = 5.46  
TOTAL STREAM AREA(ACRES) = 20.08  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 27.43

\*\*\*\*\*

FLOW PROCESS FROM NODE 2488.00 TO NODE 2473.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1250.00  
DOWNSTREAM ELEVATION(FEET) = 1200.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.92  
TOTAL AREA(ACRES) = 0.50 TOTAL RUNOFF(CFS) = 0.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 2473.00 TO NODE 2473.50 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1200.00 DOWNSTREAM(FEET) = 978.50
CHANNEL LENGTH THRU SUBAREA(FEET) = 930.00 CHANNEL SLOPE = 0.2382
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.467

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2700
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.43
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.91
AVERAGE FLOW DEPTH(FEET) = 0.32 TRAVEL TIME(MIN.) = 1.56
Tc(MIN.) = 8.67
SUBAREA AREA(ACRES) = 12.02 SUBAREA RUNOFF(CFS) = 20.99
AREA-AVERAGE RUNOFF COEFFICIENT = 0.269
TOTAL AREA(ACRES) = 12.5 PEAK FLOW RATE(CFS) = 21.80

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.46 FLOW VELOCITY(FEET/SEC.) = 12.07
LONGEST FLOWPATH FROM NODE 2488.00 TO NODE 2473.50 = 1030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2473.50 TO NODE 2473.50 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.67
RAINFALL INTENSITY(INCH/HR) = 6.47
TOTAL STREAM AREA(ACRES) = 12.52
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.80

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 44.98        | 8.67      | 6.467                 |
| 2             | 45.85        | 11.25     | 5.465                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 45.85 Tc(MIN.) = 11.25  
TOTAL AREA(ACRES) = 32.6  
LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2473.50 = 2620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2473.50 TO NODE 2472.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 978.50 DOWNSTREAM(FEET) = 976.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 410.00 CHANNEL SLOPE = 0.0061  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.010  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 55.56  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.21  
AVERAGE FLOW DEPTH(FEET) = 1.93 TRAVEL TIME(MIN.) = 1.62  
Tc(MIN.) = 12.88  
SUBAREA AREA(ACRES) = 13.37 SUBAREA RUNOFF(CFS) = 19.43  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.267  
TOTAL AREA(ACRES) = 46.0 PEAK FLOW RATE(CFS) = 61.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 2.02 FLOW VELOCITY(FEET/SEC.) = 4.33  
LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2472.00 = 3030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2472.00 TO NODE 2472.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 61.46        | 12.88     | 5.010                 | 45.97       |

LONGEST FLOWPATH FROM NODE 2477.00 TO NODE 2472.00 = 3030.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 97.15        | 15.71     | 4.407                 | 35.72       |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2472.00 = 4630.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 141.10       | 12.88     | 5.010                 |
| 2             | 151.22       | 15.71     | 4.407                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 151.22 Tc(MIN.) = 15.71  
 TOTAL AREA(ACRES) = 81.7

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2472.00 TO NODE 2472.00 IS CODE = 12

-----  
 >>>>>CLEAR MEMORY BANK # 1 <<<<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2472.00 TO NODE 2472.00 IS CODE = 7

-----  
 >>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<<  
 =====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 15.71 RAIN INTENSITY(INCH/HOUR) = 4.41  
 TOTAL AREA(ACRES) = 81.70 TOTAL RUNOFF(CFS) = 20.10

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2472.00 TO NODE 2471.00 IS CODE = 31

-----  
 >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 970.00 DOWNSTREAM(FEET) = 920.00  
 FLOW LENGTH(FEET) = 385.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 20.89  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 20.10  
 PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 16.02  
 LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2471.00 = 5015.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2471.00 TO NODE 2471.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.02  
RAINFALL INTENSITY(INCH/HR) = 4.35  
TOTAL STREAM AREA(ACRES) = 81.70  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2470.00 TO NODE 2469.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1030.00  
DOWNSTREAM ELEVATION(FEET) = 1024.00  
ELEVATION DIFFERENCE(FEET) = 6.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.420  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.589  
SUBAREA RUNOFF(CFS) = 0.97  
TOTAL AREA(ACRES) = 0.59 TOTAL RUNOFF(CFS) = 0.97

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2469.00 TO NODE 2471.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1024.00 DOWNSTREAM(FEET) = 934.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 925.00 CHANNEL SLOPE = 0.0973  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.139  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.82  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.89  
AVERAGE FLOW DEPTH(FEET) = 0.14 TRAVEL TIME(MIN.) = 3.96  
Tc(MIN.) = 12.38  
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 1.67

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 2.43

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 4.42  
LONGEST FLOWPATH FROM NODE 2470.00 TO NODE 2471.00 = 1025.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2471.00 TO NODE 2471.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.38  
RAINFALL INTENSITY(INCH/HR) = 5.14  
TOTAL STREAM AREA(ACRES) = 1.89  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.43

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.10        | 16.02     | 4.352                 | 81.70       |
| 2             | 2.43         | 12.38     | 5.139                 | 1.89        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 17.96        | 12.38     | 5.139                 |
| 2             | 22.16        | 16.02     | 4.352                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 22.16 Tc(MIN.) = 16.02  
TOTAL AREA(ACRES) = 83.6  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2471.00 = 5015.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2471.00 TO NODE 2459.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 928.00 DOWNSTREAM(FEET) = 914.00  
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013

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DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.71  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 22.16  
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 16.22  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2459.00 = 5215.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2459.00 TO NODE 2459.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2468.00 TO NODE 2467.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1255.00  
DOWNSTREAM ELEVATION(FEET) = 1197.00  
ELEVATION DIFFERENCE(FEET) = 58.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.66  
TOTAL AREA(ACRES) = 0.36 TOTAL RUNOFF(CFS) = 0.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2467.00 TO NODE 2460.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1197.00 DOWNSTREAM(FEET) = 923.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1265.00 CHANNEL SLOPE = 0.2166  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.855  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.44  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.01  
AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 3.01



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Tc(MIN.) = 10.11  
SUBAREA AREA(ACRES) = 5.11 SUBAREA RUNOFF(CFS) = 7.48  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 5.5 PEAK FLOW RATE(CFS) = 8.01

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.26 FLOW VELOCITY(FEET/SEC.) = 8.59  
LONGEST FLOWPATH FROM NODE 2468.00 TO NODE 2460.00 = 1365.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2460.00 TO NODE 2460.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2465.00 TO NODE 2464.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1225.00  
DOWNSTREAM ELEVATION(FEET) = 1215.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.45 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2464.00 TO NODE 2463.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1215.00 DOWNSTREAM(FEET) = 912.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 2135.00 CHANNEL SLOPE = 0.1419  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.112  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.71

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TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.62  
AVERAGE FLOW DEPTH(FEET) = 0.25 TRAVEL TIME(MIN.) = 5.38  
Tc(MIN.) = 12.48  
SUBAREA AREA(ACRES) = 7.44 SUBAREA RUNOFF(CFS) = 9.51  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 7.9 PEAK FLOW RATE(CFS) = 10.08

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 FLOW VELOCITY(FEET/SEC.) = 8.05  
LONGEST FLOWPATH FROM NODE 2465.00 TO NODE 2463.00 = 2235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2463.00 TO NODE 2463.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.48  
RAINFALL INTENSITY(INCH/HR) = 5.11  
TOTAL STREAM AREA(ACRES) = 7.89  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.08

\*\*\*\*\*

FLOW PROCESS FROM NODE 2462.00 TO NODE 2461.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 925.00  
DOWNSTREAM ELEVATION(FEET) = 923.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.287  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.955  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 2461.00 TO NODE 2463.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 923.00 DOWNSTREAM ELEVATION(FEET) = 916.00  
STREET LENGTH(FEET) = 590.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.20

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.34

HALFSTREET FLOOD WIDTH(FEET) = 10.53

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.52

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.85

STREET FLOW TRAVEL TIME(MIN.) = 3.89 Tc(MIN.) = 10.18

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.829

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.570

SUBAREA AREA(ACRES) = 3.38 SUBAREA RUNOFF(CFS) = 11.23

TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 11.60

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.66

FLOW VELOCITY(FEET/SEC.) = 2.92 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.17

LONGEST FLOWPATH FROM NODE 2462.00 TO NODE 2463.00 = 670.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2463.00 TO NODE 2463.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 10.18

RAINFALL INTENSITY(INCH/HR) = 5.83

TOTAL STREAM AREA(ACRES) = 3.49

PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.60

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.08        | 12.48     | 5.112                 | 7.89        |

2 11.60 10.18 5.829 3.49

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.82        | 10.18     | 5.829                 |
| 2             | 20.25        | 12.48     | 5.112                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 20.25 Tc(MIN.) = 12.48  
TOTAL AREA(ACRES) = 11.4  
LONGEST FLOWPATH FROM NODE 2465.00 TO NODE 2463.00 = 2235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2463.00 TO NODE 2460.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 913.00 DOWNSTREAM(FEET) = 912.00  
FLOW LENGTH(FEET) = 225.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.84  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.25  
PIPE TRAVEL TIME(MIN.) = 0.64 Tc(MIN.) = 13.12  
LONGEST FLOWPATH FROM NODE 2465.00 TO NODE 2460.00 = 2460.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2460.00 TO NODE 2460.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.25        | 13.12     | 4.949                 | 11.38       |

LONGEST FLOWPATH FROM NODE 2465.00 TO NODE 2460.00 = 2460.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.01         | 10.11     | 5.855                 | 5.47        |

LONGEST FLOWPATH FROM NODE 2468.00 TO NODE 2460.00 = 1365.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 23.61        | 10.11     | 5.855                 |
| 2             | 27.02        | 13.12     | 4.949                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 27.02 Tc(MIN.) = 13.12  
TOTAL AREA(ACRES) = 16.9

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2460.00 TO NODE 2460.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2460.00 TO NODE 2459.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 912.00 DOWNSTREAM(FEET) = 911.00  
FLOW LENGTH(FEET) = 145.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.37  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 27.02  
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 13.45  
LONGEST FLOWPATH FROM NODE 2465.00 TO NODE 2459.00 = 2605.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2459.00 TO NODE 2459.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK #1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 27.02        | 13.45     | 4.871                 | 16.85       |

LONGEST FLOWPATH FROM NODE 2465.00 TO NODE 2459.00 = 2605.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 22.16        | 16.22     | 4.317                 | 83.59       |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2459.00 = 5215.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 45.40        | 13.45     | 4.871                 |
| 2             | 46.11        | 16.22     | 4.317                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 46.11 Tc(MIN.) = 16.22  
TOTAL AREA(ACRES) = 100.4

\*\*\*\*\*

FLOW PROCESS FROM NODE 2459.00 TO NODE 2459.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 2459.00 TO NODE 2458.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 911.00 DOWNSTREAM(FEET) = 905.00  
FLOW LENGTH(FEET) = 635.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.34  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 46.11  
PIPE TRAVEL TIME(MIN.) = 1.13 Tc(MIN.) = 17.35  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2458.00 = 5850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2458.00 TO NODE 2458.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 2457.00 TO NODE 2456.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

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UPSTREAM ELEVATION(FEET) = 920.00  
DOWNSTREAM ELEVATION(FEET) = 917.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914  
SUBAREA RUNOFF(CFS) = 0.86  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.86

\*\*\*\*\*

FLOW PROCESS FROM NODE 2456.00 TO NODE 2456.10 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 917.00 DOWNSTREAM ELEVATION(FEET) = 910.00  
STREET LENGTH(FEET) = 355.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.77  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.34  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.39  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.20  
STREET FLOW TRAVEL TIME(MIN.) = 1.74 Tc(MIN.) = 8.08  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.765

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 2.02 SUBAREA RUNOFF(CFS) = 7.79  
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 8.52

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.41  
FLOW VELOCITY(FEET/SEC.) = 3.89 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.61  
LONGEST FLOWPATH FROM NODE 2457.00 TO NODE 2456.10 = 450.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2456.10 TO NODE 2455.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 904.00 DOWNSTREAM(FEET) = 897.00
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.86
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.52
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 8.65
LONGEST FLOWPATH FROM NODE 2457.00 TO NODE 2455.00 = 750.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2455.00 TO NODE 2455.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.65
RAINFALL INTENSITY(INCH/HR) = 6.48
TOTAL STREAM AREA(ACRES) = 2.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.52

\*\*\*\*\*
FLOW PROCESS FROM NODE 2456.20 TO NODE 2456.30 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 912.00
DOWNSTREAM ELEVATION(FEET) = 909.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.059
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.147
SUBAREA RUNOFF(CFS) = 0.42
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*
FLOW PROCESS FROM NODE 2456.30 TO NODE 2455.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<



>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 909.00 DOWNSTREAM ELEVATION(FEET) = 903.00  
STREET LENGTH(FEET) = 245.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.05  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.09  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.73  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.30  
STREET FLOW TRAVEL TIME(MIN.) = 1.10 Tc(MIN.) = 7.15  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.319

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 4.61 SUBAREA RUNOFF(CFS) = 19.23  
TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 19.61

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.59  
FLOW VELOCITY(FEET/SEC.) = 4.36 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.82  
LONGEST FLOWPATH FROM NODE 2456.20 TO NODE 2455.00 = 335.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2455.00 TO NODE 2455.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.15  
RAINFALL INTENSITY(INCH/HR) = 7.32  
TOTAL STREAM AREA(ACRES) = 4.70  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.61

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.52         | 8.65      | 6.477                 | 2.21        |
| 2             | 19.61        | 7.15      | 7.319                 | 4.70        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 26.66        | 7.15      | 7.319                 |
| 2             | 25.87        | 8.65      | 6.477                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.66 Tc(MIN.) = 7.15  
TOTAL AREA(ACRES) = 6.9  
LONGEST FLOWPATH FROM NODE 2457.00 TO NODE 2455.00 = 750.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2455.00 TO NODE 2454.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 897.00 DOWNSTREAM(FEET) = 896.00  
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.05  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.66  
PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 7.53  
LONGEST FLOWPATH FROM NODE 2457.00 TO NODE 2454.00 = 910.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2454.00 TO NODE 2453.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 902.00 DOWNSTREAM(FEET) = 901.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 35.00 CHANNEL SLOPE = 0.0286  
CHANNEL FLOW THRU SUBAREA(CFS) = 26.66  
FLOW VELOCITY(FEET/SEC) = 5.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.64  
LONGEST FLOWPATH FROM NODE 2457.00 TO NODE 2453.00 = 945.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2453.00 TO NODE 2458.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 901.00 DOWNSTREAM(FEET) = 900.00  
FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 28.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.49  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.66  
PIPE TRAVEL TIME(MIN.) = 1.91 Tc(MIN.) = 9.55  
LONGEST FLOWPATH FROM NODE 2457.00 TO NODE 2458.00 = 1460.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2458.00 TO NODE 2458.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 26.66        | 9.55      | 6.075                 | 6.91        |

LONGEST FLOWPATH FROM NODE 2457.00 TO NODE 2458.00 = 1460.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 46.11        | 17.35     | 4.133                 | 100.44      |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2458.00 = 5850.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 52.04        | 9.55      | 6.075                 |
| 2             | 64.24        | 17.35     | 4.133                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 64.24 Tc(MIN.) = 17.35  
TOTAL AREA(ACRES) = 107.3

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2458.00 TO NODE 2458.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2458.00 TO NODE 2452.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |               |                    |        |
|--|---------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                     | 902.00        | DOWNSTREAM(FEET) = | 896.00 |
| FLOW LENGTH(FEET) =                                  | 315.00        | MANNING'S N =      | 0.013  |
| DEPTH OF FLOW IN 33.0 INCH PIPE IS                   | 25.1 INCHES   |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                      | 13.24         |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =                      | 33.00         | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                     | 64.24         |                    |        |
| PIPE TRAVEL TIME(MIN.) =                             | 0.40          | Tc(MIN.) =         | 17.75  |
| LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2452.00 = | 6165.00 FEET. |                    |        |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2452.00 TO NODE 2452.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

|  |        |  |  |
|--|--------|--|--|
| TOTAL NUMBER OF STREAMS =                            | 2      |  |  |
| CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE: |        |  |  |
| TIME OF CONCENTRATION(MIN.) =                        | 17.75  |  |  |
| RAINFALL INTENSITY(INCH/HR) =                        | 4.07   |  |  |
| TOTAL STREAM AREA(ACRES) =                           | 107.35 |  |  |
| PEAK FLOW RATE(CFS) AT CONFLUENCE =                  | 64.24  |  |  |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2451.00 TO NODE 2450.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

|  |         |                     |      |
|--|---------|---------------------|------|
| USER-SPECIFIED RUNOFF COEFFICIENT =  | .2500   |                     |      |
| S.C.S. CURVE NUMBER (AMC II) =   | 0       |                     |      |
| INITIAL SUBAREA FLOW-LENGTH(FEET) =  | 100.00  |                     |      |
| UPSTREAM ELEVATION(FEET) =   | 1185.00 |                     |      |
| DOWNSTREAM ELEVATION(FEET) =   | 1150.00 |                     |      |
| ELEVATION DIFFERENCE(FEET) =   | 35.00   |                     |      |
| SUBAREA OVERLAND TIME OF FLOW(MIN.) =                                      | 7.102   |                     |      |
| WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION! |         |                     |      |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =                                   | 7.353   |                     |      |
| SUBAREA RUNOFF(CFS) =  | 0.50    |                     |      |
| TOTAL AREA(ACRES) =  | 0.27    | TOTAL RUNOFF(CFS) = | 0.50 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2450.00 TO NODE 2449.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1150.00 DOWNSTREAM(FEET) = 960.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 615.00 CHANNEL SLOPE = 0.3089  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.751  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.49  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.18  
AVERAGE FLOW DEPTH(FEET) = 0.26 TRAVEL TIME(MIN.) = 1.01  
Tc(MIN.) = 8.11  
SUBAREA AREA(ACRES) = 10.64 SUBAREA RUNOFF(CFS) = 17.96  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 10.9 PEAK FLOW RATE(CFS) = 18.41

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 FLOW VELOCITY(FEET/SEC.) = 12.64  
LONGEST FLOWPATH FROM NODE 2451.00 TO NODE 2449.00 = 715.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2449.00 TO NODE 2452.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 954.00 DOWNSTREAM(FEET) = 896.00  
FLOW LENGTH(FEET) = 820.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.20  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 18.41  
PIPE TRAVEL TIME(MIN.) = 0.84 Tc(MIN.) = 8.95  
LONGEST FLOWPATH FROM NODE 2451.00 TO NODE 2452.00 = 1535.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2452.00 TO NODE 2452.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.95

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RAINFALL INTENSITY(INCH/HR) = 6.33  
TOTAL STREAM AREA(ACRES) = 10.91  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.41

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 64.24        | 17.75     | 4.073                 | 107.35      |
| 2             | 18.41        | 8.95      | 6.334                 | 10.91       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 50.82        | 8.95      | 6.334                 |
| 2             | 76.09        | 17.75     | 4.073                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 76.09 Tc(MIN.) = 17.75  
TOTAL AREA(ACRES) = 118.3  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2452.00 = 6165.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2452.00 TO NODE 2448.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 896.00 DOWNSTREAM(FEET) = 889.00  
FLOW LENGTH(FEET) = 210.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 23.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.25  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 76.09  
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 17.95  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2448.00 = 6375.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2448.00 TO NODE 2448.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2447.00 TO NODE 2446.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====
\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 67.65
UPSTREAM ELEVATION(FEET) = 912.00
DOWNSTREAM ELEVATION(FEET) = 911.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.888
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.500
SUBAREA RUNOFF(CFS) = 0.38
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 2446.00 TO NODE 2445.00 IS CODE = 51

-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 911.00 DOWNSTREAM(FEET) = 900.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 620.00 CHANNEL SLOPE = 0.0177
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.781

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.40
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.02
AVERAGE FLOW DEPTH(FEET) = 0.39 TRAVEL TIME(MIN.) = 3.42
Tc(MIN.) = 10.31
SUBAREA AREA(ACRES) = 2.40 SUBAREA RUNOFF(CFS) = 7.91
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 8.21

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.55 FLOW VELOCITY(FEET/SEC.) = 3.67
LONGEST FLOWPATH FROM NODE 2447.00 TO NODE 2445.00 = 687.65 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2445.00 TO NODE 2445.00 IS CODE = 1

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.31

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RAINFALL INTENSITY(INCH/HR) = 5.78  
TOTAL STREAM AREA(ACRES) = 2.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.21

\*\*\*\*\*

FLOW PROCESS FROM NODE 2444.00 TO NODE 2443.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 83.33  
UPSTREAM ELEVATION(FEET) = 912.00  
DOWNSTREAM ELEVATION(FEET) = 910.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.505  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.782  
SUBAREA RUNOFF(CFS) = 0.27  
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 2443.00 TO NODE 2445.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 910.00 DOWNSTREAM ELEVATION(FEET) = 900.00  
STREET LENGTH(FEET) = 700.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.91  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.17  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.43  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.70  
STREET FLOW TRAVEL TIME(MIN.) = 4.81 Tc(MIN.) = 11.31  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.446



\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570
SUBAREA AREA(ACRES) = 1.04 SUBAREA RUNOFF(CFS) = 3.23
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 3.41

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.59
FLOW VELOCITY(FEET/SEC.) = 2.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.93
LONGEST FLOWPATH FROM NODE 2444.00 TO NODE 2445.00 = 783.33 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2445.00 TO NODE 2445.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 11.31
RAINFALL INTENSITY(INCH/HR) = 5.45
TOTAL STREAM AREA(ACRES) = 1.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.41

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.32 Tc(MIN.) = 10.31
TOTAL AREA(ACRES) = 3.6
LONGEST FLOWPATH FROM NODE 2444.00 TO NODE 2445.00 = 783.33 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2445.00 TO NODE 2448.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 894.00 DOWNSTREAM(FEET) = 889.00
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.09
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.32
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.40
LONGEST FLOWPATH FROM NODE 2444.00 TO NODE 2448.00 = 858.33 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2448.00 TO NODE 2448.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 11.32 10.40 5.749 3.59
LONGEST FLOWPATH FROM NODE 2444.00 TO NODE 2448.00 = 858.33 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 76.09 17.95 4.044 118.26
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2448.00 = 6375.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 55.41 10.40 5.749
2 84.05 17.95 4.044

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 84.05 Tc(MIN.) = 17.95
TOTAL AREA(ACRES) = 121.8

\*\*\*\*\*
FLOW PROCESS FROM NODE 2448.00 TO NODE 2448.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2448.00 TO NODE 2442.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 889.00 DOWNSTREAM(FEET) = 888.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.39
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 84.05
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 18.01
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2442.00 = 6425.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2442.00 TO NODE 2442.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 18.01
RAINFALL INTENSITY(INCH/HR) = 4.04
TOTAL STREAM AREA(ACRES) = 121.85
PEAK FLOW RATE(CFS) AT CONFLUENCE = 84.05

\*\*\*\*\*

FLOW PROCESS FROM NODE 2441.00 TO NODE 2440.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 908.00
DOWNSTREAM ELEVATION(FEET) = 905.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914
SUBAREA RUNOFF(CFS) = 0.50
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 2440.00 TO NODE 2439.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 905.00 DOWNSTREAM(FEET) = 895.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 315.00 CHANNEL SLOPE = 0.0317  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.882

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.59  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.42  
AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 1.53  
Tc(MIN.) = 7.87  
SUBAREA AREA(ACRES) = 1.57 SUBAREA RUNOFF(CFS) = 6.16  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 6.59

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.41 FLOW VELOCITY(FEET/SEC.) = 4.15  
LONGEST FLOWPATH FROM NODE 2441.00 TO NODE 2439.00 = 410.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2439.00 TO NODE 2442.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 889.00 DOWNSTREAM(FEET) = 888.00  
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.61  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.59  
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 8.23  
LONGEST FLOWPATH FROM NODE 2441.00 TO NODE 2442.00 = 530.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2442.00 TO NODE 2442.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.23  
RAINFALL INTENSITY(INCH/HR) = 6.69  
TOTAL STREAM AREA(ACRES) = 1.68  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.59

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 84.05        | 18.01     | 4.035                 | 121.85      |
| 2             | 6.59         | 8.23      | 6.688                 | 1.68        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 44.99        | 8.23      | 6.688                 |
| 2             | 88.02        | 18.01     | 4.035                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 88.02 Tc(MIN.) = 18.01  
TOTAL AREA(ACRES) = 123.5  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2442.00 = 6425.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2442.00 TO NODE 2438.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 888.00 DOWNSTREAM(FEET) = 887.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 29.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.43  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 88.02  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 18.06  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2438.00 = 6475.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2438.00 TO NODE 2438.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.06  
RAINFALL INTENSITY(INCH/HR) = 4.03  
TOTAL STREAM AREA(ACRES) = 123.53  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 88.02

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2437.00 TO NODE 2436.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 897.00  
DOWNSTREAM ELEVATION(FEET) = 895.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.287  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.955  
SUBAREA RUNOFF(CFS) = 0.59  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2436.00 TO NODE 2435.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 895.00 DOWNSTREAM ELEVATION(FEET) = 894.00  
STREET LENGTH(FEET) = 300.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.01  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.51  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.19  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.35  
STREET FLOW TRAVEL TIME(MIN.) = 4.18 Tc(MIN.) = 10.47  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.724

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570

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SUBAREA AREA(ACRES) = 0.86 SUBAREA RUNOFF(CFS) = 2.81  
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 3.23

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.47  
FLOW VELOCITY(FEET/SEC.) = 1.33 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.45  
LONGEST FLOWPATH FROM NODE 2437.00 TO NODE 2435.00 = 380.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2435.00 TO NODE 2438.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 888.00 DOWNSTREAM(FEET) = 887.00  
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.86  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.23  
PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 10.85  
LONGEST FLOWPATH FROM NODE 2437.00 TO NODE 2438.00 = 490.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2438.00 TO NODE 2438.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.85  
RAINFALL INTENSITY(INCH/HR) = 5.60  
TOTAL STREAM AREA(ACRES) = 0.99  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.23

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 88.02        | 18.06     | 4.027                 | 123.53      |
| 2             | 3.23         | 10.85     | 5.595                 | 0.99        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM | RUNOFF | Tc | INTENSITY |
|--------|--------|----|-----------|
|--------|--------|----|-----------|

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) |
|--------|-------|--------|-------------|
| 1      | 66.58 | 10.85  | 5.595       |
| 2      | 90.35 | 18.06  | 4.027       |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 90.35 Tc(MIN.) = 18.06  
TOTAL AREA(ACRES) = 124.5  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2438.00 = 6475.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2438.00 TO NODE 2434.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 889.00 DOWNSTREAM(FEET) = 887.00  
FLOW LENGTH(FEET) = 355.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.19  
ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 90.35  
PIPE TRAVEL TIME(MIN.) = 0.64 Tc(MIN.) = 18.71  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2434.00 = 6830.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2434.00 TO NODE 2434.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.71  
RAINFALL INTENSITY(INCH/HR) = 3.94  
TOTAL STREAM AREA(ACRES) = 124.52  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 90.35

\*\*\*\*\*

FLOW PROCESS FROM NODE 2433.00 TO NODE 2432.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 903.00  
DOWNSTREAM ELEVATION(FEET) = 899.00  
ELEVATION DIFFERENCE(FEET) = 4.00



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SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.759  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.419  
SUBAREA RUNOFF(CFS) = 0.72  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 2432.00 TO NODE 2431.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 899.00 DOWNSTREAM(FEET) = 896.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 510.00 CHANNEL SLOPE = 0.0059  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.072

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.89  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.24  
AVERAGE FLOW DEPTH(FEET) = 0.62 TRAVEL TIME(MIN.) = 3.80  
Tc(MIN.) = 9.56  
SUBAREA AREA(ACRES) = 2.93 SUBAREA RUNOFF(CFS) = 10.14  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 10.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.85 FLOW VELOCITY(FEET/SEC.) = 2.67  
LONGEST FLOWPATH FROM NODE 2433.00 TO NODE 2431.00 = 605.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2431.00 TO NODE 2434.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 890.00 DOWNSTREAM(FEET) = 889.00  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.87  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.66  
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 9.69  
LONGEST FLOWPATH FROM NODE 2433.00 TO NODE 2434.00 = 670.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2434.00 TO NODE 2434.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.69  
RAINFALL INTENSITY(INCH/HR) = 6.02  
TOTAL STREAM AREA(ACRES) = 3.08  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.66

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 90.35        | 18.71     | 3.937                 | 124.52      |
| 2             | 10.66        | 9.69      | 6.016                 | 3.08        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 69.78        | 9.69      | 6.016                 |
| 2             | 97.32        | 18.71     | 3.937                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 97.32 Tc(MIN.) = 18.71  
TOTAL AREA(ACRES) = 127.6  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2434.00 = 6830.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2434.00 TO NODE 2430.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 889.00 DOWNSTREAM(FEET) = 888.00  
FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 27.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.75  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 97.32  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 18.76  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2430.00 = 6875.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2430.00 TO NODE 2430.00 IS CODE = 1  
-----

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.76  
RAINFALL INTENSITY(INCH/HR) = 3.93  
TOTAL STREAM AREA(ACRES) = 127.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 97.32

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2429.00 TO NODE 2428.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1290.00  
DOWNSTREAM ELEVATION(FEET) = 1235.00  
ELEVATION DIFFERENCE(FEET) = 55.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2428.00 TO NODE 2427.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1235.00 DOWNSTREAM(FEET) = 910.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 710.00 CHANNEL SLOPE = 0.4577  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.875  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2600  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.55  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 15.15  
AVERAGE FLOW DEPTH(FEET) = 0.38 TRAVEL TIME(MIN.) = 0.78  
Tc(MIN.) = 7.88  
SUBAREA AREA(ACRES) = 23.50 SUBAREA RUNOFF(CFS) = 42.01  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.260

TOTAL AREA(ACRES) = 23.8 PEAK FLOW RATE(CFS) = 42.50

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.55 FLOW VELOCITY(FEET/SEC.) = 18.67
LONGEST FLOWPATH FROM NODE 2429.00 TO NODE 2427.00 = 810.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2427.00 TO NODE 2430.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 904.00 DOWNSTREAM(FEET) = 888.00
FLOW LENGTH(FEET) = 395.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.67
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 42.50
PIPE TRAVEL TIME(MIN.) = 0.42 Tc(MIN.) = 8.30
LONGEST FLOWPATH FROM NODE 2429.00 TO NODE 2430.00 = 1205.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2430.00 TO NODE 2430.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.30
RAINFALL INTENSITY(INCH/HR) = 6.65
TOTAL STREAM AREA(ACRES) = 23.79
PEAK FLOW RATE(CFS) AT CONFLUENCE = 42.50

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 122.45 Tc(MIN.) = 18.76

TOTAL AREA(ACRES) = 151.4

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2430.00 = 6875.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2430.00 TO NODE 2391.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 888.00 DOWNSTREAM(FEET) = 877.00

FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 39.0 INCH PIPE IS 30.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 17.81

ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 122.45

PIPE TRAVEL TIME(MIN.) = 0.37 Tc(MIN.) = 19.13

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2391.00 = 7275.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2391.00 TO NODE 2391.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.00 TO NODE 2416.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00

UPSTREAM ELEVATION(FEET) = 906.00

DOWNSTREAM ELEVATION(FEET) = 905.00

ELEVATION DIFFERENCE(FEET) = 1.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.663

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.663

SUBAREA RUNOFF(CFS) = 0.26

TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 2416.00 TO NODE 2415.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 905.00 DOWNSTREAM ELEVATION(FEET) = 895.00  
STREET LENGTH(FEET) = 325.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.83  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.85  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.26  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86  
STREET FLOW TRAVEL TIME(MIN.) = 1.66 Tc(MIN.) = 8.32  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.639

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.88 SUBAREA RUNOFF(CFS) = 7.11  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 7.34

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.24  
FLOW VELOCITY(FEET/SEC.) = 3.78 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.18  
LONGEST FLOWPATH FROM NODE 2417.00 TO NODE 2415.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.00 TO NODE 2414.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 889.00 DOWNSTREAM(FEET) = 888.00  
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.07  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.34  
PIPE TRAVEL TIME(MIN.) = 0.53 Tc(MIN.) = 8.85

LONGEST FLOWPATH FROM NODE 2417.00 TO NODE 2414.00 = 550.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2414.00 TO NODE 2414.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2400.00 TO NODE 2399.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8900

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1000.00

DOWNSTREAM ELEVATION(FEET) = 987.00

ELEVATION DIFFERENCE(FEET) = 13.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.755

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.23

TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 1.23

\*\*\*\*\*

FLOW PROCESS FROM NODE 2399.00 TO NODE 2398.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 987.00 DOWNSTREAM ELEVATION(FEET) = 940.00

STREET LENGTH(FEET) = 445.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.02

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

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STREET FLOW DEPTH(FEET) = 0.23  
 HALFSTREET FLOOD WIDTH(FEET) = 4.99  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.48  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.24  
 STREET FLOW TRAVEL TIME(MIN.) = 1.35 Tc(MIN.) = 3.11  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .8900  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.890  
 SUBAREA AREA(ACRES) = 0.68 SUBAREA RUNOFF(CFS) = 5.58  
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 6.81

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 6.71  
 FLOW VELOCITY(FEET/SEC.) = 5.99 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.56  
 LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2398.00 = 545.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2398.00 TO NODE 2397.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 934.00 DOWNSTREAM(FEET) = 908.00  
 FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.19  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 6.81  
 PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 3.65  
 LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2397.00 = 945.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2397.00 TO NODE 2397.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 3.65  
 RAINFALL INTENSITY(INCH/HR) = 9.22  
 TOTAL STREAM AREA(ACRES) = 0.83  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.81

\*\*\*\*\*



FLOW PROCESS FROM NODE 2396.00 TO NODE 2395.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 940.00

DOWNSTREAM ELEVATION(FEET) = 930.00

ELEVATION DIFFERENCE(FEET) = 10.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.428

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.95

TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.95

\*\*\*\*\*

FLOW PROCESS FROM NODE 2395.00 TO NODE 2397.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 930.00 DOWNSTREAM ELEVATION(FEET) = 916.00

STREET LENGTH(FEET) = 285.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.95

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.20

HALFSTREET FLOOD WIDTH(FEET) = 3.92

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.59

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.73

STREET FLOW TRAVEL TIME(MIN.) = 1.32 Tc(MIN.) = 5.75

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.425

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.42 SUBAREA RUNOFF(CFS) = 2.02  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.88

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.12  
FLOW VELOCITY(FEET/SEC.) = 3.79 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.87  
LONGEST FLOWPATH FROM NODE 2396.00 TO NODE 2397.00 = 385.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2397.00 TO NODE 2397.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.75  
RAINFALL INTENSITY(INCH/HR) = 8.42  
TOTAL STREAM AREA(ACRES) = 0.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.88

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.81         | 3.65      | 9.222                 | 0.83        |
| 2             | 2.88         | 5.75      | 8.425                 | 0.60        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 8.64         | 3.65      | 9.222                 |
| 2             | 9.10         | 5.75      | 8.425                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.10 Tc(MIN.) = 5.75  
TOTAL AREA(ACRES) = 1.4  
LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2397.00 = 945.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2397.00 TO NODE 2394.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

P-25d.TXT

ELEVATION DATA: UPSTREAM(FEET) = 910.00 DOWNSTREAM(FEET) = 894.00  
FLOW LENGTH(FEET) = 455.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.51  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.10  
PIPE TRAVEL TIME(MIN.) = 0.72 Tc(MIN.) = 6.47  
LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2394.00 = 1400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2394.00 TO NODE 2394.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.47  
RAINFALL INTENSITY(INCH/HR) = 7.81  
TOTAL STREAM AREA(ACRES) = 1.43  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.10

\*\*\*\*\*

FLOW PROCESS FROM NODE 2393.00 TO NODE 2392.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.50  
UPSTREAM ELEVATION(FEET) = 916.00  
DOWNSTREAM ELEVATION(FEET) = 912.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.885  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.302  
SUBAREA RUNOFF(CFS) = 0.90  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.90

\*\*\*\*\*

FLOW PROCESS FROM NODE 2392.00 TO NODE 2394.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 912.00 DOWNSTREAM ELEVATION(FEET) = 900.00  
STREET LENGTH(FEET) = 365.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.00  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.22  
HALFSTREET FLOOD WIDTH(FEET) = 4.65  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.98  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.65  
STREET FLOW TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 7.93  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.851

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.56 SUBAREA RUNOFF(CFS) = 2.19  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.93

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.85  
FLOW VELOCITY(FEET/SEC.) = 3.18 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.77  
LONGEST FLOWPATH FROM NODE 2393.00 TO NODE 2394.00 = 462.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2394.00 TO NODE 2394.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.93  
RAINFALL INTENSITY(INCH/HR) = 6.85  
TOTAL STREAM AREA(ACRES) = 0.75  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.93

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.10         | 6.47      | 7.806                 | 1.43        |
| 2             | 2.93         | 7.93      | 6.851                 | 0.75        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.50        | 6.47      | 7.806                 |
| 2             | 10.92        | 7.93      | 6.851                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.50 Tc(MIN.) = 6.47  
TOTAL AREA(ACRES) = 2.2  
LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2394.00 = 1400.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2394.00 TO NODE 2414.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 894.00 DOWNSTREAM(FEET) = 888.00  
FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.36  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.50  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 6.60  
LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2414.00 = 1505.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2414.00 TO NODE 2414.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.50        | 6.60      | 7.706                 | 2.18        |

LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2414.00 = 1505.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 7.34         | 8.85      | 6.381                 | 1.94        |

LONGEST FLOWPATH FROM NODE 2417.00 TO NODE 2414.00 = 550.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.98        | 6.60      | 7.706                 |
| 2             | 16.86        | 8.85      | 6.381                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.98 Tc(MIN.) = 6.60  
TOTAL AREA(ACRES) = 4.1

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2414.00 TO NODE 2414.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2414.00 TO NODE 2391.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 894.00 DOWNSTREAM(FEET) = 883.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 320.00 CHANNEL SLOPE = 0.0344  
CHANNEL FLOW THRU SUBAREA(CFS) = 16.98  
FLOW VELOCITY(FEET/SEC) = 5.32 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.00 Tc(MIN.) = 7.61  
LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2391.00 = 1825.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2391.00 TO NODE 2391.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.98        | 7.61      | 7.035                 | 4.12        |

LONGEST FLOWPATH FROM NODE 2400.00 TO NODE 2391.00 = 1825.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 122.45       | 19.13     | 3.881                 | 151.39      |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2391.00 = 7275.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 65.67        | 7.61      | 7.035                 |
| 2             | 131.82       | 19.13     | 3.881                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 131.82 Tc(MIN.) = 19.13  
TOTAL AREA(ACRES) = 155.5

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2391.00 TO NODE 2391.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2391.00 TO NODE 2418.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 877.00 DOWNSTREAM(FEET) = 869.00  
FLOW LENGTH(FEET) = 267.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 31.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.62  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 131.82  
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 19.37  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2418.00 = 7542.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.00 TO NODE 2418.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2425.00 TO NODE 2424.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1198.00  
DOWNSTREAM ELEVATION(FEET) = 1135.00

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ELEVATION DIFFERENCE(FEET) = 63.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.96  
TOTAL AREA(ACRES) = 0.52 TOTAL RUNOFF(CFS) = 0.96

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2424.00 TO NODE 2423.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 926.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 715.00 CHANNEL SLOPE = 0.2923  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.550  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.10  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.54  
AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 1.40  
Tc(MIN.) = 8.50  
SUBAREA AREA(ACRES) = 6.25 SUBAREA RUNOFF(CFS) = 10.23  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 6.8 PEAK FLOW RATE(CFS) = 11.09

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 10.48  
LONGEST FLOWPATH FROM NODE 2425.00 TO NODE 2423.00 = 815.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2423.00 TO NODE 2422.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 920.00 DOWNSTREAM(FEET) = 891.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 26.52  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.09  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 8.54  
LONGEST FLOWPATH FROM NODE 2425.00 TO NODE 2422.50 = 890.00 FEET.



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2422.50 TO NODE 2422.50 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.54  
RAINFALL INTENSITY(INCH/HR) = 6.53  
TOTAL STREAM AREA(ACRES) = 6.77  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.09

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2422.70 TO NODE 2422.60 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 914.00  
DOWNSTREAM ELEVATION(FEET) = 912.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 10.083  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.866  
SUBAREA RUNOFF(CFS) = 0.16  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2422.60 TO NODE 2422.50 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 912.00 DOWNSTREAM(FEET) = 897.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 550.00 CHANNEL SLOPE = 0.0273  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.433  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.51  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.67  
AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 5.48  
Tc(MIN.) = 15.57

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SUBAREA AREA(ACRES) = 0.53 SUBAREA RUNOFF(CFS) = 0.70  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.291  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 0.83

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.13 FLOW VELOCITY(FEET/SEC.) = 2.00  
LONGEST FLOWPATH FROM NODE 2422.70 TO NODE 2422.50 = 630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.50 TO NODE 2422.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.57  
RAINFALL INTENSITY(INCH/HR) = 4.43  
TOTAL STREAM AREA(ACRES) = 0.64  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.83

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.09        | 8.54      | 6.527                 | 6.77        |
| 2             | 0.83         | 15.57     | 4.433                 | 0.64        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.54        | 8.54      | 6.527                 |
| 2             | 8.36         | 15.57     | 4.433                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 11.54 Tc(MIN.) = 8.54  
TOTAL AREA(ACRES) = 7.4  
LONGEST FLOWPATH FROM NODE 2425.00 TO NODE 2422.50 = 890.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.50 TO NODE 2422.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 891.00 DOWNSTREAM(FEET) = 881.00

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FLOW LENGTH(FEET) = 350.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.27  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.54  
PIPE TRAVEL TIME(MIN.) = 0.57 Tc(MIN.) = 9.11  
LONGEST FLOWPATH FROM NODE 2425.00 TO NODE 2422.00 = 1240.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2422.00 TO NODE 2422.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2421.00 TO NODE 2420.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1185.00  
DOWNSTREAM ELEVATION(FEET) = 1143.00  
ELEVATION DIFFERENCE(FEET) = 42.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 1.03  
TOTAL AREA(ACRES) = 0.56 TOTAL RUNOFF(CFS) = 1.03

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2420.00 TO NODE 2419.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1143.00 DOWNSTREAM(FEET) = 918.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 765.00 CHANNEL SLOPE = 0.2941  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.428  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.63  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.74

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AVERAGE FLOW DEPTH(FEET) = 0.18 TRAVEL TIME(MIN.) = 1.65  
Tc(MIN.) = 8.75  
SUBAREA AREA(ACRES) = 4.46 SUBAREA RUNOFF(CFS) = 7.17  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 8.07

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 FLOW VELOCITY(FEET/SEC.) = 9.35  
LONGEST FLOWPATH FROM NODE 2421.00 TO NODE 2419.00 = 865.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2419.00 TO NODE 2422.20 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 912.00 DOWNSTREAM(FEET) = 885.00  
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.08  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.07  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 8.81  
LONGEST FLOWPATH FROM NODE 2421.00 TO NODE 2422.20 = 945.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.20 TO NODE 2422.20 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.81  
RAINFALL INTENSITY(INCH/HR) = 6.40  
TOTAL STREAM AREA(ACRES) = 5.02  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.60 TO NODE 2422.40 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 897.00

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DOWNSTREAM ELEVATION(FEET) = 895.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.490  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.100  
SUBAREA RUNOFF(CFS) = 0.26  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.40 TO NODE 2422.20 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 895.00 DOWNSTREAM(FEET) = 891.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 145.00 CHANNEL SLOPE = 0.0276  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.567

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.51  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.67  
AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 1.44  
Tc(MIN.) = 10.93  
SUBAREA AREA(ACRES) = 0.31 SUBAREA RUNOFF(CFS) = 0.52  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 0.75

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 1.95  
LONGEST FLOWPATH FROM NODE 2422.60 TO NODE 2422.20 = 225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.20 TO NODE 2422.20 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.93  
RAINFALL INTENSITY(INCH/HR) = 5.57  
TOTAL STREAM AREA(ACRES) = 0.45  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.75

\*\* CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA

| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 8.07  | 8.81   | 6.400       | 5.02   |
| 2      | 0.75  | 10.93  | 5.567       | 0.45   |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 8.67         | 8.81      | 6.400                 |
| 2             | 7.77         | 10.93     | 5.567                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.67 Tc(MIN.) = 8.81  
TOTAL AREA(ACRES) = 5.5  
LONGEST FLOWPATH FROM NODE 2421.00 TO NODE 2422.20 = 945.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.20 TO NODE 2422.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 885.00 DOWNSTREAM(FEET) = 881.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.35  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.67  
PIPE TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 9.86  
LONGEST FLOWPATH FROM NODE 2421.00 TO NODE 2422.00 = 1345.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.00 TO NODE 2422.00 IS CODE = 11

-----  
>>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.67         | 9.86      | 5.952                 | 5.47        |

LONGEST FLOWPATH FROM NODE 2421.00 TO NODE 2422.00 = 1345.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

1 11.54 9.11 6.261 7.41  
LONGEST FLOWPATH FROM NODE 2425.00 TO NODE 2422.00 = 1240.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.56        | 9.11      | 6.261                 |
| 2             | 19.64        | 9.86      | 5.952                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.64 Tc(MIN.) = 9.86  
TOTAL AREA(ACRES) = 12.9

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.00 TO NODE 2422.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2422.00 TO NODE 2418.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 881.00 DOWNSTREAM(FEET) = 869.00  
FLOW LENGTH(FEET) = 690.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 17.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.39  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.64  
PIPE TRAVEL TIME(MIN.) = 1.22 Tc(MIN.) = 11.08  
LONGEST FLOWPATH FROM NODE 2421.00 TO NODE 2418.00 = 2035.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.00 TO NODE 2418.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 19.64        | 11.08     | 5.519                 | 12.88       |

LONGEST FLOWPATH FROM NODE 2421.00 TO NODE 2418.00 = 2035.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM | RUNOFF | Tc | INTENSITY | AREA |
|--------|--------|----|-----------|------|
|--------|--------|----|-----------|------|

| NUMBER | (CFS)  | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|--------|--------|-------------|--------|
| 1      | 131.82 | 19.37  | 3.850       | 155.51 |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2418.00 = 7542.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 95.06        | 11.08     | 5.519                 |
| 2             | 145.52       | 19.37     | 3.850                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 145.52 Tc(MIN.) = 19.37  
TOTAL AREA(ACRES) = 168.4

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.00 TO NODE 2418.00 IS CODE = 12  
-----

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.00 TO NODE 2418.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.90 TO NODE 2418.80 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 922.00  
DOWNSTREAM ELEVATION(FEET) = 920.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.999  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.423  
SUBAREA RUNOFF(CFS) = 0.91  
TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.91

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.80 TO NODE 2418.20 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<



=====

UPSTREAM ELEVATION(FEET) = 920.00 DOWNSTREAM ELEVATION(FEET) = 907.00  
STREET LENGTH(FEET) = 660.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.83  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.44  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.91  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86  
STREET FLOW TRAVEL TIME(MIN.) = 3.78 Tc(MIN.) = 10.78  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.617

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.510  
SUBAREA AREA(ACRES) = 2.71 SUBAREA RUNOFF(CFS) = 7.76  
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 8.45

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.78  
FLOW VELOCITY(FEET/SEC.) = 3.30 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.13  
LONGEST FLOWPATH FROM NODE 2418.90 TO NODE 2418.20 = 740.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.20 TO NODE 2418.20 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.78  
RAINFALL INTENSITY(INCH/HR) = 5.62  
TOTAL STREAM AREA(ACRES) = 2.95  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.45

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.84 TO NODE 2417.85 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 919.00  
DOWNSTREAM ELEVATION(FEET) = 918.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.087  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.364  
SUBAREA RUNOFF(CFS) = 0.34  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.85 TO NODE 2418.20 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 918.00 DOWNSTREAM ELEVATION(FEET) = 907.00  
STREET LENGTH(FEET) = 1005.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.89  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 10.47  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.42  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.81  
STREET FLOW TRAVEL TIME(MIN.) = 6.91 Tc(MIN.) = 14.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.748

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 3.99 SUBAREA RUNOFF(CFS) = 10.80  
TOTAL AREA(ACRES) = 4.1 PEAK FLOW RATE(CFS) = 11.01

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.59  
FLOW VELOCITY(FEET/SEC.) = 2.80 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.12  
LONGEST FLOWPATH FROM NODE 2417.84 TO NODE 2418.20 = 1075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.20 TO NODE 2418.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.00  
RAINFALL INTENSITY(INCH/HR) = 4.75  
TOTAL STREAM AREA(ACRES) = 4.07  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.01

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.45         | 10.78     | 5.617                 | 2.95        |
| 2             | 11.01        | 14.00     | 4.748                 | 4.07        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.94        | 10.78     | 5.617                 |
| 2             | 18.16        | 14.00     | 4.748                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 18.16 Tc(MIN.) = 14.00  
TOTAL AREA(ACRES) = 7.0  
LONGEST FLOWPATH FROM NODE 2417.84 TO NODE 2418.20 = 1075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.20 TO NODE 2418.70 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 907.00 DOWNSTREAM(FEET) = 902.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 425.00 CHANNEL SLOPE = 0.0118  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

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MANNING'S FACTOR = 0.030    MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.399

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.02

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.04

AVERAGE FLOW DEPTH(FEET) = 0.96    TRAVEL TIME(MIN.) = 1.75

Tc(MIN.) = 15.75

SUBAREA AREA(ACRES) = 0.69    SUBAREA RUNOFF(CFS) = 1.73

AREA-AVERAGE RUNOFF COEFFICIENT = 0.547

TOTAL AREA(ACRES) = 7.7    PEAK FLOW RATE(CFS) = 18.56

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.95    FLOW VELOCITY(FEET/SEC.) = 3.99

LONGEST FLOWPATH FROM NODE 2417.84 TO NODE 2418.70 = 1500.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.70 TO NODE 2418.60 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 896.00    DOWNSTREAM(FEET) = 890.00

FLOW LENGTH(FEET) = 145.00    MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 13.01

ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 18.56

PIPE TRAVEL TIME(MIN.) = 0.19    Tc(MIN.) = 15.94

LONGEST FLOWPATH FROM NODE 2417.84 TO NODE 2418.60 = 1645.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.60 TO NODE 2418.60 IS CODE = 10

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.50 TO NODE 2418.40 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 1105.00

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DOWNSTREAM ELEVATION(FEET) = 1055.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.46  
TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 0.46

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.40 TO NODE 2418.30 IS CODE = 51

-----  
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1055.00 DOWNSTREAM(FEET) = 909.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 410.00 CHANNEL SLOPE = 0.3561  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.845

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.67  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.20  
AVERAGE FLOW DEPTH(FEET) = 0.17 TRAVEL TIME(MIN.) = 0.83  
Tc(MIN.) = 7.94  
SUBAREA AREA(ACRES) = 4.91 SUBAREA RUNOFF(CFS) = 8.40  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 5.2 PEAK FLOW RATE(CFS) = 8.83

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.24 FLOW VELOCITY(FEET/SEC.) = 10.51  
LONGEST FLOWPATH FROM NODE 2418.50 TO NODE 2418.30 = 510.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.30 TO NODE 2418.32 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 903.00 DOWNSTREAM(FEET) = 900.00  
FLOW LENGTH(FEET) = 340.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.02  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.83  
PIPE TRAVEL TIME(MIN.) = 0.94 Tc(MIN.) = 8.88  
LONGEST FLOWPATH FROM NODE 2418.50 TO NODE 2418.32 = 850.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.32 TO NODE 2418.32 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.88  
RAINFALL INTENSITY(INCH/HR) = 6.37  
TOTAL STREAM AREA(ACRES) = 5.16  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2418.10 TO NODE 2417.90 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 925.00  
DOWNSTREAM ELEVATION(FEET) = 918.00  
ELEVATION DIFFERENCE(FEET) = 7.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.072  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.41  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.90 TO NODE 2417.91 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 918.00 DOWNSTREAM ELEVATION(FEET) = 912.00  
STREET LENGTH(FEET) = 115.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.75

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.20

HALFSTREET FLOOD WIDTH(FEET) = 3.46

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.67

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.72

STREET FLOW TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 4.59

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.567

SUBAREA AREA(ACRES) = 0.51 SUBAREA RUNOFF(CFS) = 2.68

TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 3.09

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.25

FLOW VELOCITY(FEET/SEC.) = 3.92 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.91

LONGEST FLOWPATH FROM NODE 2418.10 TO NODE 2417.91 = 190.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.91 TO NODE 2417.80 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 912.00 DOWNSTREAM(FEET) = 908.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 530.00 CHANNEL SLOPE = 0.0075

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.832

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.38

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.62

AVERAGE FLOW DEPTH(FEET) = 0.65 TRAVEL TIME(MIN.) = 3.37

Tc(MIN.) = 7.96

SUBAREA AREA(ACRES) = 2.18 SUBAREA RUNOFF(CFS) = 8.49

AREA-AVERAGE RUNOFF COEFFICIENT = 0.569

TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 10.78

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.80 FLOW VELOCITY(FEET/SEC.) = 2.94

LONGEST FLOWPATH FROM NODE 2418.10 TO NODE 2417.80 = 720.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.80 TO NODE 2417.32 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 902.00 DOWNSTREAM(FEET) = 900.00  
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.50  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 10.78  
 PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 8.03  
 LONGEST FLOWPATH FROM NODE 2418.10 TO NODE 2417.32 = 770.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.32 TO NODE 2417.32 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.03  
 RAINFALL INTENSITY(INCH/HR) = 6.79  
 TOTAL STREAM AREA(ACRES) = 2.77  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.78

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.83         | 8.88      | 6.368                 | 5.16        |
| 2             | 10.78        | 8.03      | 6.792                 | 2.77        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 18.77        | 8.03      | 6.792                 |
| 2             | 18.93        | 8.88      | 6.368                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 18.93 Tc(MIN.) = 8.88  
 TOTAL AREA(ACRES) = 7.9



LONGEST FLOWPATH FROM NODE 2418.50 TO NODE 2417.32 = 850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.32 TO NODE 2417.70 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 900.00 DOWNSTREAM(FEET) = 899.00
FLOW LENGTH(FEET) = 115.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.24
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 18.93
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 9.14
LONGEST FLOWPATH FROM NODE 2418.50 TO NODE 2417.70 = 965.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.70 TO NODE 2417.70 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.60 TO NODE 2417.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1185.00
DOWNSTREAM ELEVATION(FEET) = 1145.00
ELEVATION DIFFERENCE(FEET) = 40.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.647
SUBAREA RUNOFF(CFS) = 0.78
TOTAL AREA(ACRES) = 0.34 TOTAL RUNOFF(CFS) = 0.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.50 TO NODE 2417.40 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1145.00 DOWNSTREAM(FEET) = 908.00

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CHANNEL LENGTH THRU SUBAREA(FEET) = 580.00 CHANNEL SLOPE = 0.4086  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.929

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.75  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.76  
AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 1.10  
Tc(MIN.) = 7.79  
SUBAREA AREA(ACRES) = 3.81 SUBAREA RUNOFF(CFS) = 7.92  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
TOTAL AREA(ACRES) = 4.2 PEAK FLOW RATE(CFS) = 8.63

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 FLOW VELOCITY(FEET/SEC.) = 10.75  
LONGEST FLOWPATH FROM NODE 2417.60 TO NODE 2417.40 = 680.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.40 TO NODE 2417.30 IS CODE = 31

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 902.00 DOWNSTREAM(FEET) = 899.00  
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.63  
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.98  
LONGEST FLOWPATH FROM NODE 2417.60 TO NODE 2417.30 = 790.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.30 TO NODE 2417.30 IS CODE = 1

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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.98  
RAINFALL INTENSITY(INCH/HR) = 6.82  
TOTAL STREAM AREA(ACRES) = 4.15  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.63

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.20 TO NODE 2417.10 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1190.00
DOWNSTREAM ELEVATION(FEET) = 1136.00
ELEVATION DIFFERENCE(FEET) = 54.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.647
SUBAREA RUNOFF(CFS) = 0.48
TOTAL AREA(ACRES) = 0.21 TOTAL RUNOFF(CFS) = 0.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.10 TO NODE 2417.30 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1136.00 DOWNSTREAM(FEET) = 910.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1085.00 CHANNEL SLOPE = 0.2083
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.320

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.38
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.87
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 2.30
Tc(MIN.) = 8.98
SUBAREA AREA(ACRES) = 6.18 SUBAREA RUNOFF(CFS) = 11.72
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
TOTAL AREA(ACRES) = 6.4 PEAK FLOW RATE(CFS) = 12.12

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 FLOW VELOCITY(FEET/SEC.) = 9.67
LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2417.30 = 1185.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.30 TO NODE 2417.30 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.98
RAINFALL INTENSITY(INCH/HR) = 6.32
TOTAL STREAM AREA(ACRES) = 6.39
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.12
    
```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.63         | 7.98      | 6.820                 | 4.15        |
| 2             | 12.12        | 8.98      | 6.320                 | 6.39        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.40        | 7.98      | 6.820                 |
| 2             | 20.11        | 8.98      | 6.320                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 20.11 Tc(MIN.) = 8.98
TOTAL AREA(ACRES) = 10.5
LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2417.30 = 1185.00 FEET.
    
```

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FLOW PROCESS FROM NODE 2417.30 TO NODE 2417.70 IS CODE = 31

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-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
    
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=====
ELEVATION DATA: UPSTREAM(FEET) = 904.00 DOWNSTREAM(FEET) = 899.00
FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.30
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.11
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 9.07
LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2417.70 = 1270.00 FEET.
    
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2417.70 TO NODE 2417.70 IS CODE = 1

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-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
    
```

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.07  
RAINFALL INTENSITY(INCH/HR) = 6.28  
TOTAL STREAM AREA(ACRES) = 10.54  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.70 TO NODE 2417.70 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 17.34 RAIN INTENSITY(INCH/HOUR) = 4.13  
TOTAL AREA(ACRES) = 193.00 TOTAL RUNOFF(CFS) = 310.57

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.70 TO NODE 2417.70 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.34  
RAINFALL INTENSITY(INCH/HR) = 4.13  
TOTAL STREAM AREA(ACRES) = 193.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 310.57

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.11        | 9.07      | 6.279                 | 10.54       |
| 2             | 310.57       | 17.34     | 4.135                 | 193.00      |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 182.63       | 9.07      | 6.279                 |
| 2             | 323.81       | 17.34     | 4.135                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 323.81 Tc(MIN.) = 17.34  
TOTAL AREA(ACRES) = 203.5  
LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2417.70 = 1270.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.70 TO NODE 2417.70 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 323.81       | 17.34     | 4.135                 | 203.54      |

LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2417.70 = 1270.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 18.93        | 9.14      | 6.249                 | 7.93        |

LONGEST FLOWPATH FROM NODE 2418.50 TO NODE 2417.70 = 965.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 189.65       | 9.14      | 6.249                 |
| 2             | 336.34       | 17.34     | 4.135                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 336.34 Tc(MIN.) = 17.34  
TOTAL AREA(ACRES) = 211.5

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.70 TO NODE 2417.70 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2417.70 TO NODE 2418.60 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 899.00 DOWNSTREAM(FEET) = 891.00  
FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 63.0 INCH PIPE IS 49.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.45  
ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 336.34  
PIPE TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 17.81

LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2418.60 = 1785.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.60 TO NODE 2418.60 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 336.34       | 17.81     | 4.065                 | 211.47      |

LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2418.60 = 1785.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 18.56        | 15.94     | 4.366                 | 7.71        |

LONGEST FLOWPATH FROM NODE 2417.84 TO NODE 2418.60 = 1645.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 319.59       | 15.94     | 4.366                 |
| 2             | 353.62       | 17.81     | 4.065                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 353.62 Tc(MIN.) = 17.81  
TOTAL AREA(ACRES) = 219.2

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.60 TO NODE 2418.60 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.60 TO NODE 2418.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 891.00 DOWNSTREAM(FEET) = 869.00  
FLOW LENGTH(FEET) = 745.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 57.0 INCH PIPE IS 44.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.79  
ESTIMATED PIPE DIAMETER(INCH) = 57.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 353.62

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PIPE TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 18.33  
LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2418.00 = 2530.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.00 TO NODE 2418.00 IS CODE = 11

>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 353.62       | 18.33     | 3.990                 | 219.18      |

LONGEST FLOWPATH FROM NODE 2417.20 TO NODE 2418.00 = 2530.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 145.52       | 19.37     | 3.850                 | 168.39      |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2418.00 = 7542.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 491.30       | 18.33     | 3.990                 |
| 2             | 486.74       | 19.37     | 3.850                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 491.30 Tc(MIN.) = 18.33  
TOTAL AREA(ACRES) = 387.6

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.00 TO NODE 2418.00 IS CODE = 12

>>>>>CLEAR MEMORY BANK # 1 <<<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2418.00 TO NODE 2380.20 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 869.00 DOWNSTREAM(FEET) = 858.00  
FLOW LENGTH(FEET) = 325.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 63.0 INCH PIPE IS 49.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 27.21  
ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1



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PIPE-FLOW(CFS) = 491.30  
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 18.53  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2380.20 = 7867.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.20 TO NODE 2380.20 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.90 TO NODE 2415.80 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00

UPSTREAM ELEVATION(FEET) = 915.00

DOWNSTREAM ELEVATION(FEET) = 907.00

ELEVATION DIFFERENCE(FEET) = 8.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.166

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.53

TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.80 TO NODE 2415.70 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 907.00 DOWNSTREAM ELEVATION(FEET) = 902.00

STREET LENGTH(FEET) = 395.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.84

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STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.33  
HALFSTREET FLOOD WIDTH(FEET) = 10.16  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.54  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.84  
STREET FLOW TRAVEL TIME(MIN.) = 2.59 Tc(MIN.) = 6.76  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.591  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 2.43 SUBAREA RUNOFF(CFS) = 10.51  
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 10.95

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.16  
FLOW VELOCITY(FEET/SEC.) = 2.96 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.15  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2415.70 = 480.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.70 TO NODE 2415.60 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 896.00 DOWNSTREAM(FEET) = 895.00  
FLOW LENGTH(FEET) = 245.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.85  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.95  
PIPE TRAVEL TIME(MIN.) = 0.84 Tc(MIN.) = 7.60  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2415.60 = 725.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.60 TO NODE 2415.60 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.60  
RAINFALL INTENSITY(INCH/HR) = 7.04  
TOTAL STREAM AREA(ACRES) = 2.53  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.95

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.50 TO NODE 2415.40 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 68.75  
UPSTREAM ELEVATION(FEET) = 905.00  
DOWNSTREAM ELEVATION(FEET) = 904.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.981  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.435  
SUBAREA RUNOFF(CFS) = 0.30  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2415.40 TO NODE 2415.30 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 904.00 DOWNSTREAM ELEVATION(FEET) = 898.00  
STREET LENGTH(FEET) = 420.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.59  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 7.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.38  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.68  
STREET FLOW TRAVEL TIME(MIN.) = 2.94 Tc(MIN.) = 9.92  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.926

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.93 SUBAREA RUNOFF(CFS) = 6.52  
TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 6.76

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.53  
FLOW VELOCITY(FEET/SEC.) = 2.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.93  
LONGEST FLOWPATH FROM NODE 2415.50 TO NODE 2415.30 = 488.75 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.30 TO NODE 2415.60 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 892.00 DOWNSTREAM(FEET) = 891.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.57  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.76  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 10.00  
LONGEST FLOWPATH FROM NODE 2415.50 TO NODE 2415.60 = 528.75 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.60 TO NODE 2415.60 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.00  
RAINFALL INTENSITY(INCH/HR) = 5.90  
TOTAL STREAM AREA(ACRES) = 2.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.76

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.95        | 7.60      | 7.038                 | 2.53        |
| 2             | 6.76         | 10.00     | 5.896                 | 2.00        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.08        | 7.60      | 7.038                 |

2 15.93 10.00 P-25d.TXT  
5.896

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.08 Tc(MIN.) = 7.60  
TOTAL AREA(ACRES) = 4.5  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2415.60 = 725.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2415.60 TO NODE 2415.20 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 891.00 DOWNSTREAM(FEET) = 874.00  
FLOW LENGTH(FEET) = 600.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.81  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.08  
PIPE TRAVEL TIME(MIN.) = 0.93 Tc(MIN.) = 8.53  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2415.20 = 1325.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2415.20 TO NODE 2415.20 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.53  
RAINFALL INTENSITY(INCH/HR) = 6.54  
TOTAL STREAM AREA(ACRES) = 4.53  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.08

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2415.10 TO NODE 2414.90 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 81.58  
UPSTREAM ELEVATION(FEET) = 902.00  
DOWNSTREAM ELEVATION(FEET) = 900.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.391  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.872

SUBAREA RUNOFF(CFS) = 0.54  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 2414.90 TO NODE 2415.20 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 900.00 DOWNSTREAM ELEVATION(FEET) = 880.00  
STREET LENGTH(FEET) = 725.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.15  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.77  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.46  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.05  
STREET FLOW TRAVEL TIME(MIN.) = 3.49 Tc(MIN.) = 9.88  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.944

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 3.27 SUBAREA RUNOFF(CFS) = 11.08  
TOTAL AREA(ACRES) = 3.4 PEAK FLOW RATE(CFS) = 11.49

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.47  
FLOW VELOCITY(FEET/SEC.) = 4.01 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.42  
LONGEST FLOWPATH FROM NODE 2415.10 TO NODE 2415.20 = 806.58 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.20 TO NODE 2415.20 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.88  
RAINFALL INTENSITY(INCH/HR) = 5.94  
TOTAL STREAM AREA(ACRES) = 3.39  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.49

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.08        | 8.53      | 6.535                 | 4.53        |
| 2             | 11.49        | 9.88      | 5.944                 | 3.39        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 26.00        | 8.53      | 6.535                 |
| 2             | 26.11        | 9.88      | 5.944                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.11 Tc(MIN.) = 9.88  
TOTAL AREA(ACRES) = 7.9  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2415.20 = 1325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2415.20 TO NODE 2414.80 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 874.00 DOWNSTREAM(FEET) = 849.00  
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 35.64  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.11  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 9.90  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2414.80 = 1380.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2414.80 TO NODE 2414.70 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 855.00 DOWNSTREAM(FEET) = 854.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 135.00 CHANNEL SLOPE = 0.0074  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.734

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 40.25  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.16  
AVERAGE FLOW DEPTH(FEET) = 1.57 TRAVEL TIME(MIN.) = 0.54  
Tc(MIN.) = 10.44  
SUBAREA AREA(ACRES) = 8.65 SUBAREA RUNOFF(CFS) = 28.27  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
TOTAL AREA(ACRES) = 16.6 PEAK FLOW RATE(CFS) = 54.16

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.82 FLOW VELOCITY(FEET/SEC.) = 4.49  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2414.70 = 1515.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2414.70 TO NODE 2414.70 IS CODE = 7

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>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 10.44 RAIN INTENSITY(INCH/HOUR) = 5.74  
TOTAL AREA(ACRES) = 16.60 TOTAL RUNOFF(CFS) = 3.70

\*\*\*\*\*

FLOW PROCESS FROM NODE 2414.70 TO NODE 2380.20 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 848.00 DOWNSTREAM(FEET) = 847.00  
FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.70  
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 10.78  
LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2380.20 = 1620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.20 TO NODE 2380.20 IS CODE = 11



>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.70         | 10.78     | 5.618                 | 16.60       |

LONGEST FLOWPATH FROM NODE 2415.90 TO NODE 2380.20 = 1620.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 491.30       | 18.53     | 3.962                 | 387.57      |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2380.20 = 7867.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 289.62       | 10.78     | 5.618                 |
| 2             | 493.91       | 18.53     | 3.962                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 493.91 Tc(MIN.) = 18.53  
TOTAL AREA(ACRES) = 404.2

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2380.20 TO NODE 2380.20 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2380.20 TO NODE 2380.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 847.00 DOWNSTREAM(FEET) = 831.00  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 45.0 INCH PIPE IS 32.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 58.03  
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 493.91  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 18.54  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2380.00 = 7932.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.00 TO NODE 2380.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2413.00 TO NODE 2412.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00

UPSTREAM ELEVATION(FEET) = 891.00

DOWNSTREAM ELEVATION(FEET) = 888.00

ELEVATION DIFFERENCE(FEET) = 3.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914

SUBAREA RUNOFF(CFS) = 0.45

TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 2412.00 TO NODE 2412.50 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 888.00 DOWNSTREAM ELEVATION(FEET) = 882.00

STREET LENGTH(FEET) = 358.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.96

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.34

HALFSTREET FLOOD WIDTH(FEET) = 10.84

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.06

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.05

STREET FLOW TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 8.29

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.656

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.570

SUBAREA AREA(ACRES) = 1.84 SUBAREA RUNOFF(CFS) = 6.98

TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 7.36

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.03

FLOW VELOCITY(FEET/SEC.) = 3.53 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.43

LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2412.50 = 453.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2412.50 TO NODE 2411.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 876.00 DOWNSTREAM(FEET) = 874.00

FLOW LENGTH(FEET) = 360.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.79

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 7.36

PIPE TRAVEL TIME(MIN.) = 1.25 Tc(MIN.) = 9.54

LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2411.00 = 813.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2411.00 TO NODE 2411.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 9.54

RAINFALL INTENSITY(INCH/HR) = 6.08

TOTAL STREAM AREA(ACRES) = 1.94

PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 2410.00 TO NODE 2409.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700

S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 68.75  
UPSTREAM ELEVATION(FEET) = 895.00  
DOWNSTREAM ELEVATION(FEET) = 894.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.981  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.435  
SUBAREA RUNOFF(CFS) = 0.30  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2409.00 TO NODE 2411.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 894.00 DOWNSTREAM ELEVATION(FEET) = 880.00  
STREET LENGTH(FEET) = 495.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.07  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.24  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.64  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.13  
STREET FLOW TRAVEL TIME(MIN.) = 2.27 Tc(MIN.) = 9.25  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.202

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 3.81 SUBAREA RUNOFF(CFS) = 13.47  
TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 13.72

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.28  
FLOW VELOCITY(FEET/SEC.) = 4.22 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.57  
LONGEST FLOWPATH FROM NODE 2410.00 TO NODE 2411.00 = 563.75 FEET.

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\*\*\*\*\*

FLOW PROCESS FROM NODE 2411.00 TO NODE 2411.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.25  
RAINFALL INTENSITY(INCH/HR) = 6.20  
TOTAL STREAM AREA(ACRES) = 3.88  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.72

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 7.36         | 9.54      | 6.078                 | 1.94        |
| 2             | 13.72        | 9.25      | 6.202                 | 3.88        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 20.85        | 9.25      | 6.202                 |
| 2             | 20.80        | 9.54      | 6.078                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 20.85 Tc(MIN.) = 9.25  
TOTAL AREA(ACRES) = 5.8  
LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2411.00 = 813.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2411.00 TO NODE 2408.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 874.00 DOWNSTREAM(FEET) = 873.00  
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.38  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 20.85  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 9.36  
LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2408.00 = 878.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2408.00 TO NODE 2408.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.36  
RAINFALL INTENSITY(INCH/HR) = 6.15  
TOTAL STREAM AREA(ACRES) = 5.82  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.85

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2407.00 TO NODE 2406.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 885.00  
DOWNSTREAM ELEVATION(FEET) = 883.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.613  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.700  
SUBAREA RUNOFF(CFS) = 0.44  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.44

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2406.00 TO NODE 2405.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 883.00 DOWNSTREAM ELEVATION(FEET) = 880.00  
STREET LENGTH(FEET) = 285.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

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\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.38  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.31  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.09  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.61  
STREET FLOW TRAVEL TIME(MIN.) = 2.27 Tc(MIN.) = 8.89  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.364  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.61 SUBAREA RUNOFF(CFS) = 5.84  
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 6.20

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.84  
FLOW VELOCITY(FEET/SEC.) = 2.40 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.82  
LONGEST FLOWPATH FROM NODE 2407.00 TO NODE 2405.00 = 370.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2405.00 TO NODE 2408.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 874.00 DOWNSTREAM(FEET) = 873.00  
FLOW LENGTH(FEET) = 330.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.78  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.20  
PIPE TRAVEL TIME(MIN.) = 1.46 Tc(MIN.) = 10.34  
LONGEST FLOWPATH FROM NODE 2407.00 TO NODE 2408.00 = 700.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2408.00 TO NODE 2408.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.34  
RAINFALL INTENSITY(INCH/HR) = 5.77  
TOTAL STREAM AREA(ACRES) = 1.71  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.20

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 20.85        | 9.36      | 6.152                 | 5.82        |
| 2             | 6.20         | 10.34     | 5.771                 | 1.71        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 26.47        | 9.36      | 6.152                 |
| 2             | 25.76        | 10.34     | 5.771                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 26.47 Tc(MIN.) = 9.36  
 TOTAL AREA(ACRES) = 7.5  
 LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2408.00 = 878.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2408.00 TO NODE 2404.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 873.00 DOWNSTREAM(FEET) = 867.00  
 FLOW LENGTH(FEET) = 395.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.94  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 26.47  
 PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 10.03  
 LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2404.00 = 1273.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2404.00 TO NODE 2404.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.03  
 RAINFALL INTENSITY(INCH/HR) = 5.89  
 TOTAL STREAM AREA(ACRES) = 7.53  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 26.47

\*\*\*\*\*



FLOW PROCESS FROM NODE 2403.00 TO NODE 2402.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 66.67
UPSTREAM ELEVATION(FEET) = 885.00
DOWNSTREAM ELEVATION(FEET) = 884.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.805
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.559
SUBAREA RUNOFF(CFS) = 0.56
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 2402.00 TO NODE 2404.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 884.00 DOWNSTREAM ELEVATION(FEET) = 873.00
STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.03
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 7.31
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.09
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.84
STREET FLOW TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 9.10
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.268

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570
SUBAREA AREA(ACRES) = 1.93 SUBAREA RUNOFF(CFS) = 6.89

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TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 7.36

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.63
FLOW VELOCITY(FEET/SEC.) = 3.52 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.12
LONGEST FLOWPATH FROM NODE 2403.00 TO NODE 2404.00 = 491.67 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2404.00 TO NODE 2404.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.10
RAINFALL INTENSITY(INCH/HR) = 6.27
TOTAL STREAM AREA(ACRES) = 2.06
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.36

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 33.38 Tc(MIN.) = 10.03
TOTAL AREA(ACRES) = 9.6
LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2404.00 = 1273.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2404.00 TO NODE 2401.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 867.00 DOWNSTREAM(FEET) = 830.00
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013

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DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 29.31  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 33.38  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.12  
LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2401.00 = 1433.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2401.00 TO NODE 2380.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 830.00 DOWNSTREAM(FEET) = 829.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 95.00 CHANNEL SLOPE = 0.0105  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.728

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 36.09  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.60  
AVERAGE FLOW DEPTH(FEET) = 1.37 TRAVEL TIME(MIN.) = 0.34  
Tc(MIN.) = 10.46  
SUBAREA AREA(ACRES) = 1.66 SUBAREA RUNOFF(CFS) = 5.42  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
TOTAL AREA(ACRES) = 11.2 PEAK FLOW RATE(CFS) = 36.73

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.38 FLOW VELOCITY(FEET/SEC.) = 4.63  
LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2380.00 = 1528.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2380.00 TO NODE 2380.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2390.00 TO NODE 2389.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

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UPSTREAM ELEVATION(FEET) = 900.00  
DOWNSTREAM ELEVATION(FEET) = 895.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.579  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.592  
SUBAREA RUNOFF(CFS) = 0.98  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.98

\*\*\*\*\*

FLOW PROCESS FROM NODE 2389.00 TO NODE 2389.50 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 895.00 DOWNSTREAM ELEVATION(FEET) = 876.00  
STREET LENGTH(FEET) = 565.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.68  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.52  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.17  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.75  
STREET FLOW TRAVEL TIME(MIN.) = 2.97 Tc(MIN.) = 8.55  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.526

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.91 SUBAREA RUNOFF(CFS) = 3.38  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 4.13

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 6.91  
FLOW VELOCITY(FEET/SEC.) = 3.46 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.92  
LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2389.50 = 665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2389.50 TO NODE 2388.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 870.00 DOWNSTREAM(FEET) = 867.00
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.89
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.13
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 8.69
LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2388.00 = 740.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2388.00 TO NODE 2388.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.69
RAINFALL INTENSITY(INCH/HR) = 6.46
TOTAL STREAM AREA(ACRES) = 1.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.13

\*\*\*\*\*
FLOW PROCESS FROM NODE 2387.00 TO NODE 2386.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 881.00
DOWNSTREAM ELEVATION(FEET) = 878.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914
SUBAREA RUNOFF(CFS) = 0.50
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*
FLOW PROCESS FROM NODE 2386.00 TO NODE 2385.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 878.00 DOWNSTREAM ELEVATION(FEET) = 874.00  
STREET LENGTH(FEET) = 170.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.44  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.69  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.65  
STREET FLOW TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 7.39  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.168

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.95 SUBAREA RUNOFF(CFS) = 3.88  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 4.33

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.71  
FLOW VELOCITY(FEET/SEC.) = 3.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.85  
LONGEST FLOWPATH FROM NODE 2387.00 TO NODE 2385.00 = 265.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2385.00 TO NODE 2388.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 868.00 DOWNSTREAM(FEET) = 867.00  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.99  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.33

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PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 7.46  
LONGEST FLOWPATH FROM NODE 2387.00 TO NODE 2388.00 = 300.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2388.00 TO NODE 2388.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.46  
RAINFALL INTENSITY(INCH/HR) = 7.12  
TOTAL STREAM AREA(ACRES) = 1.06  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.33

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 4.13         | 8.69      | 6.457                 | 1.11        |
| 2             | 4.33         | 7.46      | 7.122                 | 1.06        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 7.88         | 7.46      | 7.122                 |
| 2             | 8.06         | 8.69      | 6.457                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 8.06 Tc(MIN.) = 8.69  
TOTAL AREA(ACRES) = 2.2  
LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2388.00 = 740.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2388.00 TO NODE 2384.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 867.00 DOWNSTREAM(FEET) = 859.00  
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.68  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

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PIPE-FLOW(CFS) = 8.06  
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 9.00  
LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2384.00 = 940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2384.00 TO NODE 2384.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.00  
RAINFALL INTENSITY(INCH/HR) = 6.31  
TOTAL STREAM AREA(ACRES) = 2.17  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.06

\*\*\*\*\*

FLOW PROCESS FROM NODE 2383.00 TO NODE 2382.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.50  
UPSTREAM ELEVATION(FEET) = 876.00  
DOWNSTREAM ELEVATION(FEET) = 872.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.885  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.302  
SUBAREA RUNOFF(CFS) = 0.95  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.95

\*\*\*\*\*

FLOW PROCESS FROM NODE 2382.00 TO NODE 2384.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 872.00 DOWNSTREAM ELEVATION(FEET) = 865.00  
STREET LENGTH(FEET) = 150.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2



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STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.39  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.18  
HALFSTREET FLOOD WIDTH(FEET) = 2.86  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.46  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.64  
STREET FLOW TRAVEL TIME(MIN.) = 0.72 Tc(MIN.) = 6.61  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.705  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 0.88  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.76

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.20 HALFSTREET FLOOD WIDTH(FEET) = 3.72  
FLOW VELOCITY(FEET/SEC.) = 3.42 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.69  
LONGEST FLOWPATH FROM NODE 2383.00 TO NODE 2384.00 = 247.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2384.00 TO NODE 2384.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.61  
RAINFALL INTENSITY(INCH/HR) = 7.70  
TOTAL STREAM AREA(ACRES) = 0.40  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.76

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.06         | 9.00      | 6.312                 | 2.17        |
| 2             | 1.76         | 6.61      | 7.705                 | 0.40        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM | RUNOFF | Tc | INTENSITY |
|--------|--------|----|-----------|
|--------|--------|----|-----------|

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) |
|--------|-------|--------|-------------|
| 1      | 8.36  | 6.61   | 7.705       |
| 2      | 9.49  | 9.00   | 6.312       |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.49 Tc(MIN.) = 9.00  
TOTAL AREA(ACRES) = 2.6  
LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2384.00 = 940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2384.00 TO NODE 2381.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 859.00 DOWNSTREAM(FEET) = 832.00  
FLOW LENGTH(FEET) = 90.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.17  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.49  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 9.06  
LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2381.00 = 1030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2381.00 TO NODE 2380.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 832.00 DOWNSTREAM(FEET) = 830.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 80.00 CHANNEL SLOPE = 0.0250  
CHANNEL FLOW THRU SUBAREA(CFS) = 9.49  
FLOW VELOCITY(FEET/SEC) = 3.90 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 9.41  
LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2380.00 = 1110.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.00 TO NODE 2380.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.49         | 9.41      | 6.135                 | 2.57        |

LONGEST FLOWPATH FROM NODE 2390.00 TO NODE 2380.00 = 1110.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 36.73        | 10.46     | 5.728                 | 11.25       |

LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2380.00 = 1528.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 42.52        | 9.41      | 6.135                 |
| 2             | 45.59        | 10.46     | 5.728                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 45.59 Tc(MIN.) = 10.46  
 TOTAL AREA(ACRES) = 13.8

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.00 TO NODE 2380.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.00 TO NODE 2380.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 10.46 RAIN INTENSITY(INCH/HOUR) = 5.73  
 TOTAL AREA(ACRES) = 13.80 TOTAL RUNOFF(CFS) = 7.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.00 TO NODE 2380.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 7.40         | 10.46     | 5.729                 | 13.80       |

LONGEST FLOWPATH FROM NODE 2413.00 TO NODE 2380.00 = 1528.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|

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1 493.91 18.54 3.959 404.17  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2380.00 = 7932.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 285.98       | 10.46     | 5.729                 |
| 2             | 499.03       | 18.54     | 3.959                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 499.03 Tc(MIN.) = 18.54  
TOTAL AREA(ACRES) = 418.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.00 TO NODE 2380.00 IS CODE = 12

-----

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 2380.00 TO NODE 2379.00 IS CODE = 52

-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 837.00 DOWNSTREAM(FEET) = 825.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 170.00 CHANNEL SLOPE = 0.0706  
CHANNEL FLOW THRU SUBAREA(CFS) = 499.03  
FLOW VELOCITY(FEET/SEC) = 20.79 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 18.68  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2379.00 = 8102.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2379.00 TO NODE 2379.00 IS CODE = 10

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 2378.00 TO NODE 2377.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1175.00

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DOWNSTREAM ELEVATION(FEET) = 1155.00  
ELEVATION DIFFERENCE(FEET) = 20.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.548  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.749  
SUBAREA RUNOFF(CFS) = 0.19  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2377.00 TO NODE 2376.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1155.00 DOWNSTREAM(FEET) = 1070.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.2833  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.126  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.83  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.50  
AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 0.91  
Tc(MIN.) = 7.46  
SUBAREA AREA(ACRES) = 1.84 SUBAREA RUNOFF(CFS) = 3.28  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 3.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.15 FLOW VELOCITY(FEET/SEC.) = 7.00  
LONGEST FLOWPATH FROM NODE 2378.00 TO NODE 2376.00 = 385.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2376.00 TO NODE 2375.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1070.00 DOWNSTREAM(FEET) = 955.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 605.00 CHANNEL SLOPE = 0.1901  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.529  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0

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TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.96  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.30  
AVERAGE FLOW DEPTH(FEET) = 0.35 TRAVEL TIME(MIN.) = 1.08  
Tc(MIN.) = 8.54  
SUBAREA AREA(ACRES) = 10.41 SUBAREA RUNOFF(CFS) = 16.99  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 12.4 PEAK FLOW RATE(CFS) = 20.16

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.47 FLOW VELOCITY(FEET/SEC.) = 10.94  
LONGEST FLOWPATH FROM NODE 2378.00 TO NODE 2375.00 = 990.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2375.00 TO NODE 2374.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 955.00 DOWNSTREAM(FEET) = 885.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 455.00 CHANNEL SLOPE = 0.1538  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.230

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2600  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 33.21  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.80  
AVERAGE FLOW DEPTH(FEET) = 0.65 TRAVEL TIME(MIN.) = 0.64  
Tc(MIN.) = 9.18  
SUBAREA AREA(ACRES) = 16.11 SUBAREA RUNOFF(CFS) = 26.10  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.256  
TOTAL AREA(ACRES) = 28.5 PEAK FLOW RATE(CFS) = 45.33

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.77 FLOW VELOCITY(FEET/SEC.) = 12.89  
LONGEST FLOWPATH FROM NODE 2378.00 TO NODE 2374.00 = 1445.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2374.00 TO NODE 2379.20 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 885.00 DOWNSTREAM(FEET) = 855.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 420.00 CHANNEL SLOPE = 0.0714  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.944  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 49.10  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.08  
AVERAGE FLOW DEPTH(FEET) = 0.98 TRAVEL TIME(MIN.) = 0.69  
Tc(MIN.) = 9.88  
SUBAREA AREA(ACRES) = 4.23 SUBAREA RUNOFF(CFS) = 7.54  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.261  
TOTAL AREA(ACRES) = 32.7 PEAK FLOW RATE(CFS) = 50.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.00 FLOW VELOCITY(FEET/SEC.) = 10.13  
LONGEST FLOWPATH FROM NODE 2378.00 TO NODE 2379.20 = 1865.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2379.20 TO NODE 2379.20 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2373.00 TO NODE 2372.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 925.00  
DOWNSTREAM ELEVATION(FEET) = 924.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.663  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.663  
SUBAREA RUNOFF(CFS) = 0.39  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.39

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2372.00 TO NODE 2371.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 924.00 DOWNSTREAM ELEVATION(FEET) = 914.00  
STREET LENGTH(FEET) = 290.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.89  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.72  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.25  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.78  
STREET FLOW TRAVEL TIME(MIN.) = 1.49 Tc(MIN.) = 8.15  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.729

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 4.99  
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 5.33

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.78  
FLOW VELOCITY(FEET/SEC.) = 3.69 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.04  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2371.00 = 355.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2371.00 TO NODE 2370.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 908.00 DOWNSTREAM(FEET) = 906.00  
FLOW LENGTH(FEET) = 310.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.85  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.33  
PIPE TRAVEL TIME(MIN.) = 1.07 Tc(MIN.) = 9.21  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2370.00 = 665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2370.00 TO NODE 2370.00 IS CODE = 1



>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.21
RAINFALL INTENSITY(INCH/HR) = 6.22
TOTAL STREAM AREA(ACRES) = 1.39
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.33

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*****
FLOW PROCESS FROM NODE 2369.00 TO NODE 2368.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00
UPSTREAM ELEVATION(FEET) = 920.00
DOWNSTREAM ELEVATION(FEET) = 917.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914
SUBAREA RUNOFF(CFS) = 0.50
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.50

```

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*****
FLOW PROCESS FROM NODE 2368.00 TO NODE 2370.00 IS CODE = 62
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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

```

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=====
UPSTREAM ELEVATION(FEET) = 917.00 DOWNSTREAM ELEVATION(FEET) = 912.00
STREET LENGTH(FEET) = 360.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

```

```

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

```

```

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.20
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30

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HALFSTREET FLOOD WIDTH(FEET) = 8.57  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.46  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.73  
 STREET FLOW TRAVEL TIME(MIN.) = 2.44 Tc(MIN.) = 8.78  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.415  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
 SUBAREA AREA(ACRES) = 2.01 SUBAREA RUNOFF(CFS) = 7.35  
 TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 7.75

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.22  
 FLOW VELOCITY(FEET/SEC.) = 2.82 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.99  
 LONGEST FLOWPATH FROM NODE 2369.00 TO NODE 2370.00 = 455.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2370.00 TO NODE 2370.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.78  
 RAINFALL INTENSITY(INCH/HR) = 6.41  
 TOTAL STREAM AREA(ACRES) = 2.12  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.75

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 5.33         | 9.21      | 6.216                 | 1.39        |
| 2             | 7.75         | 8.78      | 6.415                 | 2.12        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.83        | 8.78      | 6.415                 |
| 2             | 12.84        | 9.21      | 6.216                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 12.84 Tc(MIN.) = 9.21  
 TOTAL AREA(ACRES) = 3.5

LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2370.00 = 665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2370.00 TO NODE 2367.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 906.00 DOWNSTREAM(FEET) = 894.00
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.98
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.84
PIPE TRAVEL TIME(MIN.) = 0.42 Tc(MIN.) = 9.63
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2367.00 = 965.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2367.00 TO NODE 2367.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.63
RAINFALL INTENSITY(INCH/HR) = 6.04
TOTAL STREAM AREA(ACRES) = 3.51
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.84

\*\*\*\*\*

FLOW PROCESS FROM NODE 2366.00 TO NODE 2365.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .5700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 81.58
UPSTREAM ELEVATION(FEET) = 911.00
DOWNSTREAM ELEVATION(FEET) = 909.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.391
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.872
SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 2365.00 TO NODE 2367.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 909.00 DOWNSTREAM ELEVATION(FEET) = 900.00  
STREET LENGTH(FEET) = 405.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.67  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.32  
HALFSTREET FLOOD WIDTH(FEET) = 9.90  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.34  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.08  
STREET FLOW TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 8.41  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.594

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.80 SUBAREA RUNOFF(CFS) = 6.77  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 6.99

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.97  
FLOW VELOCITY(FEET/SEC.) = 3.88 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.50  
LONGEST FLOWPATH FROM NODE 2366.00 TO NODE 2367.00 = 486.58 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2367.00 TO NODE 2367.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.41  
RAINFALL INTENSITY(INCH/HR) = 6.59  
TOTAL STREAM AREA(ACRES) = 1.86

PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.99

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.84        | 9.63      | 6.041                 | 3.51        |
| 2             | 6.99         | 8.41      | 6.594                 | 1.86        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 18.76        | 8.41      | 6.594                 |
| 2             | 19.25        | 9.63      | 6.041                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.25 Tc(MIN.) = 9.63  
TOTAL AREA(ACRES) = 5.4  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2367.00 = 965.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2367.00 TO NODE 2364.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 894.00 DOWNSTREAM(FEET) = 887.00  
FLOW LENGTH(FEET) = 205.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.47  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.25  
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 9.91  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2364.00 = 1170.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2364.00 TO NODE 2364.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.91  
RAINFALL INTENSITY(INCH/HR) = 5.93  
TOTAL STREAM AREA(ACRES) = 5.37  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.25

\*\*\*\*\*

FLOW PROCESS FROM NODE 2363.00 TO NODE 2362.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 83.33  
UPSTREAM ELEVATION(FEET) = 905.00  
DOWNSTREAM ELEVATION(FEET) = 903.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.505  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.782  
SUBAREA RUNOFF(CFS) = 0.44  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.44

\*\*\*\*\*

FLOW PROCESS FROM NODE 2362.00 TO NODE 2364.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 903.00 DOWNSTREAM ELEVATION(FEET) = 894.00  
STREET LENGTH(FEET) = 230.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.51  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.31  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.84  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.05  
STREET FLOW TRAVEL TIME(MIN.) = 1.00 Tc(MIN.) = 7.50  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.098

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.02 SUBAREA RUNOFF(CFS) = 4.13  
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 4.53

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.63  
FLOW VELOCITY(FEET/SEC.) = 4.33 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.38  
LONGEST FLOWPATH FROM NODE 2363.00 TO NODE 2364.00 = 313.33 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2364.00 TO NODE 2364.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.50  
RAINFALL INTENSITY(INCH/HR) = 7.10  
TOTAL STREAM AREA(ACRES) = 1.12  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.53

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 19.25        | 9.91      | 5.933                 | 5.37        |
| 2             | 4.53         | 7.50      | 7.098                 | 1.12        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 20.62        | 7.50      | 7.098                 |
| 2             | 23.04        | 9.91      | 5.933                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 23.04 Tc(MIN.) = 9.91  
TOTAL AREA(ACRES) = 6.5  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2364.00 = 1170.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2364.00 TO NODE 2361.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

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ELEVATION DATA: UPSTREAM(FEET) = 888.00 DOWNSTREAM(FEET) = 884.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.78  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 23.04  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 10.03  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2361.00 = 1270.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2361.00 TO NODE 2361.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.03  
RAINFALL INTENSITY(INCH/HR) = 5.89  
TOTAL STREAM AREA(ACRES) = 6.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 2360.00 TO NODE 2359.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 898.00  
DOWNSTREAM ELEVATION(FEET) = 895.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.914  
SUBAREA RUNOFF(CFS) = 0.63  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.63

\*\*\*\*\*

FLOW PROCESS FROM NODE 2359.00 TO NODE 2361.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 895.00 DOWNSTREAM ELEVATION(FEET) = 890.00  
STREET LENGTH(FEET) = 195.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00



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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.44  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 7.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.23  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.92  
STREET FLOW TRAVEL TIME(MIN.) = 1.00 Tc(MIN.) = 7.34  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.197

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 0.88 SUBAREA RUNOFF(CFS) = 3.61  
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 4.18

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.16  
FLOW VELOCITY(FEET/SEC.) = 3.64 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.20  
LONGEST FLOWPATH FROM NODE 2360.00 TO NODE 2361.00 = 290.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2361.00 TO NODE 2361.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<  
-----

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.34  
RAINFALL INTENSITY(INCH/HR) = 7.20  
TOTAL STREAM AREA(ACRES) = 1.02  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.18

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 23.04        | 10.03     | 5.887                 | 6.49        |
| 2             | 4.18         | 7.34      | 7.197                 | 1.02        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 23.03        | 7.34      | 7.197                 |
| 2             | 26.46        | 10.03     | 5.887                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.46 Tc(MIN.) = 10.03  
TOTAL AREA(ACRES) = 7.5  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2361.00 = 1270.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2361.00 TO NODE 2358.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 884.00 DOWNSTREAM(FEET) = 879.00  
FLOW LENGTH(FEET) = 145.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.20  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.46  
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 10.21  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2358.00 = 1415.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2358.00 TO NODE 2358.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.21  
RAINFALL INTENSITY(INCH/HR) = 5.82  
TOTAL STREAM AREA(ACRES) = 7.51  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 26.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 2357.00 TO NODE 2356.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700

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S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 895.00  
DOWNSTREAM ELEVATION(FEET) = 892.40  
ELEVATION DIFFERENCE(FEET) = 2.60  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.059  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.147  
SUBAREA RUNOFF(CFS) = 0.46  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 2356.00 TO NODE 2358.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 892.40 DOWNSTREAM ELEVATION(FEET) = 885.00  
STREET LENGTH(FEET) = 370.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.84  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.58  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.78  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.77  
STREET FLOW TRAVEL TIME(MIN.) = 2.22 Tc(MIN.) = 8.28  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.660

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.570  
SUBAREA AREA(ACRES) = 1.77 SUBAREA RUNOFF(CFS) = 6.72  
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 7.10

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 9.97  
FLOW VELOCITY(FEET/SEC.) = 3.19 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.04  
LONGEST FLOWPATH FROM NODE 2357.00 TO NODE 2358.00 = 455.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2358.00 TO NODE 2358.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.28
RAINFALL INTENSITY(INCH/HR) = 6.66
TOTAL STREAM AREA(ACRES) = 1.87
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.10

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 32.66 Tc(MIN.) = 10.21
TOTAL AREA(ACRES) = 9.4
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2358.00 = 1415.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2358.00 TO NODE 2555.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 879.00 DOWNSTREAM(FEET) = 865.00
FLOW LENGTH(FEET) = 205.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.27
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 32.66
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 10.40
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2555.00 = 1620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2555.00 TO NODE 2554.80 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

|  |        |                       |        |
|--|--------|-----------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =         | 865.00 | DOWNSTREAM(FEET) =    | 864.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) =      | 50.00  | CHANNEL SLOPE =       | 0.0200 |
| CHANNEL BASE(FEET) =                     | 3.00   | "Z" FACTOR =          | 2.000  |
| MANNING'S FACTOR =                       | 0.030  | MAXIMUM DEPTH(FEET) = | 10.00  |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.699  |                       |        |

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 33.33  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.69  
AVERAGE FLOW DEPTH(FEET) = 1.12 TRAVEL TIME(MIN.) = 0.15  
Tc(MIN.) = 10.54  
SUBAREA AREA(ACRES) = 0.78 SUBAREA RUNOFF(CFS) = 1.33  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.549  
TOTAL AREA(ACRES) = 10.2 PEAK FLOW RATE(CFS) = 32.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.11 FLOW VELOCITY(FEET/SEC.) = 5.64  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2554.80 = 1670.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2554.80 TO NODE 2379.20 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

=====

|  |        |                       |        |
|--|--------|-----------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =         | 864.00 | DOWNSTREAM(FEET) =    | 855.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) =      | 300.00 | CHANNEL SLOPE =       | 0.0300 |
| CHANNEL BASE(FEET) =                     | 3.00   | "Z" FACTOR =          | 2.000  |
| MANNING'S FACTOR =                       | 0.030  | MAXIMUM DEPTH(FEET) = | 10.00  |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 5.455  |                       |        |

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 36.44  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.75  
AVERAGE FLOW DEPTH(FEET) = 1.06 TRAVEL TIME(MIN.) = 0.74  
Tc(MIN.) = 11.28  
SUBAREA AREA(ACRES) = 4.94 SUBAREA RUNOFF(CFS) = 7.55  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.461  
TOTAL AREA(ACRES) = 15.1 PEAK FLOW RATE(CFS) = 37.99

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.08 FLOW VELOCITY(FEET/SEC.) = 6.83  
LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2379.20 = 1970.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2379.20 TO NODE 2379.20 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 37.99        | 11.28     | 5.455                 | 15.10       |

LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2379.20 = 1970.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 50.79        | 9.88      | 5.944                 | 32.69       |

LONGEST FLOWPATH FROM NODE 2378.00 TO NODE 2379.20 = 1865.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 84.05        | 9.88      | 5.944                 |
| 2             | 84.60        | 11.28     | 5.455                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 84.60 Tc(MIN.) = 11.28  
TOTAL AREA(ACRES) = 47.8

\*\*\*\*\*

FLOW PROCESS FROM NODE 2379.20 TO NODE 2379.20 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2379.20 TO NODE 2379.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 855.00 DOWNSTREAM(FEET) = 825.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 610.00 CHANNEL SLOPE = 0.0492  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000

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MANNING'S FACTOR = 0.030    MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.167  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 88.79  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.27  
 AVERAGE FLOW DEPTH(FEET) = 1.46    TRAVEL TIME(MIN.) = 0.99  
 Tc(MIN.) = 12.27  
 SUBAREA AREA(ACRES) = 5.40    SUBAREA RUNOFF(CFS) = 8.37  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.322  
 TOTAL AREA(ACRES) = 53.2    PEAK FLOW RATE(CFS) = 88.51

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 1.45    FLOW VELOCITY(FEET/SEC.) = 10.30  
 LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2379.00 = 2580.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2379.00 TO NODE 2379.00 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 88.51        | 12.27     | 5.167                 | 53.19       |

LONGEST FLOWPATH FROM NODE 2373.00 TO NODE 2379.00 = 2580.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 499.03       | 18.68     | 3.941                 | 417.97      |

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2379.00 = 8102.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 416.38       | 12.27     | 5.167                 |
| 2             | 566.53       | 18.68     | 3.941                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 566.53    Tc(MIN.) = 18.68  
 TOTAL AREA(ACRES) = 471.2

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2379.00 TO NODE 2379.00 IS CODE = 12  
 -----

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2379.00 TO NODE 2379.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 18.68  
RAINFALL INTENSITY(INCH/HR) = 3.94  
TOTAL STREAM AREA(ACRES) = 471.16  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 566.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2370.00 TO NODE 2369.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1065.00  
DOWNSTREAM ELEVATION(FEET) = 1020.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.538  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.633  
SUBAREA RUNOFF(CFS) = 0.40  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.40

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2369.00 TO NODE 2368.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1020.00 DOWNSTREAM(FEET) = 860.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 360.00 CHANNEL SLOPE = 0.4444  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2193 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.40  
FLOW VELOCITY(FEET/SEC) = 2.62 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 7.83  
LONGEST FLOWPATH FROM NODE 2370.00 TO NODE 2368.00 = 455.00 FEET.



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2369.00 TO NODE 2368.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.907  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 0.93 SUBAREA RUNOFF(CFS) = 2.70  
TOTAL AREA(ACRES) = 1.0 TOTAL RUNOFF(CFS) = 3.02  
TC(MIN.) = 7.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2368.00 TO NODE 2367.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 865.00 DOWNSTREAM(FEET) = 830.00  
FLOW LENGTH(FEET) = 115.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.68  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.02  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.94  
LONGEST FLOWPATH FROM NODE 2370.00 TO NODE 2367.00 = 570.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2367.00 TO NODE 2379.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 830.00 DOWNSTREAM(FEET) = 825.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 110.00 CHANNEL SLOPE = 0.0455  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0455 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.02  
FLOW VELOCITY(FEET/SEC) = 1.72 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.06 Tc(MIN.) = 9.00  
LONGEST FLOWPATH FROM NODE 2370.00 TO NODE 2379.00 = 680.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2379.00 TO NODE 2379.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.00  
RAINFALL INTENSITY(INCH/HR) = 6.31  
TOTAL STREAM AREA(ACRES) = 1.04  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.02

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 566.53       | 18.68     | 3.941                 | 471.16      |
| 2             | 3.02         | 9.00      | 6.310                 | 1.04        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 276.06       | 9.00      | 6.310                 |
| 2             | 568.41       | 18.68     | 3.941                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 568.41 Tc(MIN.) = 18.68  
TOTAL AREA(ACRES) = 472.2  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2379.00 = 8102.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2379.00 TO NODE 2378.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 825.00 DOWNSTREAM(FEET) = 815.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 655.00 CHANNEL SLOPE = 0.0153  
CHANNEL FLOW THRU SUBAREA(CFS) = 568.41  
FLOW VELOCITY(FEET/SEC) = 10.08 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.08 Tc(MIN.) = 19.76  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2378.00 = 8757.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2379.00 TO NODE 2378.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
-----

```
=====
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.800
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4200
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2985
SUBAREA AREA(ACRES) = 13.91 SUBAREA RUNOFF(CFS) = 22.20
TOTAL AREA(ACRES) = 486.1 TOTAL RUNOFF(CFS) = 568.41
TC(MIN.) = 19.76
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE
```

```
*****
FLOW PROCESS FROM NODE 2378.00 TO NODE 2378.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
```

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 19.76
RAINFALL INTENSITY(INCH/HR) = 3.80
TOTAL STREAM AREA(ACRES) = 486.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 568.41
```

```
*****
FLOW PROCESS FROM NODE 2366.00 TO NODE 2365.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
```

```
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4200
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1180.00
DOWNSTREAM ELEVATION(FEET) = 1175.00
ELEVATION DIFFERENCE(FEET) = 5.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.944
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.248
SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.45
```

```
*****
FLOW PROCESS FROM NODE 2365.00 TO NODE 2364.00 IS CODE = 53
-----
>>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1175.00 DOWNSTREAM(FEET) = 860.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 665.00 CHANNEL SLOPE = 0.4737
```

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .2224 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.45  
FLOW VELOCITY(FEET/SEC) = 2.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.20 Tc(MIN.) = 10.14  
LONGEST FLOWPATH FROM NODE 2366.00 TO NODE 2364.00 = 745.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2365.00 TO NODE 2364.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.844  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 3.34 SUBAREA RUNOFF(CFS) = 8.20  
TOTAL AREA(ACRES) = 3.5 TOTAL RUNOFF(CFS) = 8.52  
TC(MIN.) = 10.14

\*\*\*\*\*

FLOW PROCESS FROM NODE 2364.00 TO NODE 2363.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 860.00 DOWNSTREAM(FEET) = 842.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.72  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.52  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.23  
LONGEST FLOWPATH FROM NODE 2366.00 TO NODE 2363.00 = 845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2363.00 TO NODE 2378.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 842.00 DOWNSTREAM(FEET) = 815.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 450.00 CHANNEL SLOPE = 0.0600  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0600 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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CHANNEL FLOW THRU SUBAREA(CFS) = 8.52  
FLOW VELOCITY(FEET/SEC) = 2.80 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.68 Tc(MIN.) = 12.91  
LONGEST FLOWPATH FROM NODE 2366.00 TO NODE 2378.00 = 1295.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2378.00 TO NODE 2378.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.91  
RAINFALL INTENSITY(INCH/HR) = 5.00  
TOTAL STREAM AREA(ACRES) = 3.47  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 2362.00 TO NODE 2361.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1175.00  
DOWNSTREAM ELEVATION(FEET) = 1165.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.082  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.125  
SUBAREA RUNOFF(CFS) = 0.38  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 2361.00 TO NODE 2360.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1165.00 DOWNSTREAM(FEET) = 865.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 580.00 CHANNEL SLOPE = 0.5172  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2259 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.38  
FLOW VELOCITY(FEET/SEC) = 2.66 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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TRAVEL TIME(MIN.) = 3.63 Tc(MIN.) = 8.71  
LONGEST FLOWPATH FROM NODE 2362.00 TO NODE 2360.00 = 660.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2361.00 TO NODE 2360.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.445  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 2.99 SUBAREA RUNOFF(CFS) = 8.09  
TOTAL AREA(ACRES) = 3.1 TOTAL RUNOFF(CFS) = 8.36  
TC(MIN.) = 8.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 2360.00 TO NODE 2359.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 865.00 DOWNSTREAM(FEET) = 839.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.23  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.36  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 8.79  
LONGEST FLOWPATH FROM NODE 2362.00 TO NODE 2359.00 = 760.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2359.00 TO NODE 2378.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 839.00 DOWNSTREAM(FEET) = 815.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 310.00 CHANNEL SLOPE = 0.0774  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0774 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.36  
FLOW VELOCITY(FEET/SEC) = 3.16 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.63 Tc(MIN.) = 10.43  
LONGEST FLOWPATH FROM NODE 2362.00 TO NODE 2378.00 = 1070.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2378.00 TO NODE 2378.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.43  
 RAINFALL INTENSITY(INCH/HR) = 5.74  
 TOTAL STREAM AREA(ACRES) = 3.09  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.36

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 568.41       | 19.76     | 3.800                 | 486.11      |
| 2             | 8.52         | 12.91     | 5.002                 | 3.47        |
| 3             | 8.36         | 10.43     | 5.740                 | 3.09        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 391.55       | 10.43     | 5.740                 |
| 2             | 447.68       | 12.91     | 5.002                 |
| 3             | 580.42       | 19.76     | 3.800                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 580.42 Tc(MIN.) = 19.76  
 TOTAL AREA(ACRES) = 492.7  
 LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 2378.00 = 8757.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2378.00 TO NODE 25.00 IS CODE = 52

-----  
 >>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 815.00 DOWNSTREAM(FEET) = 795.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 935.00 CHANNEL SLOPE = 0.0214  
 CHANNEL FLOW THRU SUBAREA(CFS) = 580.42  
 FLOW VELOCITY(FEET/SEC) = 12.01 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 1.30 Tc(MIN.) = 21.06  
 LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 25.00 = 9692.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2378.00 TO NODE 25.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.648  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3013  
SUBAREA AREA(ACRES) = 4.80 SUBAREA RUNOFF(CFS) = 7.35  
TOTAL AREA(ACRES) = 497.5 TOTAL RUNOFF(CFS) = 580.42  
TC(MIN.) = 21.06  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.00 TO NODE 25.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 21.06  
RAINFALL INTENSITY(INCH/HR) = 3.65  
TOTAL STREAM AREA(ACRES) = 497.47  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 580.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.30 TO NODE 25.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1175.00  
DOWNSTREAM ELEVATION(FEET) = 1150.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.707  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.467  
SUBAREA RUNOFF(CFS) = 0.93  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.93

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.20 TO NODE 25.10 IS CODE = 53



>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1150.00 DOWNSTREAM(FEET) = 935.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 590.00 CHANNEL SLOPE = 0.3644
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .2078 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.93
FLOW VELOCITY(FEET/SEC) = 2.55 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.85 Tc(MIN.) = 9.56
LONGEST FLOWPATH FROM NODE 25.30 TO NODE 25.10 = 680.00 FEET.

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\*\*\*\*\*

FLOW PROCESS FROM NODE 25.20 TO NODE 25.10 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.071
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3800
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3800
SUBAREA AREA(ACRES) = 9.55 SUBAREA RUNOFF(CFS) = 22.03
TOTAL AREA(ACRES) = 9.8 TOTAL RUNOFF(CFS) = 22.70
TC(MIN.) = 9.56

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\*\*\*\*\*

FLOW PROCESS FROM NODE 25.10 TO NODE 25.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 935.00 DOWNSTREAM(FEET) = 795.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 2310.00 CHANNEL SLOPE = 0.0606
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .0606 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 22.70
FLOW VELOCITY(FEET/SEC) = 3.90 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 9.87 Tc(MIN.) = 19.43
LONGEST FLOWPATH FROM NODE 25.30 TO NODE 25.00 = 2990.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 25.10 TO NODE 25.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.842

```

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\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3600

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.3649

SUBAREA AREA(ACRES) = 30.51 SUBAREA RUNOFF(CFS) = 42.20

TOTAL AREA(ACRES) = 40.3 TOTAL RUNOFF(CFS) = 56.56

TC(MIN.) = 19.43

\*\*\*\*\*

FLOW PROCESS FROM NODE 25.00 TO NODE 25.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 19.43

RAINFALL INTENSITY(INCH/HR) = 3.84

TOTAL STREAM AREA(ACRES) = 40.35

PEAK FLOW RATE(CFS) AT CONFLUENCE = 56.56

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 580.42       | 21.06     | 3.648                 | 497.47      |
| 2             | 56.56        | 19.43     | 3.842                 | 40.35       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 607.63       | 19.43     | 3.842                 |
| 2             | 634.12       | 21.06     | 3.648                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 634.12 Tc(MIN.) = 21.06

TOTAL AREA(ACRES) = 537.8

LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 25.00 = 9692.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 25.00 TO NODE 24.90 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 795.00 DOWNSTREAM(FEET) = 763.00

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CHANNEL LENGTH THRU SUBAREA(FEET) = 1270.00 CHANNEL SLOPE = 0.0252  
CHANNEL FLOW THRU SUBAREA(CFS) = 634.12  
FLOW VELOCITY(FEET/SEC) = 13.42 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.58 Tc(MIN.) = 22.64  
LONGEST FLOWPATH FROM NODE 2599.00 TO NODE 24.90 = 10962.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 25.00 TO NODE 24.90 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.481  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3089  
SUBAREA AREA(ACRES) = 15.21 SUBAREA RUNOFF(CFS) = 21.71  
TOTAL AREA(ACRES) = 553.0 TOTAL RUNOFF(CFS) = 634.12  
TC(MIN.) = 22.64  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 553.0 TC(MIN.) = 22.64  
PEAK FLOW RATE(CFS) = 634.12

=====

END OF RATIONAL METHOD ANALYSIS

↑



| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2340         | 2339   | 2    | 867.7            | 865              | 75               | 0.9         | 0.11          |                |      |   |   |
| 2339         | 2338   | 6    | 865              | 853              | 700              | 0.9         | 1.50          | 1 SIDE         |      |   |   |
| 2338         | 2335   | 3    | 847              | 834              | 410              |             |               |                |      |   |   |
| 2335         | 2335   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2337         | 2336   | 2    | 854.7            | 851.9            | 85               | 0.9         | 0.11          |                |      |   |   |
| 2336         | 2335   | 6    | 851.9            | 840              | 370              | 0.9         | 1.00          | 1 SIDE         |      |   |   |
| 2335         | 2335   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2335         | 2332   | 3    | 834              | 818.2            | 355              |             |               |                |      |   |   |
| 2332         | 2332   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2334         | 2333   | 2    | 841.7            | 837.7            | 85               | 0.9         | 0.10          |                |      |   |   |
| 2333         | 2332   | 6    | 837.7            | 820              | 315              | 0.9         | 0.41          | 1 SIDE         |      |   |   |
| 2332         | 2332   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2332         | 2331   | 3    | 818.2            | 817              | 120              |             |               |                |      |   |   |
| 2331         | 2330   | 5    | 817              | 816.7            | 25               |             |               | VALLEY         |      |   |   |
| 2330         | 2330   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2358         | 2357   | 2    | 1180             | 1165             | 90               | 0.42        | 0.14          |                |      |   |   |
| 2357         | 2356   | 5    | 1165             | 1055             | 490              |             |               | MTN            |      |   |   |
| 2357         | 2356   | 8    |                  |                  |                  | 0.42        | 6.15          |                |      |   |   |
| 2356         | 2355   | 5    | 1055             | 850              | 935              |             |               | MTN            |      |   |   |
| 2356         | 2355   | 8    |                  |                  |                  | 0.42        | 13.59         |                |      |   |   |
| 2355         | 2346   | 3    | 824              | 814              | 185              |             |               |                |      |   |   |
| 2346         | 2346   | 10   |                  |                  |                  |             |               | SAVE TO BANK 2 |      |   |   |
| 2354         | 2353   | 2    | 1300             | 1275             | 100              | 0.42        | 0.09          |                |      |   |   |
| 2353         | 2352   | 5    | 1275             | 1055             | 580              |             |               | MTN            |      |   |   |
| 2353         | 2352   | 8    |                  |                  |                  | 0.42        | 5.10          |                |      |   |   |
| 2352         | 2351   | 5    | 1055             | 845              | 950              |             |               | MTN            |      |   |   |
| 2352         | 2351   | 8    |                  |                  |                  | 0.42        | 10.54         |                |      |   |   |
| 2351         | 2348   | 3    | 839              | 821              | 390              |             |               |                |      |   |   |
| 2348         | 2348   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 2350         | 2349.5 | 2    | 842              | 841              | 90               | 0.6         | 0.13          |                |      |   |   |
| 2349.5       | 2349   | 5    | 841              | 835              | 235              |             |               | VALLEY         |      |   |   |
| 2349.5       | 2349   | 8    |                  |                  |                  | 0.6         | 2.68          |                |      |   |   |
| 2349         | 2348   | 3    | 829              | 821              | 105              |             |               |                |      |   |   |
| 2348         | 2348   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2348         | 2346   | 3    | 821              | 814              | 205              |             |               |                |      |   |   |
| 2346         | 2346   | 11   |                  |                  |                  |             |               | ADD BANK 2     |      |   |   |
| 2346         | 2346   | 12   |                  |                  |                  |             |               | CLEAR BANK 2   |      |   |   |
| 2346         | 2329   | 3    | 814              | 803              | 100              |             |               |                |      |   |   |
| 2329         | 2329   | 10   |                  |                  |                  |             |               | SAVE TO BANK 2 |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2347         | 2346.5 | 2    | 832              | 830              | 100              | 0.6         | 0.13          |                |      |   |   |
| 2346.5       | 2330   | 5    | 830              | 817              | 420              |             |               | VALLEY         |      |   |   |
| 2346.5       | 2330   | 8    |                  |                  |                  | 0.6         | 2.24          |                |      |   |   |
| 2330         | 2330   | 11   |                  |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 2330         | 2330   | 12   |                  |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 2330         | 2329   | 3    | 812              | 803              | 60               |             |               |                |      |   |   |
| 2329         | 2329   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2327         | 2326.9 | 2    | 827              | 825              | 100              | 0.6         | 0.29          |                |      |   |   |
| 2326.9       | 2325.8 | 5    | 825              | 821              | 200              |             |               | VALLEY         |      |   |   |
| 2326.9       | 2325.8 | 8    |                  |                  |                  | 0.6         | 0.96          |                |      |   |   |
| 2326.8       | 2326.7 | 3    | 821              | 808.5            | 65               |             |               |                |      |   |   |
| 2326.7       | 2326.6 | 5    | 808.5            | 808              | 50               |             |               | VALLEY         |      |   |   |
| 2326.7       | 2326.6 | 8    |                  |                  |                  | 0.3         | 0.14          |                |      |   |   |
| 2326.6       | 2329   | 3    | 803.5            | 803              | 50               |             |               |                |      |   |   |
| 2329         | 2329   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2329         | 2329   | 11   |                  |                  |                  |             |               | ADD BANK 2     |      |   |   |
| 2329         | 2329   | 12   |                  |                  |                  |             |               | CLEAR BANK 2   |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2329         | 3495   | 3    | 803              | 766              |                  |             |               |                |      |   |   |
| 3495         | 3495   | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 2328         | 2326.5 | 2    | 820              | 815              | 85               | 0.9         | 0.12          |                |      |   |   |
| 2326.5       | 2326   | 6    | 815              | 803.9            | 220              | 0.9         | 0.31          |                |      |   |   |
| 2326         | 2323   | 3    | 797.9            | 787.1            | 320              |             |               |                |      |   |   |
| 2323         | 2323   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2325         | 2324   | 2    | 803.9            | 801.5            | 75               | 0.9         | 0.10          |                |      |   |   |
| 2324         | 2323   | 6    | 801.5            | 793.1            | 320              | 0.9         | 0.45          | 2 SIDES        |      |   |   |
| 2323         | 2323   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2323         | 2321   | 3    | 787.1            | 773              | 405              |             |               |                |      |   |   |
| 2321         | 2321   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2323         | 2322   | 2    | 793.1            | 791              | 75               | 0.9         | 0.10          |                |      |   |   |
| 2322         | 2321   | 6    | 791              | 783              | 325              | 0.9         | 0.46          | 2 SIDES        |      |   |   |
| 2321         | 2321   | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 2321         | 2319   | 3    | 773              | 766              | 535              |             |               |                |      |   |   |
| 2319         | 2319   | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* NO DETENTION \*
  - \* SUB-BASIN 34.9 \*
- \*\*\*\*\*

FILE NAME: P-34-9.DAT  
TIME/DATE OF STUDY: 13:37 12/08/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2340.00 TO NODE 2339.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 867.70

DOWNSTREAM ELEVATION(FEET) = 865.00

ELEVATION DIFFERENCE(FEET) = 2.70

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.034

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.91

TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 2339.00 TO NODE 2338.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 865.00 DOWNSTREAM ELEVATION(FEET) = 853.00

STREET LENGTH(FEET) = 700.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.89

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.40

HALFSTREET FLOOD WIDTH(FEET) = 13.63

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.48

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.39

STREET FLOW TRAVEL TIME(MIN.) = 3.35 Tc(MIN.) = 5.38

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.793

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000



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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 11.87  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 12.74

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.39  
FLOW VELOCITY(FEET/SEC.) = 4.05 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.92  
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2338.00 = 775.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2338.00 TO NODE 2335.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 847.00 DOWNSTREAM(FEET) = 834.00  
FLOW LENGTH(FEET) = 410.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.92  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.74  
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 6.01  
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2335.00 = 1185.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2335.00 TO NODE 2335.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.01  
RAINFALL INTENSITY(INCH/HR) = 8.19  
TOTAL STREAM AREA(ACRES) = 1.61  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.74

\*\*\*\*\*

FLOW PROCESS FROM NODE 2337.00 TO NODE 2336.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 854.70  
DOWNSTREAM ELEVATION(FEET) = 851.90

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ELEVATION DIFFERENCE(FEET) = 2.80  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.231  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.91  
 TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 2336.00 TO NODE 2335.00 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 851.90 DOWNSTREAM ELEVATION(FEET) = 840.00  
 STREET LENGTH(FEET) = 370.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.06  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.34  
 HALFSTREET FLOOD WIDTH(FEET) = 10.49  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.16  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.40  
 STREET FLOW TRAVEL TIME(MIN.) = 1.48 Tc(MIN.) = 3.71  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 8.30  
 TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 9.21

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.50  
 FLOW VELOCITY(FEET/SEC.) = 4.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.88  
 LONGEST FLOWPATH FROM NODE 2337.00 TO NODE 2335.00 = 455.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2335.00 TO NODE 2335.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.71
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 1.11
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.21

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 20.92 Tc(MIN.) = 6.01
TOTAL AREA(ACRES) = 2.7
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2335.00 = 1185.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2335.00 TO NODE 2332.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 834.00 DOWNSTREAM(FEET) = 818.20
FLOW LENGTH(FEET) = 355.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.56
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.92
PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 6.44
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2332.00 = 1540.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2332.00 TO NODE 2332.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.44
RAINFALL INTENSITY(INCH/HR) = 7.83
TOTAL STREAM AREA(ACRES) = 2.72
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 2334.00 TO NODE 2333.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00
UPSTREAM ELEVATION(FEET) = 841.70
DOWNSTREAM ELEVATION(FEET) = 837.70
ELEVATION DIFFERENCE(FEET) = 4.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.981
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.83
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 2333.00 TO NODE 2332.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 837.70 DOWNSTREAM ELEVATION(FEET) = 820.00
STREET LENGTH(FEET) = 315.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.53

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.26

HALFSTREET FLOOD WIDTH(FEET) = 6.73

AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.43

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.16

STREET FLOW TRAVEL TIME(MIN.) = 1.18 Tc(MIN.) = 3.16

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 3.40

TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 4.23

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.58

FLOW VELOCITY(FEET/SEC.) = 4.96 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.48

LONGEST FLOWPATH FROM NODE 2334.00 TO NODE 2332.00 = 400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2332.00 TO NODE 2332.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.16
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.51
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.23

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 24.52 Tc(MIN.) = 6.44  
TOTAL AREA(ACRES) = 3.2  
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2332.00 = 1540.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2332.00 TO NODE 2331.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 818.20 DOWNSTREAM(FEET) = 817.00  
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.27  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 24.52  
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 6.69  
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2331.00 = 1660.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2331.00 TO NODE 2330.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 817.00 DOWNSTREAM(FEET) = 816.70  
CHANNEL LENGTH THRU SUBAREA(FEET) = 25.00 CHANNEL SLOPE = 0.0120  
CHANNEL FLOW THRU SUBAREA(CFS) = 24.52  
FLOW VELOCITY(FEET/SEC) = 3.47 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 6.81  
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2330.00 = 1685.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2330.00 TO NODE 2330.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2358.00 TO NODE 2357.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1180.00  
DOWNSTREAM ELEVATION(FEET) = 1165.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.390  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.785  
SUBAREA RUNOFF(CFS) = 0.52  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 2357.00 TO NODE 2356.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1165.00 DOWNSTREAM(FEET) = 1055.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 490.00 CHANNEL SLOPE = 0.2245  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1715 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.52  
FLOW VELOCITY(FEET/SEC) = 2.32 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.52 Tc(MIN.) = 8.91  
LONGEST FLOWPATH FROM NODE 2358.00 TO NODE 2356.00 = 580.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2357.00 TO NODE 2356.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.352  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 6.15 SUBAREA RUNOFF(CFS) = 16.41  
TOTAL AREA(ACRES) = 6.3 TOTAL RUNOFF(CFS) = 16.78  
TC(MIN.) = 8.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 2356.00 TO NODE 2355.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1055.00 DOWNSTREAM(FEET) = 850.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 935.00 CHANNEL SLOPE = 0.2193

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SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1696 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 16.78  
FLOW VELOCITY(FEET/SEC) = 5.90 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.64 Tc(MIN.) = 11.55  
LONGEST FLOWPATH FROM NODE 2358.00 TO NODE 2355.00 = 1515.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2356.00 TO NODE 2355.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.373  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 13.59 SUBAREA RUNOFF(CFS) = 30.67  
TOTAL AREA(ACRES) = 19.9 TOTAL RUNOFF(CFS) = 44.86  
TC(MIN.) = 11.55

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2355.00 TO NODE 2346.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 824.00 DOWNSTREAM(FEET) = 814.00  
FLOW LENGTH(FEET) = 185.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.97  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 44.86  
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 11.72  
LONGEST FLOWPATH FROM NODE 2358.00 TO NODE 2346.00 = 1700.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2346.00 TO NODE 2346.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2354.00 TO NODE 2353.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):



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USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 1300.00  
 DOWNSTREAM ELEVATION(FEET) = 1275.00  
 ELEVATION DIFFERENCE(FEET) = 25.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.682  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.492  
 SUBAREA RUNOFF(CFS) = 0.32  
 TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.32

\*\*\*\*\*

FLOW PROCESS FROM NODE 2353.00 TO NODE 2352.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1275.00 DOWNSTREAM(FEET) = 1055.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 580.00 CHANNEL SLOPE = 0.3793  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .2104 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
 CHANNEL FLOW THRU SUBAREA(CFS) = 0.32  
 FLOW VELOCITY(FEET/SEC) = 2.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 3.76 Tc(MIN.) = 9.45  
 LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2352.00 = 680.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2353.00 TO NODE 2352.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.118  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
 SUBAREA AREA(ACRES) = 5.10 SUBAREA RUNOFF(CFS) = 13.11  
 TOTAL AREA(ACRES) = 5.2 TOTAL RUNOFF(CFS) = 13.34  
 TC(MIN.) = 9.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 2352.00 TO NODE 2351.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

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ELEVATION DATA: UPSTREAM(FEET) = 1055.00 DOWNSTREAM(FEET) = 845.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 950.00 CHANNEL SLOPE = 0.2211  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1704 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 13.34  
FLOW VELOCITY(FEET/SEC) = 5.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.89 Tc(MIN.) = 12.34  
LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2351.00 = 1630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2352.00 TO NODE 2351.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.150  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200  
SUBAREA AREA(ACRES) = 10.54 SUBAREA RUNOFF(CFS) = 22.80  
TOTAL AREA(ACRES) = 15.7 TOTAL RUNOFF(CFS) = 34.03  
TC(MIN.) = 12.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 2351.00 TO NODE 2348.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 839.00 DOWNSTREAM(FEET) = 821.00  
FLOW LENGTH(FEET) = 390.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.05  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 34.03  
PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 12.74  
LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2348.00 = 2020.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2348.00 TO NODE 2348.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.74  
RAINFALL INTENSITY(INCH/HR) = 5.04  
TOTAL STREAM AREA(ACRES) = 15.73

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PEAK FLOW RATE(CFS) AT CONFLUENCE = 34.03

\*\*\*\*\*

FLOW PROCESS FROM NODE 2350.00 TO NODE 2349.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00

UPSTREAM ELEVATION(FEET) = 842.00

DOWNSTREAM ELEVATION(FEET) = 841.00

ELEVATION DIFFERENCE(FEET) = 1.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.095

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 66.67

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.358

SUBAREA RUNOFF(CFS) = 0.57

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2349.50 TO NODE 2349.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 841.00 DOWNSTREAM(FEET) = 835.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 235.00 CHANNEL SLOPE = 0.0255

NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION

CHANNEL FLOW THRU SUBAREA(CFS) = 0.57

FLOW VELOCITY(FEET/SEC) = 2.40 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 1.63 Tc(MIN.) = 8.73

LONGEST FLOWPATH FROM NODE 2350.00 TO NODE 2349.00 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2349.50 TO NODE 2349.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.438

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000

SUBAREA AREA(ACRES) = 2.68 SUBAREA RUNOFF(CFS) = 10.35

TOTAL AREA(ACRES) = 2.8 TOTAL RUNOFF(CFS) = 10.85  
TC(MIN.) = 8.73

\*\*\*\*\*

FLOW PROCESS FROM NODE 2349.00 TO NODE 2348.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 829.00 DOWNSTREAM(FEET) = 821.00  
FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.65  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.85  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 8.85  
LONGEST FLOWPATH FROM NODE 2350.00 TO NODE 2348.00 = 430.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2348.00 TO NODE 2348.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.85  
RAINFALL INTENSITY(INCH/HR) = 6.38  
TOTAL STREAM AREA(ACRES) = 2.81  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.85

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 34.03        | 12.74     | 5.044                 | 15.73       |
| 2             | 10.85        | 8.85      | 6.381                 | 2.81        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 34.48        | 8.85      | 6.381                 |
| 2             | 42.60        | 12.74     | 5.044                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

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PEAK FLOW RATE(CFS) = 42.60 Tc(MIN.) = 12.74  
TOTAL AREA(ACRES) = 18.5  
LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2348.00 = 2020.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2348.00 TO NODE 2346.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 821.00 DOWNSTREAM(FEET) = 814.00  
FLOW LENGTH(FEET) = 205.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.12  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 42.60  
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 12.97  
LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2346.00 = 2225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2346.00 TO NODE 2346.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 42.60        | 12.97     | 4.987                 | 18.54       |

LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2346.00 = 2225.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 44.86        | 11.72     | 5.322                 | 19.88       |

LONGEST FLOWPATH FROM NODE 2358.00 TO NODE 2346.00 = 1700.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 83.38        | 11.72     | 5.322                 |
| 2             | 84.64        | 12.97     | 4.987                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 84.64 Tc(MIN.) = 12.97  
TOTAL AREA(ACRES) = 38.4

\*\*\*\*\*

FLOW PROCESS FROM NODE 2346.00 TO NODE 2346.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2346.00 TO NODE 2329.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 814.00 DOWNSTREAM(FEET) = 803.00
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 27.60
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 84.64
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 13.03
LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2329.00 = 2325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2329.00 TO NODE 2329.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2347.00 TO NODE 2346.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 832.00

DOWNSTREAM ELEVATION(FEET) = 830.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.389

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 80.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.873

SUBAREA RUNOFF(CFS) = 0.61

TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 2346.50 TO NODE 2330.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 830.00 DOWNSTREAM(FEET) = 817.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 420.00 CHANNEL SLOPE = 0.0310
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.61
FLOW VELOCITY(FEET/SEC) = 2.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.65 Tc(MIN.) = 9.04
LONGEST FLOWPATH FROM NODE 2347.00 TO NODE 2330.00 = 520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2346.50 TO NODE 2330.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.293
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 2.24 SUBAREA RUNOFF(CFS) = 8.46
TOTAL AREA(ACRES) = 2.4 TOTAL RUNOFF(CFS) = 8.95
TC(MIN.) = 9.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 2330.00 TO NODE 2330.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 8.95 9.04 6.293 2.37
LONGEST FLOWPATH FROM NODE 2347.00 TO NODE 2330.00 = 520.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 24.52 6.81 7.558 3.23
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2330.00 = 1685.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)

|   |       |      |       |
|---|-------|------|-------|
| 1 | 31.25 | 6.81 | 7.558 |
| 2 | 29.36 | 9.04 | 6.293 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 31.25 Tc(MIN.) = 6.81  
TOTAL AREA(ACRES) = 5.6

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2330.00 TO NODE 2330.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2330.00 TO NODE 2329.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 812.00 DOWNSTREAM(FEET) = 803.00  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.32  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 31.25  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 6.85  
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2329.00 = 1745.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2329.00 TO NODE 2329.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.85  
RAINFALL INTENSITY(INCH/HR) = 7.53  
TOTAL STREAM AREA(ACRES) = 5.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 31.25

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2327.00 TO NODE 2326.90 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6000  
S.C.S. CURVE NUMBER (AMC II) = 0



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INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 827.00

DOWNSTREAM ELEVATION(FEET) = 825.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.389

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 80.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.873

SUBAREA RUNOFF(CFS) = 1.37

TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 1.37

\*\*\*\*\*

FLOW PROCESS FROM NODE 2326.90 TO NODE 2326.80 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 825.00 DOWNSTREAM(FEET) = 821.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 200.00 CHANNEL SLOPE = 0.0200

CHANNEL FLOW THRU SUBAREA(CFS) = 1.37

FLOW VELOCITY(FEET/SEC) = 2.25 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 1.48 Tc(MIN.) = 7.87

LONGEST FLOWPATH FROM NODE 2327.00 TO NODE 2326.80 = 300.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2326.90 TO NODE 2326.80 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.883

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000

SUBAREA AREA(ACRES) = 0.96 SUBAREA RUNOFF(CFS) = 3.96

TOTAL AREA(ACRES) = 1.2 TOTAL RUNOFF(CFS) = 5.16

TC(MIN.) = 7.87

\*\*\*\*\*

FLOW PROCESS FROM NODE 2326.80 TO NODE 2326.70 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 821.00 DOWNSTREAM(FEET) = 808.50

FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013

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ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.60  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.16  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 7.93  
LONGEST FLOWPATH FROM NODE 2327.00 TO NODE 2326.70 = 365.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2326.70 TO NODE 2326.60 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|  |        |  |              |
|--|--------|--|--------------|
| ELEVATION DATA: UPSTREAM(FEET) =                     | 808.50 | DOWNSTREAM(FEET) =                     | 808.00       |
| CHANNEL LENGTH THRU SUBAREA(FEET) =                  | 50.00  | CHANNEL SLOPE =                        | 0.0100       |
| CHANNEL FLOW THRU SUBAREA(CFS) =                     | 5.16   |  |              |
| FLOW VELOCITY(FEET/SEC) =                            | 2.13   | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |              |
| TRAVEL TIME(MIN.) =                                  | 0.39   | Tc(MIN.) =                             | 8.33         |
| LONGEST FLOWPATH FROM NODE 2327.00 TO NODE 2326.60 = |        |  | 415.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2326.70 TO NODE 2326.60 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |        |                       |      |
|--|--------|-----------------------|------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 6.637  |                       |      |
| *USER SPECIFIED(SUBAREA):                |        |                       |      |
| USER-SPECIFIED RUNOFF COEFFICIENT =      | .3000  |                       |      |
| S.C.S. CURVE NUMBER (AMC II) =           | 0      |                       |      |
| AREA-AVERAGE RUNOFF COEFFICIENT =        | 0.5698 |                       |      |
| SUBAREA AREA(ACRES) =                    | 0.14   | SUBAREA RUNOFF(CFS) = | 0.28 |
| TOTAL AREA(ACRES) =                      | 1.4    | TOTAL RUNOFF(CFS) =   | 5.26 |
| TC(MIN.) =                               | 8.33   |                       |      |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2326.60 TO NODE 2329.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |            |                    |        |
|--|------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =           | 803.50     | DOWNSTREAM(FEET) = | 803.00 |
| FLOW LENGTH(FEET) =                        | 50.00      | MANNING'S N =      | 0.013  |
| ESTIMATED PIPE DIAMETER(INCH) INCREASED TO | 18.000     |                    |        |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS         | 9.3 INCHES |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =            | 5.71       |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =            | 18.00      | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                           | 5.26       |                    |        |

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PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 8.47  
LONGEST FLOWPATH FROM NODE 2327.00 TO NODE 2329.00 = 465.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2329.00 TO NODE 2329.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.47  
RAINFALL INTENSITY(INCH/HR) = 6.56  
TOTAL STREAM AREA(ACRES) = 1.39  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.26

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 31.25        | 6.85      | 7.529                 | 5.60        |
| 2             | 5.26         | 8.47      | 6.563                 | 1.39        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 35.50        | 6.85      | 7.529                 |
| 2             | 32.50        | 8.47      | 6.563                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 35.50 Tc(MIN.) = 6.85  
TOTAL AREA(ACRES) = 7.0  
LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2329.00 = 1745.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2329.00 TO NODE 2329.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 35.50        | 6.85      | 7.529                 | 6.99        |

LONGEST FLOWPATH FROM NODE 2340.00 TO NODE 2329.00 = 1745.00 FEET.

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\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 84.64        | 13.03     | 4.972                 | 38.42       |

LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 2329.00 = 2325.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 79.99        | 6.85      | 7.529                 |
| 2             | 108.09       | 13.03     | 4.972                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 108.09 Tc(MIN.) = 13.03  
TOTAL AREA(ACRES) = 45.4

\*\*\*\*\*

FLOW PROCESS FROM NODE 2329.00 TO NODE 2329.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2329.00 TO NODE 3495.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 803.00 DOWNSTREAM(FEET) = 766.00  
FLOW LENGTH(FEET) = 1635.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 29.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.11  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 108.09  
PIPE TRAVEL TIME(MIN.) = 1.69 Tc(MIN.) = 14.72  
LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 3495.00 = 3960.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3495.00 TO NODE 3495.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2328.00 TO NODE 2326.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
 UPSTREAM ELEVATION(FEET) = 820.00  
 DOWNSTREAM ELEVATION(FEET) = 815.00  
 ELEVATION DIFFERENCE(FEET) = 5.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.839  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.00  
 TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 1.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 2326.50 TO NODE 2326.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 815.00 DOWNSTREAM ELEVATION(FEET) = 803.90  
 STREET LENGTH(FEET) = 220.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.28

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.21  
 HALFSTREET FLOOD WIDTH(FEET) = 4.41  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.66  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.78  
 STREET FLOW TRAVEL TIME(MIN.) = 1.00 Tc(MIN.) = 2.84  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 0.31 SUBAREA RUNOFF(CFS) = 2.57  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.57

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END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 5.77  
FLOW VELOCITY(FEET/SEC.) = 3.95 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.96  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2326.00 = 305.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2326.00 TO NODE 2323.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 797.90 DOWNSTREAM(FEET) = 787.10  
FLOW LENGTH(FEET) = 320.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.03  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.57  
PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 3.51  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2323.00 = 625.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2323.00 TO NODE 2323.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.51  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.43  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2325.00 TO NODE 2324.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 803.90  
DOWNSTREAM ELEVATION(FEET) = 801.50  
ELEVATION DIFFERENCE(FEET) = 2.40  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.116  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 2324.00 TO NODE 2323.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 801.50 DOWNSTREAM ELEVATION(FEET) = 793.10  
STREET LENGTH(FEET) = 320.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.70  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.91  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.89  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.71  
STREET FLOW TRAVEL TIME(MIN.) = 1.85 Tc(MIN.) = 3.96  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.45 SUBAREA RUNOFF(CFS) = 3.73  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 4.56

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.69  
FLOW VELOCITY(FEET/SEC.) = 3.22 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.90  
LONGEST FLOWPATH FROM NODE 2325.00 TO NODE 2323.00 = 395.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2323.00 TO NODE 2323.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.96
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.55
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.56
    
```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.57         | 3.51      | 9.222                 | 0.43        |
| 2             | 4.56         | 3.96      | 9.222                 | 0.55        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 7.61         | 3.51      | 9.222                 |
| 2             | 8.13         | 3.96      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 8.13 Tc(MIN.) = 3.96
TOTAL AREA(ACRES) = 1.0
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2323.00 = 625.00 FEET.
    
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2323.00 TO NODE 2321.00 IS CODE = 31

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
    
```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 787.10 DOWNSTREAM(FEET) = 773.00
FLOW LENGTH(FEET) = 405.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.17
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.13
PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 4.63
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2321.00 = 1030.00 FEET.
    
```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2321.00 TO NODE 2321.00 IS CODE = 1

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-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
    
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=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.63  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.98  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.13

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2323.00 TO NODE 2322.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 793.10  
DOWNSTREAM ELEVATION(FEET) = 791.00  
ELEVATION DIFFERENCE(FEET) = 2.10  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.212  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2322.00 TO NODE 2321.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 791.00 DOWNSTREAM ELEVATION(FEET) = 783.00  
STREET LENGTH(FEET) = 325.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.74  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25

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HALFSTREET FLOOD WIDTH(FEET) = 6.11  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.78  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.69  
 STREET FLOW TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 4.16  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 0.46 SUBAREA RUNOFF(CFS) = 3.82  
 TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 4.65

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.89  
 FLOW VELOCITY(FEET/SEC.) = 3.14 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.89  
 LONGEST FLOWPATH FROM NODE 2323.00 TO NODE 2321.00 = 400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2321.00 TO NODE 2321.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 4.16  
 RAINFALL INTENSITY(INCH/HR) = 9.22  
 TOTAL STREAM AREA(ACRES) = 0.56  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.65

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.13         | 4.63      | 9.222                 | 0.98        |
| 2             | 4.65         | 4.16      | 9.222                 | 0.56        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.78        | 4.16      | 9.222                 |
| 2             | 12.78        | 4.63      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 12.78 Tc(MIN.) = 4.63

TOTAL AREA(ACRES) = 1.5  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2321.00 = 1030.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2321.00 TO NODE 2319.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 773.00 DOWNSTREAM(FEET) = 766.00  
FLOW LENGTH(FEET) = 535.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.83  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.78  
PIPE TRAVEL TIME(MIN.) = 1.14 Tc(MIN.) = 5.77  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2319.00 = 1565.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2319.00 TO NODE 2319.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.77  
RAINFALL INTENSITY(INCH/HR) = 8.41  
TOTAL STREAM AREA(ACRES) = 1.54  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 2321.00 TO NODE 2320.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 783.00  
DOWNSTREAM ELEVATION(FEET) = 781.20  
ELEVATION DIFFERENCE(FEET) = 1.80  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.329  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.91  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 2320.00 TO NODE 2319.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 781.20 DOWNSTREAM ELEVATION(FEET) = 772.00
STREET LENGTH(FEET) = 440.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.15
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 7.75
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.88
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.81
STREET FLOW TRAVEL TIME(MIN.) = 2.54 Tc(MIN.) = 4.87
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 0.78 SUBAREA RUNOFF(CFS) = 6.47
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 7.39

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.08
FLOW VELOCITY(FEET/SEC.) = 3.26 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.07
LONGEST FLOWPATH FROM NODE 2321.00 TO NODE 2319.00 = 515.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2319.00 TO NODE 2319.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

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TIME OF CONCENTRATION(MIN.) = 4.87  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.89  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.39

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.78        | 5.77      | 8.412                 | 1.54        |
| 2             | 7.39         | 4.87      | 9.222                 | 0.89        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 19.04        | 4.87      | 9.222                 |
| 2             | 19.52        | 5.77      | 8.412                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.52 Tc(MIN.) = 5.77  
TOTAL AREA(ACRES) = 2.4  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2319.00 = 1565.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2319.00 TO NODE 2318.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 766.00 DOWNSTREAM(FEET) = 760.20  
FLOW LENGTH(FEET) = 90.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.80  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.52  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.86  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2318.00 = 1655.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2318.00 TO NODE 2317.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 760.20 DOWNSTREAM(FEET) = 760.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 20.00 CHANNEL SLOPE = 0.0100

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CHANNEL FLOW THRU SUBAREA(CFS) = 19.52  
FLOW VELOCITY(FEET/SEC) = 2.98 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 5.97  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 2317.00 = 1675.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2318.00 TO NODE 2317.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.222  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7876  
SUBAREA AREA(ACRES) = 0.56 SUBAREA RUNOFF(CFS) = 1.38  
TOTAL AREA(ACRES) = 3.0 TOTAL RUNOFF(CFS) = 19.52  
TC(MIN.) = 5.97  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 2317.00 TO NODE 3500.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 760.00 DOWNSTREAM(FEET) = 759.40  
FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.88  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.52  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 6.18  
LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 3500.00 = 1760.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3500.00 TO NODE 3500.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 3575.00 TO NODE 3572.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 812.20  
 DOWNSTREAM ELEVATION(FEET) = 811.30  
 ELEVATION DIFFERENCE(FEET) = 0.90  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.831  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
 THE MAXIMUM OVERLAND FLOW LENGTH = 66.88  
 (Reference: Table 3-1B of Hydrology Manual)  
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.75  
 TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3572.00 TO NODE 3571.00 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 811.30 DOWNSTREAM ELEVATION(FEET) = 806.30  
 STREET LENGTH(FEET) = 300.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.28  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.30  
 HALFSTREET FLOOD WIDTH(FEET) = 8.58  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.67  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.80  
 STREET FLOW TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 4.70  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 0.37 SUBAREA RUNOFF(CFS) = 3.07

TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 3.82

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.69
FLOW VELOCITY(FEET/SEC.) = 3.03 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.03
LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 3571.00 = 380.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3571.00 TO NODE 3569.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 805.00 DOWNSTREAM(FEET) = 804.20
CHANNEL LENGTH THRU SUBAREA(FEET) = 80.00 CHANNEL SLOPE = 0.0100
CHANNEL FLOW THRU SUBAREA(CFS) = 3.82
FLOW VELOCITY(FEET/SEC) = 1.98 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 5.37
LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 3569.00 = 460.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3571.00 TO NODE 3569.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.803
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7929
SUBAREA AREA(ACRES) = 0.10 SUBAREA RUNOFF(CFS) = 0.26
TOTAL AREA(ACRES) = 0.6 TOTAL RUNOFF(CFS) = 3.91
TC(MIN.) = 5.37

\*\*\*\*\*

FLOW PROCESS FROM NODE 3569.00 TO NODE 3565.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 798.20 DOWNSTREAM(FEET) = 797.30
FLOW LENGTH(FEET) = 90.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.30
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.91
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 5.66



LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 3565.50 = 550.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3565.50 TO NODE 3565.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.66
RAINFALL INTENSITY(INCH/HR) = 8.52
TOTAL STREAM AREA(ACRES) = 0.56
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 2412.00 TO NODE 2411.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4200
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 985.00
DOWNSTREAM ELEVATION(FEET) = 955.00
ELEVATION DIFFERENCE(FEET) = 30.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.390
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.785
SUBAREA RUNOFF(CFS) = 0.30
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2411.00 TO NODE 2410.80 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 955.00 DOWNSTREAM(FEET) = 805.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1220.00 CHANNEL SLOPE = 0.1230
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1170 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.30
FLOW VELOCITY(FEET/SEC) = 1.92 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 10.62 Tc(MIN.) = 16.01
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 2410.80 = 1310.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2411.00 TO NODE 2410.80 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.354
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4200
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4200
SUBAREA AREA(ACRES) = 9.72 SUBAREA RUNOFF(CFS) = 17.77
TOTAL AREA(ACRES) = 9.8 TOTAL RUNOFF(CFS) = 17.92
TC(MIN.) = 16.01

\*\*\*\*\*

FLOW PROCESS FROM NODE 2410.80 TO NODE 3565.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 805.00 DOWNSTREAM(FEET) = 797.30
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.64
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 17.92
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 16.05
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3565.50 = 1360.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3565.50 TO NODE 3565.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 16.05
RAINFALL INTENSITY(INCH/HR) = 4.35
TOTAL STREAM AREA(ACRES) = 9.80
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.92

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 10.23        | 5.66      | 8.516                 |
| 2             | 19.92        | 16.05     | 4.347                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.92 Tc(MIN.) = 16.05  
TOTAL AREA(ACRES) = 10.4  
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3565.50 = 1360.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3565.50 TO NODE 3565.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 797.30 DOWNSTREAM(FEET) = 787.30  
FLOW LENGTH(FEET) = 240.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.92  
PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 16.35  
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3565.00 = 1600.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3565.00 TO NODE 3565.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.35  
RAINFALL INTENSITY(INCH/HR) = 4.29  
TOTAL STREAM AREA(ACRES) = 10.36  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.92

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3568.00 TO NODE 3567.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 806.40  
 DOWNSTREAM ELEVATION(FEET) = 803.80  
 ELEVATION DIFFERENCE(FEET) = 2.60  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.174  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.75  
 TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 3567.00 TO NODE 3566.50 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 803.80 DOWNSTREAM ELEVATION(FEET) = 794.00  
 STREET LENGTH(FEET) = 260.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.99  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.26  
 HALFSTREET FLOOD WIDTH(FEET) = 6.59  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.60  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.93  
 STREET FLOW TRAVEL TIME(MIN.) = 1.20 Tc(MIN.) = 3.38  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 2.49  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.24

END OF SUBAREA STREET FLOW HYDRAULICS:

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DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.37  
FLOW VELOCITY(FEET/SEC.) = 3.95 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.16  
LONGEST FLOWPATH FROM NODE 3568.00 TO NODE 3566.50 = 340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3566.50 TO NODE 3566.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 794.00 DOWNSTREAM(FEET) = 793.80  
CHANNEL LENGTH THRU SUBAREA(FEET) = 15.00 CHANNEL SLOPE = 0.0133  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.24  
FLOW VELOCITY(FEET/SEC) = 2.21 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 3.49  
LONGEST FLOWPATH FROM NODE 3568.00 TO NODE 3566.00 = 355.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3566.50 TO NODE 3566.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8087  
SUBAREA AREA(ACRES) = 0.07 SUBAREA RUNOFF(CFS) = 0.19  
TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 3.43  
TC(MIN.) = 3.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 3566.00 TO NODE 3565.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 787.80 DOWNSTREAM(FEET) = 787.30  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.43  
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 3.65  
LONGEST FLOWPATH FROM NODE 3568.00 TO NODE 3565.00 = 405.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3565.00 TO NODE 3565.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.65
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.46
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.43

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 21.51 Tc(MIN.) = 16.35
TOTAL AREA(ACRES) = 10.8
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3565.00 = 1600.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3565.00 TO NODE 3500.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 787.30 DOWNSTREAM(FEET) = 759.40
FLOW LENGTH(FEET) = 620.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.23
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 21.51
PIPE TRAVEL TIME(MIN.) = 0.73 Tc(MIN.) = 17.08
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3500.00 = 2220.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3500.00 TO NODE 3500.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 21.51        | 17.08     | 4.176                 | 10.82       |

LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3500.00 = 2220.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 19.52        | 6.18      | 8.045                 | 2.99        |

LONGEST FLOWPATH FROM NODE 2328.00 TO NODE 3500.00 = 1760.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 27.30        | 6.18      | 8.045                 |
| 2             | 31.64        | 17.08     | 4.176                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 31.64 Tc(MIN.) = 17.08  
TOTAL AREA(ACRES) = 13.8

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3500.00 TO NODE 3495.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 759.40 DOWNSTREAM(FEET) = 758.50  
FLOW LENGTH(FEET) = 84.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.09  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 31.64  
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 17.23  
LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3495.00 = 2304.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3495.00 TO NODE 3495.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 31.64        | 17.23     | 4.152                 | 13.81       |

LONGEST FLOWPATH FROM NODE 2412.00 TO NODE 3495.00 = 2304.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 108.09       | 14.72     | 4.596                 | 45.41       |

LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 3495.00 = 3960.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 135.12       | 14.72     | 4.596                 |
| 2             | 129.29       | 17.23     | 4.152                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 135.12 Tc(MIN.) = 14.72  
TOTAL AREA(ACRES) = 59.2

\*\*\*\*\*

FLOW PROCESS FROM NODE 3495.00 TO NODE 34.90 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 758.50 DOWNSTREAM(FEET) = 756.20  
FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 51.0 INCH PIPE IS 36.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.54  
ESTIMATED PIPE DIAMETER(INCH) = 51.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 135.12  
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 15.03  
LONGEST FLOWPATH FROM NODE 2354.00 TO NODE 34.90 = 4195.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 59.2 TC(MIN.) = 15.03  
PEAK FLOW RATE(CFS) = 135.12

END OF RATIONAL METHOD ANALYSIS







\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 35.0 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-35-0.DAT  
TIME/DATE OF STUDY: 13:12 11/22/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3515.00 TO NODE 3514.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 731.00

DOWNSTREAM ELEVATION(FEET) = 728.40

ELEVATION DIFFERENCE(FEET) = 2.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.174

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.75

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 3514.00 TO NODE 3513.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 728.40 DOWNSTREAM ELEVATION(FEET) = 725.60

STREET LENGTH(FEET) = 405.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.52

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.34

HALFSTREET FLOOD WIDTH(FEET) = 10.83

AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.95

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.67

STREET FLOW TRAVEL TIME(MIN.) = 3.46 Tc(MIN.) = 5.63

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.539

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.46 SUBAREA RUNOFF(CFS) = 3.54  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 4.23

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.43  
FLOW VELOCITY(FEET/SEC.) = 2.20 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.87  
LONGEST FLOWPATH FROM NODE 3515.00 TO NODE 3513.00 = 485.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3513.00 TO NODE 35.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 720.70 DOWNSTREAM(FEET) = 720.00  
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.41  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.23  
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 5.85  
LONGEST FLOWPATH FROM NODE 3515.00 TO NODE 35.00 = 555.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 0.6 TC(MIN.) = 5.85  
PEAK FLOW RATE(CFS) = 4.23

=====

END OF RATIONAL METHOD ANALYSIS

↑



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
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Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 35.1 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-35-1.DAT  
TIME/DATE OF STUDY: 11:57 11/22/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3524.00 TO NODE 3523.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 740.00

DOWNSTREAM ELEVATION(FEET) = 737.40

ELEVATION DIFFERENCE(FEET) = 2.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.470

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 89.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.58

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 3523.00 TO NODE 3522.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 737.40 DOWNSTREAM ELEVATION(FEET) = 729.40

STREET LENGTH(FEET) = 515.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.79

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.32

HALFSTREET FLOOD WIDTH(FEET) = 9.53

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.71

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86

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STREET FLOW TRAVEL TIME(MIN.) = 3.16 Tc(MIN.) = 5.63  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.538

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.57 SUBAREA RUNOFF(CFS) = 4.38  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 4.92

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.06  
FLOW VELOCITY(FEET/SEC.) = 3.13 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.15  
LONGEST FLOWPATH FROM NODE 3524.00 TO NODE 3522.00 = 615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3522.00 TO NODE 3521.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 728.50 DOWNSTREAM(FEET) = 728.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 50.00 CHANNEL SLOPE = 0.0100  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.92  
FLOW VELOCITY(FEET/SEC) = 2.10 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 6.03  
LONGEST FLOWPATH FROM NODE 3524.00 TO NODE 3521.00 = 665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3522.00 TO NODE 3521.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.172  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8222  
SUBAREA AREA(ACRES) = 0.08 SUBAREA RUNOFF(CFS) = 0.13  
TOTAL AREA(ACRES) = 0.7 TOTAL RUNOFF(CFS) = 4.92  
TC(MIN.) = 6.03  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 3521.00 TO NODE 3517.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====



P-35-1.TXT

ELEVATION DATA: UPSTREAM(FEET) = 726.20 DOWNSTREAM(FEET) = 725.70  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.62  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.92  
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 6.18  
LONGEST FLOWPATH FROM NODE 3524.00 TO NODE 3517.00 = 715.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3517.00 TO NODE 3517.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.18  
RAINFALL INTENSITY(INCH/HR) = 8.04  
TOTAL STREAM AREA(ACRES) = 0.72  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 3520.00 TO NODE 3519.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00  
UPSTREAM ELEVATION(FEET) = 736.00  
DOWNSTREAM ELEVATION(FEET) = 733.50  
ELEVATION DIFFERENCE(FEET) = 2.50  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.364  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.58  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 3519.00 TO NODE 3518.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 733.50 DOWNSTREAM ELEVATION(FEET) = 729.40  
STREET LENGTH(FEET) = 260.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.78

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.28

HALFSTREET FLOOD WIDTH(FEET) = 7.75

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.48

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.70

STREET FLOW TRAVEL TIME(MIN.) = 1.75 Tc(MIN.) = 3.11

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.29 SUBAREA RUNOFF(CFS) = 2.41

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 2.99

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.81

FLOW VELOCITY(FEET/SEC.) = 2.77 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.89

LONGEST FLOWPATH FROM NODE 3520.00 TO NODE 3518.00 = 305.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3518.00 TO NODE 3517.00 IS CODE = 52

-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 728.00 DOWNSTREAM(FEET) = 727.50

CHANNEL LENGTH THRU SUBAREA(FEET) = 50.00 CHANNEL SLOPE = 0.0100

CHANNEL FLOW THRU SUBAREA(CFS) = 2.99

FLOW VELOCITY(FEET/SEC) = 1.88 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 3.56

LONGEST FLOWPATH FROM NODE 3520.00 TO NODE 3517.00 = 355.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3517.00 TO NODE 3517.00 IS CODE = 1

-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.56
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.36
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.99

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.52 Tc(MIN.) = 6.18
TOTAL AREA(ACRES) = 1.1
LONGEST FLOWPATH FROM NODE 3524.00 TO NODE 3517.00 = 715.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3517.00 TO NODE 35.10 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 725.70 DOWNSTREAM(FEET) = 725.00
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.20
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.52
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 6.37
LONGEST FLOWPATH FROM NODE 3524.00 TO NODE 35.10 = 785.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.1 TC(MIN.) = 6.37
PEAK FLOW RATE(CFS) = 7.52

P-35-1.TXT

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END OF RATIONAL METHOD ANALYSIS





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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 35.2 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-35-2.DAT  
TIME/DATE OF STUDY: 11:42 11/22/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3531.00 TO NODE 3530.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00

UPSTREAM ELEVATION(FEET) = 742.30

DOWNSTREAM ELEVATION(FEET) = 739.30

ELEVATION DIFFERENCE(FEET) = 3.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.854

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.50

TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 3530.00 TO NODE 3529.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 739.30 DOWNSTREAM ELEVATION(FEET) = 737.00

STREET LENGTH(FEET) = 140.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.08

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.25

HALFSTREET FLOOD WIDTH(FEET) = 5.98

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.27

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.56

STREET FLOW TRAVEL TIME(MIN.) = 1.03 Tc(MIN.) = 2.88

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 1.16  
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.66

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.41  
FLOW VELOCITY(FEET/SEC.) = 2.49 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.68  
LONGEST FLOWPATH FROM NODE 3531.00 TO NODE 3529.00 = 210.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3529.00 TO NODE 3526.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 733.00 DOWNSTREAM(FEET) = 730.70  
FLOW LENGTH(FEET) = 228.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.19  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.66  
PIPE TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 3.79  
LONGEST FLOWPATH FROM NODE 3531.00 TO NODE 3526.00 = 438.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3526.00 TO NODE 3526.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.79  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.20  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 3528.00 TO NODE 3527.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00



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UPSTREAM ELEVATION(FEET) = 739.70  
DOWNSTREAM ELEVATION(FEET) = 736.70  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.854  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.58  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 3527.00 TO NODE 3526.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 736.70 DOWNSTREAM ELEVATION(FEET) = 733.70  
STREET LENGTH(FEET) = 190.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.37  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.80  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.36  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.62  
STREET FLOW TRAVEL TIME(MIN.) = 1.34 Tc(MIN.) = 3.20  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.19 SUBAREA RUNOFF(CFS) = 1.58  
TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 2.16

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.44  
FLOW VELOCITY(FEET/SEC.) = 2.60 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.77  
LONGEST FLOWPATH FROM NODE 3528.00 TO NODE 3526.00 = 260.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3526.00 TO NODE 3526.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 3.20
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.26
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.16

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 3.82 Tc(MIN.) = 3.79
TOTAL AREA(ACRES) = 0.5
LONGEST FLOWPATH FROM NODE 3531.00 TO NODE 3526.00 = 438.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3526.00 TO NODE 35.20 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 730.70 DOWNSTREAM(FEET) = 730.00
FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.41
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.82
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 3.99

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LONGEST FLOWPATH FROM NODE 3531.00 TO NODE 35.20 = 503.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 0.5 TC(MIN.) = 3.99

PEAK FLOW RATE(CFS) = 3.82

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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6390 Greenwich Drive  
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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 35.3 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-35-3.DAT  
TIME/DATE OF STUDY: 11:33 11/22/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3539.00 TO NODE 3538.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 748.20

DOWNSTREAM ELEVATION(FEET) = 746.30

ELEVATION DIFFERENCE(FEET) = 1.90

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.287

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.58

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 3538.00 TO NODE 3537.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 746.30 DOWNSTREAM ELEVATION(FEET) = 737.80

STREET LENGTH(FEET) = 460.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.11

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.32

HALFSTREET FLOOD WIDTH(FEET) = 9.60

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.99

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.95

STREET FLOW TRAVEL TIME(MIN.) = 2.56 Tc(MIN.) = 4.85

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.61 SUBAREA RUNOFF(CFS) = 5.06  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 5.64

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.33  
FLOW VELOCITY(FEET/SEC.) = 3.44 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.28  
LONGEST FLOWPATH FROM NODE 3539.00 TO NODE 3537.00 = 535.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3538.00 TO NODE 3537.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.9000  
SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 1.00  
TOTAL AREA(ACRES) = 0.8 TOTAL RUNOFF(CFS) = 6.64  
TC(MIN.) = 4.85

\*\*\*\*\*

FLOW PROCESS FROM NODE 3537.00 TO NODE 3533.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 741.50 DOWNSTREAM(FEET) = 735.60  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.04  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.64  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 4.92  
LONGEST FLOWPATH FROM NODE 3539.00 TO NODE 3533.00 = 595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3533.00 TO NODE 3533.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

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CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 4.92  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3535.00 TO NODE 3534.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 743.00

DOWNSTREAM ELEVATION(FEET) = 741.90

ELEVATION DIFFERENCE(FEET) = 1.10

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.721

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 70.62

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.75

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3534.00 TO NODE 3533.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 741.90 DOWNSTREAM ELEVATION(FEET) = 739.70

STREET LENGTH(FEET) = 140.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.33



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STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 6.73  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.33  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.61  
STREET FLOW TRAVEL TIME(MIN.) = 1.00 Tc(MIN.) = 3.72

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 1.16  
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.91

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.03  
FLOW VELOCITY(FEET/SEC.) = 2.50 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.72  
LONGEST FLOWPATH FROM NODE 3535.00 TO NODE 3533.00 = 220.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3533.00 TO NODE 3533.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.72  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.23  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.91

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.64         | 4.92      | 9.222                 | 0.80        |
| 2             | 1.91         | 3.72      | 9.222                 | 0.23        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 6.93         | 3.72      | 9.222                 |
| 2             | 8.55         | 4.92      | 9.222                 |

P-35-3.TXT

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.55 Tc(MIN.) = 4.92

TOTAL AREA(ACRES) = 1.0

LONGEST FLOWPATH FROM NODE 3539.00 TO NODE 3533.00 = 595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3533.00 TO NODE 35.30 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 735.60 DOWNSTREAM(FEET) = 735.00

FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 6.34

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 8.55

PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.08

LONGEST FLOWPATH FROM NODE 3539.00 TO NODE 35.30 = 655.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.0 TC(MIN.) = 5.08

PEAK FLOW RATE(CFS) = 8.55

END OF RATIONAL METHOD ANALYSIS





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 35.4 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-35-4.DAT  
TIME/DATE OF STUDY: 11:24 11/22/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3547.00 TO NODE 3546.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 754.40

DOWNSTREAM ELEVATION(FEET) = 751.00

ELEVATION DIFFERENCE(FEET) = 3.40

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.884

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.75

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 3546.00 TO NODE 3545.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 751.00 DOWNSTREAM ELEVATION(FEET) = 747.20

STREET LENGTH(FEET) = 260.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.99

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.29

HALFSTREET FLOOD WIDTH(FEET) = 8.30

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.47

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.72

STREET FLOW TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 3.64

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 2.49  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.24

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.28  
FLOW VELOCITY(FEET/SEC.) = 2.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.91  
LONGEST FLOWPATH FROM NODE 3547.00 TO NODE 3545.00 = 335.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3545.00 TO NODE 3544.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 743.80 DOWNSTREAM(FEET) = 742.50  
FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.04  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.24  
PIPE TRAVEL TIME(MIN.) = 0.43 Tc(MIN.) = 4.07  
LONGEST FLOWPATH FROM NODE 3547.00 TO NODE 3544.00 = 465.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3544.00 TO NODE 3540.50 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 742.50 DOWNSTREAM(FEET) = 741.30  
CHANNEL LENGTH THRU SUBAREA(FEET) = 120.00 CHANNEL SLOPE = 0.0100  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.24  
FLOW VELOCITY(FEET/SEC) = 1.91 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 5.12  
LONGEST FLOWPATH FROM NODE 3547.00 TO NODE 3540.50 = 585.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3544.00 TO NODE 3540.50 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.084  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7250  
SUBAREA AREA(ACRES) = 0.13 SUBAREA RUNOFF(CFS) = 0.24  
TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 3.42  
TC(MIN.) = 5.12

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3540.50 TO NODE 3540.50 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.12  
RAINFALL INTENSITY(INCH/HR) = 9.08  
TOTAL STREAM AREA(ACRES) = 0.52  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3543.00 TO NODE 3542.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 748.90  
DOWNSTREAM ELEVATION(FEET) = 746.80  
ELEVATION DIFFERENCE(FEET) = 2.10  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.334  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.58  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3542.00 TO NODE 3541.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 746.80 DOWNSTREAM ELEVATION(FEET) = 744.10  
STREET LENGTH(FEET) = 150.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.33

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.26

HALFSTREET FLOOD WIDTH(FEET) = 6.52

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.44

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.63

STREET FLOW TRAVEL TIME(MIN.) = 1.02 Tc(MIN.) = 3.36

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 1.49

TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 2.07

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.10

FLOW VELOCITY(FEET/SEC.) = 2.68 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.77

LONGEST FLOWPATH FROM NODE 3543.00 TO NODE 3541.00 = 230.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3540.50 TO NODE 3540.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 3.36

RAINFALL INTENSITY(INCH/HR) = 9.22

TOTAL STREAM AREA(ACRES) = 0.25

PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.07

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.42         | 5.12      | 9.084                 | 0.52        |
| 2             | 2.07         | 3.36      | 9.222                 | 0.25        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO



CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 4.32         | 3.36      | 9.222                 |
| 2             | 5.47         | 5.12      | 9.084                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.47 Tc(MIN.) = 5.12  
TOTAL AREA(ACRES) = 0.8  
LONGEST FLOWPATH FROM NODE 3547.00 TO NODE 3540.50 = 585.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3540.50 TO NODE 35.40 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 736.50 DOWNSTREAM(FEET) = 735.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.18  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.47  
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 5.46  
LONGEST FLOWPATH FROM NODE 3547.00 TO NODE 35.40 = 710.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 0.8 TC(MIN.) = 5.46  
PEAK FLOW RATE(CFS) = 5.47

=====

END OF RATIONAL METHOD ANALYSIS





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 35.5 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-35-5.DAT  
TIME/DATE OF STUDY: 11:08 11/22/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3552.00 TO NODE 3551.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 757.40

DOWNSTREAM ELEVATION(FEET) = 755.90

ELEVATION DIFFERENCE(FEET) = 1.50

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.581

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 78.12

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.66

TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 3551.00 TO NODE 3550.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 755.90 DOWNSTREAM ELEVATION(FEET) = 747.80

STREET LENGTH(FEET) = 250.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.83

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.26

HALFSTREET FLOOD WIDTH(FEET) = 6.59

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.30

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.85

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STREET FLOW TRAVEL TIME(MIN.) = 1.26 Tc(MIN.) = 3.84

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.28 SUBAREA RUNOFF(CFS) = 2.32

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 2.99

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.30

FLOW VELOCITY(FEET/SEC.) = 3.70 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.08

LONGEST FLOWPATH FROM NODE 3552.00 TO NODE 3550.00 = 330.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3550.00 TO NODE 3549.00 IS CODE = 52

-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 747.50 DOWNSTREAM(FEET) = 747.40

CHANNEL LENGTH THRU SUBAREA(FEET) = 10.00 CHANNEL SLOPE = 0.0100

CHANNEL FLOW THRU SUBAREA(CFS) = 2.99

FLOW VELOCITY(FEET/SEC) = 1.88 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 3.93

LONGEST FLOWPATH FROM NODE 3552.00 TO NODE 3549.00 = 340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3550.00 TO NODE 3549.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.7478

SUBAREA AREA(ACRES) = 0.10 SUBAREA RUNOFF(CFS) = 0.18

TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 3.17

TC(MIN.) = 3.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 3549.00 TO NODE 35.50 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

P-35-5.TXT

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=====
ELEVATION DATA: UPSTREAM(FEET) = 742.50 DOWNSTREAM(FEET) = 740.00
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.53
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.17
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 4.24
LONGEST FLOWPATH FROM NODE 3552.00 TO NODE 35.50 = 460.00 FEET.
=====
```

END OF STUDY SUMMARY:

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=====
TOTAL AREA(ACRES) = 0.5 TC(MIN.) = 4.24
PEAK FLOW RATE(CFS) = 3.17
=====
```

END OF RATIONAL METHOD ANALYSIS





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
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2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 35.6 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-35-6.DAT  
TIME/DATE OF STUDY: 10:52 11/22/2016

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*



\*\*\*\*\*

FLOW PROCESS FROM NODE 3559.00 TO NODE 3558.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 764.60

DOWNSTREAM ELEVATION(FEET) = 761.60

ELEVATION DIFFERENCE(FEET) = 3.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.073

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.58

TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 3558.00 TO NODE 3557.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 761.60 DOWNSTREAM ELEVATION(FEET) = 759.20

STREET LENGTH(FEET) = 130.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.08

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.24

HALFSTREET FLOOD WIDTH(FEET) = 5.77

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.39

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.58

STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 2.98

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 1.00  
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.58

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.00  
FLOW VELOCITY(FEET/SEC.) = 2.59 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.69  
LONGEST FLOWPATH FROM NODE 3559.00 TO NODE 3557.00 = 210.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3557.00 TO NODE 3554.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 753.20 DOWNSTREAM(FEET) = 749.30  
FLOW LENGTH(FEET) = 190.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.33  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.58  
PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 3.57  
LONGEST FLOWPATH FROM NODE 3559.00 TO NODE 3554.00 = 400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3554.00 TO NODE 3554.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 3.57  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.19  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 3556.00 TO NODE 3555.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

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UPSTREAM ELEVATION(FEET) = 760.90  
DOWNSTREAM ELEVATION(FEET) = 757.90  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.073  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 3555.00 TO NODE 3554.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 757.90 DOWNSTREAM ELEVATION(FEET) = 755.30  
STREET LENGTH(FEET) = 125.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.37  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 6.39  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.60  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.66  
STREET FLOW TRAVEL TIME(MIN.) = 0.80 Tc(MIN.) = 2.87  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.13 SUBAREA RUNOFF(CFS) = 1.08  
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 1.91

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.48  
FLOW VELOCITY(FEET/SEC.) = 2.82 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.78  
LONGEST FLOWPATH FROM NODE 3556.00 TO NODE 3554.00 = 205.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3554.00 TO NODE 3554.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 2.87
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.23
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.91

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 3.49 Tc(MIN.) = 3.57
TOTAL AREA(ACRES) = 0.4
LONGEST FLOWPATH FROM NODE 3559.00 TO NODE 3554.00 = 400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3554.00 TO NODE 35.60 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 749.30 DOWNSTREAM(FEET) = 743.40
FLOW LENGTH(FEET) = 135.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.75
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.49
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 3.83

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LONGEST FLOWPATH FROM NODE 3559.00 TO NODE 35.60 = 535.00 FEET.

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END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 0.4 TC(MIN.) = 3.83

PEAK FLOW RATE(CFS) = 3.49

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* NO DETENTION \*
  - \* SUB-BASIN 35.7 \*
- \*\*\*\*\*

FILE NAME: P-35-7.DAT  
TIME/DATE OF STUDY: 09:12 11/29/2016

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 3575.00 TO NODE 3574.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 812.20

DOWNSTREAM ELEVATION(FEET) = 811.20

ELEVATION DIFFERENCE(FEET) = 1.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.771

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 68.75

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.75

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 3574.00 TO NODE 3573.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 811.20 DOWNSTREAM ELEVATION(FEET) = 799.80

STREET LENGTH(FEET) = 490.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.86

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.30

HALFSTREET FLOOD WIDTH(FEET) = 8.78

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.22

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.97



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STREET FLOW TRAVEL TIME(MIN.) = 2.53 Tc(MIN.) = 5.31  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.875

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.53 SUBAREA RUNOFF(CFS) = 4.23  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 4.95

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.17  
FLOW VELOCITY(FEET/SEC.) = 3.62 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.27  
LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 3573.00 = 570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3573.00 TO NODE 3559.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 793.80 DOWNSTREAM(FEET) = 753.50  
FLOW LENGTH(FEET) = 1435.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.23  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.95  
PIPE TRAVEL TIME(MIN.) = 2.91 Tc(MIN.) = 8.21  
LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 3559.00 = 2005.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3559.00 TO NODE 3559.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.21  
RAINFALL INTENSITY(INCH/HR) = 6.70  
TOTAL STREAM AREA(ACRES) = 0.62  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.95

\*\*\*\*\*

FLOW PROCESS FROM NODE 3573.00 TO NODE 3564.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 799.80  
 DOWNSTREAM ELEVATION(FEET) = 797.20  
 ELEVATION DIFFERENCE(FEET) = 2.60  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.060  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.75  
 TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 3564.00 TO NODE 3563.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 797.20 DOWNSTREAM ELEVATION(FEET) = 777.40  
 STREET LENGTH(FEET) = 500.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.06

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.33  
 HALFSTREET FLOOD WIDTH(FEET) = 10.08  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.46  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.46  
 STREET FLOW TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 3.93  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.04 SUBAREA RUNOFF(CFS) = 8.63  
 TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 9.38

END OF SUBAREA STREET FLOW HYDRAULICS:

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DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.02  
FLOW VELOCITY(FEET/SEC.) = 5.17 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.00  
LONGEST FLOWPATH FROM NODE 3573.00 TO NODE 3563.00 = 575.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3563.00 TO NODE 3559.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 771.40 DOWNSTREAM(FEET) = 753.50  
FLOW LENGTH(FEET) = 940.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.37  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.38  
PIPE TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 5.80  
LONGEST FLOWPATH FROM NODE 3573.00 TO NODE 3559.00 = 1515.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3559.00 TO NODE 3559.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.80  
RAINFALL INTENSITY(INCH/HR) = 8.38  
TOTAL STREAM AREA(ACRES) = 1.13  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 3562.00 TO NODE 3561.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 782.90  
DOWNSTREAM ELEVATION(FEET) = 776.40  
ELEVATION DIFFERENCE(FEET) = 6.50  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.929  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.08  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 1.08

\*\*\*\*\*

FLOW PROCESS FROM NODE 3561.00 TO NODE 3560.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 776.40 DOWNSTREAM ELEVATION(FEET) = 760.60  
STREET LENGTH(FEET) = 535.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.85  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.38  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.14  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.47  
STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 4.08  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.15 SUBAREA RUNOFF(CFS) = 9.54  
TOTAL AREA(ACRES) = 1.3 PEAK FLOW RATE(CFS) = 10.62

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.52  
FLOW VELOCITY(FEET/SEC.) = 4.77 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.99  
LONGEST FLOWPATH FROM NODE 3562.00 TO NODE 3560.00 = 635.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3560.00 TO NODE 3559.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 757.50 DOWNSTREAM(FEET) = 753.50

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FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.77  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.62  
PIPE TRAVEL TIME(MIN.) = 0.98 Tc(MIN.) = 5.07  
LONGEST FLOWPATH FROM NODE 3562.00 TO NODE 3559.00 = 1035.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3559.00 TO NODE 3559.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.07  
RAINFALL INTENSITY(INCH/HR) = 9.14  
TOTAL STREAM AREA(ACRES) = 1.28  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.62

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3559.40 TO NODE 3559.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
UPSTREAM ELEVATION(FEET) = 767.10  
DOWNSTREAM ELEVATION(FEET) = 763.80  
ELEVATION DIFFERENCE(FEET) = 3.30  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.796  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.58  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3559.20 TO NODE 3559.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 763.80 DOWNSTREAM ELEVATION(FEET) = 754.00  
STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.82  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.17  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.96  
STREET FLOW TRAVEL TIME(MIN.) = 2.23 Tc(MIN.) = 4.03  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.54 SUBAREA RUNOFF(CFS) = 4.48  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 5.06

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.31  
FLOW VELOCITY(FEET/SEC.) = 3.62 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.28  
LONGEST FLOWPATH FROM NODE 3559.40 TO NODE 3559.00 = 495.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3559.00 TO NODE 3559.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 4 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.03  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.61  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.06

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 4.95         | 8.21      | 6.697                 | 0.62        |
| 2             | 9.38         | 5.80      | 8.381                 | 1.13        |

|   |       |      |            |      |
|---|-------|------|------------|------|
|   |       |      | P-35-7.TXT |      |
| 3 | 10.62 | 5.07 | 9.144      | 1.28 |
| 4 | 5.06  | 4.03 | 9.222      | 0.61 |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 4 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | RUNOFF<br>(CFS) | Tc<br>(MIN.) | INTENSITY<br>(INCH/HOUR) |
|------------------|-----------------|--------------|--------------------------|
| 1                | 22.45           | 4.03         | 9.222                    |
| 2                | 26.89           | 5.07         | 9.144                    |
| 3                | 27.21           | 5.80         | 8.381                    |
| 4                | 23.90           | 8.21         | 6.697                    |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 27.21 Tc(MIN.) = 5.80  
TOTAL AREA(ACRES) = 3.6  
LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 3559.00 = 2005.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3559.00 TO NODE 3558.90 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 754.00 DOWNSTREAM(FEET) = 753.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 100.00 CHANNEL SLOPE = 0.0100  
CHANNEL FLOW THRU SUBAREA(CFS) = 27.21  
FLOW VELOCITY(FEET/SEC) = 3.26 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.51 Tc(MIN.) = 6.31  
LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 3558.90 = 2105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3559.00 TO NODE 3558.90 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.937  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8434  
SUBAREA AREA(ACRES) = 0.32 SUBAREA RUNOFF(CFS) = 0.51  
TOTAL AREA(ACRES) = 4.0 TOTAL RUNOFF(CFS) = 27.21  
TC(MIN.) = 6.31  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 3558.90 TO NODE 35.70 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |               |                    |        |
|--|---------------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =                   | 748.00        | DOWNSTREAM(FEET) = | 745.00 |
| FLOW LENGTH(FEET) =                                | 30.00         | MANNING'S N =      | 0.013  |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS                 | 12.9 INCHES   |                    |        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                    | 20.07         |                    |        |
| ESTIMATED PIPE DIAMETER(INCH) =                    | 18.00         | NUMBER OF PIPES =  | 1      |
| PIPE-FLOW(CFS) =                                   | 27.21         |                    |        |
| PIPE TRAVEL TIME(MIN.) =                           | 0.02          | Tc(MIN.) =         | 6.33   |
| LONGEST FLOWPATH FROM NODE 3575.00 TO NODE 35.70 = | 2135.00 FEET. |                    |        |

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 4.0 TC(MIN.) = 6.33  
PEAK FLOW RATE(CFS) = 27.21

=====

=====

END OF RATIONAL METHOD ANALYSIS







| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------|------|---|---|
|              |      |      |                  |                  |                  |             |               |          | 1    | 2 | 3 |
| 60           | 55   | 2    | 1168             | 1140             | 80               | 0.36        | 0.10          |          |      |   |   |
| 55           | 40   | 5    | 1140             | 757              | 1590             |             |               | VALLEY   |      |   |   |
| 55           | 40   | 8    |                  |                  |                  | 0.36        | 11.91         |          |      |   |   |
| 40           | 40   | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |
|              |      |      |                  |                  |                  |             |               |          |      |   |   |
| 50           | 45   | 2    | 1160             | 1125             | 80               | 0.36        | 0.16          |          |      |   |   |
| 45           | 40   | 5    | 1125             | 757              | 1950             |             |               | VALLEY   |      |   |   |
| 45           | 40   | 8    |                  |                  |                  | 0.36        | 19.80         |          |      |   |   |
| 40           | 40   | 1    |                  |                  |                  |             |               | 2 OF 2   |      |   |   |
|              |      |      |                  |                  |                  |             |               |          |      |   |   |
| 40           | 35   | 5    | 757              | 735              | 540              |             |               | VALLEY   |      |   |   |
| 40           | 35   | 8    |                  |                  |                  | 0.4         | 13.01         |          |      |   |   |
| 35           | 30   | 5    | 735              | 688              | 1770             |             |               | VALLEY   |      |   |   |
| 35           | 30   | 8    |                  |                  |                  | 0.4         | 43.69         |          |      |   |   |
| 30           | 5    | 5    | 688              | 676              | 1270             |             |               | VALLEY   |      |   |   |
| 30           | 5    | 8    |                  |                  |                  | 0.41        | 10.87         |          |      |   |   |
| 5            | 5    | 1    |                  |                  |                  |             |               | 1 OF 4   |      |   |   |
|              |      |      |                  |                  |                  |             |               |          |      |   |   |
| 25           | 20   | 2    | 1205             | 1165             | 80               | 0.36        | 0.17          |          |      |   |   |
| 20           | 15   | 5    | 1165             | 840              | 1610             |             |               | MTN      |      |   |   |
| 20           | 15   | 8    |                  |                  |                  | 0.36        | 17.12         |          |      |   |   |
| 15           | 10   | 5    | 840              | 775              | 1025             |             |               | VALLEY   |      |   |   |
| 15           | 10   | 8    |                  |                  |                  | 0.36        | 11.50         |          |      |   |   |
| 10           | 9    | 5    | 775              | 690              | 2230             |             |               | VALLEY   |      |   |   |
| 10           | 9    | 8    |                  |                  |                  | 0.38        | 40.07         |          |      |   |   |
| 9            | 5    | 5    | 690              | 676              | 1020             |             |               | VALLEY   |      |   |   |
| 9            | 5    | 8    |                  |                  |                  | 0.4         | 30.65         |          |      |   |   |
| 5            | 5    | 1    |                  |                  |                  |             |               | 2 OF 4   |      |   |   |
|              |      |      |                  |                  |                  |             |               |          |      |   |   |
| 4938         | 4936 | 2    | 701              | 700.4            | 85               | 0.9         | 0.10          |          |      |   |   |
| 4936         | 4934 | 6    | 700.4            | 689.9            | 860              | 0.9         | 1.13          |          |      |   |   |
| 4934         | 5    | 3    | 683.9            | 676              | 740              |             |               |          |      |   |   |
| 5            | 5    | 1    |                  |                  |                  |             |               | 3 OF 4   |      |   |   |
|              |      |      |                  |                  |                  |             |               |          |      |   |   |
| 7            | 6    | 2    | 689.8            | 688              | 85               | 0.9         | 0.10          |          |      |   |   |
| 6            | 5    | 6    | 688              | 680.6            | 670              | 0.9         | 0.75          | ONE SIDE |      |   |   |
| 5            | 5    | 1    |                  |                  |                  |             |               | 4 OF 4   |      |   |   |
|              |      |      |                  |                  |                  |             |               |          |      |   |   |
| 5            | 1    | 3    | 676              | 674.5            | 135              |             |               |          |      |   |   |
| 1            | 1    | 1    |                  |                  |                  |             |               | 1 OF 2   |      |   |   |
| 4            | 3    | 2    | 700.7            | 700              | 65               | 0.9         | 0.08          |          |      |   |   |
| 3            | 2    | 6    | 700              | 680.8            | 1675             | 0.9         | 1.99          |          |      |   |   |
| 2            | 1    | 3    | 674.5            | 674              | 50               |             |               |          |      |   |   |
| 1            | 1    | 1    |                  |                  |                  |             | <b>203.20</b> | 2 OF 2   |      |   |   |

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 1 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-1.DAT  
TIME/DATE OF STUDY: 10:24 12/05/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|--|--------------|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020                                       | 0.50                   | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 60.00 TO NODE 55.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1168.00  
DOWNSTREAM ELEVATION(FEET) = 1140.00  
ELEVATION DIFFERENCE(FEET) = 28.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.530  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.641  
SUBAREA RUNOFF(CFS) = 0.31  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.31

\*\*\*\*\*

FLOW PROCESS FROM NODE 55.00 TO NODE 40.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1140.00 DOWNSTREAM(FEET) = 757.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1590.00 CHANNEL SLOPE = 0.2409  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.31  
FLOW VELOCITY(FEET/SEC) = 4.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 5.59 Tc(MIN.) = 11.12  
LONGEST FLOWPATH FROM NODE 60.00 TO NODE 40.00 = 1670.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 55.00 TO NODE 40.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.508  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600  
SUBAREA AREA(ACRES) = 11.91 SUBAREA RUNOFF(CFS) = 23.62  
TOTAL AREA(ACRES) = 12.0 TOTAL RUNOFF(CFS) = 23.81  
TC(MIN.) = 11.12

P-1.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.12  
RAINFALL INTENSITY(INCH/HR) = 5.51  
TOTAL STREAM AREA(ACRES) = 12.01  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.81

\*\*\*\*\*  
FLOW PROCESS FROM NODE 50.00 TO NODE 45.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1160.00  
DOWNSTREAM ELEVATION(FEET) = 1125.00  
ELEVATION DIFFERENCE(FEET) = 35.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.530  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.641  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 45.00 TO NODE 40.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1125.00 DOWNSTREAM(FEET) = 757.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1950.00 CHANNEL SLOPE = 0.1887  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.50  
FLOW VELOCITY(FEET/SEC) = 4.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 6.85 Tc(MIN.) = 12.38  
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 40.00 = 2030.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 45.00 TO NODE 40.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.138
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600
SUBAREA AREA(ACRES) = 19.80 SUBAREA RUNOFF(CFS) = 36.62
TOTAL AREA(ACRES) = 20.0 TOTAL RUNOFF(CFS) = 36.92
TC(MIN.) = 12.38

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 1

```

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.38
RAINFALL INTENSITY(INCH/HR) = 5.14
TOTAL STREAM AREA(ACRES) = 19.96
PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.92

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 23.81        | 11.12     | 5.508                 | 12.01       |
| 2             | 36.92        | 12.38     | 5.138                 | 19.96       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 56.96        | 11.12     | 5.508                 |
| 2             | 59.13        | 12.38     | 5.138                 |

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 59.13 Tc(MIN.) = 12.38
TOTAL AREA(ACRES) = 32.0
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 40.00 = 2030.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 35.00 IS CODE = 52

```

-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

```

P-1.TXT

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 757.00 DOWNSTREAM(FEET) = 735.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 540.00 CHANNEL SLOPE = 0.0407  
CHANNEL FLOW THRU SUBAREA(CFS) = 59.13  
FLOW VELOCITY(FEET/SEC) = 8.20 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.10 Tc(MIN.) = 13.48  
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 35.00 = 2570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 40.00 TO NODE 35.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.864  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3716  
SUBAREA AREA(ACRES) = 13.01 SUBAREA RUNOFF(CFS) = 25.31  
TOTAL AREA(ACRES) = 45.0 TOTAL RUNOFF(CFS) = 81.30  
TC(MIN.) = 13.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 35.00 TO NODE 30.00 IS CODE = 52

-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 735.00 DOWNSTREAM(FEET) = 688.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1770.00 CHANNEL SLOPE = 0.0266  
CHANNEL FLOW THRU SUBAREA(CFS) = 81.30  
FLOW VELOCITY(FEET/SEC) = 7.27 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.06 Tc(MIN.) = 17.54  
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 30.00 = 4340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 35.00 TO NODE 30.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.105  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3856  
SUBAREA AREA(ACRES) = 43.69 SUBAREA RUNOFF(CFS) = 71.74  
TOTAL AREA(ACRES) = 88.7 TOTAL RUNOFF(CFS) = 140.34

TC(MIN.) = 17.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 30.00 TO NODE 5.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 688.00 DOWNSTREAM(FEET) = 676.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1270.00 CHANNEL SLOPE = 0.0094
CHANNEL FLOW THRU SUBAREA(CFS) = 140.34
FLOW VELOCITY(FEET/SEC) = 5.11 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.14 Tc(MIN.) = 21.68
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 5.00 = 5610.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 30.00 TO NODE 5.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.580
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3882
SUBAREA AREA(ACRES) = 10.87 SUBAREA RUNOFF(CFS) = 15.96
TOTAL AREA(ACRES) = 99.5 TOTAL RUNOFF(CFS) = 140.34
TC(MIN.) = 21.68
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 4
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 21.68
RAINFALL INTENSITY(INCH/HR) = 3.58
TOTAL STREAM AREA(ACRES) = 99.54
PEAK FLOW RATE(CFS) AT CONFLUENCE = 140.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 25.00 TO NODE 20.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 1205.00  
 DOWNSTREAM ELEVATION(FEET) = 1165.00  
 ELEVATION DIFFERENCE(FEET) = 40.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.530  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.641  
 SUBAREA RUNOFF(CFS) = 0.53  
 TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 20.00 TO NODE 15.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1165.00 DOWNSTREAM(FEET) = 840.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1610.00 CHANNEL SLOPE = 0.2019  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .1609 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
 CHANNEL FLOW THRU SUBAREA(CFS) = 0.53  
 FLOW VELOCITY(FEET/SEC) = 2.25 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 11.94 Tc(MIN.) = 17.47  
 LONGEST FLOWPATH FROM NODE 25.00 TO NODE 15.00 = 1690.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 20.00 TO NODE 15.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.114  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600  
 SUBAREA AREA(ACRES) = 17.12 SUBAREA RUNOFF(CFS) = 25.36  
 TOTAL AREA(ACRES) = 17.3 TOTAL RUNOFF(CFS) = 25.61  
 TC(MIN.) = 17.47

\*\*\*\*\*

FLOW PROCESS FROM NODE 15.00 TO NODE 10.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====



P-1.TXT

ELEVATION DATA: UPSTREAM(FEET) = 840.00 DOWNSTREAM(FEET) = 775.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1025.00 CHANNEL SLOPE = 0.0634
CHANNEL FLOW THRU SUBAREA(CFS) = 25.61
FLOW VELOCITY(FEET/SEC) = 8.07 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.12 Tc(MIN.) = 19.59
LONGEST FLOWPATH FROM NODE 25.00 TO NODE 10.00 = 2715.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 15.00 TO NODE 10.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.822
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600
SUBAREA AREA(ACRES) = 11.50 SUBAREA RUNOFF(CFS) = 15.82
TOTAL AREA(ACRES) = 28.8 TOTAL RUNOFF(CFS) = 39.61
TC(MIN.) = 19.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 10.00 TO NODE 9.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 775.00 DOWNSTREAM(FEET) = 690.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 2230.00 CHANNEL SLOPE = 0.0381
CHANNEL FLOW THRU SUBAREA(CFS) = 39.61
FLOW VELOCITY(FEET/SEC) = 7.07 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 5.26 Tc(MIN.) = 24.85
LONGEST FLOWPATH FROM NODE 25.00 TO NODE 9.00 = 4945.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 10.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.278
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3800
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3716
SUBAREA AREA(ACRES) = 40.07 SUBAREA RUNOFF(CFS) = 49.92
TOTAL AREA(ACRES) = 68.9 TOTAL RUNOFF(CFS) = 83.90
TC(MIN.) = 24.85

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9.00 TO NODE 5.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |  |                      |
|-------------------------------------|---------|--|----------------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 690.00  | DOWNSTREAM(FEET) =                     | 676.00               |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1020.00 | CHANNEL SLOPE =                        | 0.0137               |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 83.90   |  |                      |
| FLOW VELOCITY(FEET/SEC) =           | 5.28    | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |                      |
| TRAVEL TIME(MIN.) =                 | 3.22    | Tc(MIN.) =                             | 28.07                |
| LONGEST FLOWPATH FROM NODE          | 25.00   | TO NODE                                | 5.00 = 5965.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9.00 TO NODE 5.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |        |                       |        |
|--|--------|-----------------------|--------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.031  |                       |        |
| *USER SPECIFIED(SUBAREA):                |        |                       |        |
| USER-SPECIFIED RUNOFF COEFFICIENT =      | .4000  |                       |        |
| S.C.S. CURVE NUMBER (AMC II) =           | 0      |                       |        |
| AREA-AVERAGE RUNOFF COEFFICIENT =        | 0.3804 |                       |        |
| SUBAREA AREA(ACRES) =                    | 30.65  | SUBAREA RUNOFF(CFS) = | 37.15  |
| TOTAL AREA(ACRES) =                      | 99.5   | TOTAL RUNOFF(CFS) =   | 114.71 |
| TC(MIN.) =                               | 28.07  |                       |        |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

|  |        |
|--|--------|
| TOTAL NUMBER OF STREAMS =                            | 4      |
| CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE: |        |
| TIME OF CONCENTRATION(MIN.) =                        | 28.07  |
| RAINFALL INTENSITY(INCH/HR) =                        | 3.03   |
| TOTAL STREAM AREA(ACRES) =                           | 99.51  |
| PEAK FLOW RATE(CFS) AT CONFLUENCE =                  | 114.71 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4938.00 TO NODE 4936.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

|                                     |       |
|-------------------------------------|-------|
| *USER SPECIFIED(SUBAREA):           |       |
| USER-SPECIFIED RUNOFF COEFFICIENT = | .9000 |
| S.C.S. CURVE NUMBER (AMC II) =      | 0     |
| INITIAL SUBAREA FLOW-LENGTH(FEET) = | 85.00 |

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UPSTREAM ELEVATION(FEET) = 701.00  
 DOWNSTREAM ELEVATION(FEET) = 700.40  
 ELEVATION DIFFERENCE(FEET) = 0.60  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.030  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
 THE MAXIMUM OVERLAND FLOW LENGTH = 56.18  
 (Reference: Table 3-1B of Hydrology Manual)  
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.83  
 TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 4936.00 TO NODE 4934.00 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 700.40 DOWNSTREAM ELEVATION(FEET) = 689.90  
 STREET LENGTH(FEET) = 860.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.31  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.37  
 HALFSTREET FLOOD WIDTH(FEET) = 12.06  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.74  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.01  
 STREET FLOW TRAVEL TIME(MIN.) = 5.23 Tc(MIN.) = 8.26  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.673

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.13 SUBAREA RUNOFF(CFS) = 6.79  
 TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 7.39

END OF SUBAREA STREET FLOW HYDRAULICS:

P-1.TXT

DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 15.00  
FLOW VELOCITY(FEET/SEC.) = 3.12 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.33  
LONGEST FLOWPATH FROM NODE 4938.00 TO NODE 4934.00 = 945.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4934.00 TO NODE 5.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 683.90 DOWNSTREAM(FEET) = 676.00  
FLOW LENGTH(FEET) = 740.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.34  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.39  
PIPE TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 10.20  
LONGEST FLOWPATH FROM NODE 4938.00 TO NODE 5.00 = 1685.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.20  
RAINFALL INTENSITY(INCH/HR) = 5.82  
TOTAL STREAM AREA(ACRES) = 1.23  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.39

\*\*\*\*\*

FLOW PROCESS FROM NODE 7.00 TO NODE 6.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 689.80  
DOWNSTREAM ELEVATION(FEET) = 688.00  
ELEVATION DIFFERENCE(FEET) = 1.80  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.535  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 81.76  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

P-1.TXT

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 6.00 TO NODE 5.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 688.00 DOWNSTREAM ELEVATION(FEET) = 680.60  
STREET LENGTH(FEET) = 670.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.37  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.10  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.49  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.87  
STREET FLOW TRAVEL TIME(MIN.) = 4.48 Tc(MIN.) = 7.01  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.414

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.75 SUBAREA RUNOFF(CFS) = 5.00  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 5.67

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.77  
FLOW VELOCITY(FEET/SEC.) = 2.82 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.13  
LONGEST FLOWPATH FROM NODE 7.00 TO NODE 5.00 = 755.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 4
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 4 ARE:
TIME OF CONCENTRATION(MIN.) = 7.01
RAINFALL INTENSITY(INCH/HR) = 7.41
TOTAL STREAM AREA(ACRES) = 0.85
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.67

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 140.34       | 21.68     | 3.580                 | 99.54       |
| 2             | 114.71       | 28.07     | 3.031                 | 99.51       |
| 3             | 7.39         | 10.20     | 5.821                 | 1.23        |
| 4             | 5.67         | 7.01      | 7.414                 | 0.85        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 4 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 107.18       | 7.01      | 7.414                 |
| 2             | 139.85       | 10.20     | 5.821                 |
| 3             | 236.21       | 21.68     | 3.580                 |
| 4             | 239.66       | 28.07     | 3.031                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 239.66 Tc(MIN.) = 28.07
TOTAL AREA(ACRES) = 201.1
LONGEST FLOWPATH FROM NODE 25.00 TO NODE 5.00 = 5965.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 5.00 TO NODE 1.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 676.00 DOWNSTREAM(FEET) = 674.50
FLOW LENGTH(FEET) = 135.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 45.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.05
ESTIMATED PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 239.66
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 28.22
LONGEST FLOWPATH FROM NODE 25.00 TO NODE 1.00 = 6100.00 FEET.

```

P-1.TXT

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1.00 TO NODE 1.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 28.22  
RAINFALL INTENSITY(INCH/HR) = 3.02  
TOTAL STREAM AREA(ACRES) = 201.13  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 239.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4.00 TO NODE 3.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 700.70  
DOWNSTREAM ELEVATION(FEET) = 700.00  
ELEVATION DIFFERENCE(FEET) = 0.70  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.832  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.66  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3.00 TO NODE 2.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 700.00 DOWNSTREAM ELEVATION(FEET) = 680.80  
STREET LENGTH(FEET) = 1675.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.47  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.39  
HALFSTREET FLOOD WIDTH(FEET) = 13.43  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.85  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.12  
STREET FLOW TRAVEL TIME(MIN.) = 9.81 Tc(MIN.) = 12.64  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.069  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.99 SUBAREA RUNOFF(CFS) = 9.08  
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 9.44

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.46 HALFSTREET FLOOD WIDTH(FEET) = 16.71  
FLOW VELOCITY(FEET/SEC.) = 3.24 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.49  
\*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,  
AND L = 1675.0 FT WITH ELEVATION-DROP = 19.2 FT, IS 16.5 CFS,  
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 2.00  
LONGEST FLOWPATH FROM NODE 4.00 TO NODE 2.00 = 1740.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2.00 TO NODE 1.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 674.50 DOWNSTREAM(FEET) = 674.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.44  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 12.77  
LONGEST FLOWPATH FROM NODE 4.00 TO NODE 1.00 = 1790.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1.00 TO NODE 1.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.77



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RAINFALL INTENSITY(INCH/HR) = 5.04  
TOTAL STREAM AREA(ACRES) = 2.07  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.44

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 239.66       | 28.22     | 3.020                 | 201.13      |
| 2             | 9.44         | 12.77     | 5.036                 | 2.07        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 153.18       | 12.77     | 5.036                 |
| 2             | 245.33       | 28.22     | 3.020                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 245.33 Tc(MIN.) = 28.22  
TOTAL AREA(ACRES) = 203.2  
LONGEST FLOWPATH FROM NODE 25.00 TO NODE 1.00 = 6100.00 FEET.

=====  
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 203.2 TC(MIN.) = 28.22  
PEAK FLOW RATE(CFS) = 245.33  
=====

=====  
END OF RATIONAL METHOD ANALYSIS

↑



Newland Sierra

Job #: 2660-02

Run Name:  
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Page 1  
of 2

| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 4998         | 4996 | 2    | 731.2            | 728.5            | 110              | 0.9         | 0.08          |                |      |   |   |
| 4996         | 4994 | 6    | 728.5            | 721.9            | 820              | 0.9         | 1.72          |                |      |   |   |
| 4994         | 4988 | 5    | 718.5            | 717              | 120              |             |               | VALLEY         |      |   |   |
| 4994         | 4988 | 8    |                  |                  |                  | 0.2         | 0.20          |                |      |   |   |
| 4988         | 4986 | 3    | 713.7            | 713              | 70               |             |               |                |      |   |   |
| 4986         | 4986 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 4992         | 4990 | 2    | 727.5            | 727.1            | 80               | 0.9         | 0.09          |                |      |   |   |
| 4990         | 4986 | 6    | 727.1            | 723.6            | 350              | 0.9         | 0.67          |                |      |   |   |
| 4986         | 4986 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 4986         | 4980 | 3    | 713              | 708              | 470              |             |               |                |      |   |   |
| 4980         | 4980 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 4985         | 4984 | 2    | 722.6            | 722.4            | 80               | 0.9         | 0.10          |                |      |   |   |
| 4984         | 4983 | 6    | 722.4            | 720              | 210              | 0.9         | 0.31          |                |      |   |   |
| 4983         | 4982 | 5    | 717.5            | 717.3            | 20               |             |               | VALLEY         |      |   |   |
| 4983         | 4982 | 8    |                  |                  |                  | 0.2         | 0.10          |                |      |   |   |
| 4982         | 4980 | 3    | 712.5            | 708              | 70               |             |               |                |      |   |   |
| 4980         | 4980 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 4980         | 4970 | 3    | 708              | 704              | 400              |             |               |                |      |   |   |
| 4970         | 4970 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 4978         | 4976 | 2    | 725.2            | 723.5            | 75               | 0.9         | 0.09          |                |      |   |   |
| 4976         | 4974 | 6    | 723.5            | 720.5            | 315              | 0.9         | 1.44          |                |      |   |   |
| 4974         | 4972 | 5    | 717.5            | 717.3            | 50               |             |               | VALLEY         |      |   |   |
| 4974         | 4972 | 8    |                  |                  |                  | 0.3         | 0.25          |                |      |   |   |
| 4972         | 4970 | 3    | 717.3            | 716.7            | 60               |             |               |                |      |   |   |
| 4970         | 4970 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 4970         | 4961 | 3    | 716.7            | 708.5            | 820              |             |               |                |      |   |   |
| 4961         | 4961 | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 4968         | 4966 | 2    | 723.5            | 721              | 80               | 0.9         | 0.10          |                |      |   |   |
| 4966         | 4964 | 6    | 721              | 715              | 400              | 0.9         | 0.70          |                |      |   |   |
| 4964         | 4964 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
|              |      |      |                  |                  |                  |             |               |                |      |   |   |
| 2030         | 2029 | 2    | 1176             | 1150             | 84               | 0.36        | 0.07          |                |      |   |   |
| 2029         | 2028 | 5    | 1150             | 745              | 1562             |             |               | MTN            |      |   |   |
| 2029         | 2028 | 8    |                  |                  |                  | 0.34        | 13.66         |                |      |   |   |
| 2028         | 4964 | 5    | 745              | 713              | 1840             |             |               | VALLEY         |      |   |   |
| 2028         | 4964 | 8    |                  |                  |                  | 0.33        | 41.90         |                |      |   |   |
| 4964         | 4964 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* NO DETENTION \*
  - \* SUB-BASIN 2000 \*
- \*\*\*\*\*

FILE NAME: P-2000.DAT  
TIME/DATE OF STUDY: 15:43 12/08/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 4985.00 TO NODE 4984.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 722.60

DOWNSTREAM ELEVATION(FEET) = 722.40

ELEVATION DIFFERENCE(FEET) = 0.20

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.207

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 50.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.83

TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 4984.00 TO NODE 4983.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 722.40 DOWNSTREAM ELEVATION(FEET) = 720.00

STREET LENGTH(FEET) = 210.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.12

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.31

HALFSTREET FLOOD WIDTH(FEET) = 8.99

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.29

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.70

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STREET FLOW TRAVEL TIME(MIN.) = 1.53 Tc(MIN.) = 4.74

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.31 SUBAREA RUNOFF(CFS) = 2.57

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.40

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.04

FLOW VELOCITY(FEET/SEC.) = 2.55 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.88

LONGEST FLOWPATH FROM NODE 4985.00 TO NODE 4983.00 = 290.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4983.00 TO NODE 4982.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 717.50 DOWNSTREAM(FEET) = 717.30

CHANNEL LENGTH THRU SUBAREA(FEET) = 20.00 CHANNEL SLOPE = 0.0100

CHANNEL FLOW THRU SUBAREA(CFS) = 3.40

FLOW VELOCITY(FEET/SEC) = 1.93 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 4.91

LONGEST FLOWPATH FROM NODE 4985.00 TO NODE 4982.00 = 310.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4983.00 TO NODE 4982.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.7627

SUBAREA AREA(ACRES) = 0.10 SUBAREA RUNOFF(CFS) = 0.18

TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 3.59

TC(MIN.) = 4.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 4982.00 TO NODE 4970.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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=====

ELEVATION DATA: UPSTREAM(FEET) = 712.50 DOWNSTREAM(FEET) = 704.00  
FLOW LENGTH(FEET) = 470.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.43  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.59  
PIPE TRAVEL TIME(MIN.) = 1.22 Tc(MIN.) = 6.13  
LONGEST FLOWPATH FROM NODE 4985.00 TO NODE 4970.00 = 780.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4970.00 TO NODE 4970.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.13  
RAINFALL INTENSITY(INCH/HR) = 8.09  
TOTAL STREAM AREA(ACRES) = 0.51  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.59

\*\*\*\*\*

FLOW PROCESS FROM NODE 4978.00 TO NODE 4976.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 725.20  
DOWNSTREAM ELEVATION(FEET) = 723.50  
ELEVATION DIFFERENCE(FEET) = 1.70  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.373  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 4976.00 TO NODE 4974.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 723.50 DOWNSTREAM ELEVATION(FEET) = 720.50

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STREET LENGTH(FEET) = 315.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.72  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.43  
HALFSTREET FLOOD WIDTH(FEET) = 15.14  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.79  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.20  
STREET FLOW TRAVEL TIME(MIN.) = 1.88 Tc(MIN.) = 4.26  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.44 SUBAREA RUNOFF(CFS) = 11.95  
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 12.70

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.51 HALFSTREET FLOOD WIDTH(FEET) = 20.17  
FLOW VELOCITY(FEET/SEC.) = 3.26 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.68  
\*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,  
AND L = 315.0 FT WITH ELEVATION-DROP = 3.0 FT, IS 12.0 CFS,  
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 4974.00  
LONGEST FLOWPATH FROM NODE 4978.00 TO NODE 4974.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4974.00 TO NODE 4972.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 717.50 DOWNSTREAM(FEET) = 717.30  
CHANNEL LENGTH THRU SUBAREA(FEET) = 50.00 CHANNEL SLOPE = 0.0040  
CHANNEL FLOW THRU SUBAREA(CFS) = 12.70  
FLOW VELOCITY(FEET/SEC) = 1.68 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 4.75  
LONGEST FLOWPATH FROM NODE 4978.00 TO NODE 4972.00 = 440.00 FEET.



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\*\*\*\*\*

FLOW PROCESS FROM NODE 4974.00 TO NODE 4972.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8157  
SUBAREA AREA(ACRES) = 0.25 SUBAREA RUNOFF(CFS) = 0.69  
TOTAL AREA(ACRES) = 1.8 TOTAL RUNOFF(CFS) = 13.39  
TC(MIN.) = 4.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 4972.00 TO NODE 4970.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 717.30 DOWNSTREAM(FEET) = 716.70  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.06  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 13.39  
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 4.89  
LONGEST FLOWPATH FROM NODE 4978.00 TO NODE 4970.00 = 500.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4970.00 TO NODE 4970.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.89  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.78  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.39

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.59         | 6.13      | 8.087                 | 0.51        |

2 13.39 4.89 P-2000.TXT  
9.222 1.78

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.25        | 4.89      | 9.222                 |
| 2             | 15.33        | 6.13      | 8.087                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.25 Tc(MIN.) = 4.89  
TOTAL AREA(ACRES) = 2.3  
LONGEST FLOWPATH FROM NODE 4985.00 TO NODE 4970.00 = 780.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4970.00 TO NODE 4961.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 716.70 DOWNSTREAM(FEET) = 708.50  
FLOW LENGTH(FEET) = 820.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.51  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.25  
PIPE TRAVEL TIME(MIN.) = 1.82 Tc(MIN.) = 6.71  
LONGEST FLOWPATH FROM NODE 4985.00 TO NODE 4961.00 = 1600.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4961.00 TO NODE 4961.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 4968.00 TO NODE 4966.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 723.50  
DOWNSTREAM ELEVATION(FEET) = 721.00

P-2000.TXT

ELEVATION DIFFERENCE(FEET) = 2.50  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.202  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.83  
 TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 4966.00 TO NODE 4964.00 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 721.00 DOWNSTREAM ELEVATION(FEET) = 715.00  
 STREET LENGTH(FEET) = 400.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.73  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.34  
 HALFSTREET FLOOD WIDTH(FEET) = 10.83  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.89  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.99  
 STREET FLOW TRAVEL TIME(MIN.) = 2.30 Tc(MIN.) = 4.51  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 0.70 SUBAREA RUNOFF(CFS) = 5.81  
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 6.64

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.77  
 FLOW VELOCITY(FEET/SEC.) = 3.30 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.32  
 LONGEST FLOWPATH FROM NODE 4968.00 TO NODE 4964.00 = 480.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4964.00 TO NODE 4964.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.51
RAINFALL INTENSITY(INCH/HR) = 9.22
TOTAL STREAM AREA(ACRES) = 0.80
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 2030.00 TO NODE 2029.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3600
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 84.00
UPSTREAM ELEVATION(FEET) = 1176.00
DOWNSTREAM ELEVATION(FEET) = 1150.00
ELEVATION DIFFERENCE(FEET) = 26.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.667
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.506
SUBAREA RUNOFF(CFS) = 0.21
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.21

\*\*\*\*\*

FLOW PROCESS FROM NODE 2029.00 TO NODE 2028.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1150.00 DOWNSTREAM(FEET) = 745.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1562.00 CHANNEL SLOPE = 0.2593
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1831 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.21
FLOW VELOCITY(FEET/SEC) = 2.40 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 10.86 Tc(MIN.) = 16.53
LONGEST FLOWPATH FROM NODE 2030.00 TO NODE 2028.00 = 1646.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2029.00 TO NODE 2028.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.264
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3400
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3401
SUBAREA AREA(ACRES) = 13.66 SUBAREA RUNOFF(CFS) = 19.80
TOTAL AREA(ACRES) = 13.7 TOTAL RUNOFF(CFS) = 19.91
TC(MIN.) = 16.53

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2028.00 TO NODE 4964.00 IS CODE = 52

```

-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 745.00 DOWNSTREAM(FEET) = 713.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1840.00 CHANNEL SLOPE = 0.0174
CHANNEL FLOW THRU SUBAREA(CFS) = 19.91
FLOW VELOCITY(FEET/SEC) = 3.95 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 7.77 Tc(MIN.) = 24.30
LONGEST FLOWPATH FROM NODE 2030.00 TO NODE 4964.00 = 3486.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2028.00 TO NODE 4964.00 IS CODE = 81

```

-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.326
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3325
SUBAREA AREA(ACRES) = 41.90 SUBAREA RUNOFF(CFS) = 45.99
TOTAL AREA(ACRES) = 55.6 TOTAL RUNOFF(CFS) = 61.52
TC(MIN.) = 24.30

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 4964.00 TO NODE 4964.00 IS CODE = 1

```

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 24.30
RAINFALL INTENSITY(INCH/HR) = 3.33

```

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TOTAL STREAM AREA(ACRES) = 55.63  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 61.52

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.64         | 4.51      | 9.222                 | 0.80        |
| 2             | 61.52        | 24.30     | 3.326                 | 55.63       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 18.05        | 4.51      | 9.222                 |
| 2             | 63.91        | 24.30     | 3.326                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 63.91 Tc(MIN.) = 24.30  
TOTAL AREA(ACRES) = 56.4  
LONGEST FLOWPATH FROM NODE 2030.00 TO NODE 4964.00 = 3486.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4964.00 TO NODE 4961.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 709.00 DOWNSTREAM(FEET) = 708.50  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 26.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.33  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 63.91  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 24.36  
LONGEST FLOWPATH FROM NODE 2030.00 TO NODE 4961.00 = 3526.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4961.00 TO NODE 4961.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 63.91        | 24.36     | 3.321                 | 56.43       |

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LONGEST FLOWPATH FROM NODE 2030.00 TO NODE 4961.00 = 3526.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.25        | 6.71      | 7.626                 | 2.29        |

LONGEST FLOWPATH FROM NODE 4985.00 TO NODE 4961.00 = 1600.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 33.87        | 6.71      | 7.626                 |
| 2             | 70.99        | 24.36     | 3.321                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 70.99 Tc(MIN.) = 24.36  
TOTAL AREA(ACRES) = 58.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 4961.00 TO NODE 2000.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 708.50 DOWNSTREAM(FEET) = 708.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 29.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.70  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 70.99  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 24.44  
LONGEST FLOWPATH FROM NODE 2030.00 TO NODE 2000.00 = 3576.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 58.7 TC(MIN.) = 24.44  
PEAK FLOW RATE(CFS) = 70.99

=====

END OF RATIONAL METHOD ANALYSIS







\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 4000 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-4000.DAT  
TIME/DATE OF STUDY: 14:26 12/09/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 4932.00 TO NODE 4930.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00

UPSTREAM ELEVATION(FEET) = 723.10

DOWNSTREAM ELEVATION(FEET) = 722.20

ELEVATION DIFFERENCE(FEET) = 0.90

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.867

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 65.88

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 2.07

TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 2.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 4930.00 TO NODE 4000.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 722.20 DOWNSTREAM ELEVATION(FEET) = 718.80

STREET LENGTH(FEET) = 190.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.11

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.32

HALFSTREET FLOOD WIDTH(FEET) = 9.67

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.96

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.94

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STREET FLOW TRAVEL TIME(MIN.) = 1.07 Tc(MIN.) = 3.94

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.25 SUBAREA RUNOFF(CFS) = 2.07

TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 4.15

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 10.97

FLOW VELOCITY(FEET/SEC.) = 3.14 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.09

LONGEST FLOWPATH FROM NODE 4932.00 TO NODE 4000.00 = 275.00 FEET.

=====  
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 0.5 TC(MIN.) = 3.94

PEAK FLOW RATE(CFS) = 4.15  
=====

=====  
END OF RATIONAL METHOD ANALYSIS

↑



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUB-BASIN 5000 \*  
\* \*  
\*\*\*\*\*

FILE NAME: P-5000.DAT  
TIME/DATE OF STUDY: 14:27 12/09/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 4928.00 TO NODE 4926.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00

UPSTREAM ELEVATION(FEET) = 718.80

DOWNSTREAM ELEVATION(FEET) = 717.00

ELEVATION DIFFERENCE(FEET) = 1.80

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.535

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 81.76

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.83

TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 4926.00 TO NODE 5000.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 717.00 DOWNSTREAM ELEVATION(FEET) = 711.00

STREET LENGTH(FEET) = 955.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.80

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.41

HALFSTREET FLOOD WIDTH(FEET) = 14.39

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.20

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.91

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STREET FLOW TRAVEL TIME(MIN.) = 7.25 Tc(MIN.) = 9.78  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.981

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 1.42 SUBAREA RUNOFF(CFS) = 7.64

TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 8.18

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 17.80

FLOW VELOCITY(FEET/SEC.) = 2.49 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.20

\*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,

AND L = 955.0 FT WITH ELEVATION-DROP = 6.0 FT, IS 11.8 CFS,

WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 5000.00

LONGEST FLOWPATH FROM NODE 4928.00 TO NODE 5000.00 = 1040.00 FEET.

=====  
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 1.5 TC(MIN.) = 9.78

PEAK FLOW RATE(CFS) = 8.18  
=====

=====  
END OF RATIONAL METHOD ANALYSIS  
=====

↑



| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 1110         | 1100 | 2    | 1128.5           | 1123             | 57               | 0.36        | 0.44          |                |      |   |   |
| 1100         | 1015 | 5    | 1123             | 715              | 3490             |             |               | MTN            |      |   |   |
| 1100         | 1015 | 8    |                  |                  |                  | 0.34        | 50.24         |                |      |   |   |
| 1015         | 1015 | 10   |                  |                  |                  |             |               | SAVE TO BANK 1 |      |   |   |
| 1090         | 1080 | 2    | 1246             | 1232             | 100              | 0.36        | 0.23          |                |      |   |   |
| 1080         | 1050 | 5    | 1232             | 880              | 1411             |             |               | MTN            |      |   |   |
| 1080         | 1050 | 8    |                  |                  |                  | 0.36        | 20.39         |                |      |   |   |
| 1050         | 1050 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 1070         | 1060 | 2    | 1145             | 1137             | 85               | 0.36        | 0.29          |                |      |   |   |
| 1060         | 1050 | 5    | 1137             | 880              | 909              |             |               | MTN            |      |   |   |
| 1060         | 1050 | 8    |                  |                  |                  | 0.36        | 6.46          |                |      |   |   |
| 1050         | 1050 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 1050         | 1020 | 5    | 880              | 763              | 1286             |             |               | MTN            |      |   |   |
| 1050         | 1020 | 8    |                  |                  |                  | 0.36        | 13.54         |                |      |   |   |
| 1020         | 1020 | 1    |                  |                  |                  |             |               | 1 OF 2         |      |   |   |
| 1040         | 1030 | 2    | 781              | 775              | 66               | 0.48        | 0.60          |                |      |   |   |
| 1030         | 1020 | 5    | 775              | 763              | 269              |             |               | VALLEY         |      |   |   |
| 1030         | 1020 | 8    |                  |                  |                  | 0.45        | 2.06          |                |      |   |   |
| 1020         | 1020 | 1    |                  |                  |                  |             |               | 2 OF 2         |      |   |   |
| 1020         | 1015 | 5    | 763              | 715              | 1236             |             |               | VALLEY         |      |   |   |
| 1020         | 1015 | 8    |                  |                  |                  | 0.35        | 13.75         |                |      |   |   |
| 1015         | 1015 | 11   |                  |                  |                  |             |               | ADD BANK 1     |      |   |   |
| 1015         | 1015 | 12   |                  |                  |                  |             |               | CLEAR BANK 1   |      |   |   |
| 1015         | 4942 | 5    | 715              | 698              | 936              |             |               | MTN            |      |   |   |
| 1015         | 4942 | 8    |                  |                  |                  | 0.32        | 22.83         |                |      |   |   |
| 4942         | 4942 | 1    |                  |                  |                  |             |               | 1 OF 4         |      |   |   |
| 4958         | 4956 | 2    | 714              | 713.3            | 80               | 0.9         | 0.10          |                |      |   |   |
| 4956         | 4954 | 6    | 713.3            | 710              | 475              | 0.9         | 0.75          |                |      |   |   |
| 4954         | 4942 | 3    | 704              | 695              | 590              |             |               |                |      |   |   |
| 4942         | 4942 | 1    |                  |                  |                  |             |               | 2 OF 4         |      |   |   |
| 4948         | 4946 | 2    | 710              | 708              | 80               | 0.9         | 0.09          |                |      |   |   |
| 4946         | 4944 | 6    | 708              | 701              | 520              | 0.9         | 0.72          |                |      |   |   |
| 4944         | 4942 | 3    | 696              | 695              | 80               |             |               |                |      |   |   |
| 4942         | 4942 | 1    |                  |                  |                  |             |               | 3 OF 4         |      |   |   |
| 4952         | 4950 | 2    | 710              | 708.5            | 85               | 0.9         | 0.10          |                |      |   |   |





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* NEWLAND SIERRA - PROPOSED HYDROLOGY \*
  - \* NO DETENTION \*
  - \* SUB-BASIN 6000 \*
- \*\*\*\*\*

FILE NAME: P-49-4.DAT  
TIME/DATE OF STUDY: 15:41 12/08/2016

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 39.0                   | 20.0                          | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1110.00 TO NODE 1100.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3600

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 57.00

UPSTREAM ELEVATION(FEET) = 1128.50

DOWNSTREAM ELEVATION(FEET) = 1123.00

ELEVATION DIFFERENCE(FEET) = 5.50

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.724

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.46

TOTAL AREA(ACRES) = 0.44 TOTAL RUNOFF(CFS) = 1.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 1100.00 TO NODE 1015.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1123.00 DOWNSTREAM(FEET) = 715.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 3490.00 CHANNEL SLOPE = 0.1169

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1127 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 1.46

FLOW VELOCITY(FEET/SEC) = 2.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 27.28 Tc(MIN.) = 32.00

LONGEST FLOWPATH FROM NODE 1110.00 TO NODE 1015.00 = 3547.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1100.00 TO NODE 1015.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.785

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3400

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.3402

SUBAREA AREA(ACRES) = 50.24 SUBAREA RUNOFF(CFS) = 47.57

TOTAL AREA(ACRES) = 50.7 TOTAL RUNOFF(CFS) = 48.01

TC(MIN.) = 32.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1090.00 TO NODE 1080.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1246.00  
DOWNSTREAM ELEVATION(FEET) = 1232.00  
ELEVATION DIFFERENCE(FEET) = 14.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.183  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.041  
SUBAREA RUNOFF(CFS) = 0.67  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 0.67

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1080.00 TO NODE 1050.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1232.00 DOWNSTREAM(FEET) = 880.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1411.00 CHANNEL SLOPE = 0.2495  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1798 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.67  
FLOW VELOCITY(FEET/SEC) = 2.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 9.90 Tc(MIN.) = 16.09  
LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 1050.00 = 1511.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1080.00 TO NODE 1050.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.340  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600  
SUBAREA AREA(ACRES) = 20.39 SUBAREA RUNOFF(CFS) = 31.86  
TOTAL AREA(ACRES) = 20.6 TOTAL RUNOFF(CFS) = 32.22  
TC(MIN.) = 16.09

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1050.00 TO NODE 1050.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.09  
RAINFALL INTENSITY(INCH/HR) = 4.34  
TOTAL STREAM AREA(ACRES) = 20.62  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 32.22

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1070.00 TO NODE 1060.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1145.00  
DOWNSTREAM ELEVATION(FEET) = 1137.00  
ELEVATION DIFFERENCE(FEET) = 8.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.817  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.364  
SUBAREA RUNOFF(CFS) = 0.87  
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.87

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1060.00 TO NODE 1050.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1137.00 DOWNSTREAM(FEET) = 880.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 909.00 CHANNEL SLOPE = 0.2827  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1907 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.87  
FLOW VELOCITY(FEET/SEC) = 2.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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TRAVEL TIME(MIN.) = 6.20 Tc(MIN.) = 12.01  
LONGEST FLOWPATH FROM NODE 1070.00 TO NODE 1050.00 = 994.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1060.00 TO NODE 1050.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.239  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600  
SUBAREA AREA(ACRES) = 6.46 SUBAREA RUNOFF(CFS) = 12.18  
TOTAL AREA(ACRES) = 6.8 TOTAL RUNOFF(CFS) = 12.73  
TC(MIN.) = 12.01

\*\*\*\*\*

FLOW PROCESS FROM NODE 1050.00 TO NODE 1050.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.01  
RAINFALL INTENSITY(INCH/HR) = 5.24  
TOTAL STREAM AREA(ACRES) = 6.75  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.73

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 32.22        | 16.09     | 4.340                 | 20.62       |
| 2             | 12.73        | 12.01     | 5.239                 | 6.75        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 36.79        | 12.01     | 5.239                 |
| 2             | 42.76        | 16.09     | 4.340                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 42.76 Tc(MIN.) = 16.09  
TOTAL AREA(ACRES) = 27.4

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LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 1050.00 = 1511.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1050.00 TO NODE 1020.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 880.00 DOWNSTREAM(FEET) = 763.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1286.00 CHANNEL SLOPE = 0.0910  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0910 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 42.76  
FLOW VELOCITY(FEET/SEC) = 5.90 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.63 Tc(MIN.) = 19.72  
LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 1020.00 = 2797.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1050.00 TO NODE 1020.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.806  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600  
SUBAREA AREA(ACRES) = 13.54 SUBAREA RUNOFF(CFS) = 18.55  
TOTAL AREA(ACRES) = 40.9 TOTAL RUNOFF(CFS) = 56.05  
TC(MIN.) = 19.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 1020.00 TO NODE 1020.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 19.72  
RAINFALL INTENSITY(INCH/HR) = 3.81  
TOTAL STREAM AREA(ACRES) = 40.91  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 56.05

\*\*\*\*\*

FLOW PROCESS FROM NODE 1040.00 TO NODE 1030.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

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\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4800

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 66.00

UPSTREAM ELEVATION(FEET) = 781.00

DOWNSTREAM ELEVATION(FEET) = 775.00

ELEVATION DIFFERENCE(FEET) = 6.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.344

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 2.66

TOTAL AREA(ACRES) = 0.60 TOTAL RUNOFF(CFS) = 2.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 1030.00 TO NODE 1020.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 775.00 DOWNSTREAM(FEET) = 763.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 269.00 CHANNEL SLOPE = 0.0446

CHANNEL FLOW THRU SUBAREA(CFS) = 2.66

FLOW VELOCITY(FEET/SEC) = 3.86 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 1.16 Tc(MIN.) = 5.51

LONGEST FLOWPATH FROM NODE 1040.00 TO NODE 1020.00 = 335.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1030.00 TO NODE 1020.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.666

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.4568

SUBAREA AREA(ACRES) = 2.06 SUBAREA RUNOFF(CFS) = 8.03

TOTAL AREA(ACRES) = 2.7 TOTAL RUNOFF(CFS) = 10.53

TC(MIN.) = 5.51

\*\*\*\*\*

FLOW PROCESS FROM NODE 1020.00 TO NODE 1020.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:



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TIME OF CONCENTRATION(MIN.) = 5.51  
RAINFALL INTENSITY(INCH/HR) = 8.67  
TOTAL STREAM AREA(ACRES) = 2.66  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.53

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 56.05        | 19.72     | 3.806                 | 40.91       |
| 2             | 10.53        | 5.51      | 8.666                 | 2.66        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 35.14        | 5.51      | 8.666                 |
| 2             | 60.67        | 19.72     | 3.806                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 60.67 Tc(MIN.) = 19.72  
TOTAL AREA(ACRES) = 43.6  
LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 1020.00 = 2797.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1020.00 TO NODE 1015.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 763.00 DOWNSTREAM(FEET) = 715.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1236.00 CHANNEL SLOPE = 0.0388  
CHANNEL FLOW THRU SUBAREA(CFS) = 60.67  
FLOW VELOCITY(FEET/SEC) = 8.07 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 22.27  
LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 1015.00 = 4033.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1020.00 TO NODE 1015.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.518  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3621

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SUBAREA AREA(ACRES) = 13.75 SUBAREA RUNOFF(CFS) = 16.93  
TOTAL AREA(ACRES) = 57.3 TOTAL RUNOFF(CFS) = 73.02  
TC(MIN.) = 22.27

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 73.02        | 22.27     | 3.518                 | 57.32       |

LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 1015.00 = 4033.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 48.01        | 32.00     | 2.785                 | 50.68       |

LONGEST FLOWPATH FROM NODE 1110.00 TO NODE 1015.00 = 3547.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 106.44       | 22.27     | 3.518                 |
| 2             | 105.82       | 32.00     | 2.785                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 106.44 Tc(MIN.) = 22.27  
TOTAL AREA(ACRES) = 108.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 1015.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 4942.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 715.00 DOWNSTREAM(FEET) = 698.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 936.00 CHANNEL SLOPE = 0.0182  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0182 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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CHANNEL FLOW THRU SUBAREA(CFS) = 106.44  
FLOW VELOCITY(FEET/SEC) = 3.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.37 Tc(MIN.) = 26.64  
LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 4942.00 = 4969.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 1015.00 TO NODE 4942.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.134  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3463  
SUBAREA AREA(ACRES) = 22.83 SUBAREA RUNOFF(CFS) = 22.90  
TOTAL AREA(ACRES) = 130.8 TOTAL RUNOFF(CFS) = 141.99  
TC(MIN.) = 26.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 4942.00 TO NODE 4942.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 26.64  
RAINFALL INTENSITY(INCH/HR) = 3.13  
TOTAL STREAM AREA(ACRES) = 130.83  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 141.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 4958.00 TO NODE 4956.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 714.00  
DOWNSTREAM ELEVATION(FEET) = 713.30  
ELEVATION DIFFERENCE(FEET) = 0.70  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.946  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 61.25  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 4956.00 TO NODE 4954.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 713.30 DOWNSTREAM ELEVATION(FEET) = 710.00  
STREET LENGTH(FEET) = 475.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.44  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.37  
HALFSTREET FLOOD WIDTH(FEET) = 12.33  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.10  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.78  
STREET FLOW TRAVEL TIME(MIN.) = 3.78 Tc(MIN.) = 6.72  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.618

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.75 SUBAREA RUNOFF(CFS) = 5.14  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 5.83

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 15.27  
FLOW VELOCITY(FEET/SEC.) = 2.38 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.03  
LONGEST FLOWPATH FROM NODE 4958.00 TO NODE 4954.00 = 555.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4954.00 TO NODE 4942.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 704.00 DOWNSTREAM(FEET) = 695.00  
FLOW LENGTH(FEET) = 590.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.87  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.83  
PIPE TRAVEL TIME(MIN.) = 1.43 Tc(MIN.) = 8.15  
LONGEST FLOWPATH FROM NODE 4958.00 TO NODE 4942.00 = 1145.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4942.00 TO NODE 4942.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.15  
RAINFALL INTENSITY(INCH/HR) = 6.73  
TOTAL STREAM AREA(ACRES) = 0.85  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 4948.00 TO NODE 4946.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 710.00  
DOWNSTREAM ELEVATION(FEET) = 708.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.373  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 4946.00 TO NODE 4944.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

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UPSTREAM ELEVATION(FEET) = 708.00 DOWNSTREAM ELEVATION(FEET) = 701.00  
STREET LENGTH(FEET) = 520.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.55  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 10.90  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.72  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.94  
STREET FLOW TRAVEL TIME(MIN.) = 3.19 Tc(MIN.) = 5.56  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.614

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.72 SUBAREA RUNOFF(CFS) = 5.58  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 6.28

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.77  
FLOW VELOCITY(FEET/SEC.) = 3.12 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.25  
LONGEST FLOWPATH FROM NODE 4948.00 TO NODE 4944.00 = 600.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4944.00 TO NODE 4942.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 696.00 DOWNSTREAM(FEET) = 695.00  
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.49  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.28  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 5.76  
LONGEST FLOWPATH FROM NODE 4948.00 TO NODE 4942.00 = 680.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4942.00 TO NODE 4942.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.76  
RAINFALL INTENSITY(INCH/HR) = 8.41  
TOTAL STREAM AREA(ACRES) = 0.81  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 4952.00 TO NODE 4950.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 710.00  
DOWNSTREAM ELEVATION(FEET) = 708.50  
ELEVATION DIFFERENCE(FEET) = 1.50  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.605  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 76.47  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 4950.00 TO NODE 4942.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 708.50 DOWNSTREAM ELEVATION(FEET) = 701.00  
STREET LENGTH(FEET) = 520.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 39.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.96  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.24  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.86  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.01  
STREET FLOW TRAVEL TIME(MIN.) = 3.03 Tc(MIN.) = 5.63  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.541

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.81 SUBAREA RUNOFF(CFS) = 6.23  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 6.99

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.18  
FLOW VELOCITY(FEET/SEC.) = 3.29 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.35  
LONGEST FLOWPATH FROM NODE 4952.00 TO NODE 4942.00 = 605.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4942.00 TO NODE 4942.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 4  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 4 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.63  
RAINFALL INTENSITY(INCH/HR) = 8.54  
TOTAL STREAM AREA(ACRES) = 0.91  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.99

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 141.99       | 26.64     | 3.134                 | 130.83      |
| 2             | 5.83         | 8.15      | 6.726                 | 0.85        |
| 3             | 6.28         | 5.76      | 8.414                 | 0.81        |
| 4             | 6.99         | 5.63      | 8.541                 | 0.91        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO



CONFLUENCE FORMULA USED FOR 4 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 47.17        | 5.63      | 8.541                 |
| 2             | 48.01        | 5.76      | 8.414                 |
| 3             | 59.82        | 8.15      | 6.726                 |
| 4             | 149.61       | 26.64     | 3.134                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 149.61 Tc(MIN.) = 26.64  
TOTAL AREA(ACRES) = 133.4  
LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 4942.00 = 4969.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4942.00 TO NODE 6000.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 695.00 DOWNSTREAM(FEET) = 694.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 54.0 INCH PIPE IS 39.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.87  
ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 149.61  
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 26.82  
LONGEST FLOWPATH FROM NODE 1090.00 TO NODE 6000.00 = 5094.00 FEET.

=====

END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 133.4 TC(MIN.) = 26.82  
PEAK FLOW RATE(CFS) = 149.61

=====

-----

END OF RATIONAL METHOD ANALYSIS



# APPENDIX A

AES  
Rational Method Hydrology

Proposed Condition

BASIN C





| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2681         | 2676 | 3    | 1362             | 1359             | 80               |             |               |                |      |   |   |
| 2676         | 2676 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2680         | 2679 | 2    | 1447             | 1443             | 75               | 0.52        | 0.13          |                |      |   |   |
| 2679         | 2678 | 6    | 1443             | 1369.5           | 730              | 0.52        | 1.38          | One side       |      |   |   |
| 2678         | 2677 | 3    | 1365             | 1364             | 40               |             |               |                |      |   |   |
| 2677         | 2676 | 3    | 1364             | 1359             | 50               |             |               |                |      |   |   |
| 2676         | 2676 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2676         | 2672 | 3    | 1359             | 1323             | 320              |             |               |                |      |   |   |
| 2672         | 2672 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2675         | 2674 | 2    | 1427             | 1420             | 75               | 0.35        | 0.05          |                |      |   |   |
| 2674         | 2673 | 5    | 1420             | 1330             | 440              |             |               |                |      |   |   |
| 2674         | 2673 | 8    |                  |                  |                  | 0.35        | 2.36          |                |      |   |   |
| 2673         | 2672 | 3    | 1324             | 1323             | 20               |             |               |                |      |   |   |
| 2672         | 2672 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2672         | 2651 | 3    | 1323             | 1309             | 250              |             |               |                |      |   |   |
| 2651         | 2651 | 10   |                  |                  |                  |             |               | Save to bank 1 |      |   |   |
| 2671         | 2670 | 2    | 1445             | 1420             | 100              | 0.25        | 0.27          |                |      |   |   |
| 2670         | 2669 | 5    | 1420             | 1385             | 280              |             |               |                |      |   |   |
| 2670         | 2669 | 8    |                  |                  |                  | 0.29        | 4.07          |                |      |   |   |
| 2669         | 2668 | 3    | 1379             | 1375             | 415              |             |               |                |      |   |   |
| 2668         | 2663 | 5    | 1375             | 1348             | 600              |             |               |                |      |   |   |
| 2663         | 2663 | 1    |                  |                  |                  |             |               | 1 of 3         |      |   |   |
| 2667         | 2666 | 2    | 1420             | 1405             | 100              | 0.35        | 0.19          |                |      |   |   |
| 2666         | 2663 | 5    | 1405             | 1348             | 680              |             |               |                |      |   |   |
| 2666         | 2663 | 8    |                  |                  |                  | 0.35        | 2.98          |                |      |   |   |
| 2663         | 2663 | 1    |                  |                  |                  |             |               | 2 of 3         |      |   |   |
| 2665.5       | 2665 | 2    | 1363             | 1361             | 80               | 0.45        | 0.25          |                |      |   |   |
| 2665         | 2664 | 6    | 1361             | 1350             | 550              | 0.46        | 4.22          | Two sides      |      |   |   |
| 2664         | 2663 | 3    | 1344             | 1342             | 110              |             |               |                |      |   |   |
| 2663         | 2663 | 1    |                  |                  |                  |             |               | 3 of 3         |      |   |   |
| 2663         | 2657 | 3    | 1342             | 1312             | 372              |             |               |                |      |   |   |
| 2657         | 2657 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2662         | 2661 | 2    | 1400             | 1399             | 66.67            | 0.45        | 0.16          |                |      |   |   |
| 2661         | 2660 | 6    | 1399             | 1355             | 935              | 0.45        | 3.60          | One side       |      |   |   |
| 2660         | 2659 | 3    | 1349             | 1348.4           | 60               |             |               |                |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2659         | 2658   | 5    | 1348.4           | 1347.6           | 80               | 0.25        | 0.17          |                |      |   |   |
| 2658         | 2657   | 3    | 1342             | 1313             | 540              |             |               |                |      |   |   |
| 2657         | 2657   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2657         | 2650.6 | 3    | 1312             | 1308             | 100              |             |               |                |      |   |   |
| 2650.6       | 2650.6 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2650.9       | 2650.8 | 2    | 1356             | 1354             | 80               | 0.45        | 0.10          |                |      |   |   |
| 2650.8       | 2650.7 | 6    | 1354             | 1315             | 690              | 0.45        | 3.79          | One side       |      |   |   |
| 2650.7       | 2650.6 | 3    | 1309             | 1308             | 75               |             |               |                |      |   |   |
| 2650.6       | 2650.6 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2650.6       | 2650   | 3    | 1308             | 1298.2           | 500              |             |               |                |      |   |   |
| 2650         | 2650   | 10   |                  |                  |                  |             |               | Save to bank 2 |      |   |   |
| 2656         | 2655   | 2    | 1390             | 1389.5           | 55               | 0.52        | 0.15          |                |      |   |   |
| 2655         | 2654   | 6    | 1389.5           | 1315             | 970              | 0.52        | 1.50          | One side       |      |   |   |
| 2654         | 2653   | 3    | 1309             | 1305             | 50               |             |               |                |      |   |   |
| 2653         | 2652   | 5    | 1305             | 1304.7           | 30               |             | 3.18          |                |      |   |   |
| 2652         | 2651   | 3    | 1299             | 1298.5           | 40               |             |               |                |      |   |   |
| 2651         | 2651   | 11   |                  |                  |                  |             |               | Add bank 1     |      |   |   |
| 2651         | 2651   | 12   |                  |                  |                  |             |               | Clear bank 1   |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2651         | 2650   | 3    | 1298.5           | 1298.2           | 30               |             |               |                |      |   |   |
| 2650         | 2650   | 11   |                  |                  |                  |             |               | Add bank 2     |      |   |   |
| 2650         | 2650   | 12   |                  |                  |                  |             |               | Clear bank 2   |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2650         | 2635   | 3    | 1298.2           | 1292.5           | 160              |             |               |                |      |   |   |
| 2635         | 2635   | 10   |                  |                  |                  |             |               | Save to bank 1 |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2649         | 2648   | 2    | 1400             | 1398             | 80               | 0.45        | 0.25          |                |      |   |   |
| 2648         | 2647   | 6    | 1398             | 1380             | 720              | 0.47        | 5.78          | One side       |      |   |   |
| 2647         | 2643   | 3    | 1374             | 1361             | 300              |             |               |                |      |   |   |
| 2643         | 2643   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2646         | 2645   | 2    | 1395             | 1393             | 80               | 0.45        | 0.08          |                |      |   |   |
| 2645         | 2644   | 6    | 1393             | 1368             | 730              | 0.45        | 4.06          | Two sides      |      |   |   |
| 2644         | 2643   | 3    | 1362             | 1361             | 50               |             |               |                |      |   |   |
| 2643         | 2643   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2643         | 2640   | 3    | 1361             | 1356             | 200              |             |               |                |      |   |   |
| 2640         | 2640   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
|              |        |      |                  |                  |                  |             |               |                |      |   |   |
| 2642         | 2641   | 2    | 1378             | 1376             | 81.58            | 0.45        | 0.22          |                |      |   |   |
| 2641         | 2640   | 6    | 1376             | 1362             | 610              | 0.47        | 5.99          | Two sides      |      |   |   |



| Node to Node |      | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |      |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2640         | 2640 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2640         | 2639 | 3    | 1362             | 1342             | 210              |             |               |                |      |   |   |
| 2639         | 2638 | 3    | 1342             | 1314             | 380              |             |               |                |      |   |   |
| 2638         | 2637 | 3    | 1314             | 1295             | 380              |             |               |                |      |   |   |
| 2637         | 2636 | 5    | 1295             | 1293             | 200              | 0.52        | 1.02          |                |      |   |   |
| 2636         | 2635 | 3    | 1293             | 1292.5           | 20               |             |               |                |      |   |   |
| 2635         | 2635 | 11   |                  |                  |                  |             |               | Add bank 1     |      |   |   |
| 2635         | 2635 | 12   |                  |                  |                  |             |               | Clear bank 1   |      |   |   |
| 2635         | 2631 | 3    | 1292.5           | 1278.5           | 195              |             |               |                |      |   |   |
| 2631         | 2631 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2634         | 2633 | 2    | 1435             | 1405             | 50               | 0.35        | 0.07          |                |      |   |   |
| 2633         | 2632 | 5    | 1405             | 1285             | 540              | 0.35        | 4.39          |                |      |   |   |
| 2632         | 2631 | 3    | 1279             | 1278.5           | 50               |             |               |                |      |   |   |
| 2631         | 2631 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2631         | 2627 | 3    | 1278.5           | 1253             | 600              |             |               |                |      |   |   |
| 2627         | 2627 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2630         | 2629 | 2    | 1390             | 1352             | 100              | 0.25        | 0.18          |                |      |   |   |
| 2629         | 2628 | 5    | 1352             | 1262             | 1370             | 0.25        | 4.60          |                |      |   |   |
| 2628         | 2627 | 3    | 1256             | 1253             | 125              |             |               |                |      |   |   |
| 2627         | 2627 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2627         | 2623 | 3    | 1253             | 1197             | 1335             |             |               |                |      |   |   |
| 2623         | 2623 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2626         | 2625 | 2    | 1330             | 1280             | 80               | 0.25        | 0.19          |                |      |   |   |
| 2625         | 2624 | 5    | 1280             | 1207             | 440              | 0.25        | 4.59          |                |      |   |   |
| 2624         | 2623 | 3    | 1201             | 1197             | 125              |             |               |                |      |   |   |
| 2623         | 2623 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2623         | 287  | 3    | 1196             | 1185.5           | 130              |             |               |                |      |   |   |
| 287          | 287  | 10   |                  |                  |                  |             |               | Save to bank 1 |      |   |   |
| 2622         | 2621 | 2    | 1435             | 1395             | 100              | 0.35        | 0.27          |                |      |   |   |
| 2621         | 2620 | 5    | 1395             | 1275             | 645              |             |               |                |      |   |   |
| 2621         | 2620 | 8    |                  |                  |                  | 0.35        | 3.37          |                |      |   |   |
| 2620         | 2616 | 3    | 1261             | 1231             | 380              |             |               |                |      |   |   |
| 2616         | 2616 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2619         | 2618 | 2    | 1249             | 1247.7           | 65               | 0.45        | 0.17          |                |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2618         | 2617   | 5    | 1247.7           | 1239             | 420              | 0.45        | 3.59          |                |      |   |   |
| 2617         | 2616   | 3    | 1236             | 1231             | 415              |             |               |                |      |   |   |
| 2616         | 2616   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2616         | 2616.8 | 3    | 1231             | 1223             | 540              |             |               |                |      |   |   |
| 2616.8       | 2616.8 | 10   |                  |                  |                  |             |               | Save to Bank 2 |      |   |   |
| 2611         | 2610   | 2    | 1292             | 1290             | 80               | 0.52        | 0.12          |                |      |   |   |
| 2610         | 2609   | 6    | 1290             | 1265             | 435              | 0.48        | 1.90          | One side       |      |   |   |
| 2609         | 2606.2 | 3    | 1259             | 1241             | 275              |             |               |                |      |   |   |
| 2606.2       | 2606.2 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2606.6       | 2606.4 | 2    | 1267             | 1265             | 80               | 0.45        | 0.13          |                |      |   |   |
| 2606.4       | 2606.2 | 6    | 1265             | 1248             | 215              | 0.45        | 0.92          | One side       |      |   |   |
| 2606.2       | 2606.2 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2606.2       | 2606   | 3    | 1242             | 1232             | 170              |             |               |                |      |   |   |
| 2606         | 2606   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2608         | 2607   | 2    | 1254             | 1252             | 80               | 0.45        | 0.12          |                |      |   |   |
| 2607         | 2606   | 6    | 1252             | 1238             | 170              | 0.45        | 0.63          | One side       |      |   |   |
| 2606         | 2606   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2606         | 2602   | 3    | 1232             | 1226             | 150              |             |               |                |      |   |   |
| 2602         | 2602   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2605         | 2604   | 2    | 1244             | 1242             | 80               | 0.45        | 0.12          |                |      |   |   |
| 2604         | 2602   | 6    | 1242             | 1226             | 495              | 0.45        | 2.00          | One side       |      |   |   |
| 2602         | 2602   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2602         | 298    | 5    | 1226             | 1222             | 130              | 0.45        | 0.22          |                |      |   |   |
| 298          | 2616.8 | 3    | 1216             | 1214             | 160              |             |               |                |      |   |   |
| 2616.8       | 2616.8 | 11   |                  |                  |                  |             |               | Add Bank 2     |      |   |   |
| 2616.8       | 2616.8 | 12   |                  |                  |                  |             |               | Clear Bank 2   |      |   |   |
| 2616.8       | 2612   | 3    | 1214             | 1212             | 130              |             |               |                |      |   |   |
| 2612         | 2612   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2615         | 2614   | 2    | 1275             | 1230             | 100              | 0.25        | 0.22          |                |      |   |   |
| 2614         | 2613   | 5    | 1230             | 1219             | 260              |             |               |                |      |   |   |
| 2614         | 2613   | 8    |                  |                  |                  | 0.25        | 0.67          |                |      |   |   |
| 2613         | 2612   | 3    | 1213             | 1212             | 50               |             |               |                |      |   |   |
| 2612         | 2612   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |



| Node to Node |       | Code | Elev 1<br>(feet)         | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK                               |   |   |  |
|--------------|-------|------|--------------------------|------------------|------------------|-------------|---------------|----------------|------------------------------------|---|---|--|
|              |       |      |                          |                  |                  |             |               |                | 1                                  | 2 | 3 |  |
| 2612         | 292   | 3    | 1212                     | 1196             | 515              |             |               |                |                                    |   |   |  |
| 292          | 292   | 10   |                          |                  |                  |             |               | Save to bank 2 |                                    |   |   |  |
| 297          | 296   | 2    | 1236                     | 1234             | 80               | 0.45        | 0.15          |                |                                    |   |   |  |
| 296          | 295   | 6    | 1236                     | 1215             | 475              | 0.45        | 2.67          | One side       |                                    |   |   |  |
| 295          | 294   | 3    | 1209                     | 1206             | 125              |             |               |                |                                    |   |   |  |
| 294          | 294   | 10   |                          |                  |                  |             |               | Save to Bank 3 |                                    |   |   |  |
| 294.9        | 294.8 | 2    | 1245                     | 1243             | 80.00            | 0.45        | 0.14          |                |                                    |   |   |  |
| 294.8        | 294.7 | 6    | 1243                     | 1238             | 270              | 0.45        | 1.09          | Two sides      |                                    |   |   |  |
| 294.7        | 294.1 | 3    | 1236                     | 1223             | 605              |             |               |                |                                    |   |   |  |
| 294.1        | 294.1 | 1    |                          |                  |                  |             |               | 1 of 2         |                                    |   |   |  |
| 294.6        | 294.5 | 2    | 1236                     | 1234             | 80               | 0.45        | 0.10          |                |                                    |   |   |  |
| 294.5        | 294.4 | 6    | 1234                     | 1233             | 100              | 0.45        | 0.89          | 2 sides        |                                    |   |   |  |
| 294.4        | 294.1 | 3    | 1227                     | 1223             | 350              |             |               |                |                                    |   |   |  |
| 294.1        | 294.1 | 1    |                          |                  |                  |             |               | 2 of 2         |                                    |   |   |  |
| 294.1        | 294   | 3    | 1223                     | 1204             | 750              |             |               |                |                                    |   |   |  |
| 294          | 294   | 11   |                          |                  |                  |             |               | add bank 3     |                                    |   |   |  |
| 294          | 294   | 12   |                          |                  |                  |             |               | clear bank 3   |                                    |   |   |  |
| 294          | 293.5 | 3    | 1204                     | 1200             | 150              |             |               |                |                                    |   |   |  |
| 293.5        | 293   | 5    | 1200                     | 1199             | 100              | 0.45        | 0.21          |                |                                    |   |   |  |
| 293          | 292   | 3    | 1199                     | 1196             | 50               |             |               |                |                                    |   |   |  |
| 292          | 292   | 11   |                          |                  |                  |             |               | add bank 2     |                                    |   |   |  |
| 292          | 292   | 12   |                          |                  |                  |             |               | clear bank 2   |                                    |   |   |  |
| 292          | 288   | 3    | 1196                     | 1189             | 270              |             |               |                |                                    |   |   |  |
| 288          | 288   | 1    |                          |                  |                  |             |               | 1 of 2         |                                    |   |   |  |
| 291          | 290   | 2    | 1300                     | 1270             | 100              | 0.25        | 0.20          |                |                                    |   |   |  |
| 290          | 289   | 5    | 1270                     | 1195             | 840              |             |               |                |                                    |   |   |  |
| 290          | 289   | 8    |                          |                  |                  | 0.25        | 2.84          |                |                                    |   |   |  |
| 289          | 288   | 3    | 1189                     | 1187             | 170              |             |               |                |                                    |   |   |  |
| 288          | 288   | 1    |                          |                  |                  |             |               | 2 of 2         |                                    |   |   |  |
| 288          | 287   | 3    | 1187                     | 1185.5           | 275              |             |               |                |                                    |   |   |  |
| 287          | 287   | 11   |                          |                  |                  |             |               | add bank 1     |                                    |   |   |  |
| 287          | 287   | 12   |                          |                  |                  |             |               | clear bank 1   |                                    |   |   |  |
| 287          | 246   | 3    | 1185.5                   | 1178             | 480              |             |               |                |                                    |   |   |  |
| 246          | 246   | 7    | Tc=16.15 A=99.5 Q=138.38 |                  |                  |             |               |                | Allow Q10 to pass, divert higher Q |   |   |  |
| 246          | 246   | 10   |                          |                  |                  |             |               | save to bank 1 |                                    |   |   |  |





| Node to Node |       | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|-------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |       |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 286          | 285   | 2    | 1218             | 1216             | 80               | 0.45        | 0.13          |                |      |   |   |
| 285          | 284   | 6    | 1216             | 1203             | 380              | 0.45        | 2.74          | one side       |      |   |   |
| 284          | 259   | 3    | 1197             | 1195             | 180              |             |               |                |      |   |   |
| 259          | 259   | 10   |                  |                  |                  |             |               | save to bank 2 |      |   |   |
| 283          | 282   | 2    | 1268             | 1266             | 80               | 0.46        | 0.23          |                |      |   |   |
| 282          | 281   | 6    | 1266             | 1262             | 220              | 0.45        | 2.06          | 2 sides        |      |   |   |
| 281          | 280.6 | 3    | 1256             | 1241             | 270              |             |               |                |      |   |   |
| 280.6        | 280.6 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 280.9        | 280.8 | 2    | 1269             | 1266             | 80               | 0.45        | 0.16          |                |      |   |   |
| 280.8        | 280.7 | 6    | 1266             | 1248             | 300              | 0.45        | 0.56          | 1 side         |      |   |   |
| 280.7        | 280.6 | 3    | 1242             | 1241             | 40               |             |               |                |      |   |   |
| 280.6        | 280.6 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 280.6        | 277   | 3    | 1241             | 1238             | 70               |             |               |                |      |   |   |
| 277          | 277   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 280          | 279   | 2    | 1257             | 1255             | 80               | 0.45        | 0.24          |                |      |   |   |
| 279          | 278   | 6    | 1255             | 1244             | 340              | 0.45        | 2.58          | 2 sides        |      |   |   |
| 278          | 277   | 3    | 1239             | 1238             | 50               |             |               |                |      |   |   |
| 277          | 277   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 277          | 275   | 3    | 1238             | 1228             | 180              |             |               |                |      |   |   |
| 275          | 275   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 275.3        | 275.2 | 2    | 1247             | 1243             | 80               | 0.45        | 0.14          |                |      |   |   |
| 275.2        | 275.1 | 6    | 1243             | 1235             | 165              | 0.45        | 0.29          | 1 side         |      |   |   |
| 275.1        | 275   | 3    | 1229             | 1228             | 40               |             |               |                |      |   |   |
| 275          | 275   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 275          | 293.2 | 3    | 1228             | 1218             | 330              |             |               |                |      |   |   |
| 293.2        | 293.2 | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 293.8        | 293.6 | 2    | 1236             | 1234             | 80               | 0.45        | 0.11          |                |      |   |   |
| 293.6        | 293.4 | 6    | 1234             | 1224             | 390              | 0.45        | 1.90          | 1 side         |      |   |   |
| 293.4        | 293.2 | 3    | 1219             | 1218             | 40               |             |               |                |      |   |   |
| 293.2        | 293.2 | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 293.2        | 264   | 3    | 1218             | 1216             | 45               |             |               |                |      |   |   |
| 264          | 264   | 10   |                  |                  |                  |             |               | save to bank 3 |      |   |   |
| 272          | 271   | 2    | 1246             | 1244             | 80               | 0.45        | 0.07          |                |      |   |   |
| 271          | 270   | 6    | 1244             | 1233             | 850              | 0.45        | 2.74          | 2 sides        |      |   |   |



| Node to Node |       | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments               | BANK |   |   |
|--------------|-------|------|------------------|------------------|------------------|-------------|---------------|------------------------|------|---|---|
|              |       |      |                  |                  |                  |             |               |                        | 1    | 2 | 3 |
| 270          | 265   | 3    | 1227             | 1217             | 560              |             |               |                        |      |   |   |
| 265          | 265   | 1    |                  |                  |                  |             |               | 1 of 2                 |      |   |   |
| 269          | 268   | 2    | 1235             | 1233             | 80               | 0.45        | 0.11          |                        |      |   |   |
| 268          | 265   | 6    | 1233             | 1222             | 520              | 0.45        | 2.51          | 2 sides                |      |   |   |
| 265          | 265   | 1    |                  |                  |                  |             |               | 2 of 2                 |      |   |   |
| 265          | 264   | 3    | 1217             | 1216             | 70               |             |               |                        |      |   |   |
| 264          | 264   | 11   |                  |                  |                  |             |               | add bank 3             |      |   |   |
| 264          | 264   | 12   |                  |                  |                  |             |               | clear bank 3           |      |   |   |
| 264          | 260.4 | 3    | 1216             | 1201             | 515              |             |               |                        |      |   |   |
| 260.4        | 260.4 | 1    |                  |                  |                  |             |               | 1 of 2                 |      |   |   |
| 260.7        | 260.6 | 2    | 1230             | 1228             | 80               | 0.45        | 0.08          |                        |      |   |   |
| 260.6        | 260.5 | 6    | 1228             | 1207             | 740              | 0.45        | 3.29          |                        |      |   |   |
| 260.5        | 260.4 | 3    | 1202             | 1201             | 20               |             |               |                        |      |   |   |
| 260.4        | 260.4 | 1    |                  |                  |                  |             |               | 2 of 2                 |      |   |   |
| 260.4        | 260   | 3    | 1201             | 1186             | 512              |             |               |                        |      |   |   |
| 260          | 260   | 1    |                  |                  |                  |             |               | 1 of 2                 |      |   |   |
| 260.3        | 260.2 | 2    | 1209             | 1207             | 80               | 0.45        | 0.13          |                        |      |   |   |
| 260.2        | 260.1 | 6    | 1207             | 1192             | 510              | 0.45        | 1.91          |                        |      |   |   |
| 260.1        | 260   | 3    | 1188             | 1187.5           | 25               |             |               |                        |      |   |   |
| 260          | 260   | 1    |                  |                  |                  |             |               | 2 of 2                 |      |   |   |
| 260          | 259   | 3    | 1187.5           | 1186             | 140              |             |               |                        |      |   |   |
| 259          | 259   | 11   |                  |                  |                  |             |               | add bank 2             |      |   |   |
| 259          | 259   | 12   |                  |                  |                  |             |               | clear bank 2           |      |   |   |
| 259          | 258   | 3    | 1186             | 1184             | 160              |             |               |                        |      |   |   |
| 258          | 246   | 5    | 1184             | 1172             | 300              | 0.25        | 1.93          |                        |      |   |   |
| 246          | 246   | 10   |                  |                  |                  |             |               | save "dirty" to bank 2 |      |   |   |
| 257          | 256   | 2    | 1205             | 1203             | 80               | 0.45        | 0.17          |                        |      |   |   |
| 256          | 255   | 6    | 1203             | 1185             | 670              | 0.45        | 4.27          | one side               |      |   |   |
| 255          | 248   | 3    | 1179             | 1175             | 355              |             |               |                        |      |   |   |
| 248          | 248   | 1    |                  |                  |                  |             |               | 1 of 3                 |      |   |   |
| 254          | 253   | 2    | 1188             | 1186             | 80               | 0.45        | 0.12          |                        |      |   |   |
| 253          | 248   | 6    | 1186             | 1181             | 330              | 0.45        | 2.82          | one side               |      |   |   |
| 248          | 248   | 1    |                  |                  |                  |             |               | 2 of 3                 |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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6390 Greenwich Drive  
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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* PROPOSED HYDROLOGY \*  
\* WITH DETENTION AT NODE 246 \*  
\* NOTE: "CLEAN" LINE ALLOWS Q10 TO PASS THROUGH. LARGER AMOUNTS DETAINED \*  
\*\*\*\*\*

FILE NAME: P-26D.DAT  
TIME/DATE OF STUDY: 14:33 01/26/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP<br>(FT) (FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 2.00 0.0313                                  | 0.125        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 2695.00 TO NODE 2694.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 1454.00

DOWNSTREAM ELEVATION(FEET) = 1452.50

ELEVATION DIFFERENCE(FEET) = 1.50

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.176

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.304

SUBAREA RUNOFF(CFS) = 0.53

TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2694.00 TO NODE 2693.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1452.50 DOWNSTREAM ELEVATION(FEET) = 1447.00

STREET LENGTH(FEET) = 250.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.30

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.23

HALFSTREET FLOOD WIDTH(FEET) = 5.78

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.71

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.63

STREET FLOW TRAVEL TIME(MIN.) = 1.54 Tc(MIN.) = 8.72

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.444

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200

S.C.S. CURVE NUMBER (AMC II) = 0

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 0.46 SUBAREA RUNOFF(CFS) = 1.54  
TOTAL AREA(ACRES) = 0.6 PEAK FLOW RATE(CFS) = 2.01

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 7.34  
FLOW VELOCITY(FEET/SEC.) = 2.93 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.77  
LONGEST FLOWPATH FROM NODE 2695.00 TO NODE 2693.00 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2693.00 TO NODE 2692.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1441.00 DOWNSTREAM(FEET) = 1440.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.90  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.01  
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 8.97  
LONGEST FLOWPATH FROM NODE 2695.00 TO NODE 2692.00 = 400.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2692.00 TO NODE 2692.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.97  
RAINFALL INTENSITY(INCH/HR) = 6.32  
TOTAL STREAM AREA(ACRES) = 0.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.01

\*\*\*\*\*

FLOW PROCESS FROM NODE 2691.00 TO NODE 2690.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1464.00  
DOWNSTREAM ELEVATION(FEET) = 1461.00

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ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.936  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.467  
SUBAREA RUNOFF(CFS) = 0.89  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 0.89

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2690.00 TO NODE 2692.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1461.00 DOWNSTREAM ELEVATION(FEET) = 1448.00  
STREET LENGTH(FEET) = 500.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.90  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.36  
HALFSTREET FLOOD WIDTH(FEET) = 12.34  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.13  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.50  
STREET FLOW TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 8.96  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.332

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 3.63 SUBAREA RUNOFF(CFS) = 11.95  
TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 12.71

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 15.84  
FLOW VELOCITY(FEET/SEC.) = 4.78 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.07  
LONGEST FLOWPATH FROM NODE 2691.00 TO NODE 2692.00 = 595.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2692.00 TO NODE 2692.00 IS CODE = 1  
-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.96
RAINFALL INTENSITY(INCH/HR) = 6.33
TOTAL STREAM AREA(ACRES) = 3.86
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.71

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.72 Tc(MIN.) = 8.96
TOTAL AREA(ACRES) = 4.5
LONGEST FLOWPATH FROM NODE 2691.00 TO NODE 2692.00 = 595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2692.00 TO NODE 2689.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1434.00 DOWNSTREAM(FEET) = 1433.60
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.10
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 14.72
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 9.02
LONGEST FLOWPATH FROM NODE 2691.00 TO NODE 2689.00 = 625.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2689.00 TO NODE 2689.00 IS CODE = 1



>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.02
RAINFALL INTENSITY(INCH/HR) = 6.30
TOTAL STREAM AREA(ACRES) = 4.46
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.72

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*****
FLOW PROCESS FROM NODE 2696.00 TO NODE 2695.50 IS CODE = 21
-----

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1464.00
DOWNSTREAM ELEVATION(FEET) = 1461.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.772
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.938
SUBAREA RUNOFF(CFS) = 1.04
TOTAL AREA(ACRES) = 0.43 TOTAL RUNOFF(CFS) = 1.04

```

```

*****
FLOW PROCESS FROM NODE 2695.50 TO NODE 2689.00 IS CODE = 31
-----

```

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1458.00 DOWNSTREAM(FEET) = 1433.60
FLOW LENGTH(FEET) = 600.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.99
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.04
PIPE TRAVEL TIME(MIN.) = 1.67 Tc(MIN.) = 9.44
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2689.00 = 680.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 2689.00 TO NODE 2689.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.44  
RAINFALL INTENSITY(INCH/HR) = 6.12  
TOTAL STREAM AREA(ACRES) = 0.43  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.04

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 14.72        | 9.02      | 6.304                 | 4.46        |
| 2             | 1.04         | 9.44      | 6.120                 | 0.43        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 15.71        | 9.02      | 6.304                 |
| 2             | 15.33        | 9.44      | 6.120                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.71 Tc(MIN.) = 9.02  
TOTAL AREA(ACRES) = 4.9  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2689.00 = 680.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2689.00 TO NODE 2688.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1433.60 DOWNSTREAM(FEET) = 1363.00  
FLOW LENGTH(FEET) = 975.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.77  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.71  
PIPE TRAVEL TIME(MIN.) = 1.03 Tc(MIN.) = 10.05  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2688.00 = 1655.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2688.00 TO NODE 2688.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.05  
RAINFALL INTENSITY(INCH/HR) = 5.88  
TOTAL STREAM AREA(ACRES) = 4.89  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.71

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2699.00 TO NODE 2698.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1605.00  
DOWNSTREAM ELEVATION(FEET) = 1590.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.778  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.401  
SUBAREA RUNOFF(CFS) = 0.68  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 0.68

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2698.00 TO NODE 2697.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1590.00 DOWNSTREAM(FEET) = 1494.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 475.00 CHANNEL SLOPE = 0.2021  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1611 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.68  
FLOW VELOCITY(FEET/SEC) = 2.25 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.52 Tc(MIN.) = 9.30  
LONGEST FLOWPATH FROM NODE 2699.00 TO NODE 2697.00 = 560.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2698.00 TO NODE 2697.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.180  
\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.66 SUBAREA RUNOFF(CFS) = 3.59  
TOTAL AREA(ACRES) = 1.9 TOTAL RUNOFF(CFS) = 4.09  
TC(MIN.) = 9.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2697.00 TO NODE 2690.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1494.00 DOWNSTREAM(FEET) = 1375.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 515.00 CHANNEL SLOPE = 0.2311  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1737 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 4.09  
FLOW VELOCITY(FEET/SEC) = 3.73 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.30 Tc(MIN.) = 11.60  
LONGEST FLOWPATH FROM NODE 2699.00 TO NODE 2690.00 = 1075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2697.00 TO NODE 2690.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.358  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 6.14 SUBAREA RUNOFF(CFS) = 11.52  
TOTAL AREA(ACRES) = 8.0 TOTAL RUNOFF(CFS) = 15.06  
TC(MIN.) = 11.60

\*\*\*\*\*

FLOW PROCESS FROM NODE 2690.00 TO NODE 2688.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1369.00 DOWNSTREAM(FEET) = 1363.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.86  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

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PIPE-FLOW(CFS) = 15.06  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 11.65  
LONGEST FLOWPATH FROM NODE 2699.00 TO NODE 2688.00 = 1125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2688.00 TO NODE 2688.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.65  
RAINFALL INTENSITY(INCH/HR) = 5.35  
TOTAL STREAM AREA(ACRES) = 8.03  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.06

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 15.71        | 10.05     | 5.879                 | 4.89        |
| 2             | 15.06        | 11.65     | 5.345                 | 8.03        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 28.71        | 10.05     | 5.879                 |
| 2             | 29.35        | 11.65     | 5.345                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 29.35 Tc(MIN.) = 11.65  
TOTAL AREA(ACRES) = 12.9  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2688.00 = 1655.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2688.00 TO NODE 2681.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1363.00 DOWNSTREAM(FEET) = 1362.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.01  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1

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PIPE-FLOW(CFS) = 29.35  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 11.72  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2681.00 = 1705.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2681.00 TO NODE 2681.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 2687.00 TO NODE 2686.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1411.00  
DOWNSTREAM ELEVATION(FEET) = 1409.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.63  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.63

\*\*\*\*\*

FLOW PROCESS FROM NODE 2686.00 TO NODE 2685.50 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1409.00 DOWNSTREAM ELEVATION(FEET) = 1390.00  
STREET LENGTH(FEET) = 415.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.44  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

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STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.84  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.87  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.52  
STREET FLOW TRAVEL TIME(MIN.) = 1.42 Tc(MIN.) = 9.13  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.253  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.516  
SUBAREA AREA(ACRES) = 2.96 SUBAREA RUNOFF(CFS) = 9.62  
TOTAL AREA(ACRES) = 3.2 PEAK FLOW RATE(CFS) = 10.19

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.91  
FLOW VELOCITY(FEET/SEC.) = 5.62 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.10  
LONGEST FLOWPATH FROM NODE 2687.00 TO NODE 2685.50 = 495.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2685.50 TO NODE 2685.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1384.00 DOWNSTREAM(FEET) = 1380.00  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.71  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.19  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 9.20  
LONGEST FLOWPATH FROM NODE 2687.00 TO NODE 2685.00 = 555.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2685.00 TO NODE 2682.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1380.00 DOWNSTREAM(FEET) = 1379.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 85.00 CHANNEL SLOPE = 0.0118  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.046  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0

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TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.45  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.40  
AVERAGE FLOW DEPTH(FEET) = 0.70 TRAVEL TIME(MIN.) = 0.42  
Tc(MIN.) = 9.62  
SUBAREA AREA(ACRES) = 0.25 SUBAREA RUNOFF(CFS) = 0.53  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.503  
TOTAL AREA(ACRES) = 3.4 PEAK FLOW RATE(CFS) = 10.38

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.70 FLOW VELOCITY(FEET/SEC.) = 3.39  
LONGEST FLOWPATH FROM NODE 2687.00 TO NODE 2682.00 = 640.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2682.00 TO NODE 2682.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.62  
RAINFALL INTENSITY(INCH/HR) = 6.05  
TOTAL STREAM AREA(ACRES) = 3.41  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 2684.00 TO NODE 2683.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1467.00  
DOWNSTREAM ELEVATION(FEET) = 1423.00  
ELEVATION DIFFERENCE(FEET) = 44.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 1.26  
TOTAL AREA(ACRES) = 0.45 TOTAL RUNOFF(CFS) = 1.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 2683.00 TO NODE 2682.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====



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ELEVATION DATA: UPSTREAM(FEET) = 1417.00 DOWNSTREAM(FEET) = 1373.00  
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.13  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.26  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 6.40  
LONGEST FLOWPATH FROM NODE 2684.00 TO NODE 2682.00 = 210.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2682.00 TO NODE 2682.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.40  
RAINFALL INTENSITY(INCH/HR) = 7.87  
TOTAL STREAM AREA(ACRES) = 0.45  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.26

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.38        | 9.62      | 6.046                 | 3.41        |
| 2             | 1.26         | 6.40      | 7.867                 | 0.45        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 8.16         | 6.40      | 7.867                 |
| 2             | 11.34        | 9.62      | 6.046                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 11.34 Tc(MIN.) = 9.62  
TOTAL AREA(ACRES) = 3.9  
LONGEST FLOWPATH FROM NODE 2687.00 TO NODE 2682.00 = 640.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2682.00 TO NODE 2681.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1373.00  DOWNSTREAM(FEET) = 1362.00
FLOW LENGTH(FEET) = 415.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.93
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.34
PIPE TRAVEL TIME(MIN.) = 0.70  Tc(MIN.) = 10.32
LONGEST FLOWPATH FROM NODE 2687.00 TO NODE 2681.00 = 1055.00 FEET.

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*****
FLOW PROCESS FROM NODE 2681.00 TO NODE 2681.00 IS CODE = 11

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-----
>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<
=====

```

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.34        | 10.32     | 5.779                 | 3.86        |

LONGEST FLOWPATH FROM NODE 2687.00 TO NODE 2681.00 = 1055.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 29.35        | 11.72     | 5.323                 | 12.92       |

LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2681.00 = 1705.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 37.18        | 10.32     | 5.779                 |
| 2             | 39.79        | 11.72     | 5.323                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 39.79 Tc(MIN.) = 11.72  
TOTAL AREA(ACRES) = 16.8

```

*****
FLOW PROCESS FROM NODE 2681.00 TO NODE 2681.00 IS CODE = 12

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-----
>>>>>CLEAR MEMORY BANK # 1 <<<<<
=====

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*****
FLOW PROCESS FROM NODE 2681.00 TO NODE 2676.00 IS CODE = 31

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-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

```

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1362.00 DOWNSTREAM(FEET) = 1359.00  
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.06  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 39.79  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 11.81  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2676.00 = 1785.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2676.00 TO NODE 2676.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.81  
RAINFALL INTENSITY(INCH/HR) = 5.30  
TOTAL STREAM AREA(ACRES) = 16.78  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 39.79

\*\*\*\*\*

FLOW PROCESS FROM NODE 2680.00 TO NODE 2679.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1447.00  
DOWNSTREAM ELEVATION(FEET) = 1443.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.175  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.019  
SUBAREA RUNOFF(CFS) = 0.61  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 2679.00 TO NODE 2678.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1443.00 DOWNSTREAM ELEVATION(FEET) = 1369.50  
STREET LENGTH(FEET) = 730.00 CURB HEIGHT(INCHES) = 6.0

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STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.24

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.24

HALFSTREET FLOOD WIDTH(FEET) = 6.28

AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.97

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.44

STREET FLOW TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 7.21

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.281

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.520

SUBAREA AREA(ACRES) = 1.38 SUBAREA RUNOFF(CFS) = 5.22

TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 5.72

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 8.41

FLOW VELOCITY(FEET/SEC.) = 6.69 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.90

LONGEST FLOWPATH FROM NODE 2680.00 TO NODE 2678.00 = 805.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2678.00 TO NODE 2677.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1365.00 DOWNSTREAM(FEET) = 1364.00

FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 8.21

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 5.72

PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 7.29

LONGEST FLOWPATH FROM NODE 2680.00 TO NODE 2677.00 = 845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2677.00 TO NODE 2676.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1364.00 DOWNSTREAM(FEET) = 1359.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.54
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.72
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 7.36
LONGEST FLOWPATH FROM NODE 2680.00 TO NODE 2676.00 = 895.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2676.00 TO NODE 2676.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.36
RAINFALL INTENSITY(INCH/HR) = 7.19
TOTAL STREAM AREA(ACRES) = 1.51
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.72

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 44.01 Tc(MIN.) = 11.81
TOTAL AREA(ACRES) = 18.3
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2676.00 = 1785.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2676.00 TO NODE 2672.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1359.00 DOWNSTREAM(FEET) = 1323.00  
FLOW LENGTH(FEET) = 320.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.62  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 44.01  
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 12.04  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2672.00 = 2105.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2672.00 TO NODE 2672.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.04  
RAINFALL INTENSITY(INCH/HR) = 5.23  
TOTAL STREAM AREA(ACRES) = 18.29  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 44.01

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2675.00 TO NODE 2674.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1427.00  
DOWNSTREAM ELEVATION(FEET) = 1420.00  
ELEVATION DIFFERENCE(FEET) = 7.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.553  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.618  
SUBAREA RUNOFF(CFS) = 0.15  
TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.15

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2674.00 TO NODE 2673.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1420.00 DOWNSTREAM(FEET) = 1330.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 440.00 CHANNEL SLOPE = 0.2045
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1623 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.15
FLOW VELOCITY(FEET/SEC) = 2.26 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.25 Tc(MIN.) = 8.80
LONGEST FLOWPATH FROM NODE 2675.00 TO NODE 2673.00 = 515.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 2674.00 TO NODE 2673.00 IS CODE = 81
-----

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.402
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 2.36 SUBAREA RUNOFF(CFS) = 5.29
TOTAL AREA(ACRES) = 2.4 TOTAL RUNOFF(CFS) = 5.40
TC(MIN.) = 8.80

```

```

*****
FLOW PROCESS FROM NODE 2673.00 TO NODE 2672.00 IS CODE = 31
-----

```

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1324.00 DOWNSTREAM(FEET) = 1323.00
FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.39
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.40
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 8.84
LONGEST FLOWPATH FROM NODE 2675.00 TO NODE 2672.00 = 535.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 2672.00 TO NODE 2672.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====

```

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.84  
RAINFALL INTENSITY(INCH/HR) = 6.39  
TOTAL STREAM AREA(ACRES) = 2.41  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.40

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 44.01        | 12.04     | 5.233                 | 18.29       |
| 2             | 5.40         | 8.84      | 6.387                 | 2.41        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 41.45        | 8.84      | 6.387                 |
| 2             | 48.43        | 12.04     | 5.233                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 48.43 Tc(MIN.) = 12.04  
TOTAL AREA(ACRES) = 20.7  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2672.00 = 2105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2672.00 TO NODE 2651.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1323.00 DOWNSTREAM(FEET) = 1309.00  
FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.40  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 48.43  
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 12.26  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2651.00 = 2355.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2651.00 TO NODE 2651.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2671.00 TO NODE 2670.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1445.00  
DOWNSTREAM ELEVATION(FEET) = 1420.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2670.00 TO NODE 2669.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1420.00 DOWNSTREAM(FEET) = 1385.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 280.00 CHANNEL SLOPE = 0.1250  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1183 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.50  
FLOW VELOCITY(FEET/SEC) = 1.93 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.42 Tc(MIN.) = 9.52  
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2669.00 = 380.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2670.00 TO NODE 2669.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.085  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2875  
SUBAREA AREA(ACRES) = 4.07 SUBAREA RUNOFF(CFS) = 7.18  
TOTAL AREA(ACRES) = 4.3 TOTAL RUNOFF(CFS) = 7.59  
TC(MIN.) = 9.52

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2669.00 TO NODE 2668.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1379.00 DOWNSTREAM(FEET) = 1375.00  
FLOW LENGTH(FEET) = 415.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.59  
PIPE TRAVEL TIME(MIN.) = 1.13 Tc(MIN.) = 10.66  
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2668.00 = 795.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2668.00 TO NODE 2663.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1375.00 DOWNSTREAM(FEET) = 1348.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.0450  
CHANNEL FLOW THRU SUBAREA(CFS) = 7.59  
FLOW VELOCITY(FEET/SEC) = 4.95 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 12.68  
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2663.00 = 1395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2663.00 TO NODE 2663.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.68  
RAINFALL INTENSITY(INCH/HR) = 5.06  
TOTAL STREAM AREA(ACRES) = 4.34  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.59

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2667.00 TO NODE 2666.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1420.00  
DOWNSTREAM ELEVATION(FEET) = 1405.00  
ELEVATION DIFFERENCE(FEET) = 15.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2666.00 TO NODE 2663.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1405.00 DOWNSTREAM(FEET) = 1348.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 680.00 CHANNEL SLOPE = 0.0838  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0838 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.53  
FLOW VELOCITY(FEET/SEC) = 1.62 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 6.99 Tc(MIN.) = 13.26  
LONGEST FLOWPATH FROM NODE 2667.00 TO NODE 2663.00 = 780.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2666.00 TO NODE 2663.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.917  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.98 SUBAREA RUNOFF(CFS) = 5.13  
TOTAL AREA(ACRES) = 3.2 TOTAL RUNOFF(CFS) = 5.46  
TC(MIN.) = 13.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 2663.00 TO NODE 2663.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.26

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RAINFALL INTENSITY(INCH/HR) = 4.92  
TOTAL STREAM AREA(ACRES) = 3.17  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 2665.50 TO NODE 2665.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1363.00  
DOWNSTREAM ELEVATION(FEET) = 1361.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.78  
TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 0.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 2665.00 TO NODE 2664.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1361.00 DOWNSTREAM ELEVATION(FEET) = 1350.00  
STREET LENGTH(FEET) = 550.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.32  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 9.28  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.13  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.95  
STREET FLOW TRAVEL TIME(MIN.) = 2.93 Tc(MIN.) = 10.64  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.666

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.459
SUBAREA AREA(ACRES) = 4.22 SUBAREA RUNOFF(CFS) = 11.00
TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 11.64

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 12.16
FLOW VELOCITY(FEET/SEC.) = 3.58 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.29
LONGEST FLOWPATH FROM NODE 2665.50 TO NODE 2664.00 = 630.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2664.00 TO NODE 2663.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1344.00 DOWNSTREAM(FEET) = 1342.00
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.56
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.64
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 10.85
LONGEST FLOWPATH FROM NODE 2665.50 TO NODE 2663.00 = 740.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2663.00 TO NODE 2663.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 10.85
RAINFALL INTENSITY(INCH/HR) = 5.59
TOTAL STREAM AREA(ACRES) = 4.47
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.64

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows 1-3.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 22.60        | 10.85     | 5.594                 |
| 2             | 23.34        | 12.68     | 5.061                 |
| 3             | 23.06        | 13.26     | 4.917                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 23.34 Tc(MIN.) = 12.68  
TOTAL AREA(ACRES) = 12.0  
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2663.00 = 1395.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2663.00 TO NODE 2657.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1342.00 DOWNSTREAM(FEET) = 1312.00  
FLOW LENGTH(FEET) = 372.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.89  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 23.34  
PIPE TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 13.02  
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2657.00 = 1767.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2657.00 TO NODE 2657.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.02  
RAINFALL INTENSITY(INCH/HR) = 4.97  
TOTAL STREAM AREA(ACRES) = 11.98  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 2662.00 TO NODE 2661.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500

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S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 66.67  
UPSTREAM ELEVATION(FEET) = 1400.00  
DOWNSTREAM ELEVATION(FEET) = 1399.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.346  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.627  
SUBAREA RUNOFF(CFS) = 0.48  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 2661.00 TO NODE 2660.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1399.00 DOWNSTREAM ELEVATION(FEET) = 1355.00  
STREET LENGTH(FEET) = 935.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.85  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 9.28  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.81  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.45  
STREET FLOW TRAVEL TIME(MIN.) = 3.24 Tc(MIN.) = 11.59  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.363

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 3.60 SUBAREA RUNOFF(CFS) = 8.69  
TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 9.07

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 12.22  
FLOW VELOCITY(FEET/SEC.) = 5.53 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.99  
LONGEST FLOWPATH FROM NODE 2662.00 TO NODE 2660.00 = 1001.67 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2660.00 TO NODE 2659.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|  |               |                    |         |
|--|---------------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =                     | 1349.00       | DOWNSTREAM(FEET) = | 1348.40 |
| FLOW LENGTH(FEET) =                                  | 60.00         | MANNING'S N =      | 0.013   |
| DEPTH OF FLOW IN 18.0 INCH PIPE IS                   | 13.5 INCHES   |                    |         |
| PIPE-FLOW VELOCITY(FEET/SEC.) =                      | 6.39          |                    |         |
| ESTIMATED PIPE DIAMETER(INCH) =                      | 18.00         | NUMBER OF PIPES =  | 1       |
| PIPE-FLOW(CFS) =                                     | 9.07          |                    |         |
| PIPE TRAVEL TIME(MIN.) =                             | 0.16          | Tc(MIN.) =         | 11.74   |
| LONGEST FLOWPATH FROM NODE 2662.00 TO NODE 2659.00 = | 1061.67 FEET. |                    |         |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2659.00 TO NODE 2658.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

|   |         |                       |         |
|---|---------|-----------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =                        | 1348.40 | DOWNSTREAM(FEET) =    | 1347.60 |
| CHANNEL LENGTH THRU SUBAREA(FEET) =                     | 80.00   | CHANNEL SLOPE =       | 0.0100  |
| CHANNEL BASE(FEET) =                                    | 3.00    | "Z" FACTOR =          | 2.000   |
| MANNING'S FACTOR =                                      | 0.030   | MAXIMUM DEPTH(FEET) = | 10.00   |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =                | 5.194   |                       |         |
| *USER SPECIFIED(SUBAREA):                               |         |                       |         |
| USER-SPECIFIED RUNOFF COEFFICIENT =                     | .2500   |                       |         |
| S.C.S. CURVE NUMBER (AMC II) =                          | 0       |                       |         |
| TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =        | 9.18    |                       |         |
| TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = | 3.09    |                       |         |
| AVERAGE FLOW DEPTH(FEET) =                              | 0.68    | TRAVEL TIME(MIN.) =   | 0.43    |
| Tc(MIN.) =  | 12.17   |                       |         |
| SUBAREA AREA(ACRES) =                                   | 0.17    | SUBAREA RUNOFF(CFS) = | 0.22    |
| AREA-AVERAGE RUNOFF COEFFICIENT =                       | 0.441   |                       |         |
| TOTAL AREA(ACRES) =                                     | 3.9     | PEAK FLOW RATE(CFS) = | 9.07    |

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.68 FLOW VELOCITY(FEET/SEC.) = 3.08  
LONGEST FLOWPATH FROM NODE 2662.00 TO NODE 2658.00 = 1141.67 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2658.00 TO NODE 2657.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<



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ELEVATION DATA: UPSTREAM(FEET) = 1342.00 DOWNSTREAM(FEET) = 1313.00  
FLOW LENGTH(FEET) = 540.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.29  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.07  
PIPE TRAVEL TIME(MIN.) = 0.73 Tc(MIN.) = 12.91  
LONGEST FLOWPATH FROM NODE 2662.00 TO NODE 2657.00 = 1681.67 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2657.00 TO NODE 2657.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.91  
RAINFALL INTENSITY(INCH/HR) = 5.00  
TOTAL STREAM AREA(ACRES) = 3.93  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.07

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 23.34        | 13.02     | 4.973                 | 11.98       |
| 2             | 9.07         | 12.91     | 5.002                 | 3.93        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 32.28        | 12.91     | 5.002                 |
| 2             | 32.36        | 13.02     | 4.973                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 32.36 Tc(MIN.) = 13.02  
TOTAL AREA(ACRES) = 15.9  
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2657.00 = 1767.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2657.00 TO NODE 2650.60 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1312.00 DOWNSTREAM(FEET) = 1308.00  
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.01  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 32.36  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 13.13  
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2650.60 = 1867.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2650.60 TO NODE 2650.60 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.13  
RAINFALL INTENSITY(INCH/HR) = 4.95  
TOTAL STREAM AREA(ACRES) = 15.91  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 32.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 2650.90 TO NODE 2650.80 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1356.00  
DOWNSTREAM ELEVATION(FEET) = 1354.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.31  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.31

\*\*\*\*\*

FLOW PROCESS FROM NODE 2650.80 TO NODE 2650.70 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1354.00 DOWNSTREAM ELEVATION(FEET) = 1315.00  
STREET LENGTH(FEET) = 690.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.40  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 9.34  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.29  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.60  
STREET FLOW TRAVEL TIME(MIN.) = 2.17 Tc(MIN.) = 9.88  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.941

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 3.79 SUBAREA RUNOFF(CFS) = 10.13  
TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 10.40

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.47  
FLOW VELOCITY(FEET/SEC.) = 6.11 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.23  
LONGEST FLOWPATH FROM NODE 2650.90 TO NODE 2650.70 = 770.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2650.70 TO NODE 2650.60 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1309.00 DOWNSTREAM(FEET) = 1308.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.38  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.40  
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 10.05  
LONGEST FLOWPATH FROM NODE 2650.90 TO NODE 2650.60 = 845.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2650.60 TO NODE 2650.60 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.05
RAINFALL INTENSITY(INCH/HR) = 5.88
TOTAL STREAM AREA(ACRES) = 3.89
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.40

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 41.11 Tc(MIN.) = 13.13
TOTAL AREA(ACRES) = 19.8
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2650.60 = 1867.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2650.60 TO NODE 2650.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1308.00 DOWNSTREAM(FEET) = 1298.20
FLOW LENGTH(FEET) = 500.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 22.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.79
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 41.11
PIPE TRAVEL TIME(MIN.) = 0.71 Tc(MIN.) = 13.84
LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2650.00 = 2367.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2650.00 TO NODE 2650.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2656.00 TO NODE 2655.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 55.00  
UPSTREAM ELEVATION(FEET) = 1390.00  
DOWNSTREAM ELEVATION(FEET) = 1389.50  
ELEVATION DIFFERENCE(FEET) = 0.50  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.992  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.814  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2655.00 TO NODE 2654.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1389.50 DOWNSTREAM ELEVATION(FEET) = 1315.00  
STREET LENGTH(FEET) = 970.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.69  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 6.09  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.19  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.23  
STREET FLOW TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 11.11  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.510

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 4.30  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 4.73

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 8.22  
FLOW VELOCITY(FEET/SEC.) = 5.74 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.61  
LONGEST FLOWPATH FROM NODE 2656.00 TO NODE 2654.00 = 1025.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2654.00 TO NODE 2653.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1309.00 DOWNSTREAM(FEET) = 1305.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.84  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.73  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 11.18  
LONGEST FLOWPATH FROM NODE 2656.00 TO NODE 2653.00 = 1075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2653.00 TO NODE 2652.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1305.00 DOWNSTREAM(FEET) = 1304.70  
CHANNEL LENGTH THRU SUBAREA(FEET) = 30.00 CHANNEL SLOPE = 0.0100  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.434

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.75  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.93  
AVERAGE FLOW DEPTH(FEET) = 0.62 TRAVEL TIME(MIN.) = 0.17  
Tc(MIN.) = 11.35  
SUBAREA AREA(ACRES) = 3.18 SUBAREA RUNOFF(CFS) = 6.05  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.408  
TOTAL AREA(ACRES) = 4.8 PEAK FLOW RATE(CFS) = 10.71

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.74 FLOW VELOCITY(FEET/SEC.) = 3.21  
LONGEST FLOWPATH FROM NODE 2656.00 TO NODE 2652.00 = 1105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2652.00 TO NODE 2651.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1299.00 DOWNSTREAM(FEET) = 1298.50  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.18  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.71  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 11.44  
LONGEST FLOWPATH FROM NODE 2656.00 TO NODE 2651.00 = 1145.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2651.00 TO NODE 2651.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.71        | 11.44     | 5.406                 | 4.83        |

LONGEST FLOWPATH FROM NODE 2656.00 TO NODE 2651.00 = 1145.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 48.43        | 12.26     | 5.170                 | 20.70       |

LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2651.00 = 2355.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 55.91        | 11.44     | 5.406                 |
| 2             | 58.68        | 12.26     | 5.170                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 58.68 Tc(MIN.) = 12.26  
TOTAL AREA(ACRES) = 25.5

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 2651.00 TO NODE 2651.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2651.00 TO NODE 2650.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1298.50 DOWNSTREAM(FEET) = 1298.20  
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.17  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 58.68  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 12.31  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2650.00 = 2385.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2650.00 TO NODE 2650.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 58.68        | 12.31     | 5.157                 | 25.53       |

LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2650.00 = 2385.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 41.11        | 13.84     | 4.782                 | 19.80       |

LONGEST FLOWPATH FROM NODE 2671.00 TO NODE 2650.00 = 2367.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 95.25        | 12.31     | 5.157                 |
| 2             | 95.52        | 13.84     | 4.782                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 95.52 Tc(MIN.) = 13.84  
TOTAL AREA(ACRES) = 45.3



\*\*\*\*\*  
FLOW PROCESS FROM NODE 2650.00 TO NODE 2650.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2650.00 TO NODE 2635.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 1298.20 DOWNSTREAM(FEET) = 1292.50  
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 24.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.77  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 95.52  
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 13.98  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2635.00 = 2545.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2635.00 TO NODE 2635.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2649.00 TO NODE 2648.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

-----  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1400.00  
DOWNSTREAM ELEVATION(FEET) = 1398.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.78  
TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 0.78

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2648.00 TO NODE 2647.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1398.00 DOWNSTREAM ELEVATION(FEET) = 1380.00
STREET LENGTH(FEET) = 720.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.59
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 13.66
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.27
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.66
STREET FLOW TRAVEL TIME(MIN.) = 2.81 Tc(MIN.) = 10.52
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.706

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.469
SUBAREA AREA(ACRES) = 5.78 SUBAREA RUNOFF(CFS) = 15.50
TOTAL AREA(ACRES) = 6.0 PEAK FLOW RATE(CFS) = 16.14

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.59
FLOW VELOCITY(FEET/SEC.) = 4.98 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.33
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2647.00 = 800.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2647.00 TO NODE 2643.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1374.00 DOWNSTREAM(FEET) = 1361.00
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.97
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 16.14

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PIPE TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 10.91  
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2643.00 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2643.00 TO NODE 2643.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.91  
RAINFALL INTENSITY(INCH/HR) = 5.58  
TOTAL STREAM AREA(ACRES) = 6.03  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.14

\*\*\*\*\*

FLOW PROCESS FROM NODE 2646.00 TO NODE 2645.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1395.00  
DOWNSTREAM ELEVATION(FEET) = 1393.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.25  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.25

\*\*\*\*\*

FLOW PROCESS FROM NODE 2645.00 TO NODE 2644.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1393.00 DOWNSTREAM ELEVATION(FEET) = 1368.00  
STREET LENGTH(FEET) = 730.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

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Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.36  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.59  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.70  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.99  
STREET FLOW TRAVEL TIME(MIN.) = 3.29 Tc(MIN.) = 11.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.546  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 4.06 SUBAREA RUNOFF(CFS) = 10.13  
TOTAL AREA(ACRES) = 4.1 PEAK FLOW RATE(CFS) = 10.33

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 10.28  
FLOW VELOCITY(FEET/SEC.) = 4.29 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.38  
LONGEST FLOWPATH FROM NODE 2646.00 TO NODE 2644.00 = 810.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2644.00 TO NODE 2643.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1362.00 DOWNSTREAM(FEET) = 1361.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.71  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.33  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 11.09  
LONGEST FLOWPATH FROM NODE 2646.00 TO NODE 2643.00 = 860.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2643.00 TO NODE 2643.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.09  
RAINFALL INTENSITY(INCH/HR) = 5.52

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TOTAL STREAM AREA(ACRES) = 4.14  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.33

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.14        | 10.91     | 5.575                 | 6.03        |
| 2             | 10.33        | 11.09     | 5.516                 | 4.14        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 26.31        | 10.91     | 5.575                 |
| 2             | 26.30        | 11.09     | 5.516                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.31 Tc(MIN.) = 10.91  
TOTAL AREA(ACRES) = 10.2  
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2643.00 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2643.00 TO NODE 2640.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1361.00 DOWNSTREAM(FEET) = 1356.00  
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.93  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 26.31  
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 11.19  
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2640.00 = 1300.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2640.00 TO NODE 2640.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.19  
RAINFALL INTENSITY(INCH/HR) = 5.49  
TOTAL STREAM AREA(ACRES) = 10.17

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PEAK FLOW RATE(CFS) AT CONFLUENCE = 26.31

\*\*\*\*\*

FLOW PROCESS FROM NODE 2642.00 TO NODE 2641.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 81.58

UPSTREAM ELEVATION(FEET) = 1378.00

DOWNSTREAM ELEVATION(FEET) = 1376.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.837

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.901

SUBAREA RUNOFF(CFS) = 0.68

TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 0.68

\*\*\*\*\*

FLOW PROCESS FROM NODE 2641.00 TO NODE 2640.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1376.00 DOWNSTREAM ELEVATION(FEET) = 1362.00

STREET LENGTH(FEET) = 610.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.67

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.32

HALFSTREET FLOOD WIDTH(FEET) = 10.41

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.52

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.14

STREET FLOW TRAVEL TIME(MIN.) = 2.89 Tc(MIN.) = 10.72

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.637

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4700

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.469  
SUBAREA AREA(ACRES) = 5.99 SUBAREA RUNOFF(CFS) = 15.87  
TOTAL AREA(ACRES) = 6.2 PEAK FLOW RATE(CFS) = 16.43

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.66  
FLOW VELOCITY(FEET/SEC.) = 4.08 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.59  
LONGEST FLOWPATH FROM NODE 2642.00 TO NODE 2640.00 = 691.58 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2640.00 TO NODE 2640.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.72  
RAINFALL INTENSITY(INCH/HR) = 5.64  
TOTAL STREAM AREA(ACRES) = 6.21  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.43

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 26.31        | 11.19     | 5.485                 | 10.17       |
| 2             | 16.43        | 10.72     | 5.637                 | 6.21        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 42.02        | 10.72     | 5.637                 |
| 2             | 42.29        | 11.19     | 5.485                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 42.29 Tc(MIN.) = 11.19  
TOTAL AREA(ACRES) = 16.4  
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2640.00 = 1300.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2640.00 TO NODE 2639.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1362.00  DOWNSTREAM(FEET) = 1342.00
FLOW LENGTH(FEET) = 210.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.86
ESTIMATED PIPE DIAMETER(INCH) = 21.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 42.29
PIPE TRAVEL TIME(MIN.) = 0.16  Tc(MIN.) = 11.35
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2639.00 = 1510.00 FEET.
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 2639.00 TO NODE 2638.00 IS CODE = 31
```

```
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1342.00  DOWNSTREAM(FEET) = 1314.00
FLOW LENGTH(FEET) = 380.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.22
ESTIMATED PIPE DIAMETER(INCH) = 24.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 42.29
PIPE TRAVEL TIME(MIN.) = 0.31  Tc(MIN.) = 11.66
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2638.00 = 1890.00 FEET.
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 2638.00 TO NODE 2637.00 IS CODE = 31
```

```
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1314.00  DOWNSTREAM(FEET) = 1295.00
FLOW LENGTH(FEET) = 380.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.24
ESTIMATED PIPE DIAMETER(INCH) = 24.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 42.29
PIPE TRAVEL TIME(MIN.) = 0.37  Tc(MIN.) = 12.03
LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2637.00 = 2270.00 FEET.
```

\*\*\*\*\*

```
FLOW PROCESS FROM NODE 2637.00 TO NODE 2636.00 IS CODE = 51
```

```
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1295.00  DOWNSTREAM(FEET) = 1293.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 200.00  CHANNEL SLOPE = 0.0100
```



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CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.047  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 43.63  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.75  
 AVERAGE FLOW DEPTH(FEET) = 1.52 TRAVEL TIME(MIN.) = 0.70  
 Tc(MIN.) = 12.73  
 SUBAREA AREA(ACRES) = 1.02 SUBAREA RUNOFF(CFS) = 2.68  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.468  
 TOTAL AREA(ACRES) = 17.4 PEAK FLOW RATE(CFS) = 42.29

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 1.50 FLOW VELOCITY(FEET/SEC.) = 4.71  
 LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2636.00 = 2470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2636.00 TO NODE 2635.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1293.00 DOWNSTREAM(FEET) = 1292.50  
 FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.24  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 42.29  
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 12.76  
 LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2635.00 = 2490.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2635.00 TO NODE 2635.00 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 42.29        | 12.76     | 5.040                 | 17.40       |

LONGEST FLOWPATH FROM NODE 2649.00 TO NODE 2635.00 = 2490.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|               |              |           |                       |             |

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1 95.52 13.98 4.751 45.33  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2635.00 = 2545.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 129.44       | 12.76     | 5.040                 |
| 2             | 135.38       | 13.98     | 4.751                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 135.38 Tc(MIN.) = 13.98  
TOTAL AREA(ACRES) = 62.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 2635.00 TO NODE 2635.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2635.00 TO NODE 2631.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1292.50 DOWNSTREAM(FEET) = 1278.50  
FLOW LENGTH(FEET) = 195.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 24.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 26.64  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 135.38  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 14.10  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2631.00 = 2740.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2631.00 TO NODE 2631.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.10  
RAINFALL INTENSITY(INCH/HR) = 4.72  
TOTAL STREAM AREA(ACRES) = 62.73  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 135.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 2634.00 TO NODE 2633.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00  
UPSTREAM ELEVATION(FEET) = 1435.00  
DOWNSTREAM ELEVATION(FEET) = 1405.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.431  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN T<sub>c</sub> CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON T<sub>c</sub> = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.23  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.23

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2633.00 TO NODE 2632.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1405.00 DOWNSTREAM(FEET) = 1285.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 540.00 CHANNEL SLOPE = 0.2222  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.642

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.89  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.19  
AVERAGE FLOW DEPTH(FEET) = 0.24 TRAVEL TIME(MIN.) = 1.10  
T<sub>c</sub>(MIN.) = 5.53  
SUBAREA AREA(ACRES) = 4.39 SUBAREA RUNOFF(CFS) = 13.28  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 13.49

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 FLOW VELOCITY(FEET/SEC.) = 10.22  
LONGEST FLOWPATH FROM NODE 2634.00 TO NODE 2632.00 = 590.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2632.00 TO NODE 2631.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1279.00  DOWNSTREAM(FEET) = 1278.50
FLOW LENGTH(FEET) = 50.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.07
ESTIMATED PIPE DIAMETER(INCH) = 21.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 13.49
PIPE TRAVEL TIME(MIN.) = 0.12  Tc(MIN.) = 5.65
LONGEST FLOWPATH FROM NODE 2634.00 TO NODE 2631.00 = 640.00 FEET.

```

\*\*\*\*\*

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FLOW PROCESS FROM NODE 2631.00 TO NODE 2631.00 IS CODE = 1

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-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.65
RAINFALL INTENSITY(INCH/HR) = 8.53
TOTAL STREAM AREA(ACRES) = 4.46
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.49

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 135.38       | 14.10     | 4.724                 | 62.73       |
| 2             | 13.49        | 5.65      | 8.525                 | 4.46        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 67.70        | 5.65      | 8.525                 |
| 2             | 142.86       | 14.10     | 4.724                 |

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 142.86  Tc(MIN.) = 14.10
TOTAL AREA(ACRES) = 67.2
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2631.00 = 2740.00 FEET.

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\*\*\*\*\*

```

FLOW PROCESS FROM NODE 2631.00 TO NODE 2627.00 IS CODE = 31

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-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====

ELEVATION DATA: UPSTREAM(FEET) = 1278.50 DOWNSTREAM(FEET) = 1253.00  
FLOW LENGTH(FEET) = 600.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 28.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.98  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 142.86  
PIPE TRAVEL TIME(MIN.) = 0.45 Tc(MIN.) = 14.56  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2627.00 = 3340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2627.00 TO NODE 2627.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.56  
RAINFALL INTENSITY(INCH/HR) = 4.63  
TOTAL STREAM AREA(ACRES) = 67.19  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 142.86

\*\*\*\*\*

FLOW PROCESS FROM NODE 2630.00 TO NODE 2629.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1390.00  
DOWNSTREAM ELEVATION(FEET) = 1352.00  
ELEVATION DIFFERENCE(FEET) = 38.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.33  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 2629.00 TO NODE 2628.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1352.00 DOWNSTREAM(FEET) = 1262.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1370.00 CHANNEL SLOPE = 0.0657

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CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.131  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.36  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.30  
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 5.31  
Tc(MIN.) = 12.41  
SUBAREA AREA(ACRES) = 4.60 SUBAREA RUNOFF(CFS) = 5.90  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 4.8 PEAK FLOW RATE(CFS) = 6.13

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 FLOW VELOCITY(FEET/SEC.) = 5.20  
LONGEST FLOWPATH FROM NODE 2630.00 TO NODE 2628.00 = 1470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2628.00 TO NODE 2627.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1256.00 DOWNSTREAM(FEET) = 1253.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.23  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.13  
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 12.66  
LONGEST FLOWPATH FROM NODE 2630.00 TO NODE 2627.00 = 1595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2627.00 TO NODE 2627.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.66  
RAINFALL INTENSITY(INCH/HR) = 5.06  
TOTAL STREAM AREA(ACRES) = 4.78  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.13

\*\* CONFLUENCE DATA \*\*

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| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 142.86       | 14.56     | 4.628                 | 67.19       |
| 2             | 6.13         | 12.66     | 5.065                 | 4.78        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 136.68       | 12.66     | 5.065                 |
| 2             | 148.46       | 14.56     | 4.628                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 148.46 Tc(MIN.) = 14.56  
TOTAL AREA(ACRES) = 72.0  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2627.00 = 3340.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2627.00 TO NODE 2623.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1253.00 DOWNSTREAM(FEET) = 1197.00  
FLOW LENGTH(FEET) = 1335.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 29.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.96  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 148.46  
PIPE TRAVEL TIME(MIN.) = 1.01 Tc(MIN.) = 15.57  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2623.00 = 4675.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2623.00 TO NODE 2623.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.57  
RAINFALL INTENSITY(INCH/HR) = 4.43  
TOTAL STREAM AREA(ACRES) = 71.97  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 148.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 2626.00 TO NODE 2625.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1330.00  
DOWNSTREAM ELEVATION(FEET) = 1280.00  
ELEVATION DIFFERENCE(FEET) = 50.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.352  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.902  
SUBAREA RUNOFF(CFS) = 0.38  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2625.00 TO NODE 2624.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1280.00 DOWNSTREAM(FEET) = 1207.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 440.00 CHANNEL SLOPE = 0.1659  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.106

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.46  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.45  
AVERAGE FLOW DEPTH(FEET) = 0.20 TRAVEL TIME(MIN.) = 1.14  
Tc(MIN.) = 7.49  
SUBAREA AREA(ACRES) = 4.59 SUBAREA RUNOFF(CFS) = 8.15  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250  
TOTAL AREA(ACRES) = 4.8 PEAK FLOW RATE(CFS) = 8.49

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 8.03  
LONGEST FLOWPATH FROM NODE 2626.00 TO NODE 2624.00 = 520.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2624.00 TO NODE 2623.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<



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ELEVATION DATA: UPSTREAM(FEET) = 1201.00 DOWNSTREAM(FEET) = 1197.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.96  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.49  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 7.70  
LONGEST FLOWPATH FROM NODE 2626.00 TO NODE 2623.00 = 645.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2623.00 TO NODE 2623.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.70  
RAINFALL INTENSITY(INCH/HR) = 6.98  
TOTAL STREAM AREA(ACRES) = 4.78  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.49

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 148.46       | 15.57     | 4.432                 | 71.97       |
| 2             | 8.49         | 7.70      | 6.981                 | 4.78        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 102.74       | 7.70      | 6.981                 |
| 2             | 153.85       | 15.57     | 4.432                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 153.85 Tc(MIN.) = 15.57  
TOTAL AREA(ACRES) = 76.8  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 2623.00 = 4675.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2623.00 TO NODE 287.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1196.00 DOWNSTREAM(FEET) = 1185.50  
FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.59  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 153.85  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 15.65  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 287.00 = 4805.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 287.00 TO NODE 287.00 IS CODE = 10

-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2622.00 TO NODE 2621.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1435.00  
DOWNSTREAM ELEVATION(FEET) = 1395.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 2621.00 TO NODE 2620.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1395.00 DOWNSTREAM(FEET) = 1275.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 645.00 CHANNEL SLOPE = 0.1860  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1530 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.75  
FLOW VELOCITY(FEET/SEC) = 2.19 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.91 Tc(MIN.) = 11.17

LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 2620.00 = 745.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2621.00 TO NODE 2620.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.490
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3400
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3407
SUBAREA AREA(ACRES) = 3.37 SUBAREA RUNOFF(CFS) = 6.29
TOTAL AREA(ACRES) = 3.6 TOTAL RUNOFF(CFS) = 6.81
TC(MIN.) = 11.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 2620.00 TO NODE 2616.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1261.00 DOWNSTREAM(FEET) = 1231.00
FLOW LENGTH(FEET) = 380.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.07
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.81
PIPE TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 11.66
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 2616.00 = 1125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2616.00 TO NODE 2616.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.66
RAINFALL INTENSITY(INCH/HR) = 5.34
TOTAL STREAM AREA(ACRES) = 3.64
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.81

\*\*\*\*\*

FLOW PROCESS FROM NODE 2619.00 TO NODE 2618.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1249.00  
DOWNSTREAM ELEVATION(FEET) = 1247.70  
ELEVATION DIFFERENCE(FEET) = 1.30  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.487  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.107  
SUBAREA RUNOFF(CFS) = 0.54  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 2618.00 TO NODE 2617.00 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1247.70 DOWNSTREAM(FEET) = 1239.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 420.00 CHANNEL SLOPE = 0.0207  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.084

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.48  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.43  
AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 2.04  
Tc(MIN.) = 9.53  
SUBAREA AREA(ACRES) = 3.59 SUBAREA RUNOFF(CFS) = 9.83  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 10.29

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.60 FLOW VELOCITY(FEET/SEC.) = 4.10  
LONGEST FLOWPATH FROM NODE 2619.00 TO NODE 2617.00 = 485.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2617.00 TO NODE 2616.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1236.00 DOWNSTREAM(FEET) = 1231.00  
FLOW LENGTH(FEET) = 415.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.9 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 7.04  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.29  
PIPE TRAVEL TIME(MIN.) = 0.98 Tc(MIN.) = 10.51  
LONGEST FLOWPATH FROM NODE 2619.00 TO NODE 2616.00 = 900.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2616.00 TO NODE 2616.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.51  
RAINFALL INTENSITY(INCH/HR) = 5.71  
TOTAL STREAM AREA(ACRES) = 3.76  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.29

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.81         | 11.66     | 5.341                 | 3.64        |
| 2             | 10.29        | 10.51     | 5.711                 | 3.76        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.43        | 10.51     | 5.711                 |
| 2             | 16.44        | 11.66     | 5.341                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 16.44 Tc(MIN.) = 11.66  
TOTAL AREA(ACRES) = 7.4  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 2616.00 = 1125.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2616.00 TO NODE 2616.80 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1231.00 DOWNSTREAM(FEET) = 1223.00  
FLOW LENGTH(FEET) = 540.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.6 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 8.60  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.44  
PIPE TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 12.70  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 2616.80 = 1665.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2616.80 TO NODE 2616.80 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2611.00 TO NODE 2610.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1292.00  
DOWNSTREAM ELEVATION(FEET) = 1290.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.880  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.506  
SUBAREA RUNOFF(CFS) = 0.47  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2610.00 TO NODE 2609.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1290.00 DOWNSTREAM ELEVATION(FEET) = 1265.00  
STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

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\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.49  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.27  
 HALFSTREET FLOOD WIDTH(FEET) = 7.59  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.83  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.29  
 STREET FLOW TRAVEL TIME(MIN.) = 1.50 Tc(MIN.) = 8.38  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.608  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.482  
 SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 6.03  
 TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 6.44

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 10.09  
 FLOW VELOCITY(FEET/SEC.) = 5.52 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.76  
 LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2609.00 = 515.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2609.00 TO NODE 2606.20 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1259.00 DOWNSTREAM(FEET) = 1241.00  
 FLOW LENGTH(FEET) = 275.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.03  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 6.44  
 PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 8.76  
 LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2606.20 = 790.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.20 TO NODE 2606.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.76  
 RAINFALL INTENSITY(INCH/HR) = 6.42  
 TOTAL STREAM AREA(ACRES) = 2.02  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.44

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.60 TO NODE 2606.40 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1267.00
DOWNSTREAM ELEVATION(FEET) = 1265.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974
SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.40 TO NODE 2606.20 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1265.00 DOWNSTREAM ELEVATION(FEET) = 1248.00
STREET LENGTH(FEET) = 215.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.77
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.21
HALFSTREET FLOOD WIDTH(FEET) = 4.59
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.94
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.03
STREET FLOW TRAVEL TIME(MIN.) = 0.73 Tc(MIN.) = 8.44
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.581

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450



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SUBAREA AREA(ACRES) = 0.92 SUBAREA RUNOFF(CFS) = 2.72  
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 3.11

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.59  
FLOW VELOCITY(FEET/SEC.) = 5.34 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.32  
LONGEST FLOWPATH FROM NODE 2606.60 TO NODE 2606.20 = 295.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.20 TO NODE 2606.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.44  
RAINFALL INTENSITY(INCH/HR) = 6.58  
TOTAL STREAM AREA(ACRES) = 1.05  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.11

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.44         | 8.76      | 6.421                 | 2.02        |
| 2             | 3.11         | 8.44      | 6.581                 | 1.05        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 9.31         | 8.44      | 6.581                 |
| 2             | 9.47         | 8.76      | 6.421                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.47 Tc(MIN.) = 8.76  
TOTAL AREA(ACRES) = 3.1  
LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2606.20 = 790.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.20 TO NODE 2606.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1242.00 DOWNSTREAM(FEET) = 1232.00

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FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.85  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.47  
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 8.98  
LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2606.00 = 960.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.00 TO NODE 2606.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.98  
RAINFALL INTENSITY(INCH/HR) = 6.32  
TOTAL STREAM AREA(ACRES) = 3.07  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.47

\*\*\*\*\*

FLOW PROCESS FROM NODE 2608.00 TO NODE 2607.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1254.00  
DOWNSTREAM ELEVATION(FEET) = 1252.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.38  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 2607.00 TO NODE 2606.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1252.00 DOWNSTREAM ELEVATION(FEET) = 1238.00  
STREET LENGTH(FEET) = 170.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.32  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.19  
HALFSTREET FLOOD WIDTH(FEET) = 3.47  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.93  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.92  
STREET FLOW TRAVEL TIME(MIN.) = 0.57 Tc(MIN.) = 8.29  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.658

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 0.63 SUBAREA RUNOFF(CFS) = 1.89  
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 2.25

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.22 HALFSTREET FLOOD WIDTH(FEET) = 5.34  
FLOW VELOCITY(FEET/SEC.) = 5.19 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.16  
LONGEST FLOWPATH FROM NODE 2608.00 TO NODE 2606.00 = 250.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.00 TO NODE 2606.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
-----

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.29  
RAINFALL INTENSITY(INCH/HR) = 6.66  
TOTAL STREAM AREA(ACRES) = 0.75  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.25

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.47         | 8.98      | 6.319                 | 3.07        |
| 2             | 2.25         | 8.29      | 6.658                 | 0.75        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.24        | 8.29      | 6.658                 |
| 2             | 11.61        | 8.98      | 6.319                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.61 Tc(MIN.) = 8.98  
TOTAL AREA(ACRES) = 3.8  
LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2606.00 = 960.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2606.00 TO NODE 2602.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1232.00 DOWNSTREAM(FEET) = 1226.00  
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.71  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.61  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 9.20  
LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2602.00 = 1110.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2602.00 TO NODE 2602.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.20  
RAINFALL INTENSITY(INCH/HR) = 6.22  
TOTAL STREAM AREA(ACRES) = 3.82  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 2605.00 TO NODE 2604.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

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USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 1244.00  
 DOWNSTREAM ELEVATION(FEET) = 1242.00  
 ELEVATION DIFFERENCE(FEET) = 2.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
 SUBAREA RUNOFF(CFS) = 0.38  
 TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 2604.00 TO NODE 2602.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1242.00 DOWNSTREAM ELEVATION(FEET) = 1226.00  
 STREET LENGTH(FEET) = 495.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.06  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.28  
 HALFSTREET FLOOD WIDTH(FEET) = 8.22  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.72  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.04  
 STREET FLOW TRAVEL TIME(MIN.) = 2.22 Tc(MIN.) = 9.93  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.923

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
 SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 5.33  
 TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 5.65

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.84  
 FLOW VELOCITY(FEET/SEC.) = 4.27 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.42

LONGEST FLOWPATH FROM NODE 2605.00 TO NODE 2602.00 = 575.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2602.00 TO NODE 2602.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.93
RAINFALL INTENSITY(INCH/HR) = 5.92
TOTAL STREAM AREA(ACRES) = 2.12
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.65

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.84 Tc(MIN.) = 9.20
TOTAL AREA(ACRES) = 5.9
LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2602.00 = 1110.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2602.00 TO NODE 298.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1226.00 DOWNSTREAM(FEET) = 1222.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 130.00 CHANNEL SLOPE = 0.0308
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.058
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500

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S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.14  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.51  
 AVERAGE FLOW DEPTH(FEET) = 0.70 TRAVEL TIME(MIN.) = 0.39  
 Tc(MIN.) = 9.59  
 SUBAREA AREA(ACRES) = 0.22 SUBAREA RUNOFF(CFS) = 0.60  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.461  
 TOTAL AREA(ACRES) = 6.2 PEAK FLOW RATE(CFS) = 17.19

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.71 FLOW VELOCITY(FEET/SEC.) = 5.51  
 LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 298.00 = 1240.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 298.00 TO NODE 2616.80 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1216.00 DOWNSTREAM(FEET) = 1214.00  
 FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.30  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 17.19  
 PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 9.91  
 LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2616.80 = 1400.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2616.80 TO NODE 2616.80 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 17.19        | 9.91      | 5.931                 | 6.16        |

LONGEST FLOWPATH FROM NODE 2611.00 TO NODE 2616.80 = 1400.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 16.44        | 12.70     | 5.054                 | 7.40        |

LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 2616.80 = 1665.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM | RUNOFF | Tc | INTENSITY |
|--------|--------|----|-----------|
|--------|--------|----|-----------|

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| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) |
|--------|-------|--------|-------------|
| 1      | 30.01 | 9.91   | 5.931       |
| 2      | 31.08 | 12.70  | 5.054       |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 31.08 Tc(MIN.) = 12.70  
TOTAL AREA(ACRES) = 13.6

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2616.80 TO NODE 2616.80 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2616.80 TO NODE 2612.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1214.00 DOWNSTREAM(FEET) = 1212.00  
FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.29  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 31.08  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 12.91  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 2612.00 = 1795.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2612.00 TO NODE 2612.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 12.91  
RAINFALL INTENSITY(INCH/HR) = 5.00  
TOTAL STREAM AREA(ACRES) = 13.56  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 31.08

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2615.00 TO NODE 2614.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500



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S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1275.00  
DOWNSTREAM ELEVATION(FEET) = 1230.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.40  
TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 0.40

\*\*\*\*\*

FLOW PROCESS FROM NODE 2614.00 TO NODE 2613.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1230.00 DOWNSTREAM(FEET) = 1219.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 260.00 CHANNEL SLOPE = 0.0423  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0423 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.40  
FLOW VELOCITY(FEET/SEC) = 1.15 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.76 Tc(MIN.) = 10.86  
LONGEST FLOWPATH FROM NODE 2615.00 TO NODE 2613.00 = 360.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2614.00 TO NODE 2613.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.590  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 0.67 SUBAREA RUNOFF(CFS) = 0.94  
TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 1.24  
TC(MIN.) = 10.86

\*\*\*\*\*

FLOW PROCESS FROM NODE 2613.00 TO NODE 2612.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1214.00 DOWNSTREAM(FEET) = 1212.00

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FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.26  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.24  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 11.00  
LONGEST FLOWPATH FROM NODE 2615.00 TO NODE 2612.00 = 410.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2612.00 TO NODE 2612.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.00  
RAINFALL INTENSITY(INCH/HR) = 5.55  
TOTAL STREAM AREA(ACRES) = 0.89  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.24

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 31.08        | 12.91     | 5.000                 | 13.56       |
| 2             | 1.24         | 11.00     | 5.546                 | 0.89        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 27.71        | 11.00     | 5.546                 |
| 2             | 32.21        | 12.91     | 5.000                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 32.21 Tc(MIN.) = 12.91  
TOTAL AREA(ACRES) = 14.4  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 2612.00 = 1795.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2612.00 TO NODE 292.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

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ELEVATION DATA: UPSTREAM(FEET) = 1212.00 DOWNSTREAM(FEET) = 1196.00  
FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.52  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 32.21  
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 13.55  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 292.00 = 2310.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 292.00 TO NODE 292.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 297.00 TO NODE 296.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1236.00  
DOWNSTREAM ELEVATION(FEET) = 1234.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.47  
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*

FLOW PROCESS FROM NODE 296.00 TO NODE 295.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1236.00 DOWNSTREAM ELEVATION(FEET) = 1215.00  
STREET LENGTH(FEET) = 475.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

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Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.15  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.52  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.32  
STREET FLOW TRAVEL TIME(MIN.) = 1.75 Tc(MIN.) = 9.46  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.111  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 2.67 SUBAREA RUNOFF(CFS) = 7.34  
TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 7.75

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.59  
FLOW VELOCITY(FEET/SEC.) = 5.20 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.81  
LONGEST FLOWPATH FROM NODE 297.00 TO NODE 295.00 = 555.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 295.00 TO NODE 294.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1209.00 DOWNSTREAM(FEET) = 1206.00  
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.75  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.75  
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 9.70  
LONGEST FLOWPATH FROM NODE 297.00 TO NODE 294.00 = 680.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 294.00 TO NODE 294.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 294.90 TO NODE 294.80 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====
\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1245.00
DOWNSTREAM ELEVATION(FEET) = 1243.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974
SUBAREA RUNOFF(CFS) = 0.44
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.44

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.80 TO NODE 294.70 IS CODE = 62

-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 1243.00 DOWNSTREAM ELEVATION(FEET) = 1238.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.93
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.22
HALFSTREET FLOOD WIDTH(FEET) = 5.03
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.41
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.52
STREET FLOW TRAVEL TIME(MIN.) = 1.87 Tc(MIN.) = 9.58
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.063

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
SUBAREA AREA(ACRES) = 1.09 SUBAREA RUNOFF(CFS) = 2.97
TOTAL AREA(ACRES) = 1.2 PEAK FLOW RATE(CFS) = 3.36

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.26 HALFSTREET FLOOD WIDTH(FEET) = 6.97  
FLOW VELOCITY(FEET/SEC.) = 2.65 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.68  
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 294.70 = 350.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.70 TO NODE 294.10 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1236.00 DOWNSTREAM(FEET) = 1223.00  
FLOW LENGTH(FEET) = 605.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.71  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.36  
PIPE TRAVEL TIME(MIN.) = 1.50 Tc(MIN.) = 11.08  
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 294.10 = 955.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.10 TO NODE 294.10 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.08  
RAINFALL INTENSITY(INCH/HR) = 5.52  
TOTAL STREAM AREA(ACRES) = 1.23  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.60 TO NODE 294.50 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1236.00  
DOWNSTREAM ELEVATION(FEET) = 1234.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.31

TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.31

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.50 TO NODE 294.40 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1234.00 DOWNSTREAM ELEVATION(FEET) = 1233.00
STREET LENGTH(FEET) = 100.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.61
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.23
HALFSTREET FLOOD WIDTH(FEET) = 5.47
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.81
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.41
STREET FLOW TRAVEL TIME(MIN.) = 0.92 Tc(MIN.) = 8.63
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.483

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
SUBAREA AREA(ACRES) = 0.89 SUBAREA RUNOFF(CFS) = 2.60
TOTAL AREA(ACRES) = 1.0 PEAK FLOW RATE(CFS) = 2.89

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.53
FLOW VELOCITY(FEET/SEC.) = 2.02 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.54
LONGEST FLOWPATH FROM NODE 294.60 TO NODE 294.40 = 180.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.40 TO NODE 294.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1227.00 DOWNSTREAM(FEET) = 1223.00

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FLOW LENGTH(FEET) = 350.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.13  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.89  
PIPE TRAVEL TIME(MIN.) = 1.14 Tc(MIN.) = 9.77  
LONGEST FLOWPATH FROM NODE 294.60 TO NODE 294.10 = 530.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.10 TO NODE 294.10 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.77  
RAINFALL INTENSITY(INCH/HR) = 5.99  
TOTAL STREAM AREA(ACRES) = 0.99  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.89

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 3.36         | 11.08     | 5.519                 | 1.23        |
| 2             | 2.89         | 9.77      | 5.986                 | 0.99        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 5.85         | 9.77      | 5.986                 |
| 2             | 6.02         | 11.08     | 5.519                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 6.02 Tc(MIN.) = 11.08  
TOTAL AREA(ACRES) = 2.2  
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 294.10 = 955.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.10 TO NODE 294.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====



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ELEVATION DATA: UPSTREAM(FEET) = 1223.00 DOWNSTREAM(FEET) = 1204.00  
FLOW LENGTH(FEET) = 750.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.36  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.02  
PIPE TRAVEL TIME(MIN.) = 1.49 Tc(MIN.) = 12.58  
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 294.00 = 1705.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.00 TO NODE 294.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.02         | 12.58     | 5.087                 | 2.22        |

LONGEST FLOWPATH FROM NODE 294.90 TO NODE 294.00 = 1705.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 7.75         | 9.70      | 6.014                 | 2.82        |

LONGEST FLOWPATH FROM NODE 297.00 TO NODE 294.00 = 680.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.40        | 9.70      | 6.014                 |
| 2             | 12.58        | 12.58     | 5.087                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.58 Tc(MIN.) = 12.58  
TOTAL AREA(ACRES) = 5.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.00 TO NODE 294.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 3 <<<<<  
=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 294.00 TO NODE 293.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1204.00 DOWNSTREAM(FEET) = 1200.00
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.17
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.58
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 12.82
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 293.50 = 1855.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 293.50 TO NODE 293.00 IS CODE = 51

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-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1200.00 DOWNSTREAM(FEET) = 1199.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 100.00 CHANNEL SLOPE = 0.0100
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.903
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.81
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.40
AVERAGE FLOW DEPTH(FEET) = 0.81 TRAVEL TIME(MIN.) = 0.49
Tc(MIN.) = 13.31
SUBAREA AREA(ACRES) = 0.21 SUBAREA RUNOFF(CFS) = 0.46
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
TOTAL AREA(ACRES) = 5.2 PEAK FLOW RATE(CFS) = 12.58

```

```

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.81 FLOW VELOCITY(FEET/SEC.) = 3.38
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 293.00 = 1955.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 293.00 TO NODE 292.00 IS CODE = 31

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1199.00 DOWNSTREAM(FEET) = 1196.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.92

```

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ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.58  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 13.37  
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 292.00 = 2005.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 292.00 TO NODE 292.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 12.58 13.37 4.889 5.25  
LONGEST FLOWPATH FROM NODE 294.90 TO NODE 292.00 = 2005.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 32.21 13.55 4.848 14.45  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 292.00 = 2310.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY  
NUMBER (CFS) (MIN.) (INCH/HOUR)  
1 44.36 13.37 4.889  
2 44.68 13.55 4.848

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 44.68 Tc(MIN.) = 13.55  
TOTAL AREA(ACRES) = 19.7

\*\*\*\*\*

FLOW PROCESS FROM NODE 292.00 TO NODE 292.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 292.00 TO NODE 288.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1196.00 DOWNSTREAM(FEET) = 1189.00  
FLOW LENGTH(FEET) = 270.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.9 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 13.53  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 44.68  
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 13.88  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 288.00 = 2580.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 288.00 TO NODE 288.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.88  
RAINFALL INTENSITY(INCH/HR) = 4.77  
TOTAL STREAM AREA(ACRES) = 19.70  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 44.68

\*\*\*\*\*  
FLOW PROCESS FROM NODE 291.00 TO NODE 290.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1300.00  
DOWNSTREAM ELEVATION(FEET) = 1270.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.37  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*  
FLOW PROCESS FROM NODE 290.00 TO NODE 289.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1270.00 DOWNSTREAM(FEET) = 1195.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 840.00 CHANNEL SLOPE = 0.0893  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.37  
FLOW VELOCITY(FEET/SEC) = 4.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 10.23

LONGEST FLOWPATH FROM NODE 291.00 TO NODE 289.00 = 940.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 290.00 TO NODE 289.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.813
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500
SUBAREA AREA(ACRES) = 2.84 SUBAREA RUNOFF(CFS) = 4.13
TOTAL AREA(ACRES) = 3.0 TOTAL RUNOFF(CFS) = 4.42
TC(MIN.) = 10.23

\*\*\*\*\*

FLOW PROCESS FROM NODE 289.00 TO NODE 288.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1189.00 DOWNSTREAM(FEET) = 1187.00
FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.81
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.42
PIPE TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 10.71
LONGEST FLOWPATH FROM NODE 291.00 TO NODE 288.00 = 1110.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 288.00 TO NODE 288.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.71
RAINFALL INTENSITY(INCH/HR) = 5.64
TOTAL STREAM AREA(ACRES) = 3.04
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.42

\*\* CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

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|   |       |       |       |       |
|---|-------|-------|-------|-------|
| 1 | 44.68 | 13.88 | 4.773 | 19.70 |
| 2 | 4.42  | 10.71 | 5.641 | 3.04  |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 38.90        | 10.71     | 5.641                 |
| 2             | 48.41        | 13.88     | 4.773                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 48.41 Tc(MIN.) = 13.88  
TOTAL AREA(ACRES) = 22.7  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 288.00 = 2580.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 288.00 TO NODE 287.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1187.00 DOWNSTREAM(FEET) = 1185.50  
FLOW LENGTH(FEET) = 275.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 27.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.81  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 48.41  
PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 14.47  
LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 287.00 = 2855.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 287.00 TO NODE 287.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK #1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 48.41        | 14.47     | 4.647                 | 22.74       |

LONGEST FLOWPATH FROM NODE 2622.00 TO NODE 287.00 = 2855.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 153.85       | 15.65     | 4.418                 | 76.75       |

LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 287.00 = 4805.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 190.67       | 14.47     | 4.647                 |
| 2             | 199.88       | 15.65     | 4.418                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 199.88 Tc(MIN.) = 15.65  
 TOTAL AREA(ACRES) = 99.5

\*\*\*\*\*

FLOW PROCESS FROM NODE 287.00 TO NODE 287.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 287.00 TO NODE 246.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1185.50 DOWNSTREAM(FEET) = 1178.00  
 FLOW LENGTH(FEET) = 480.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 51.0 INCH PIPE IS 41.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.09  
 ESTIMATED PIPE DIAMETER(INCH) = 51.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 199.88  
 PIPE TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 16.15  
 LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 246.00 = 5285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 246.00 TO NODE 246.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
 TC(MIN) = 16.15 RAIN INTENSITY(INCH/HOUR) = 4.33  
 TOTAL AREA(ACRES) = 99.50 TOTAL RUNOFF(CFS) = 138.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 246.00 TO NODE 246.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 286.00 TO NODE 285.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1218.00  
DOWNSTREAM ELEVATION(FEET) = 1216.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.41  
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 285.00 TO NODE 284.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1216.00 DOWNSTREAM ELEVATION(FEET) = 1203.00  
STREET LENGTH(FEET) = 380.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.24  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 9.41  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.11  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.25  
STREET FLOW TRAVEL TIME(MIN.) = 1.54 Tc(MIN.) = 9.25  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.200

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450



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SUBAREA AREA(ACRES) = 2.74 SUBAREA RUNOFF(CFS) = 7.64  
TOTAL AREA(ACRES) = 2.9 PEAK FLOW RATE(CFS) = 8.01

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 12.41  
FLOW VELOCITY(FEET/SEC.) = 4.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.73  
LONGEST FLOWPATH FROM NODE 286.00 TO NODE 284.00 = 460.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 284.00 TO NODE 259.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1197.00 DOWNSTREAM(FEET) = 1195.00  
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.54  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.01  
PIPE TRAVEL TIME(MIN.) = 0.46 Tc(MIN.) = 9.71  
LONGEST FLOWPATH FROM NODE 286.00 TO NODE 259.00 = 640.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 259.00 TO NODE 259.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 283.00 TO NODE 282.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1268.00  
DOWNSTREAM ELEVATION(FEET) = 1266.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.592  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.044  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 282.00 TO NODE 281.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
-----

UPSTREAM ELEVATION(FEET) = 1266.00 DOWNSTREAM ELEVATION(FEET) = 1262.00  
STREET LENGTH(FEET) = 220.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.69  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 7.34  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.68  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.71  
STREET FLOW TRAVEL TIME(MIN.) = 1.37 Tc(MIN.) = 8.96  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.331

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.451  
SUBAREA AREA(ACRES) = 2.06 SUBAREA RUNOFF(CFS) = 5.87  
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 6.54

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.66  
FLOW VELOCITY(FEET/SEC.) = 3.03 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.94  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 281.00 = 300.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 281.00 TO NODE 280.60 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
-----

ELEVATION DATA: UPSTREAM(FEET) = 1256.00 DOWNSTREAM(FEET) = 1241.00  
FLOW LENGTH(FEET) = 270.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.38

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ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.54  
PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 9.35  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 280.60 = 570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 280.60 TO NODE 280.60 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.35  
RAINFALL INTENSITY(INCH/HR) = 6.16  
TOTAL STREAM AREA(ACRES) = 2.29  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 280.90 TO NODE 280.80 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1269.00  
DOWNSTREAM ELEVATION(FEET) = 1266.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.736  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.609  
SUBAREA RUNOFF(CFS) = 0.55  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 280.80 TO NODE 280.70 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1266.00 DOWNSTREAM ELEVATION(FEET) = 1248.00  
STREET LENGTH(FEET) = 300.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

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SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.41  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.20  
HALFSTREET FLOOD WIDTH(FEET) = 4.28  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.27  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.86  
STREET FLOW TRAVEL TIME(MIN.) = 1.17 Tc(MIN.) = 7.91  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.862  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 0.56 SUBAREA RUNOFF(CFS) = 1.73  
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.22

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 5.91  
FLOW VELOCITY(FEET/SEC.) = 4.48 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.05  
LONGEST FLOWPATH FROM NODE 280.90 TO NODE 280.70 = 380.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 280.70 TO NODE 280.60 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1242.00 DOWNSTREAM(FEET) = 1241.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.30  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.22  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 8.01  
LONGEST FLOWPATH FROM NODE 280.90 TO NODE 280.60 = 420.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 280.60 TO NODE 280.60 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 8.01
RAINFALL INTENSITY(INCH/HR) = 6.80
TOTAL STREAM AREA(ACRES) = 0.72
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.22

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.55 Tc(MIN.) = 9.35
TOTAL AREA(ACRES) = 3.0
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 280.60 = 570.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 280.60 TO NODE 277.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1241.00 DOWNSTREAM(FEET) = 1238.00
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.12
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.55
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.46
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 277.00 = 640.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 277.00 TO NODE 277.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 9.46  
RAINFALL INTENSITY(INCH/HR) = 6.11  
TOTAL STREAM AREA(ACRES) = 3.01  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 280.00 TO NODE 279.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1257.00  
DOWNSTREAM ELEVATION(FEET) = 1255.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 279.00 TO NODE 278.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1255.00 DOWNSTREAM ELEVATION(FEET) = 1244.00  
STREET LENGTH(FEET) = 340.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.34  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 6.91  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.47  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.88

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STREET FLOW TRAVEL TIME(MIN.) = 1.63 Tc(MIN.) = 9.34  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.162

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 2.58 SUBAREA RUNOFF(CFS) = 7.15  
TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 7.82

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 9.16  
FLOW VELOCITY(FEET/SEC.) = 3.97 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.19  
LONGEST FLOWPATH FROM NODE 280.00 TO NODE 278.00 = 420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 278.00 TO NODE 277.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1239.00 DOWNSTREAM(FEET) = 1238.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.18  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.82  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.44  
LONGEST FLOWPATH FROM NODE 280.00 TO NODE 277.00 = 470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 277.00 TO NODE 277.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.44  
RAINFALL INTENSITY(INCH/HR) = 6.12  
TOTAL STREAM AREA(ACRES) = 2.82  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.82

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 8.55         | 9.46      | 6.113                 | 3.01        |
| 2             | 7.82         | 9.44      | 6.119                 | 2.82        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 16.36        | 9.44      | 6.119                 |
| 2             | 16.36        | 9.46      | 6.113                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.36 Tc(MIN.) = 9.46  
TOTAL AREA(ACRES) = 5.8  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 277.00 = 640.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 277.00 TO NODE 275.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1238.00 DOWNSTREAM(FEET) = 1228.00  
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.37  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.36  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 9.67  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 275.00 = 820.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 275.00 TO NODE 275.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.67  
RAINFALL INTENSITY(INCH/HR) = 6.03  
TOTAL STREAM AREA(ACRES) = 5.83  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.36

\*\*\*\*\*  
FLOW PROCESS FROM NODE 275.30 TO NODE 275.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):



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USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 1247.00  
 DOWNSTREAM ELEVATION(FEET) = 1243.00  
 ELEVATION DIFFERENCE(FEET) = 4.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.120  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.094  
 SUBAREA RUNOFF(CFS) = 0.51  
 TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.51

\*\*\*\*\*

FLOW PROCESS FROM NODE 275.20 TO NODE 275.10 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1243.00 DOWNSTREAM ELEVATION(FEET) = 1235.00  
 STREET LENGTH(FEET) = 165.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.00  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.18  
 HALFSTREET FLOOD WIDTH(FEET) = 3.41  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.80  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.70  
 STREET FLOW TRAVEL TIME(MIN.) = 0.72 Tc(MIN.) = 6.84  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.531

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
 SUBAREA AREA(ACRES) = 0.29 SUBAREA RUNOFF(CFS) = 0.98  
 TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.46

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 4.78  
 FLOW VELOCITY(FEET/SEC.) = 3.87 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.82

LONGEST FLOWPATH FROM NODE 275.30 TO NODE 275.10 = 245.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 275.10 TO NODE 275.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1229.00 DOWNSTREAM(FEET) = 1228.00
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.57
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.46
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 6.96
LONGEST FLOWPATH FROM NODE 275.30 TO NODE 275.00 = 285.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 275.00 TO NODE 275.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.96
RAINFALL INTENSITY(INCH/HR) = 7.45
TOTAL STREAM AREA(ACRES) = 0.43
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.46

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 17.54 Tc(MIN.) = 9.67

TOTAL AREA(ACRES) = 6.3  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 275.00 = 820.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 275.00 TO NODE 293.20 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1228.00 DOWNSTREAM(FEET) = 1218.00  
FLOW LENGTH(FEET) = 330.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.66  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 17.54  
PIPE TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 10.14  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 293.20 = 1150.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 293.20 TO NODE 293.20 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.14  
RAINFALL INTENSITY(INCH/HR) = 5.84  
TOTAL STREAM AREA(ACRES) = 6.26  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.54

\*\*\*\*\*

FLOW PROCESS FROM NODE 293.80 TO NODE 293.60 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1236.00  
DOWNSTREAM ELEVATION(FEET) = 1234.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.35  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.35

\*\*\*\*\*

FLOW PROCESS FROM NODE 293.60 TO NODE 293.40 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1234.00 DOWNSTREAM ELEVATION(FEET) = 1224.00
STREET LENGTH(FEET) = 390.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.94
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 8.47
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.40
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.97
STREET FLOW TRAVEL TIME(MIN.) = 1.91 Tc(MIN.) = 9.62
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.045

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 5.17
TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 5.47

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 11.22
FLOW VELOCITY(FEET/SEC.) = 3.89 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.32
LONGEST FLOWPATH FROM NODE 293.80 TO NODE 293.40 = 470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 293.40 TO NODE 293.20 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1219.00 DOWNSTREAM(FEET) = 1218.00
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 8.11  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 5.47  
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 9.71  
LONGEST FLOWPATH FROM NODE 293.80 TO NODE 293.20 = 510.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 293.20 TO NODE 293.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.71  
RAINFALL INTENSITY(INCH/HR) = 6.01  
TOTAL STREAM AREA(ACRES) = 2.01  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.47

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 17.54        | 10.14     | 5.845                 | 6.26        |
| 2             | 5.47         | 9.71      | 6.012                 | 2.01        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 22.52        | 9.71      | 6.012                 |
| 2             | 22.86        | 10.14     | 5.845                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 22.86 Tc(MIN.) = 10.14  
TOTAL AREA(ACRES) = 8.3  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 293.20 = 1150.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 293.20 TO NODE 264.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1218.00 DOWNSTREAM(FEET) = 1216.00  
FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.2 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 14.35  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 22.86  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 10.19  
LONGEST FLOWPATH FROM NODE 283.00 TO NODE 264.00 = 1195.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 264.00 TO NODE 264.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 272.00 TO NODE 271.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1246.00  
DOWNSTREAM ELEVATION(FEET) = 1244.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.22  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.22

\*\*\*\*\*  
FLOW PROCESS FROM NODE 271.00 TO NODE 270.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1244.00 DOWNSTREAM ELEVATION(FEET) = 1233.00  
STREET LENGTH(FEET) = 850.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

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\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.22  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.27  
 HALFSTREET FLOOD WIDTH(FEET) = 7.47  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.28  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.61  
 STREET FLOW TRAVEL TIME(MIN.) = 6.21 Tc(MIN.) = 13.92  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.765  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
 SUBAREA AREA(ACRES) = 2.74 SUBAREA RUNOFF(CFS) = 5.87  
 TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 6.03

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 10.03  
 FLOW VELOCITY(FEET/SEC.) = 2.61 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.83  
 LONGEST FLOWPATH FROM NODE 272.00 TO NODE 270.00 = 930.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 270.00 TO NODE 265.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1227.00 DOWNSTREAM(FEET) = 1217.00  
 FLOW LENGTH(FEET) = 560.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.35  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 6.03  
 PIPE TRAVEL TIME(MIN.) = 1.27 Tc(MIN.) = 15.19  
 LONGEST FLOWPATH FROM NODE 272.00 TO NODE 265.00 = 1490.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 265.00 TO NODE 265.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 15.19  
 RAINFALL INTENSITY(INCH/HR) = 4.50  
 TOTAL STREAM AREA(ACRES) = 2.81  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.03

\*\*\*\*\*

FLOW PROCESS FROM NODE 269.00 TO NODE 268.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 1235.00

DOWNSTREAM ELEVATION(FEET) = 1233.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974

SUBAREA RUNOFF(CFS) = 0.35

TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.35

\*\*\*\*\*

FLOW PROCESS FROM NODE 268.00 TO NODE 265.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1233.00 DOWNSTREAM ELEVATION(FEET) = 1222.00

STREET LENGTH(FEET) = 520.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.54

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.25

HALFSTREET FLOOD WIDTH(FEET) = 6.91

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.83

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.72

STREET FLOW TRAVEL TIME(MIN.) = 3.06 Tc(MIN.) = 10.77

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.621

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.450



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SUBAREA AREA(ACRES) = 2.51 SUBAREA RUNOFF(CFS) = 6.35  
TOTAL AREA(ACRES) = 2.6 PEAK FLOW RATE(CFS) = 6.63

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 9.41  
FLOW VELOCITY(FEET/SEC.) = 3.21 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.98  
LONGEST FLOWPATH FROM NODE 269.00 TO NODE 265.00 = 600.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 265.00 TO NODE 265.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.77  
RAINFALL INTENSITY(INCH/HR) = 5.62  
TOTAL STREAM AREA(ACRES) = 2.62  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.63

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 6.03         | 15.19     | 4.504                 | 2.81        |
| 2             | 6.63         | 10.77     | 5.621                 | 2.62        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 10.90        | 10.77     | 5.621                 |
| 2             | 11.33        | 15.19     | 4.504                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.33 Tc(MIN.) = 15.19  
TOTAL AREA(ACRES) = 5.4  
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 265.00 = 1490.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 265.00 TO NODE 264.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1217.00 DOWNSTREAM(FEET) = 1216.00

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FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.67  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.33  
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 15.34  
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 264.00 = 1560.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 264.00 TO NODE 264.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.33        | 15.34     | 4.475                 | 5.43        |

LONGEST FLOWPATH FROM NODE 272.00 TO NODE 264.00 = 1560.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 22.86        | 10.19     | 5.825                 | 8.27        |

LONGEST FLOWPATH FROM NODE 283.00 TO NODE 264.00 = 1195.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 30.39        | 10.19     | 5.825                 |
| 2             | 28.89        | 15.34     | 4.475                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 30.39 Tc(MIN.) = 10.19  
TOTAL AREA(ACRES) = 13.7

\*\*\*\*\*  
FLOW PROCESS FROM NODE 264.00 TO NODE 264.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 3 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 264.00 TO NODE 260.40 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1216.00 DOWNSTREAM(FEET) = 1201.00  
FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.03  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 30.39  
PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 10.85  
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 260.40 = 2075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.40 TO NODE 260.40 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.85  
RAINFALL INTENSITY(INCH/HR) = 5.59  
TOTAL STREAM AREA(ACRES) = 13.70  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.39

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.70 TO NODE 260.60 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1230.00  
DOWNSTREAM ELEVATION(FEET) = 1228.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.25  
TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.25

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.60 TO NODE 260.50 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1228.00 DOWNSTREAM ELEVATION(FEET) = 1207.00  
STREET LENGTH(FEET) = 740.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.42  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.32  
HALFSTREET FLOOD WIDTH(FEET) = 9.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.87  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.22  
STREET FLOW TRAVEL TIME(MIN.) = 3.19 Tc(MIN.) = 10.90  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.579

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 3.29 SUBAREA RUNOFF(CFS) = 8.26  
TOTAL AREA(ACRES) = 3.4 PEAK FLOW RATE(CFS) = 8.46

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 13.22  
FLOW VELOCITY(FEET/SEC.) = 4.46 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.70  
LONGEST FLOWPATH FROM NODE 260.70 TO NODE 260.50 = 820.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.50 TO NODE 260.40 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 1202.00 DOWNSTREAM(FEET) = 1201.00  
FLOW LENGTH(FEET) = 20.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.75  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.46  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 10.93  
LONGEST FLOWPATH FROM NODE 260.70 TO NODE 260.40 = 840.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.40 TO NODE 260.40 IS CODE = 1  
-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.93
RAINFALL INTENSITY(INCH/HR) = 5.57
TOTAL STREAM AREA(ACRES) = 3.37
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.46

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 38.79 Tc(MIN.) = 10.85
TOTAL AREA(ACRES) = 17.1
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 260.40 = 2075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.40 TO NODE 260.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1201.00 DOWNSTREAM(FEET) = 1186.00
FLOW LENGTH(FEET) = 512.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.96
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 38.79
PIPE TRAVEL TIME(MIN.) = 0.61 Tc(MIN.) = 11.46
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 260.00 = 2587.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.00 TO NODE 260.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.46
RAINFALL INTENSITY(INCH/HR) = 5.40
TOTAL STREAM AREA(ACRES) = 17.07
PEAK FLOW RATE(CFS) AT CONFLUENCE = 38.79

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.30 TO NODE 260.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1209.00
DOWNSTREAM ELEVATION(FEET) = 1207.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974
SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.41

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.20 TO NODE 260.10 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

```

=====
UPSTREAM ELEVATION(FEET) = 1207.00 DOWNSTREAM ELEVATION(FEET) = 1192.00
STREET LENGTH(FEET) = 510.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

```

```

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

```

```

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

```

```

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.94
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28

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HALFSTREET FLOOD WIDTH(FEET) = 8.22  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.57  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.00  
 STREET FLOW TRAVEL TIME(MIN.) = 2.38 Tc(MIN.) = 10.09  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.864  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
 SUBAREA AREA(ACRES) = 1.91 SUBAREA RUNOFF(CFS) = 5.04  
 TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 5.38

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.84  
 FLOW VELOCITY(FEET/SEC.) = 4.07 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.35  
 LONGEST FLOWPATH FROM NODE 260.30 TO NODE 260.10 = 590.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.10 TO NODE 260.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 1188.00 DOWNSTREAM(FEET) = 1187.50  
 FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.44  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 5.38  
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 10.14  
 LONGEST FLOWPATH FROM NODE 260.30 TO NODE 260.00 = 615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.00 TO NODE 260.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.14  
 RAINFALL INTENSITY(INCH/HR) = 5.84  
 TOTAL STREAM AREA(ACRES) = 2.04  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.38

\*\* CONFLUENCE DATA \*\*

| STREAM | RUNOFF | Tc | INTENSITY | AREA |
|--------|--------|----|-----------|------|
|--------|--------|----|-----------|------|

| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 38.79 | 11.46  | 5.400       | 17.07  |
| 2      | 5.38  | 10.14  | 5.843       | 2.04   |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 41.24        | 10.14     | 5.843                 |
| 2             | 43.76        | 11.46     | 5.400                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 43.76 Tc(MIN.) = 11.46  
TOTAL AREA(ACRES) = 19.1  
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 260.00 = 2587.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 260.00 TO NODE 259.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1187.50 DOWNSTREAM(FEET) = 1186.00  
FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 23.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.80  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 43.76  
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 11.70  
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 259.00 = 2727.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 259.00 TO NODE 259.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 43.76        | 11.70     | 5.329                 | 19.11       |

LONGEST FLOWPATH FROM NODE 272.00 TO NODE 259.00 = 2727.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
|---------------|--------------|-----------|-----------------------|-------------|



1 8.01 9.71 6.010 2.87  
LONGEST FLOWPATH FROM NODE 286.00 TO NODE 259.00 = 640.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 44.33        | 9.71      | 6.010                 |
| 2             | 50.86        | 11.70     | 5.329                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 50.86 Tc(MIN.) = 11.70  
TOTAL AREA(ACRES) = 22.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 259.00 TO NODE 259.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 259.00 TO NODE 258.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1186.00 DOWNSTREAM(FEET) = 1184.00  
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 24.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.70  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 50.86  
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 11.95  
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 258.00 = 2887.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 258.00 TO NODE 246.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1184.00 DOWNSTREAM(FEET) = 1172.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.0400  
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.092  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0

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TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 52.09  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.26  
AVERAGE FLOW DEPTH(FEET) = 1.18 TRAVEL TIME(MIN.) = 0.61  
Tc(MIN.) = 12.55  
SUBAREA AREA(ACRES) = 1.93 SUBAREA RUNOFF(CFS) = 2.46  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.434  
TOTAL AREA(ACRES) = 23.9 PEAK FLOW RATE(CFS) = 52.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 1.19 FLOW VELOCITY(FEET/SEC.) = 8.30  
LONGEST FLOWPATH FROM NODE 272.00 TO NODE 246.00 = 3187.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 246.00 TO NODE 246.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 257.00 TO NODE 256.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1205.00  
DOWNSTREAM ELEVATION(FEET) = 1203.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 256.00 TO NODE 255.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 1203.00 DOWNSTREAM ELEVATION(FEET) = 1185.00  
STREET LENGTH(FEET) = 670.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.07  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.59  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.07  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.42  
STREET FLOW TRAVEL TIME(MIN.) = 2.74 Tc(MIN.) = 10.45  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.730

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 4.27 SUBAREA RUNOFF(CFS) = 11.01  
TOTAL AREA(ACRES) = 4.4 PEAK FLOW RATE(CFS) = 11.45

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 15.09  
FLOW VELOCITY(FEET/SEC.) = 4.72 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.97  
LONGEST FLOWPATH FROM NODE 257.00 TO NODE 255.00 = 750.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 255.00 TO NODE 248.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1179.00 DOWNSTREAM(FEET) = 1175.00  
FLOW LENGTH(FEET) = 355.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.21  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.45  
PIPE TRAVEL TIME(MIN.) = 0.82 Tc(MIN.) = 11.28  
LONGEST FLOWPATH FROM NODE 257.00 TO NODE 248.00 = 1105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 248.00 TO NODE 248.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

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TIME OF CONCENTRATION(MIN.) = 11.28  
RAINFALL INTENSITY(INCH/HR) = 5.46  
TOTAL STREAM AREA(ACRES) = 4.44  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.45

\*\*\*\*\*

FLOW PROCESS FROM NODE 254.00 TO NODE 253.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1188.00  
DOWNSTREAM ELEVATION(FEET) = 1186.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974  
SUBAREA RUNOFF(CFS) = 0.38  
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 253.00 TO NODE 248.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1186.00 DOWNSTREAM ELEVATION(FEET) = 1181.00  
STREET LENGTH(FEET) = 330.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.24  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 11.28  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.99  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.02  
STREET FLOW TRAVEL TIME(MIN.) = 1.84 Tc(MIN.) = 9.55

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.074

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.450

SUBAREA AREA(ACRES) = 2.82 SUBAREA RUNOFF(CFS) = 7.71

TOTAL AREA(ACRES) = 2.9 PEAK FLOW RATE(CFS) = 8.04

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.72

FLOW VELOCITY(FEET/SEC.) = 3.47 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.43

LONGEST FLOWPATH FROM NODE 254.00 TO NODE 248.00 = 410.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 248.00 TO NODE 248.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.55

RAINFALL INTENSITY(INCH/HR) = 6.07

TOTAL STREAM AREA(ACRES) = 2.94

PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 251.00 TO NODE 250.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00

UPSTREAM ELEVATION(FEET) = 1203.00

DOWNSTREAM ELEVATION(FEET) = 1201.00

ELEVATION DIFFERENCE(FEET) = 2.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.711

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.974

SUBAREA RUNOFF(CFS) = 0.28

TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 250.00 TO NODE 248.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

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UPSTREAM ELEVATION(FEET) = 1201.00 DOWNSTREAM ELEVATION(FEET) = 1181.00  
STREET LENGTH(FEET) = 890.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.19  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.40  
HALFSTREET FLOOD WIDTH(FEET) = 14.34  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.17  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.68  
STREET FLOW TRAVEL TIME(MIN.) = 3.56 Tc(MIN.) = 11.27  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.459

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
SUBAREA AREA(ACRES) = 7.17 SUBAREA RUNOFF(CFS) = 17.61  
TOTAL AREA(ACRES) = 7.3 PEAK FLOW RATE(CFS) = 17.84

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 18.00  
FLOW VELOCITY(FEET/SEC.) = 4.79 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.28  
LONGEST FLOWPATH FROM NODE 251.00 TO NODE 248.00 = 970.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 248.00 TO NODE 248.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.27  
RAINFALL INTENSITY(INCH/HR) = 5.46  
TOTAL STREAM AREA(ACRES) = 7.26  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.84

\*\* CONFLUENCE DATA \*\*

| STREAM | RUNOFF | Tc | INTENSITY | AREA |
|--------|--------|----|-----------|------|
|--------|--------|----|-----------|------|

| NUMBER | (CFS) | (MIN.) | (INCH/HOUR) | (ACRE) |
|--------|-------|--------|-------------|--------|
| 1      | 11.45 | 11.28  | 5.458       | 4.44   |
| 2      | 8.04  | 9.55   | 6.074       | 2.94   |
| 3      | 17.84 | 11.27  | 5.459       | 7.26   |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 32.85        | 9.55      | 6.074                 |
| 2             | 36.50        | 11.27     | 5.459                 |
| 3             | 36.50        | 11.28     | 5.458                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 36.50 Tc(MIN.) = 11.27  
TOTAL AREA(ACRES) = 14.6  
LONGEST FLOWPATH FROM NODE 257.00 TO NODE 248.00 = 1105.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 248.00 TO NODE 246.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1175.00 DOWNSTREAM(FEET) = 1172.00  
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.79  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 36.50  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 11.48  
LONGEST FLOWPATH FROM NODE 257.00 TO NODE 246.00 = 1255.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 246.00 TO NODE 246.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 36.50        | 11.48     | 5.394                 | 14.64       |

LONGEST FLOWPATH FROM NODE 257.00 TO NODE 246.00 = 1255.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

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| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 52.84        | 12.55     | 5.092                 | 23.91       |

LONGEST FLOWPATH FROM NODE 272.00 TO NODE 246.00 = 3187.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 84.83        | 11.48     | 5.394                 |
| 2             | 87.30        | 12.55     | 5.092                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 87.30 Tc(MIN.) = 12.55  
TOTAL AREA(ACRES) = 38.5

\*\*\*\*\*  
FLOW PROCESS FROM NODE 246.00 TO NODE 246.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 12.55 RAIN INTENSITY(INCH/HOUR) = 5.09  
TOTAL AREA(ACRES) = 38.50 TOTAL RUNOFF(CFS) = 7.40

\*\*\*\*\*  
FLOW PROCESS FROM NODE 246.00 TO NODE 246.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 7.40         | 12.55     | 5.093                 | 38.50       |

LONGEST FLOWPATH FROM NODE 272.00 TO NODE 246.00 = 3187.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 138.38       | 16.15     | 4.329                 | 99.50       |

LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 246.00 = 5285.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 114.93       | 12.55     | 5.093                 |
| 2             | 144.67       | 16.15     | 4.329                 |



COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 144.67 Tc(MIN.) = 16.15  
TOTAL AREA(ACRES) = 138.0

\*\*\*\*\*

FLOW PROCESS FROM NODE 246.00 TO NODE 245.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1175.00 DOWNSTREAM(FEET) = 1170.00  
FLOW LENGTH(FEET) = 450.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 51.0 INCH PIPE IS 36.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.38  
ESTIMATED PIPE DIAMETER(INCH) = 51.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 144.67  
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 16.71  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 245.50 = 5735.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 245.50 TO NODE 245.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1170.00 DOWNSTREAM(FEET) = 1098.00  
FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 52.87  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 144.67  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 16.76  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 245.00 = 5905.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 245.00 TO NODE 26.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1098.00 DOWNSTREAM(FEET) = 970.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1180.00 CHANNEL SLOPE = 0.1085  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1064 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 144.67  
FLOW VELOCITY(FEET/SEC) = 9.57 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.05 Tc(MIN.) = 18.82  
LONGEST FLOWPATH FROM NODE 2696.00 TO NODE 26.00 = 7085.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 245.00 TO NODE 26.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |        |
|--|--------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.922  |
| *USER SPECIFIED(SUBAREA):                |        |
| USER-SPECIFIED RUNOFF COEFFICIENT =      | .2500  |
| S.C.S. CURVE NUMBER (AMC II) =           | 0      |
| AREA-AVERAGE RUNOFF COEFFICIENT =        | 0.2439 |
| SUBAREA AREA(ACRES) =                    | 39.89  |
| SUBAREA RUNOFF(CFS) =                    | 39.11  |
| TOTAL AREA(ACRES) =                      | 177.9  |
| TOTAL RUNOFF(CFS) =                      | 170.19 |
| TC(MIN.) =                               | 18.82  |

=====

END OF STUDY SUMMARY:

|                     |   |        |            |       |
|---------------------|---|--------|------------|-------|
| TOTAL AREA(ACRES)   | = | 177.9  | TC(MIN.) = | 18.82 |
| PEAK FLOW RATE(CFS) | = | 170.19 |            |       |

=====

END OF RATIONAL METHOD ANALYSIS





Newland Sierra

Job #: 2660-02

Run Name:

P-27d.dat

Page 1

of 3

| Node to Node |        | Code | Elev 1<br>(feet) | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments       | BANK |   |   |
|--------------|--------|------|------------------|------------------|------------------|-------------|---------------|----------------|------|---|---|
|              |        |      |                  |                  |                  |             |               |                | 1    | 2 | 3 |
| 2799         | 2798   | 2    | 1498.6           | 1495.6           | 95               | 0.52        | 0.27          |                |      |   |   |
| 2798         | 2797   | 6    | 1495.6           | 1469             | 525              | 0.52        | 2.32          | One side       |      |   |   |
| 2797         | 2794   | 3    | 1463             | 1442             | 420              |             |               |                |      |   |   |
| 2794         | 2794   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2796         | 2795   | 2    | 1474.8           | 1471.8           | 95               | 0.52        | 0.25          |                |      |   |   |
| 2795         | 2794   | 6    | 1471.8           | 1448             | 380              | 0.52        | 1.88          | One side       |      |   |   |
| 2794         | 2794   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2794         | 2791   | 3    | 1442             | 1427             | 195              |             |               |                |      |   |   |
| 2791         | 2791   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2793         | 2792   | 2    | 1451             | 1448             | 95               | 0.52        | 0.24          |                |      |   |   |
| 2792         | 2791   | 6    | 1448             | 1433             | 195              | 0.52        | 1.58          | One side       |      |   |   |
| 2791         | 2791   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2791         | 2788   | 3    | 1427             | 1408             | 400              |             |               |                |      |   |   |
| 2788         | 2788   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2790         | 2789   | 2    | 1436             | 1434             | 80               | 0.52        | 0.19          |                |      |   |   |
| 2789         | 2788   | 6    | 1434             | 1414             | 325              | 0.48        | 2.58          | One side       |      |   |   |
| 2788         | 2788   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2788         | 2787   | 3    | 1408             | 1384             |                  |             |               |                |      |   |   |
| 2787         | 2787   | 10   |                  |                  |                  |             |               | Save to bank 1 |      |   |   |
| 2785.5       | 2785   | 2    | 1605             | 1585             | 90               | 0.35        | 0.11          |                |      |   |   |
| 2785         | 2780   | 5    | 1585             | 1432             | 1200             |             |               |                |      |   |   |
| 2785         | 2780   | 8    |                  |                  |                  | 0.35        | 4.19          |                |      |   |   |
| 2780         | 2780   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2784         | 2783   | 2    | 1605             | 1592             | 100              | 0.35        | 0.25          |                |      |   |   |
| 2783         | 2780   | 5    | 1592             | 1432             | 1200             |             |               |                |      |   |   |
| 2783         | 2780   | 8    |                  |                  |                  | 0.35        | 2.18          |                |      |   |   |
| 2780         | 2780   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |
| 2780         | 2779   | 3    | 1426             | 1396             | 50               |             |               |                |      |   |   |
| 2779         | 2779   | 1    |                  |                  |                  |             |               | 1 of 2         |      |   |   |
| 2779.4       | 2779.2 | 2    | 1494             | 1491             | 95               | 0.35        | 0.38          |                |      |   |   |
| 2779.2       | 2779   | 5    | 1491             | 1403             | 1265             |             |               |                |      |   |   |
| 2779.2       | 2779   | 8    |                  |                  |                  | 0.35        | 1.67          |                |      |   |   |
| 2779         | 2779   | 1    |                  |                  |                  |             |               | 2 of 2         |      |   |   |



| Node to Node |        | Code | Elev 1<br>(feet)        | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments     | BANK |   |   |  |
|--------------|--------|------|-------------------------|------------------|------------------|-------------|---------------|--------------|------|---|---|--|
|              |        |      |                         |                  |                  |             |               |              | 1    | 2 | 3 |  |
| 2779         | 2787   | 3    | 1397                    | 1384             | 685              |             |               |              |      |   |   |  |
| 2787         | 2787   | 1    |                         |                  |                  |             |               | 1 of 2       |      |   |   |  |
| 2787.4       | 2787.2 | 2    | 1405                    | 1400             | 65               | 0.35        | 0.30          |              |      |   |   |  |
| 2787.2       | 2787   | 5    | 1405                    | 1390             | 155              |             |               |              |      |   |   |  |
| 2787.2       | 2787   | 8    |                         |                  |                  | 0.28        | 1.79          |              |      |   |   |  |
| 2787         | 2787   | 1    |                         |                  |                  |             |               | 2 of 2       |      |   |   |  |
| 2787         | 2787   | 11   |                         |                  |                  |             |               | Add bank 1   |      |   |   |  |
| 2787         | 2787   | 12   |                         |                  |                  |             |               | Clear bank 1 |      |   |   |  |
| 2787         | 2787   | 7    | Tc=10.16 A=20.2 Q=14.33 |                  |                  |             |               |              |      |   |   |  |
| 2787         | 2786   | 3    | 1384                    | 1350             | 200              |             |               |              |      |   |   |  |
| 2786         | 2783   | 5    | 1350                    | 1300             | 400              |             |               |              |      |   |   |  |
| 2786         | 2783   | 8    |                         |                  |                  | 0.25        | 3.89          |              |      |   |   |  |
| 2783         | 2783   | 1    |                         |                  |                  |             |               | 1 of 2       |      |   |   |  |
| 2783.4       | 2783.2 | 2    | 1745                    | 1730             | 90               | 0.3         | 0.29          |              |      |   |   |  |
| 2783.2       | 2783   | 5    | 1730                    | 1300             | 1275             |             |               |              |      |   |   |  |
| 2783.2       | 2783   | 8    |                         |                  |                  | 0.34        | 14.91         |              |      |   |   |  |
| 2783         | 2783   | 1    |                         |                  |                  |             |               | 2 of 2       |      |   |   |  |
| 2783         | 2782   | 5    | 1300                    | 1135             | 1410             |             |               |              |      |   |   |  |
| 2783         | 2782   | 8    |                         |                  |                  | 0.3         | 28.13         |              |      |   |   |  |
| 2782         | 2777   | 5    | 1135                    | 1040             | 670              |             |               |              |      |   |   |  |
| 2782         | 2777   | 8    |                         |                  |                  | 0.25        | 8.96          |              |      |   |   |  |
| 2777         | 2777   | 1    |                         |                  |                  |             |               | 1 of 2       |      |   |   |  |
| 2781         | 2780   | 2    | 1445                    | 1435             | 75               | 0.25        | 0.14          |              |      |   |   |  |
| 2780         | 2779   | 5    | 1435                    | 1395             | 300              |             |               |              |      |   |   |  |
| 2780         | 2779   | 8    |                         |                  |                  | 0.25        | 1.76          |              |      |   |   |  |
| 2779         | 2778   | 5    | 1395                    | 1305             | 585              |             |               |              |      |   |   |  |
| 2779         | 2778   | 8    |                         |                  |                  | 0.25        | 5.55          |              |      |   |   |  |
| 2778         | 2777   | 5    | 1305                    | 1040             | 1335             |             |               |              |      |   |   |  |
| 2778         | 2777   | 8    |                         |                  |                  | 0.25        | 16.86         |              |      |   |   |  |
| 2777         | 2777   | 1    |                         |                  |                  |             |               | 2 of 2       |      |   |   |  |
| 2777         | 2776   | 5    | 1040                    | 970              | 1200             |             |               |              |      |   |   |  |
| 2777         | 2776   | 8    |                         |                  |                  | 0.28        | 21.24         |              |      |   |   |  |
| 2776         | 2772   | 5    | 970                     | 930              | 930              |             |               |              |      |   |   |  |
| 2776         | 2772   | 8    |                         |                  |                  | 0.29        | 16.81         |              |      |   |   |  |
| 2772         | 2772   | 1    |                         |                  |                  |             |               | 1 of 2       |      |   |   |  |
| 2775         | 2774   | 2    | 1155                    | 1140             | 75               | 0.25        | 0.16          |              |      |   |   |  |
| 2774         | 2773   | 5    | 1140                    | 1035             | 440              |             |               |              |      |   |   |  |
| 2774         | 2773   | 8    |                         |                  |                  | 0.25        | 14.38         |              |      |   |   |  |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* PROPOSED HYDROLOGY \*
  - \* DETENTION AT NODE 2787 \*
  - \* JANUARY 2017 \*
- \*\*\*\*\*

FILE NAME: P-27D.DAT  
TIME/DATE OF STUDY: 14:39 01/26/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2799.00 TO NODE 2798.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1498.60  
DOWNSTREAM ELEVATION(FEET) = 1495.60  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.936  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.467  
SUBAREA RUNOFF(CFS) = 1.05  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 1.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2798.00 TO NODE 2797.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1495.60 DOWNSTREAM ELEVATION(FEET) = 1469.00  
STREET LENGTH(FEET) = 525.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.95  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.31  
HALFSTREET FLOOD WIDTH(FEET) = 9.44  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.91  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.55  
STREET FLOW TRAVEL TIME(MIN.) = 1.78 Tc(MIN.) = 8.72  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.442

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 2.32 SUBAREA RUNOFF(CFS) = 7.77  
TOTAL AREA(ACRES) = 2.6 PEAK FLOW RATE(CFS) = 8.68

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 11.97  
FLOW VELOCITY(FEET/SEC.) = 5.60 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.05  
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2797.00 = 620.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2797.00 TO NODE 2794.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1463.00 DOWNSTREAM(FEET) = 1442.00  
FLOW LENGTH(FEET) = 420.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.83  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.68  
PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 9.31  
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2794.00 = 1040.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2794.00 TO NODE 2794.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.31  
RAINFALL INTENSITY(INCH/HR) = 6.18  
TOTAL STREAM AREA(ACRES) = 2.59  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.68

\*\*\*\*\*

FLOW PROCESS FROM NODE 2796.00 TO NODE 2795.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1474.80  
DOWNSTREAM ELEVATION(FEET) = 1471.80



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ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.936  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.467  
SUBAREA RUNOFF(CFS) = 0.97  
TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 0.97

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2795.00 TO NODE 2794.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1471.80 DOWNSTREAM ELEVATION(FEET) = 1448.00  
STREET LENGTH(FEET) = 380.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.26  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.44  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.13  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.51  
STREET FLOW TRAVEL TIME(MIN.) = 1.23 Tc(MIN.) = 8.17  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.718

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
SUBAREA AREA(ACRES) = 1.88 SUBAREA RUNOFF(CFS) = 6.57  
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 7.44

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.72  
FLOW VELOCITY(FEET/SEC.) = 5.87 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.00  
LONGEST FLOWPATH FROM NODE 2796.00 TO NODE 2794.00 = 475.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2794.00 TO NODE 2794.00 IS CODE = 1  
-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.17
RAINFALL INTENSITY(INCH/HR) = 6.72
TOTAL STREAM AREA(ACRES) = 2.13
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.44

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.52 Tc(MIN.) = 9.31
TOTAL AREA(ACRES) = 4.7
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2794.00 = 1040.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2794.00 TO NODE 2791.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1442.00 DOWNSTREAM(FEET) = 1427.00
FLOW LENGTH(FEET) = 195.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.09
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.52
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 9.51
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2791.00 = 1235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2791.00 TO NODE 2791.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.51  
RAINFALL INTENSITY(INCH/HR) = 6.09  
TOTAL STREAM AREA(ACRES) = 4.72  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 2793.00 TO NODE 2792.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1451.00  
DOWNSTREAM ELEVATION(FEET) = 1448.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.936  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.467  
SUBAREA RUNOFF(CFS) = 0.93  
TOTAL AREA(ACRES) = 0.24 TOTAL RUNOFF(CFS) = 0.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 2792.00 TO NODE 2791.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1448.00 DOWNSTREAM ELEVATION(FEET) = 1433.00  
STREET LENGTH(FEET) = 195.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.84  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

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STREET FLOW DEPTH(FEET) = 0.28  
 HALFSTREET FLOOD WIDTH(FEET) = 7.64  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.47  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.53  
 STREET FLOW TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 7.53  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.081  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.520  
 SUBAREA AREA(ACRES) = 1.58 SUBAREA RUNOFF(CFS) = 5.82  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 6.70

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.83  
 FLOW VELOCITY(FEET/SEC.) = 6.18 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.99  
 LONGEST FLOWPATH FROM NODE 2793.00 TO NODE 2791.00 = 290.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2791.00 TO NODE 2791.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.53  
 RAINFALL INTENSITY(INCH/HR) = 7.08  
 TOTAL STREAM AREA(ACRES) = 1.82  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.70

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 15.52        | 9.51      | 6.090                 | 4.72        |
| 2             | 6.70         | 7.53      | 7.081                 | 1.82        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 20.05        | 7.53      | 7.081                 |
| 2             | 21.28        | 9.51      | 6.090                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 21.28 Tc(MIN.) = 9.51

TOTAL AREA(ACRES) = 6.5  
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2791.00 = 1235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2791.00 TO NODE 2788.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1427.00 DOWNSTREAM(FEET) = 1408.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.01  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 21.28  
PIPE TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 9.99  
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2788.00 = 1635.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2788.00 TO NODE 2788.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.99  
RAINFALL INTENSITY(INCH/HR) = 5.90  
TOTAL STREAM AREA(ACRES) = 6.54  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.28

\*\*\*\*\*

FLOW PROCESS FROM NODE 2790.00 TO NODE 2789.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .5200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1436.00  
DOWNSTREAM ELEVATION(FEET) = 1434.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.880  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.506  
SUBAREA RUNOFF(CFS) = 0.74  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.74

\*\*\*\*\*

FLOW PROCESS FROM NODE 2789.00 TO NODE 2788.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1434.00 DOWNSTREAM ELEVATION(FEET) = 1414.00
STREET LENGTH(FEET) = 325.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.00
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.31
HALFSTREET FLOOD WIDTH(FEET) = 9.10
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.28
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.63
STREET FLOW TRAVEL TIME(MIN.) = 1.03 Tc(MIN.) = 7.91
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.862
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4800
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.483
SUBAREA AREA(ACRES) = 2.58 SUBAREA RUNOFF(CFS) = 8.50
TOTAL AREA(ACRES) = 2.8 PEAK FLOW RATE(CFS) = 9.18

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.78
FLOW VELOCITY(FEET/SEC.) = 6.09 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.20
LONGEST FLOWPATH FROM NODE 2790.00 TO NODE 2788.00 = 405.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2788.00 TO NODE 2788.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.91
RAINFALL INTENSITY(INCH/HR) = 6.86

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TOTAL STREAM AREA(ACRES) = 2.77  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.18

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 21.28        | 9.99      | 5.901                 | 6.54        |
| 2             | 9.18         | 7.91      | 6.862                 | 2.77        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 27.48        | 7.91      | 6.862                 |
| 2             | 29.17        | 9.99      | 5.901                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 29.17 Tc(MIN.) = 9.99  
TOTAL AREA(ACRES) = 9.3  
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2788.00 = 1635.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2788.00 TO NODE 2787.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1408.00 DOWNSTREAM(FEET) = 1384.00  
FLOW LENGTH(FEET) = 215.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.25  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 29.17  
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 10.16  
LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2787.00 = 1850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.00 TO NODE 2787.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2785.50 TO NODE 2785.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 1605.00
DOWNSTREAM ELEVATION(FEET) = 1585.00
ELEVATION DIFFERENCE(FEET) = 20.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.945
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.247
SUBAREA RUNOFF(CFS) = 0.32
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.32
=====
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*****
FLOW PROCESS FROM NODE 2785.00 TO NODE 2780.00 IS CODE = 53
-----
```

```
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1585.00 DOWNSTREAM(FEET) = 1432.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1200.00 CHANNEL SLOPE = 0.1275
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1200 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.32
FLOW VELOCITY(FEET/SEC) = 1.94 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 10.31 Tc(MIN.) = 16.25
LONGEST FLOWPATH FROM NODE 2785.50 TO NODE 2780.00 = 1290.00 FEET.
=====
```

```
*****
FLOW PROCESS FROM NODE 2785.00 TO NODE 2780.00 IS CODE = 81
-----
```

```
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
```

```
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.311
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 4.19 SUBAREA RUNOFF(CFS) = 6.32
TOTAL AREA(ACRES) = 4.3 TOTAL RUNOFF(CFS) = 6.49
TC(MIN.) = 16.25
=====
```

```
*****
FLOW PROCESS FROM NODE 2780.00 TO NODE 2780.00 IS CODE = 1
-----
```

```
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
```



=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.25  
RAINFALL INTENSITY(INCH/HR) = 4.31  
TOTAL STREAM AREA(ACRES) = 4.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2784.00 TO NODE 2783.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1605.00  
DOWNSTREAM ELEVATION(FEET) = 1592.00  
ELEVATION DIFFERENCE(FEET) = 13.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.70  
TOTAL AREA(ACRES) = 0.25 TOTAL RUNOFF(CFS) = 0.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2783.00 TO NODE 2780.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1592.00 DOWNSTREAM(FEET) = 1432.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1200.00 CHANNEL SLOPE = 0.1333  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1239 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.70  
FLOW VELOCITY(FEET/SEC) = 1.97 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 10.15 Tc(MIN.) = 16.41  
LONGEST FLOWPATH FROM NODE 2784.00 TO NODE 2780.00 = 1300.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2783.00 TO NODE 2780.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.284

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 2.18 SUBAREA RUNOFF(CFS) = 3.27
TOTAL AREA(ACRES) = 2.4 TOTAL RUNOFF(CFS) = 3.64
TC(MIN.) = 16.41

\*\*\*\*\*
FLOW PROCESS FROM NODE 2780.00 TO NODE 2780.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 16.41
RAINFALL INTENSITY(INCH/HR) = 4.28
TOTAL STREAM AREA(ACRES) = 2.43
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.64

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for streams 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for streams 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 10.10 Tc(MIN.) = 16.25
TOTAL AREA(ACRES) = 6.7
LONGEST FLOWPATH FROM NODE 2784.00 TO NODE 2780.00 = 1300.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2780.00 TO NODE 2779.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1426.00 DOWNSTREAM(FEET) = 1396.00

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FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 30.21  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 10.10  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 16.28  
LONGEST FLOWPATH FROM NODE 2784.00 TO NODE 2779.00 = 1350.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2779.00 TO NODE 2779.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 16.28  
RAINFALL INTENSITY(INCH/HR) = 4.31  
TOTAL STREAM AREA(ACRES) = 6.73  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.10

\*\*\*\*\*

FLOW PROCESS FROM NODE 2779.40 TO NODE 2779.20 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1494.00  
DOWNSTREAM ELEVATION(FEET) = 1491.00  
ELEVATION DIFFERENCE(FEET) = 3.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.969  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.326  
SUBAREA RUNOFF(CFS) = 0.84  
TOTAL AREA(ACRES) = 0.38 TOTAL RUNOFF(CFS) = 0.84

\*\*\*\*\*

FLOW PROCESS FROM NODE 2779.20 TO NODE 2779.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1491.00 DOWNSTREAM(FEET) = 1403.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1265.00 CHANNEL SLOPE = 0.0696  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0696 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.84  
FLOW VELOCITY(FEET/SEC) = 1.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 14.27 Tc(MIN.) = 23.24  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2779.00 = 1360.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2779.20 TO NODE 2779.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.423  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.67 SUBAREA RUNOFF(CFS) = 2.00  
TOTAL AREA(ACRES) = 2.0 TOTAL RUNOFF(CFS) = 2.46  
TC(MIN.) = 23.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2779.00 TO NODE 2779.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 23.24  
RAINFALL INTENSITY(INCH/HR) = 3.42  
TOTAL STREAM AREA(ACRES) = 2.05  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.46

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 10.10        | 16.28     | 4.306                 | 6.73        |
| 2             | 2.46         | 23.24     | 3.423                 | 2.05        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.82        | 16.28     | 4.306                 |
| 2             | 10.48        | 23.24     | 3.423                 |

P-27d.TXT

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.82 Tc(MIN.) = 16.28  
TOTAL AREA(ACRES) = 8.8  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2779.00 = 1360.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2779.00 TO NODE 2787.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1397.00 DOWNSTREAM(FEET) = 1384.00  
FLOW LENGTH(FEET) = 685.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.74  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.82  
PIPE TRAVEL TIME(MIN.) = 1.31 Tc(MIN.) = 17.59  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2787.00 = 2045.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.00 TO NODE 2787.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.59  
RAINFALL INTENSITY(INCH/HR) = 4.10  
TOTAL STREAM AREA(ACRES) = 8.78  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.40 TO NODE 2787.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 1405.00  
DOWNSTREAM ELEVATION(FEET) = 1400.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.514  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.658  
SUBAREA RUNOFF(CFS) = 0.91  
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.91

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.20 TO NODE 2787.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1405.00 DOWNSTREAM(FEET) = 1390.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 155.00 CHANNEL SLOPE = 0.0968  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0968 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.91  
FLOW VELOCITY(FEET/SEC) = 1.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.48 Tc(MIN.) = 7.00  
LONGEST FLOWPATH FROM NODE 2787.40 TO NODE 2787.00 = 220.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.20 TO NODE 2787.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.425  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2900  
SUBAREA AREA(ACRES) = 1.79 SUBAREA RUNOFF(CFS) = 3.72  
TOTAL AREA(ACRES) = 2.1 TOTAL RUNOFF(CFS) = 4.50  
TC(MIN.) = 7.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.00 TO NODE 2787.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.00  
RAINFALL INTENSITY(INCH/HR) = 7.42  
TOTAL STREAM AREA(ACRES) = 2.09  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.50

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.82        | 17.59     | 4.097                 | 8.78        |

2 4.50 7.00 7.425 2.09

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.02        | 7.00      | 7.425                 |
| 2             | 14.30        | 17.59     | 4.097                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 14.30 Tc(MIN.) = 17.59  
TOTAL AREA(ACRES) = 10.9  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2787.00 = 2045.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.00 TO NODE 2787.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 14.30        | 17.59     | 4.097                 | 10.87       |

LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2787.00 = 2045.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 29.17        | 10.16     | 5.838                 | 9.31        |

LONGEST FLOWPATH FROM NODE 2799.00 TO NODE 2787.00 = 1850.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 37.43        | 10.16     | 5.838                 |
| 2             | 34.77        | 17.59     | 4.097                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 37.43 Tc(MIN.) = 10.16  
TOTAL AREA(ACRES) = 20.2

\*\*\*\*\*

FLOW PROCESS FROM NODE 2787.00 TO NODE 2787.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2787.00 TO NODE 2787.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 10.16 RAIN INTENSITY(INCH/HOUR) = 5.84  
TOTAL AREA(ACRES) = 20.20 TOTAL RUNOFF(CFS) = 11.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2787.00 TO NODE 2786.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1384.00 DOWNSTREAM(FEET) = 1350.00  
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.70  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.00  
PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 10.33  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2786.00 = 2245.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2786.00 TO NODE 2783.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1350.00 DOWNSTREAM(FEET) = 1300.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.1250  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1183 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 11.00  
FLOW VELOCITY(FEET/SEC) = 4.28 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.56 Tc(MIN.) = 11.89  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2783.00 = 2645.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2786.00 TO NODE 2783.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.275



\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.1186
SUBAREA AREA(ACRES) = 3.89 SUBAREA RUNOFF(CFS) = 5.13
TOTAL AREA(ACRES) = 24.1 TOTAL RUNOFF(CFS) = 15.07
TC(MIN.) = 11.89

\*\*\*\*\*
FLOW PROCESS FROM NODE 2783.00 TO NODE 2783.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.89
RAINFALL INTENSITY(INCH/HR) = 5.28
TOTAL STREAM AREA(ACRES) = 24.09
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.07

\*\*\*\*\*
FLOW PROCESS FROM NODE 2783.40 TO NODE 2783.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 1745.00
DOWNSTREAM ELEVATION(FEET) = 1730.00
ELEVATION DIFFERENCE(FEET) = 15.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.341
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.911
SUBAREA RUNOFF(CFS) = 0.69
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.69

\*\*\*\*\*
FLOW PROCESS FROM NODE 2783.20 TO NODE 2783.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1730.00 DOWNSTREAM(FEET) = 1300.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1275.00 CHANNEL SLOPE = 0.3373
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .2030 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.69  
FLOW VELOCITY(FEET/SEC) = 2.52 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 8.42 Tc(MIN.) = 14.76  
LONGEST FLOWPATH FROM NODE 2783.40 TO NODE 2783.00 = 1365.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2783.20 TO NODE 2783.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.587  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3400  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3392  
SUBAREA AREA(ACRES) = 14.91 SUBAREA RUNOFF(CFS) = 23.25  
TOTAL AREA(ACRES) = 15.2 TOTAL RUNOFF(CFS) = 23.65  
TC(MIN.) = 14.76

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2783.00 TO NODE 2783.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.76  
RAINFALL INTENSITY(INCH/HR) = 4.59  
TOTAL STREAM AREA(ACRES) = 15.20  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.65

\*\* CONFLUENCE DATA \*\*

| STREAM<br>NUMBER | RUNOFF<br>(CFS) | Tc<br>(MIN.) | INTENSITY<br>(INCH/HOUR) | AREA<br>(ACRE) |
|------------------|-----------------|--------------|--------------------------|----------------|
| 1                | 15.07           | 11.89        | 5.275                    | 24.09          |
| 2                | 23.65           | 14.76        | 4.587                    | 15.20          |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM<br>NUMBER | RUNOFF<br>(CFS) | Tc<br>(MIN.) | INTENSITY<br>(INCH/HOUR) |
|------------------|-----------------|--------------|--------------------------|
| 1                | 34.11           | 11.89        | 5.275                    |
| 2                | 36.76           | 14.76        | 4.587                    |

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COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 36.76 Tc(MIN.) = 14.76

TOTAL AREA(ACRES) = 39.3

LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2783.00 = 2645.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2783.00 TO NODE 2782.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1300.00 DOWNSTREAM(FEET) = 1135.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1410.00 CHANNEL SLOPE = 0.1170

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1128 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 36.76

FLOW VELOCITY(FEET/SEC) = 6.25 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 3.76 Tc(MIN.) = 18.53

LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2782.00 = 4055.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2783.00 TO NODE 2782.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.962

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.2440

SUBAREA AREA(ACRES) = 28.13 SUBAREA RUNOFF(CFS) = 33.44

TOTAL AREA(ACRES) = 67.4 TOTAL RUNOFF(CFS) = 65.19

TC(MIN.) = 18.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2782.00 TO NODE 2777.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1135.00 DOWNSTREAM(FEET) = 1040.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 670.00 CHANNEL SLOPE = 0.1418

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1295 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 65.19

FLOW VELOCITY(FEET/SEC) = 8.10 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 1.38 Tc(MIN.) = 19.90

LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2777.00 = 4725.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2782.00 TO NODE 2777.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |        |
|--|--------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 3.783  |
| *USER SPECIFIED(SUBAREA):                |        |
| USER-SPECIFIED RUNOFF COEFFICIENT =      | .2500  |
| S.C.S. CURVE NUMBER (AMC II) =           | 0      |
| AREA-AVERAGE RUNOFF COEFFICIENT =        | 0.2447 |
| SUBAREA AREA(ACRES) =                    | 8.96   |
| SUBAREA RUNOFF(CFS) =                    | 8.47   |
| TOTAL AREA(ACRES) =                      | 76.4   |
| TOTAL RUNOFF(CFS) =                      | 70.71  |
| TC(MIN.) =                               | 19.90  |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2777.00 TO NODE 2777.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

|  |       |
|--|-------|
| TOTAL NUMBER OF STREAMS =                            | 2     |
| CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE: |       |
| TIME OF CONCENTRATION(MIN.) =                        | 19.90 |
| RAINFALL INTENSITY(INCH/HR) =                        | 3.78  |
| TOTAL STREAM AREA(ACRES) =                           | 76.38 |
| PEAK FLOW RATE(CFS) AT CONFLUENCE =                  | 70.71 |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2781.00 TO NODE 2780.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

|  |         |
|--|---------|
| *USER SPECIFIED(SUBAREA):  |         |
| USER-SPECIFIED RUNOFF COEFFICIENT =  | .2500   |
| S.C.S. CURVE NUMBER (AMC II) =   | 0       |
| INITIAL SUBAREA FLOW-LENGTH(FEET) =  | 75.00   |
| UPSTREAM ELEVATION(FEET) =   | 1445.00 |
| DOWNSTREAM ELEVATION(FEET) =   | 1435.00 |
| ELEVATION DIFFERENCE(FEET) =   | 10.00   |
| SUBAREA OVERLAND TIME OF FLOW(MIN.) =                                      | 6.151   |
| WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION! |         |
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =                                   | 8.068   |
| SUBAREA RUNOFF(CFS) =  | 0.28    |
| TOTAL AREA(ACRES) =  | 0.14    |
| TOTAL RUNOFF(CFS) =  | 0.28    |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2780.00 TO NODE 2779.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1435.00 DOWNSTREAM(FEET) = 1395.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1333
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1239 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.28
FLOW VELOCITY(FEET/SEC) = 1.97 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.54 Tc(MIN.) = 8.69
LONGEST FLOWPATH FROM NODE 2781.00 TO NODE 2779.00 = 375.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2780.00 TO NODE 2779.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.457
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500
SUBAREA AREA(ACRES) = 1.76 SUBAREA RUNOFF(CFS) = 2.84
TOTAL AREA(ACRES) = 1.9 TOTAL RUNOFF(CFS) = 3.07
TC(MIN.) = 8.69

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2779.00 TO NODE 2778.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1395.00 DOWNSTREAM(FEET) = 1305.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 585.00 CHANNEL SLOPE = 0.1538
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1369 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 3.07
FLOW VELOCITY(FEET/SEC) = 3.01 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.24 Tc(MIN.) = 11.93
LONGEST FLOWPATH FROM NODE 2781.00 TO NODE 2778.00 = 960.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2779.00 TO NODE 2778.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.264

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500

SUBAREA AREA(ACRES) = 5.55 SUBAREA RUNOFF(CFS) = 7.30

TOTAL AREA(ACRES) = 7.5 TOTAL RUNOFF(CFS) = 9.80

TC(MIN.) = 11.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 2778.00 TO NODE 2777.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1305.00 DOWNSTREAM(FEET) = 1040.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1335.00 CHANNEL SLOPE = 0.1985

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1593 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 9.80

FLOW VELOCITY(FEET/SEC) = 4.78 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 4.66 Tc(MIN.) = 16.58

LONGEST FLOWPATH FROM NODE 2781.00 TO NODE 2777.00 = 2295.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2778.00 TO NODE 2777.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.256

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500

SUBAREA AREA(ACRES) = 16.86 SUBAREA RUNOFF(CFS) = 17.94

TOTAL AREA(ACRES) = 24.3 TOTAL RUNOFF(CFS) = 25.86

TC(MIN.) = 16.58

\*\*\*\*\*

FLOW PROCESS FROM NODE 2777.00 TO NODE 2777.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 16.58

RAINFALL INTENSITY(INCH/HR) = 4.26

TOTAL STREAM AREA(ACRES) = 24.31

PEAK FLOW RATE(CFS) AT CONFLUENCE = 25.86

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 70.71        | 19.90     | 3.783                 | 76.38       |
| 2             | 25.86        | 16.58     | 4.256                 | 24.31       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 88.72        | 16.58     | 4.256                 |
| 2             | 93.70        | 19.90     | 3.783                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 93.70 Tc(MIN.) = 19.90  
 TOTAL AREA(ACRES) = 100.7  
 LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2777.00 = 4725.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2777.00 TO NODE 2776.00 IS CODE = 53

-----  
 >>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1040.00 DOWNSTREAM(FEET) = 970.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1200.00 CHANNEL SLOPE = 0.0583  
 SLOPE ADJUSTMENT CURVE USED:  
 EFFECTIVE SLOPE = .0583 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 CHANNEL FLOW THRU SUBAREA(CFS) = 93.70  
 FLOW VELOCITY(FEET/SEC) = 6.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
 TRAVEL TIME(MIN.) = 3.26 Tc(MIN.) = 23.17  
 LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2776.00 = 5925.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2777.00 TO NODE 2776.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.430  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.2519  
 SUBAREA AREA(ACRES) = 21.24 SUBAREA RUNOFF(CFS) = 20.40

TOTAL AREA(ACRES) = 121.9 TOTAL RUNOFF(CFS) = 105.37  
TC(MIN.) = 23.17

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2776.00 TO NODE 2772.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 970.00 DOWNSTREAM(FEET) = 930.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 930.00 CHANNEL SLOPE = 0.0430  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0430 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 105.37  
FLOW VELOCITY(FEET/SEC) = 5.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.83 Tc(MIN.) = 26.00  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2772.00 = 6855.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2776.00 TO NODE 2772.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.184  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2565  
SUBAREA AREA(ACRES) = 16.81 SUBAREA RUNOFF(CFS) = 15.52  
TOTAL AREA(ACRES) = 138.7 TOTAL RUNOFF(CFS) = 113.34  
TC(MIN.) = 26.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2772.00 TO NODE 2772.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 26.00  
RAINFALL INTENSITY(INCH/HR) = 3.18  
TOTAL STREAM AREA(ACRES) = 138.74  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 113.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2775.00 TO NODE 2774.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<



```
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00
UPSTREAM ELEVATION(FEET) = 1155.00
DOWNSTREAM ELEVATION(FEET) = 1140.00
ELEVATION DIFFERENCE(FEET) = 15.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.151
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.068
SUBAREA RUNOFF(CFS) = 0.32
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.32
```

```
*****
FLOW PROCESS FROM NODE 2774.00 TO NODE 2773.00 IS CODE = 53
```

```
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 1140.00 DOWNSTREAM(FEET) = 1035.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 440.00 CHANNEL SLOPE = 0.2386
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1762 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.32
FLOW VELOCITY(FEET/SEC) = 2.35 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 9.27
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2773.00 = 515.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 2774.00 TO NODE 2773.00 IS CODE = 81
```

```
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
```

```
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.193
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500
SUBAREA AREA(ACRES) = 14.38 SUBAREA RUNOFF(CFS) = 22.26
TOTAL AREA(ACRES) = 14.5 TOTAL RUNOFF(CFS) = 22.51
TC(MIN.) = 9.27
```

```
*****
FLOW PROCESS FROM NODE 2773.00 TO NODE 2772.00 IS CODE = 53
```

```
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
```

>>>>TRAVELTIME THRU SUBAREA<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1035.00 DOWNSTREAM(FEET) = 930.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 990.00 CHANNEL SLOPE = 0.1061
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1045 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 22.51
FLOW VELOCITY(FEET/SEC) = 5.11 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.23 Tc(MIN.) = 12.50
LONGEST FLOWPATH FROM NODE 2775.00 TO NODE 2772.00 = 1505.00 FEET.

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2773.00 TO NODE 2772.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.106
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2549
SUBAREA AREA(ACRES) = 14.24 SUBAREA RUNOFF(CFS) = 18.91
TOTAL AREA(ACRES) = 28.8 TOTAL RUNOFF(CFS) = 37.47
TC(MIN.) = 12.50

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 2772.00 TO NODE 2772.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.50
RAINFALL INTENSITY(INCH/HR) = 5.11
TOTAL STREAM AREA(ACRES) = 28.78
PEAK FLOW RATE(CFS) AT CONFLUENCE = 37.47

```

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 113.34       | 26.00     | 3.184                 | 138.74      |
| 2             | 37.47        | 12.50     | 5.106                 | 28.78       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 108.15       | 12.50     | 5.106                 |
| 2             | 136.71       | 26.00     | 3.184                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 136.71 Tc(MIN.) = 26.00  
TOTAL AREA(ACRES) = 167.5  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 2772.00 = 6855.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2772.00 TO NODE 27.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 930.00 DOWNSTREAM(FEET) = 920.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 385.00 CHANNEL SLOPE = 0.0260  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0260 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 136.71  
FLOW VELOCITY(FEET/SEC) = 4.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.38 Tc(MIN.) = 27.38  
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 27.00 = 7240.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2772.00 TO NODE 27.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.080  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2578  
SUBAREA AREA(ACRES) = 3.57 SUBAREA RUNOFF(CFS) = 3.63  
TOTAL AREA(ACRES) = 171.1 TOTAL RUNOFF(CFS) = 136.71  
TC(MIN.) = 27.38  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 27.00 TO NODE 27.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2771.00 TO NODE 2770.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1450.00  
DOWNSTREAM ELEVATION(FEET) = 1445.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.196  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.705  
SUBAREA RUNOFF(CFS) = 0.59  
TOTAL AREA(ACRES) = 0.35 TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2770.00 TO NODE 2769.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1445.00 DOWNSTREAM(FEET) = 1390.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 305.00 CHANNEL SLOPE = 0.1803  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1502 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.59  
FLOW VELOCITY(FEET/SEC) = 2.17 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.34 Tc(MIN.) = 10.54  
LONGEST FLOWPATH FROM NODE 2771.00 TO NODE 2769.00 = 395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2770.00 TO NODE 2769.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.701  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 1.97 SUBAREA RUNOFF(CFS) = 2.81  
TOTAL AREA(ACRES) = 2.3 TOTAL RUNOFF(CFS) = 3.31  
TC(MIN.) = 10.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2769.00 TO NODE 2765.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1390.00 DOWNSTREAM(FEET) = 1170.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 820.00 CHANNEL SLOPE = 0.2683  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1861 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.31  
FLOW VELOCITY(FEET/SEC) = 3.60 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.80 Tc(MIN.) = 14.34  
LONGEST FLOWPATH FROM NODE 2771.00 TO NODE 2765.00 = 1215.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2769.00 TO NODE 2765.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.674  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 8.79 SUBAREA RUNOFF(CFS) = 10.27  
TOTAL AREA(ACRES) = 11.1 TOTAL RUNOFF(CFS) = 12.98  
TC(MIN.) = 14.34

\*\*\*\*\*

FLOW PROCESS FROM NODE 2765.00 TO NODE 2765.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.34  
RAINFALL INTENSITY(INCH/HR) = 4.67  
TOTAL STREAM AREA(ACRES) = 11.11  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.98

\*\*\*\*\*

FLOW PROCESS FROM NODE 2768.00 TO NODE 2767.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 1300.00

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DOWNSTREAM ELEVATION(FEET) = 1295.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.041  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.395  
SUBAREA RUNOFF(CFS) = 0.57  
TOTAL AREA(ACRES) = 0.31 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2767.00 TO NODE 2766.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1295.00 DOWNSTREAM(FEET) = 1230.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 430.00 CHANNEL SLOPE = 0.1512  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1356 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.57  
FLOW VELOCITY(FEET/SEC) = 2.06 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.48 Tc(MIN.) = 10.52  
LONGEST FLOWPATH FROM NODE 2768.00 TO NODE 2766.00 = 505.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2767.00 TO NODE 2766.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.709  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 5.63 SUBAREA RUNOFF(CFS) = 8.04  
TOTAL AREA(ACRES) = 5.9 TOTAL RUNOFF(CFS) = 8.48  
TC(MIN.) = 10.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 2766.00 TO NODE 2765.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1230.00 DOWNSTREAM(FEET) = 1170.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 650.00 CHANNEL SLOPE = 0.0923  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0923 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.48

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FLOW VELOCITY(FEET/SEC) = 3.47 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 13.64  
LONGEST FLOWPATH FROM NODE 2768.00 TO NODE 2765.00 = 1155.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2766.00 TO NODE 2765.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.827  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 15.49 SUBAREA RUNOFF(CFS) = 18.69  
TOTAL AREA(ACRES) = 21.4 TOTAL RUNOFF(CFS) = 25.86  
TC(MIN.) = 13.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 2765.00 TO NODE 2765.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.64  
RAINFALL INTENSITY(INCH/HR) = 4.83  
TOTAL STREAM AREA(ACRES) = 21.43  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 25.86

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.98        | 14.34     | 4.674                 | 11.11       |
| 2             | 25.86        | 13.64     | 4.827                 | 21.43       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 38.21        | 13.64     | 4.827                 |
| 2             | 38.03        | 14.34     | 4.674                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 38.21 Tc(MIN.) = 13.64

TOTAL AREA(ACRES) = 32.5  
LONGEST FLOWPATH FROM NODE 2771.00 TO NODE 2765.00 = 1215.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2765.00 TO NODE 2711.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |         |
|-------------------------------------|---------|--------------------|---------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1170.00 | DOWNSTREAM(FEET) = | 1105.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 600.00  | CHANNEL SLOPE =    | 0.1083  |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1063 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 38.21  
FLOW VELOCITY(FEET/SEC) = 6.14 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.63 Tc(MIN.) = 15.27  
LONGEST FLOWPATH FROM NODE 2771.00 TO NODE 2711.00 = 1815.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2765.00 TO NODE 2711.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

|  |       |
|--|-------|
| 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = | 4.488 |
|--|-------|

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2500  
SUBAREA AREA(ACRES) = 11.00 SUBAREA RUNOFF(CFS) = 12.34  
TOTAL AREA(ACRES) = 43.5 TOTAL RUNOFF(CFS) = 48.85  
TC(MIN.) = 15.27

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2711.00 TO NODE 27.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |         |                    |        |
|-------------------------------------|---------|--------------------|--------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 1105.00 | DOWNSTREAM(FEET) = | 920.00 |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 1460.00 | CHANNEL SLOPE =    | 0.1267 |

SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1195 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 48.85  
FLOW VELOCITY(FEET/SEC) = 7.07 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.44 Tc(MIN.) = 18.71  
LONGEST FLOWPATH FROM NODE 2771.00 TO NODE 27.00 = 3275.00 FEET.

\*\*\*\*\*



FLOW PROCESS FROM NODE 2711.00 TO NODE 27.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.936
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2529
SUBAREA AREA(ACRES) = 18.20 SUBAREA RUNOFF(CFS) = 18.63
TOTAL AREA(ACRES) = 61.7 TOTAL RUNOFF(CFS) = 61.48
TC(MIN.) = 18.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 27.00 TO NODE 27.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 61.48 18.71 3.936 61.74
LONGEST FLOWPATH FROM NODE 2771.00 TO NODE 27.00 = 3275.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 136.71 27.38 3.080 171.09
LONGEST FLOWPATH FROM NODE 2779.40 TO NODE 27.00 = 7240.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 154.92 18.71 3.936
2 184.80 27.38 3.080

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 184.80 Tc(MIN.) = 27.38
TOTAL AREA(ACRES) = 232.8

END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 232.8 TC(MIN.) = 27.38
PEAK FLOW RATE(CFS) = 184.80

END OF RATIONAL METHOD ANALYSIS

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# APPENDIX A

AES  
Rational Method Hydrology

Proposed Condition

BASIN D

THE FOLLOWING SUBBASINS OF MAJOR BASIN D  
HAVE NO GRADING, THUS THERE IS NO CHANGE IN HYDROLOGY FOR  
THE PROPOSED CONDITION.

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Newland Sierra

Job #: 2660-02

Run Name:  
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of 3

| Node to Node |      | Code | Elev 1<br>(feet)  | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments    | BANK |   |   |
|--------------|------|------|-------------------|------------------|------------------|-------------|---------------|-------------|------|---|---|
|              |      |      |                   |                  |                  |             |               |             | 1    | 2 | 3 |
| 2860         | 2859 | 2    | 1407              | 1395             | 60               | 0.9         | 0.05          |             |      |   |   |
| 2859         | 2858 | 6    | 1395              | 1216             | 1068             | 0.89        | 0.81          | 2 sides     |      |   |   |
| 2858         | 2857 | 3    | 1210              | 1140             | 400              |             |               |             |      |   |   |
| 2857         | 2857 | 1    |                   |                  |                  |             |               | 1 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2856         | 2855 | 2    | 1215              | 1198             | 90               | 0.88        | 0.07          |             |      |   |   |
| 2855         | 2857 | 6    | 1198              | 1146             | 295              | 0.88        | 0.23          | 2 sides     |      |   |   |
| 2857         | 2857 | 1    |                   |                  |                  |             |               | 2 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2857         | 2854 | 3    | 1140              | 1080             | 410              |             |               |             |      |   |   |
| 2854         | 2854 | 1    |                   |                  |                  |             |               | 1 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2853         | 2852 | 2    | 1146              | 1133             | 90               | 0.88        | 0.07          |             |      |   |   |
| 2852         | 2854 | 6    | 1133              | 1086             | 308              | 0.88        | 0.23          | 2 sides     |      |   |   |
| 2854         | 2854 | 1    |                   |                  |                  |             |               | 2 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2854         | 2851 | 3    | 1080              | 1019             | 328              |             |               |             |      |   |   |
| 2851         | 2851 | 1    |                   |                  |                  |             |               | 1 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2850         | 2849 | 2    | 1086              | 1070             | 92               | 0.88        | 0.07          |             |      |   |   |
| 2849         | 2851 | 6    | 1070              | 1025             | 233              | 0.89        | 0.18          | 2 sides     |      |   |   |
| 2851         | 2851 | 1    |                   |                  |                  |             |               | 2 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2851         | 2848 | 3    | 1019              | 980              | 328              |             |               |             |      |   |   |
| 2848         | 2828 | 5    | 980               | 979              | 15               |             | *             |             |      |   |   |
| 2828         | 2828 | 7    | Tc=5.34 A=1.7 Q=1 |                  |                  |             |               |             |      |   |   |
| 2828         | 2828 | 10   |                   |                  |                  |             |               | Save Bank 1 |      |   |   |
| 2847         | 2846 | 2    | 1730              | 1695             | 100              | 0.35        | 0.33          |             |      |   |   |
| 2846         | 2845 | 5    | 1695              | 1440             | 515              |             |               |             |      |   |   |
| 2846         | 2845 | 8    |                   |                  |                  | 0.35        | 3.06          |             |      |   |   |
| 2845         | 2844 | 5    | 1440              | 1325             | 395              |             |               |             |      |   |   |
| 2845         | 2844 | 8    |                   |                  |                  | 0.33        | 9.88          |             |      |   |   |
| 2844         | 2843 | 3    | 1325              | 1305             | 80               |             |               |             |      |   |   |
| 2843         | 2843 | 1    |                   |                  |                  |             |               | 1 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2842         | 2841 | 2    | 1395              | 1390             | 100              | 0.35        | 0.11          |             |      |   |   |
| 2841         | 2840 | 5    | 1390              | 1345             | 253              |             |               |             |      |   |   |
| 2841         | 2840 | 8    |                   |                  |                  | 0.29        | 1.72          |             |      |   |   |
| 2840         | 2839 | 3    | 1339              | 1329             | 37               |             |               |             |      |   |   |
| 2839         | 2843 | 5    | 1335              | 1305             | 178              |             | *             |             |      |   |   |
| 2843         | 2843 | 1    |                   |                  |                  |             |               | 2 of 2      |      |   |   |
|              |      |      |                   |                  |                  |             |               |             |      |   |   |
| 2843         | 2838 | 5    | 1305              | 1165             | 773              |             |               |             |      |   |   |
| 2843         | 2838 | 8    |                   |                  |                  | 0.25        | 6.24          |             |      |   |   |
| 2838         | 2838 | 1    |                   |                  |                  |             |               | 1 of 2      |      |   |   |



Newland Sierra

Job #: 2660-02

Run Name:  
P-28d.dat  
Page 2  
of 3

| Node to Node |        | Code | Elev 1<br>(feet)    | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments     | BANK |   |   |
|--------------|--------|------|---------------------|------------------|------------------|-------------|---------------|--------------|------|---|---|
|              |        |      |                     |                  |                  |             |               |              | 1    | 2 | 3 |
| 2837         | 2836   | 2    | 1670                | 1640             | 95               | 0.35        | 0.14          |              |      |   |   |
| 2836         | 2835   | 5    | 1640                | 1166             | 1224             |             |               |              |      |   |   |
| 2836         | 2835   | 8    |                     |                  |                  | 0.28        | 14.49         |              |      |   |   |
| 2835         | 2838   | 3    | 1166                | 1160             | 50               |             |               |              |      |   |   |
| 2838         | 2838   | 1    |                     |                  |                  |             |               | 2 of 2       |      |   |   |
|              |        |      |                     |                  |                  |             |               |              |      |   |   |
| 2838         | 2838.5 | 5    | 1160                | 1115             | 340              |             | *             |              |      |   |   |
| 2838.5       | 2838.5 | 1    |                     |                  |                  |             |               | 1 OF 2       |      |   |   |
|              |        |      |                     |                  |                  |             |               |              |      |   |   |
| 2834         | 2833   | 2    | 1380                | 1355             | 80               | 0.25        | 0.06          |              |      |   |   |
| 2833         | 2838.5 | 5    | 1355                | 1115             | 665              |             | *             |              |      |   |   |
| 2838.5       | 2838.5 | 1    |                     |                  |                  |             |               | 2 OF 2       |      |   |   |
| 2838.5       | 2832   | 5    | 1115                | 996              | 720              |             |               |              |      |   |   |
| 2838.5       | 2832   | 8    |                     |                  |                  | 0.25        | 8.35          |              |      |   |   |
| 2832         | 2832   | 1    |                     |                  |                  |             |               | 1 OF 2       |      |   |   |
|              |        |      |                     |                  |                  |             |               |              |      |   |   |
| 2831         | 2830   | 2    | 1250                | 1205             | 100              | 0.25        | 0.18          |              |      |   |   |
| 2830         | 2829   | 5    | 1205                | 1005             | 425              |             |               |              |      |   |   |
| 2830         | 2829   | 8    |                     |                  |                  | 0.32        | 7.31          |              |      |   |   |
| 2829         | 2832   | 3    | 1005                | 995              | 56               |             |               |              |      |   |   |
| 2832         | 2832   | 1    |                     |                  |                  |             |               | 2 of 2       |      |   |   |
|              |        |      |                     |                  |                  |             |               |              |      |   |   |
| 2832         | 2828   | 3    | 995                 | 979              | 73               |             |               |              |      |   |   |
| 2828         | 2828   | 11   |                     |                  |                  |             |               | Add Bank 1   |      |   |   |
| 2828         | 2828   | 12   |                     |                  |                  |             |               | Clear Bank 1 |      |   |   |
|              |        |      |                     |                  |                  |             |               |              |      |   |   |
| 2828         | 2827   | 3    | 979                 | 946              | 358              |             |               |              |      |   |   |
| 2827         | 2827   | 1    |                     |                  |                  |             |               | 1 of 2       |      |   |   |
|              |        |      |                     |                  |                  |             |               |              |      |   |   |
| 2826         | 2825   | 2    | 1025                | 1012             | 95               | 0.88        | 0.07          |              |      |   |   |
| 2825         | 2824   | 6    | 1012                | 960              | 394              | 0.88        | 0.37          | 2 Sides      |      |   |   |
| 2824         | 2823   | 3    | 954                 | 947              | 85               |             |               |              |      |   |   |
| 2823         | 2827   | 5    | 947                 | 946              | 26               |             | *             |              |      |   |   |
| 2823         | 2827   | 7    | Tc=3.27 A=0.4 Q=0.1 |                  |                  |             |               |              |      |   |   |
| 2827         | 2827   | 1    |                     |                  |                  |             |               | 2 of 2       |      |   |   |
| 2827         | 2822   | 3    | 946                 | 945              | 15               |             |               |              |      |   |   |
| 2822         | 28     | 5    | 945                 | 925              | 112              |             | *             |              |      |   |   |
| 28           | 28     | 10   |                     |                  |                  |             |               | Save Bank 1  |      |   |   |
|              |        |      |                     |                  |                  |             |               |              |      |   |   |
| 2821         | 2820   | 2    | 1736                | 1707             | 100              | 0.35        | 0.28          |              |      |   |   |
| 2820         | 2819   | 5    | 1707                | 1500             | 460              |             |               |              |      |   |   |
| 2820         | 2819   | 8    |                     |                  |                  | 0.35        | 3.50          |              |      |   |   |
| 2819         | 2818   | 5    | 1500                | 1200             | 1130             |             |               |              |      |   |   |
| 2819         | 2818   | 8    |                     |                  |                  | 0.3         | 16.92         |              |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

Fusco Engineering  
6390 Greenwich Drive  
Suite 200  
San Diego, CA 92122

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

- \* PROPOSED HYDROLOGY \*
  - \* SUBBASIN 28 WITH DETENTION AT NODE 2828 \*
  - \* JANUARY 2017 \*
- \*\*\*\*\*

FILE NAME: P-28D.DAT  
TIME/DATE OF STUDY: 09:20 01/30/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT- / PARK-<br>SIDE / SIDE / WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH LIP HIKE<br>(FT) (FT) (FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|--|------------------------|--|--------------------------|
| 1   | 18.0                   | 8.0                           | 0.020/0.020/0.020  | 0.50                   | 1.50 0.0313 0.125                                      | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*



\*\*\*\*\*

FLOW PROCESS FROM NODE 2860.00 TO NODE 2859.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00

UPSTREAM ELEVATION(FEET) = 1407.00

DOWNSTREAM ELEVATION(FEET) = 1395.00

ELEVATION DIFFERENCE(FEET) = 12.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.294

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.41

TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 2859.00 TO NODE 2858.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1395.00 DOWNSTREAM ELEVATION(FEET) = 1216.00

STREET LENGTH(FEET) = 1068.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.74

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.21

HALFSTREET FLOOD WIDTH(FEET) = 4.06

AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.61

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.37

STREET FLOW TRAVEL TIME(MIN.) = 2.69 Tc(MIN.) = 3.99

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.891  
SUBAREA AREA(ACRES) = 0.81 SUBAREA RUNOFF(CFS) = 6.65  
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 7.06

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 6.05  
FLOW VELOCITY(FEET/SEC.) = 7.30 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.80  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2858.00 = 1128.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2858.00 TO NODE 2857.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1210.00 DOWNSTREAM(FEET) = 1140.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.57  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.06  
PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 4.37  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2857.00 = 1528.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2857.00 TO NODE 2857.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.37  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.86  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.06

\*\*\*\*\*

FLOW PROCESS FROM NODE 2856.00 TO NODE 2855.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
 UPSTREAM ELEVATION(FEET) = 1215.00  
 DOWNSTREAM ELEVATION(FEET) = 1198.00  
 ELEVATION DIFFERENCE(FEET) = 17.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.744  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.57  
 TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2855.00 TO NODE 2857.00 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1198.00 DOWNSTREAM ELEVATION(FEET) = 1146.00  
 STREET LENGTH(FEET) = 295.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.50  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.16  
 HALFSTREET FLOOD WIDTH(FEET) = 1.50  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.92  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.24  
 STREET FLOW TRAVEL TIME(MIN.) = 0.62 Tc(MIN.) = 2.36  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
 SUBAREA AREA(ACRES) = 0.23 SUBAREA RUNOFF(CFS) = 1.87  
 TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 2.43

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.18 HALFSTREET FLOOD WIDTH(FEET) = 2.46

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FLOW VELOCITY(FEET/SEC.) = 6.81 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.19  
LONGEST FLOWPATH FROM NODE 2856.00 TO NODE 2857.00 = 385.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2857.00 TO NODE 2857.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.36  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.43

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 7.06         | 4.37      | 9.222                 | 0.86        |
| 2             | 2.43         | 2.36      | 9.222                 | 0.30        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 6.26         | 2.36      | 9.222                 |
| 2             | 9.50         | 4.37      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 9.50 Tc(MIN.) = 4.37  
TOTAL AREA(ACRES) = 1.2  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2857.00 = 1528.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2857.00 TO NODE 2854.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1140.00 DOWNSTREAM(FEET) = 1080.00  
FLOW LENGTH(FEET) = 410.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.91  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 9.50  
PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 4.75  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2854.00 = 1938.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2854.00 TO NODE 2854.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 4.75  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 1.16  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 2853.00 TO NODE 2852.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
UPSTREAM ELEVATION(FEET) = 1146.00  
DOWNSTREAM ELEVATION(FEET) = 1133.00  
ELEVATION DIFFERENCE(FEET) = 13.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.744  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.57  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2852.00 TO NODE 2854.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1133.00 DOWNSTREAM ELEVATION(FEET) = 1086.00  
STREET LENGTH(FEET) = 308.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.50  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.16  
HALFSTREET FLOOD WIDTH(FEET) = 1.50  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.37  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.15  
STREET FLOW TRAVEL TIME(MIN.) = 0.70 Tc(MIN.) = 2.44  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
SUBAREA AREA(ACRES) = 0.23 SUBAREA RUNOFF(CFS) = 1.87  
TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 2.43

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.18 HALFSTREET FLOOD WIDTH(FEET) = 2.73  
FLOW VELOCITY(FEET/SEC.) = 6.32 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.14  
LONGEST FLOWPATH FROM NODE 2853.00 TO NODE 2854.00 = 398.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2854.00 TO NODE 2854.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.44  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.43

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.50         | 4.75      | 9.222                 | 1.16        |
| 2             | 2.43         | 2.44      | 9.222                 | 0.30        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 11.93        | 2.44      | 9.222                 |
| 2             | 11.93        | 4.75      | 9.222                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.93 Tc(MIN.) = 4.75  
TOTAL AREA(ACRES) = 1.5  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2854.00 = 1938.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2854.00 TO NODE 2851.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1080.00 DOWNSTREAM(FEET) = 1019.00  
FLOW LENGTH(FEET) = 328.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.81  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.93  
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 5.01  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2851.00 = 2266.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2851.00 TO NODE 2851.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.01  
RAINFALL INTENSITY(INCH/HR) = 9.21  
TOTAL STREAM AREA(ACRES) = 1.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 2850.00 TO NODE 2849.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 92.00  
UPSTREAM ELEVATION(FEET) = 1086.00  
DOWNSTREAM ELEVATION(FEET) = 1070.00  
ELEVATION DIFFERENCE(FEET) = 16.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.763  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.57  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2849.00 TO NODE 2851.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1070.00 DOWNSTREAM ELEVATION(FEET) = 1025.00  
STREET LENGTH(FEET) = 233.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.31  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.16  
HALFSTREET FLOOD WIDTH(FEET) = 1.50  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.29  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.30  
STREET FLOW TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 2.23

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.887  
SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 1.48  
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 2.05

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.16 HALFSTREET FLOOD WIDTH(FEET) = 1.50



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FLOW VELOCITY(FEET/SEC.) = 8.29 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.30  
LONGEST FLOWPATH FROM NODE 2850.00 TO NODE 2851.00 = 325.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2851.00 TO NODE 2851.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.23  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.25  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.05

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 11.93        | 5.01      | 9.210                 | 1.46        |
| 2             | 2.05         | 2.23      | 9.222                 | 0.25        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 13.96        | 2.23      | 9.222                 |
| 2             | 13.97        | 5.01      | 9.210                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.97 Tc(MIN.) = 5.01  
TOTAL AREA(ACRES) = 1.7  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2851.00 = 2266.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2851.00 TO NODE 2848.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1019.00 DOWNSTREAM(FEET) = 980.00  
FLOW LENGTH(FEET) = 328.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.45  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

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PIPE-FLOW(CFS) = 13.97  
PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 5.31  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2848.00 = 2594.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2848.00 TO NODE 2828.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 980.00 DOWNSTREAM(FEET) = 979.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 15.00 CHANNEL SLOPE = 0.0667  
CHANNEL FLOW THRU SUBAREA(CFS) = 13.97  
FLOW VELOCITY(FEET/SEC) = 7.03 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 5.34  
LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2828.00 = 2609.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2828.00 TO NODE 2828.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 5.30 RAIN INTENSITY(INCH/HOUR) = 8.88  
TOTAL AREA(ACRES) = 1.70 TOTAL RUNOFF(CFS) = 1.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 2828.00 TO NODE 2828.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2847.00 TO NODE 2846.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1730.00  
DOWNSTREAM ELEVATION(FEET) = 1695.00  
ELEVATION DIFFERENCE(FEET) = 35.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.92

TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 0.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 2846.00 TO NODE 2845.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1695.00 DOWNSTREAM(FEET) = 1440.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 515.00 CHANNEL SLOPE = 0.4951
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .2245 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.92
FLOW VELOCITY(FEET/SEC) = 2.65 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.23 Tc(MIN.) = 9.50
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2845.00 = 615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2846.00 TO NODE 2845.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.095
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 3.06 SUBAREA RUNOFF(CFS) = 6.53
TOTAL AREA(ACRES) = 3.4 TOTAL RUNOFF(CFS) = 7.23
TC(MIN.) = 9.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 2845.00 TO NODE 2844.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1440.00 DOWNSTREAM(FEET) = 1325.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 395.00 CHANNEL SLOPE = 0.2911
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1928 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 7.23
FLOW VELOCITY(FEET/SEC) = 4.75 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.39 Tc(MIN.) = 10.89
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2844.00 = 1010.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2845.00 TO NODE 2844.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.583  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3351  
SUBAREA AREA(ACRES) = 9.88 SUBAREA RUNOFF(CFS) = 18.20  
TOTAL AREA(ACRES) = 13.3 TOTAL RUNOFF(CFS) = 24.83  
TC(MIN.) = 10.89

\*\*\*\*\*

FLOW PROCESS FROM NODE 2844.00 TO NODE 2843.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1325.00 DOWNSTREAM(FEET) = 1305.00  
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.17  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 24.83  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 10.93  
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2843.00 = 1090.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2843.00 TO NODE 2843.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.93  
RAINFALL INTENSITY(INCH/HR) = 5.57  
TOTAL STREAM AREA(ACRES) = 13.27  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 24.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 2842.00 TO NODE 2841.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500

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S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1395.00  
DOWNSTREAM ELEVATION(FEET) = 1390.00  
ELEVATION DIFFERENCE(FEET) = 5.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.895  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.868  
SUBAREA RUNOFF(CFS) = 0.26  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 2841.00 TO NODE 2840.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1390.00 DOWNSTREAM(FEET) = 1345.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 253.00 CHANNEL SLOPE = 0.1779  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1489 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.26  
FLOW VELOCITY(FEET/SEC) = 2.16 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 9.85  
LONGEST FLOWPATH FROM NODE 2842.00 TO NODE 2840.00 = 353.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2841.00 TO NODE 2840.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.956  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2936  
SUBAREA AREA(ACRES) = 1.72 SUBAREA RUNOFF(CFS) = 2.97  
TOTAL AREA(ACRES) = 1.8 TOTAL RUNOFF(CFS) = 3.20  
TC(MIN.) = 9.85

\*\*\*\*\*

FLOW PROCESS FROM NODE 2840.00 TO NODE 2839.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1339.00 DOWNSTREAM(FEET) = 1329.00  
FLOW LENGTH(FEET) = 37.00 MANNING'S N = 0.013

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ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.28  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.20  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 9.88  
LONGEST FLOWPATH FROM NODE 2842.00 TO NODE 2839.00 = 390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2839.00 TO NODE 2843.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1335.00 DOWNSTREAM(FEET) = 1305.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 178.00 CHANNEL SLOPE = 0.1685  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1443 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.20  
FLOW VELOCITY(FEET/SEC) = 3.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.95 Tc(MIN.) = 10.83  
LONGEST FLOWPATH FROM NODE 2842.00 TO NODE 2843.00 = 568.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2843.00 TO NODE 2843.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.83  
RAINFALL INTENSITY(INCH/HR) = 5.60  
TOTAL STREAM AREA(ACRES) = 1.83  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.20

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 24.83        | 10.93     | 5.567                 | 13.27       |
| 2             | 3.20         | 10.83     | 5.601                 | 1.83        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
|---------------|--------------|-----------|-----------------------|

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|   |       |       |       |
|---|-------|-------|-------|
| 1 | 27.79 | 10.83 | 5.601 |
| 2 | 28.01 | 10.93 | 5.567 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 28.01 Tc(MIN.) = 10.93

TOTAL AREA(ACRES) = 15.1

LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2843.00 = 1090.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2843.00 TO NODE 2838.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1305.00 DOWNSTREAM(FEET) = 1165.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 773.00 CHANNEL SLOPE = 0.1811

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1506 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 28.01

FLOW VELOCITY(FEET/SEC) = 6.59 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 12.89

LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2838.00 = 1863.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2843.00 TO NODE 2838.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.007

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.3067

SUBAREA AREA(ACRES) = 6.24 SUBAREA RUNOFF(CFS) = 7.81

TOTAL AREA(ACRES) = 21.3 TOTAL RUNOFF(CFS) = 32.77

TC(MIN.) = 12.89

\*\*\*\*\*

FLOW PROCESS FROM NODE 2838.00 TO NODE 2838.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.89

RAINFALL INTENSITY(INCH/HR) = 5.01

TOTAL STREAM AREA(ACRES) = 21.34

PEAK FLOW RATE(CFS) AT CONFLUENCE = 32.77

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2837.00 TO NODE 2836.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1670.00  
DOWNSTREAM ELEVATION(FEET) = 1640.00  
ELEVATION DIFFERENCE(FEET) = 30.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.108  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.105  
SUBAREA RUNOFF(CFS) = 0.40  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.40

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2836.00 TO NODE 2835.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1640.00 DOWNSTREAM(FEET) = 1166.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1224.00 CHANNEL SLOPE = 0.3873  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2118 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.40  
FLOW VELOCITY(FEET/SEC) = 2.58 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 7.92 Tc(MIN.) = 14.02  
LONGEST FLOWPATH FROM NODE 2837.00 TO NODE 2835.00 = 1319.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2836.00 TO NODE 2835.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.741  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2807  
SUBAREA AREA(ACRES) = 14.49 SUBAREA RUNOFF(CFS) = 19.24  
TOTAL AREA(ACRES) = 14.6 TOTAL RUNOFF(CFS) = 19.47  
TC(MIN.) = 14.02



\*\*\*\*\*

FLOW PROCESS FROM NODE 2835.00 TO NODE 2838.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1166.00 DOWNSTREAM(FEET) = 1160.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.12  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.47  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 14.07  
LONGEST FLOWPATH FROM NODE 2837.00 TO NODE 2838.00 = 1369.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2838.00 TO NODE 2838.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 14.07  
RAINFALL INTENSITY(INCH/HR) = 4.73  
TOTAL STREAM AREA(ACRES) = 14.63  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.47

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 32.77        | 12.89     | 5.007                 | 21.34       |
| 2             | 19.47        | 14.07     | 4.732                 | 14.63       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 50.61        | 12.89     | 5.007                 |
| 2             | 50.44        | 14.07     | 4.732                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 50.61 Tc(MIN.) = 12.89  
TOTAL AREA(ACRES) = 36.0

LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2838.00 = 1863.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2838.00 TO NODE 2838.50 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1160.00 DOWNSTREAM(FEET) = 1115.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 340.00 CHANNEL SLOPE = 0.1324
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1232 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 50.61
FLOW VELOCITY(FEET/SEC) = 7.26 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 0.78 Tc(MIN.) = 13.67
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2838.50 = 2203.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2838.50 TO NODE 2838.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.67
RAINFALL INTENSITY(INCH/HR) = 4.82
TOTAL STREAM AREA(ACRES) = 35.97
PEAK FLOW RATE(CFS) AT CONFLUENCE = 50.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 2834.00 TO NODE 2833.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 1380.00
DOWNSTREAM ELEVATION(FEET) = 1355.00
ELEVATION DIFFERENCE(FEET) = 25.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.352
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.902
SUBAREA RUNOFF(CFS) = 0.12
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.12

\*\*\*\*\*

FLOW PROCESS FROM NODE 2833.00 TO NODE 2838.50 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1355.00 DOWNSTREAM(FEET) = 1115.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 665.00 CHANNEL SLOPE = 0.3609
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .2072 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.12
FLOW VELOCITY(FEET/SEC) = 2.55 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.35 Tc(MIN.) = 10.70
LONGEST FLOWPATH FROM NODE 2834.00 TO NODE 2838.50 = 745.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2838.50 TO NODE 2838.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.70
RAINFALL INTENSITY(INCH/HR) = 5.65
TOTAL STREAM AREA(ACRES) = 0.06
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.12

\*\* CONFLUENCE DATA \*\*

Table with 5 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR), AREA (ACRE). Rows for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 4 columns: STREAM NUMBER, RUNOFF (CFS), Tc (MIN.), INTENSITY (INCH/HOUR). Rows for stream 1 and 2.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 50.71 Tc(MIN.) = 13.67
TOTAL AREA(ACRES) = 36.0
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2838.50 = 2203.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2838.50 TO NODE 2832.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1115.00 DOWNSTREAM(FEET) = 996.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 720.00 CHANNEL SLOPE = 0.1653  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1426 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 50.71  
FLOW VELOCITY(FEET/SEC) = 7.82 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.53 Tc(MIN.) = 15.20  
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2832.00 = 2923.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2838.50 TO NODE 2832.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.501  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2874  
SUBAREA AREA(ACRES) = 8.35 SUBAREA RUNOFF(CFS) = 9.40  
TOTAL AREA(ACRES) = 44.4 TOTAL RUNOFF(CFS) = 57.40  
TC(MIN.) = 15.20

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2832.00 TO NODE 2832.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.20  
RAINFALL INTENSITY(INCH/HR) = 4.50  
TOTAL STREAM AREA(ACRES) = 44.38  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 57.40

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2831.00 TO NODE 2830.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500

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S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1250.00  
DOWNSTREAM ELEVATION(FEET) = 1205.00  
ELEVATION DIFFERENCE(FEET) = 45.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.33  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 2830.00 TO NODE 2829.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1205.00 DOWNSTREAM(FEET) = 1005.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 425.00 CHANNEL SLOPE = 0.4706  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2221 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.33  
FLOW VELOCITY(FEET/SEC) = 2.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.68 Tc(MIN.) = 9.79  
LONGEST FLOWPATH FROM NODE 2831.00 TO NODE 2829.00 = 525.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2830.00 TO NODE 2829.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.980  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3183  
SUBAREA AREA(ACRES) = 7.31 SUBAREA RUNOFF(CFS) = 13.99  
TOTAL AREA(ACRES) = 7.5 TOTAL RUNOFF(CFS) = 14.26  
TC(MIN.) = 9.79

\*\*\*\*\*

FLOW PROCESS FROM NODE 2829.00 TO NODE 2832.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1005.00 DOWNSTREAM(FEET) = 995.00

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FLOW LENGTH(FEET) = 56.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.52  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.26  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 9.83  
LONGEST FLOWPATH FROM NODE 2831.00 TO NODE 2832.00 = 581.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2832.00 TO NODE 2832.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.83  
RAINFALL INTENSITY(INCH/HR) = 5.96  
TOTAL STREAM AREA(ACRES) = 7.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.26

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 57.40        | 15.20     | 4.501                 | 44.38       |
| 2             | 14.26        | 9.83      | 5.963                 | 7.49        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 57.58        | 9.83      | 5.963                 |
| 2             | 68.16        | 15.20     | 4.501                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 68.16 Tc(MIN.) = 15.20  
TOTAL AREA(ACRES) = 51.9  
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2832.00 = 2923.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2832.00 TO NODE 2828.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

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ELEVATION DATA: UPSTREAM(FEET) = 995.00 DOWNSTREAM(FEET) = 979.00  
FLOW LENGTH(FEET) = 73.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 33.33  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 68.16  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 15.24  
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2828.00 = 2996.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2828.00 TO NODE 2828.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 68.16        | 15.24     | 4.494                 | 51.87       |

LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2828.00 = 2996.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 1.00         | 5.30      | 8.881                 | 1.70        |

LONGEST FLOWPATH FROM NODE 2860.00 TO NODE 2828.00 = 2609.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 24.70        | 5.30      | 8.881                 |
| 2             | 68.66        | 15.24     | 4.494                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 68.66 Tc(MIN.) = 15.24  
TOTAL AREA(ACRES) = 53.6

\*\*\*\*\*

FLOW PROCESS FROM NODE 2828.00 TO NODE 2828.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 2828.00 TO NODE 2827.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 979.00 DOWNSTREAM(FEET) = 946.00  
FLOW LENGTH(FEET) = 358.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.75  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 68.66  
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 15.48  
LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2827.00 = 3354.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2827.00 TO NODE 2827.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 15.48  
RAINFALL INTENSITY(INCH/HR) = 4.45  
TOTAL STREAM AREA(ACRES) = 53.57  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 68.66

\*\*\*\*\*

FLOW PROCESS FROM NODE 2826.00 TO NODE 2825.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 95.00  
UPSTREAM ELEVATION(FEET) = 1025.00  
DOWNSTREAM ELEVATION(FEET) = 1012.00  
ELEVATION DIFFERENCE(FEET) = 13.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.792  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.57  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 2825.00 TO NODE 2824.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 1012.00 DOWNSTREAM ELEVATION(FEET) = 960.00



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STREET LENGTH(FEET) = 394.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.07  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.17  
HALFSTREET FLOOD WIDTH(FEET) = 2.33  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.00  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.04  
STREET FLOW TRAVEL TIME(MIN.) = 1.09 Tc(MIN.) = 2.89

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .8800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.880  
SUBAREA AREA(ACRES) = 0.37 SUBAREA RUNOFF(CFS) = 3.00  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.57

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 4.26  
FLOW VELOCITY(FEET/SEC.) = 5.97 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.26  
LONGEST FLOWPATH FROM NODE 2826.00 TO NODE 2824.00 = 489.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2824.00 TO NODE 2823.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 954.00 DOWNSTREAM(FEET) = 947.00  
FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.04  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.57  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 3.01  
LONGEST FLOWPATH FROM NODE 2826.00 TO NODE 2823.00 = 574.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2823.00 TO NODE 2827.00 IS CODE = 53

-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 947.00 DOWNSTREAM(FEET) = 946.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 26.00 CHANNEL SLOPE = 0.0385

SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .0385 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 3.57

FLOW VELOCITY(FEET/SEC) = 1.68 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 3.27

LONGEST FLOWPATH FROM NODE 2826.00 TO NODE 2827.00 = 600.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2827.00 TO NODE 2827.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 3.27

RAINFALL INTENSITY(INCH/HR) = 9.22

TOTAL STREAM AREA(ACRES) = 0.44

PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.57

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 68.66        | 15.48     | 4.448                 | 53.57       |
| 2             | 3.57         | 3.27      | 9.222                 | 0.44        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 18.08        | 3.27      | 9.222                 |
| 2             | 70.39        | 15.48     | 4.448                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 70.39 Tc(MIN.) = 15.48

TOTAL AREA(ACRES) = 54.0

LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 2827.00 = 3354.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2827.00 TO NODE 2822.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

|                                  |                   |                    |               |
|----------------------------------|-------------------|--------------------|---------------|
| ELEVATION DATA: UPSTREAM(FEET) = | 946.00            | DOWNSTREAM(FEET) = | 945.00        |
| FLOW LENGTH(FEET) =              | 15.00             | MANNING'S N =      | 0.013         |
| DEPTH OF FLOW IN                 | 27.0 INCH PIPE IS | 20.6               | INCHES        |
| PIPE-FLOW VELOCITY(FEET/SEC.) =  | 21.67             |                    |               |
| ESTIMATED PIPE DIAMETER(INCH) =  | 27.00             | NUMBER OF PIPES =  | 1             |
| PIPE-FLOW(CFS) =                 | 70.39             |                    |               |
| PIPE TRAVEL TIME(MIN.) =         | 0.01              | Tc(MIN.) =         | 15.49         |
| LONGEST FLOWPATH FROM NODE       | 2847.00 TO NODE   | 2822.00 =          | 3369.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2822.00 TO NODE 28.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

|                                     |                 |  |               |
|-------------------------------------|-----------------|--|---------------|
| ELEVATION DATA: UPSTREAM(FEET) =    | 945.00          | DOWNSTREAM(FEET) =                     | 925.00        |
| CHANNEL LENGTH THRU SUBAREA(FEET) = | 112.00          | CHANNEL SLOPE =                        | 0.1786        |
| SLOPE ADJUSTMENT CURVE USED:        |                 |  |               |
| EFFECTIVE SLOPE =                   | .1493           | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |               |
| CHANNEL FLOW THRU SUBAREA(CFS) =    | 70.39           |  |               |
| FLOW VELOCITY(FEET/SEC) =           | 8.92            | (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL) |               |
| TRAVEL TIME(MIN.) =                 | 0.21            | Tc(MIN.) =                             | 15.70         |
| LONGEST FLOWPATH FROM NODE          | 2847.00 TO NODE | 28.00 =                                | 3481.00 FEET. |

\*\*\*\*\*  
FLOW PROCESS FROM NODE 28.00 TO NODE 28.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2821.00 TO NODE 2820.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1736.00  
DOWNSTREAM ELEVATION(FEET) = 1707.00

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ELEVATION DIFFERENCE(FEET) = 29.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.78  
TOTAL AREA(ACRES) = 0.28 TOTAL RUNOFF(CFS) = 0.78

\*\*\*\*\*

FLOW PROCESS FROM NODE 2820.00 TO NODE 2819.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1707.00 DOWNSTREAM(FEET) = 1500.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 460.00 CHANNEL SLOPE = 0.4500  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2200 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.78  
FLOW VELOCITY(FEET/SEC) = 2.63 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.92 Tc(MIN.) = 9.19  
LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 2819.00 = 560.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2820.00 TO NODE 2819.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.229  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 3.50 SUBAREA RUNOFF(CFS) = 7.63  
TOTAL AREA(ACRES) = 3.8 TOTAL RUNOFF(CFS) = 8.24  
TC(MIN.) = 9.19

\*\*\*\*\*

FLOW PROCESS FROM NODE 2819.00 TO NODE 2818.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1500.00 DOWNSTREAM(FEET) = 1200.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1130.00 CHANNEL SLOPE = 0.2655  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1852 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 8.24

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FLOW VELOCITY(FEET/SEC) = 4.86 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.87 Tc(MIN.) = 13.06  
LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 2818.00 = 1690.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2819.00 TO NODE 2818.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.965  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3091  
SUBAREA AREA(ACRES) = 16.92 SUBAREA RUNOFF(CFS) = 25.20  
TOTAL AREA(ACRES) = 20.7 TOTAL RUNOFF(CFS) = 31.77  
TC(MIN.) = 13.06

\*\*\*\*\*

FLOW PROCESS FROM NODE 2818.00 TO NODE 2817.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1200.00 DOWNSTREAM(FEET) = 1070.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 890.00 CHANNEL SLOPE = 0.1461  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1324 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 31.77  
FLOW VELOCITY(FEET/SEC) = 6.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.30 Tc(MIN.) = 15.36  
LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 2817.00 = 2580.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2818.00 TO NODE 2817.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.471  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2883  
SUBAREA AREA(ACRES) = 11.28 SUBAREA RUNOFF(CFS) = 12.61  
TOTAL AREA(ACRES) = 32.0 TOTAL RUNOFF(CFS) = 41.22  
TC(MIN.) = 15.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 2817.00 TO NODE 2816.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1070.00 DOWNSTREAM(FEET) = 980.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 655.00 CHANNEL SLOPE = 0.1374
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1266 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
CHANNEL FLOW THRU SUBAREA(CFS) = 41.22
FLOW VELOCITY(FEET/SEC) = 6.87 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.59 Tc(MIN.) = 16.95
LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 2816.00 = 3235.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 2817.00 TO NODE 2816.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.196
\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2900
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2885
SUBAREA AREA(ACRES) = 5.72 SUBAREA RUNOFF(CFS) = 6.96
TOTAL AREA(ACRES) = 37.7 TOTAL RUNOFF(CFS) = 45.65
TC(MIN.) = 16.95

\*\*\*\*\*
FLOW PROCESS FROM NODE 2816.00 TO NODE 2816.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.95
RAINFALL INTENSITY(INCH/HR) = 4.20
TOTAL STREAM AREA(ACRES) = 37.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 45.65

\*\*\*\*\*
FLOW PROCESS FROM NODE 2815.00 TO NODE 2814.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0

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INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1260.00  
DOWNSTREAM ELEVATION(FEET) = 1235.00  
ELEVATION DIFFERENCE(FEET) = 25.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.353  
SUBAREA RUNOFF(CFS) = 0.55  
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 2814.00 TO NODE 2816.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1235.00 DOWNSTREAM(FEET) = 980.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1510.00 CHANNEL SLOPE = 0.1689  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1444 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.55  
FLOW VELOCITY(FEET/SEC) = 2.13 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 11.82 Tc(MIN.) = 18.93  
LONGEST FLOWPATH FROM NODE 2815.00 TO NODE 2816.00 = 1610.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2814.00 TO NODE 2816.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.908  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2893  
SUBAREA AREA(ACRES) = 15.71 SUBAREA RUNOFF(CFS) = 17.80  
TOTAL AREA(ACRES) = 16.0 TOTAL RUNOFF(CFS) = 18.10  
TC(MIN.) = 18.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 2816.00 TO NODE 2816.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

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TIME OF CONCENTRATION(MIN.) = 18.93  
RAINFALL INTENSITY(INCH/HR) = 3.91  
TOTAL STREAM AREA(ACRES) = 16.01  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.10

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 45.65        | 16.95     | 4.196                 | 37.70       |
| 2             | 18.10        | 18.93     | 3.908                 | 16.01       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 61.85        | 16.95     | 4.196                 |
| 2             | 60.60        | 18.93     | 3.908                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 61.85 Tc(MIN.) = 16.95  
TOTAL AREA(ACRES) = 53.7  
LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 2816.00 = 3235.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2816.00 TO NODE 2813.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 980.00 DOWNSTREAM(FEET) = 956.00  
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 38.56  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 61.85  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 16.98  
LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 2813.00 = 3310.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2813.00 TO NODE 28.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 965.00 DOWNSTREAM(FEET) = 925.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 375.00 CHANNEL SLOPE = 0.1067



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SLOPE ADJUSTMENT CURVE USED:

EFFECTIVE SLOPE = .1050 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

CHANNEL FLOW THRU SUBAREA(CFS) = 61.85

FLOW VELOCITY(FEET/SEC) = 7.17 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 0.87 Tc(MIN.) = 17.85

LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 28.00 = 3685.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 28.00 TO NODE 28.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 61.85        | 17.85     | 4.058                 | 53.71       |

LONGEST FLOWPATH FROM NODE 2821.00 TO NODE 28.00 = 3685.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 70.39        | 15.70     | 4.408                 | 54.01       |

LONGEST FLOWPATH FROM NODE 2847.00 TO NODE 28.00 = 3481.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 124.79       | 15.70     | 4.408                 |
| 2             | 126.65       | 17.85     | 4.058                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 126.65 Tc(MIN.) = 17.85

TOTAL AREA(ACRES) = 107.7

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 107.7 TC(MIN.) = 17.85

PEAK FLOW RATE(CFS) = 126.65

END OF RATIONAL METHOD ANALYSIS





| Node to Node |         | Code | Elev 1<br>(feet)     | Elev 2<br>(feet) | Length<br>(feet) | C<br>Factor | Area<br>(ac.) | Comments         | BANK |   |   |
|--------------|---------|------|----------------------|------------------|------------------|-------------|---------------|------------------|------|---|---|
|              |         |      |                      |                  |                  |             |               |                  | 1    | 2 | 3 |
| 2916         | 2915.2  | 2    | 1485                 | 1483             | 80               | 0.9         | 0.27          |                  |      |   |   |
| 2915.2       | 2915    | 5    | 1483                 | 1475             | 120              |             |               | valley           |      |   |   |
| 2915.2       | 2915    | 8    |                      |                  |                  | 0.9         | 0.30          |                  |      |   |   |
| 2915         | 2915    | 7    | Tc=5min A=0.57 Q=0.3 |                  |                  |             |               |                  |      |   |   |
| 2915         | 2917    | 3    | 1469                 | 1460             | 60               |             |               | WQ outlet        |      |   |   |
| 2917         | 2914.15 | 5    | 1460                 | 1410             | 170              |             |               | mtn              |      |   |   |
| 2917         | 2914.15 | 8    |                      |                  |                  | 0.35        | 3.21          |                  |      |   |   |
| 2914.15      | 2914.15 | 1    |                      |                  |                  |             |               | 1 of 2           |      |   |   |
| 2919.5       | 2919    | 2    | 1664                 | 1640             | 85               | 0.35        | 0.04          |                  |      |   |   |
| 2919         | 2918    | 5    | 1640                 | 1420             | 690              |             |               | mtn              |      |   |   |
| 2919         | 2918    | 8    |                      |                  |                  | 0.35        | 2.36          |                  |      |   |   |
| 2918         | 2914.15 | 3    | 1420                 | 1410             | 60               |             |               |                  |      |   |   |
| 2914.15      | 2914.15 | 1    |                      |                  |                  |             |               | 2 of 2           |      |   |   |
| 2914.15      | 2914    | 3    | 1410                 | 1405             | 35               |             |               |                  |      |   |   |
| 2914         | 2914    | 1    |                      |                  |                  |             |               | 1 of 2           |      |   |   |
| 2914.3       | 2914.2  | 2    | 1484                 | 1477             | 70               | 0.9         | 0.06          |                  |      |   |   |
| 2914.2       | 2914.1  | 6    | 1477                 | 1408             | 425              | 0.9         | 0.39          |                  |      |   |   |
| 2914.1       | 2914    | 3    | 1406                 | 1405             | 40               |             |               |                  |      |   |   |
| 2914         | 2914    | 1    |                      |                  |                  |             |               | 2 of 2 WQ outlet |      |   |   |
| 2914         | 2913    | 3    | 1399                 | 1398             | 50               |             |               |                  |      |   |   |
| 2913         | 2912    | 5    | 1398                 | 1290             | 575              |             |               | mtn              |      |   |   |
| 2913         | 2912    | 8    |                      |                  |                  | 0.35        | 4.69          |                  |      |   |   |
| 2912         | 2911    | 5    | 1290                 | 1025             | 1175             |             |               | mtn              |      |   |   |
| 2912         | 2911    | 8    |                      |                  |                  | 0.43        | 19.17         |                  |      |   |   |
| 2911         | 2910    | 5    | 1025                 | 835              | 830              |             |               | mtn              |      |   |   |
| 2911         | 2910    | 8    |                      |                  |                  | 0.43        | 23.79         |                  |      |   |   |
| 2910         | 29      | 5    | 835                  | 800              | 455              |             |               | valley           |      |   |   |
| 29           | 29      | 1    |                      |                  |                  |             |               | 1 of 2           |      |   |   |
| 2927         | 2926    | 2    | 1603                 | 1570             | 100              | 0.35        | 0.19          |                  |      |   |   |
| 2926         | 2925    | 5    | 1570                 | 1470             | 307              |             |               | mtn              |      |   |   |
| 2926         | 2925    | 8    |                      |                  |                  | 0.35        | 1.15          |                  |      |   |   |
| 2925         | 2924    | 5    | 1470                 | 1390             | 520              |             |               | mtn              |      |   |   |
| 2925         | 2924    | 8    |                      |                  |                  | 0.35        | 6.88          |                  |      |   |   |
| 2924         | 2922    | 5    | 1390                 | 1370             | 361              |             |               | mtn              |      |   |   |
| 2924         | 2922    | 8    |                      |                  |                  | 0.35        | 9.30          |                  |      |   |   |
| 2922         | 2921    | 5    | 1370                 | 1300             | 1235             |             |               | mtn              |      |   |   |
| 2922         | 2921    | 8    |                      |                  |                  | 0.43        | 29.57         |                  |      |   |   |
| 2921         | 2920    | 5    | 1300                 | 893              | 1300             |             |               | mtn              |      |   |   |
| 2921         | 2920    | 8    |                      |                  |                  | 0.44        | 15.07         |                  |      |   |   |
| 2920         | 29      | 5    | 893                  | 800              | 335              |             |               | mtn              |      |   |   |



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL

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Ver. 21.0 Release Date: 06/01/2014 License ID 1355

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* NEWLAND SIERRA - PROPOSED HYDROLOGY \*  
\* SUBBASIN 29 WITH DETENTION AT NODE 2915 \*  
\* JANUARY 2017 \*  
\*\*\*\*\*

FILE NAME: P-29D.DAT  
TIME/DATE OF STUDY: 15:28 01/30/2017

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.500  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

| NO. | HALF-<br>WIDTH<br>(FT) | CROWN TO<br>CROSSFALL<br>(FT) | STREET-CROSSFALL:<br>IN- / OUT-/<br>SIDE / SIDE/<br>WAY | CURB<br>HEIGHT<br>(FT) | GUTTER-GEOMETRIES:<br>WIDTH<br>(FT) | LIP<br>(FT) | HIKE<br>(FT) | MANNING<br>FACTOR<br>(n) |
|-----|------------------------|-------------------------------|---|------------------------|-------------------------------------|-------------|--------------|--------------------------|
| 1   | 30.0                   | 20.0                          | 0.018/0.018/0.020                                       | 0.67                   | 2.00                                | 0.0313      | 0.167        | 0.0150                   |

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

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FLOW PROCESS FROM NODE 2916.00 TO NODE 2915.20 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
UPSTREAM ELEVATION(FEET) = 1485.00  
DOWNSTREAM ELEVATION(FEET) = 1483.00  
ELEVATION DIFFERENCE(FEET) = 2.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.373  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 2.24  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 2.24

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FLOW PROCESS FROM NODE 2915.20 TO NODE 2915.00 IS CODE = 52

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>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1483.00 DOWNSTREAM(FEET) = 1475.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 120.00 CHANNEL SLOPE = 0.0667  
CHANNEL FLOW THRU SUBAREA(CFS) = 2.24  
FLOW VELOCITY(FEET/SEC) = 4.55 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 2.81  
LONGEST FLOWPATH FROM NODE 2916.00 TO NODE 2915.00 = 200.00 FEET.

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FLOW PROCESS FROM NODE 2915.20 TO NODE 2915.00 IS CODE = 81

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.9000  
SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 2.49  
TOTAL AREA(ACRES) = 0.6 TOTAL RUNOFF(CFS) = 4.73  
TC(MIN.) = 2.81

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FLOW PROCESS FROM NODE 2915.00 TO NODE 2915.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 5.00 RAIN INTENSITY(INCH/HOUR) = 9.22
TOTAL AREA(ACRES) = 0.60 TOTAL RUNOFF(CFS) = 0.30

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FLOW PROCESS FROM NODE 2915.00 TO NODE 2917.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1469.00 DOWNSTREAM(FEET) = 1460.00
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.57
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.30
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 5.15
LONGEST FLOWPATH FROM NODE 2916.00 TO NODE 2917.00 = 260.00 FEET.

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FLOW PROCESS FROM NODE 2917.00 TO NODE 2914.15 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1460.00 DOWNSTREAM(FEET) = 1410.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 170.00 CHANNEL SLOPE = 0.2941
SLOPE ADJUSTMENT CURVE USED:
EFFECTIVE SLOPE = .1935 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.30
FLOW VELOCITY(FEET/SEC) = 2.46 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.15 Tc(MIN.) = 6.30
LONGEST FLOWPATH FROM NODE 2916.00 TO NODE 2914.15 = 430.00 FEET.

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FLOW PROCESS FROM NODE 2917.00 TO NODE 2914.15 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.943
\*USER SPECIFIED(SUBAREA):
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3034  
SUBAREA AREA(ACRES) = 3.21 SUBAREA RUNOFF(CFS) = 8.92  
TOTAL AREA(ACRES) = 3.8 TOTAL RUNOFF(CFS) = 9.18  
TC(MIN.) = 6.30

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FLOW PROCESS FROM NODE 2914.15 TO NODE 2914.15 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.30  
RAINFALL INTENSITY(INCH/HR) = 7.94  
TOTAL STREAM AREA(ACRES) = 3.81  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.18

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FLOW PROCESS FROM NODE 2919.50 TO NODE 2919.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 1664.00  
DOWNSTREAM ELEVATION(FEET) = 1640.00  
ELEVATION DIFFERENCE(FEET) = 24.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.778  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.401  
SUBAREA RUNOFF(CFS) = 0.12  
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.12

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FLOW PROCESS FROM NODE 2919.00 TO NODE 2918.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1640.00 DOWNSTREAM(FEET) = 1420.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 690.00 CHANNEL SLOPE = 0.3188  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1997 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.12

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FLOW VELOCITY(FEET/SEC) = 2.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.60 Tc(MIN.) = 10.37  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2918.00 = 775.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2919.00 TO NODE 2918.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.760  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 2.36 SUBAREA RUNOFF(CFS) = 4.76  
TOTAL AREA(ACRES) = 2.4 TOTAL RUNOFF(CFS) = 4.84  
TC(MIN.) = 10.37

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FLOW PROCESS FROM NODE 2918.00 TO NODE 1914.15 IS CODE = 31

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1420.00 DOWNSTREAM(FEET) = 1410.00  
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.48  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 4.84  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 10.44  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 1914.15 = 835.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2914.15 TO NODE 2914.15 IS CODE = 1

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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.44  
RAINFALL INTENSITY(INCH/HR) = 5.74  
TOTAL STREAM AREA(ACRES) = 2.40  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.84

\*\* CONFLUENCE DATA \*\*



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| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 9.18         | 6.30      | 7.943                 | 3.81        |
| 2             | 4.84         | 10.44     | 5.737                 | 2.40        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 12.10        | 6.30      | 7.943                 |
| 2             | 11.47        | 10.44     | 5.737                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.10 Tc(MIN.) = 6.30  
TOTAL AREA(ACRES) = 6.2  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2914.15 = 835.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2914.15 TO NODE 2914.00 IS CODE = 31

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1410.00 DOWNSTREAM(FEET) = 1405.00  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.99  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.10  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 6.33  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2914.00 = 870.00 FEET.

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FLOW PROCESS FROM NODE 2914.00 TO NODE 2914.00 IS CODE = 1

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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.33  
RAINFALL INTENSITY(INCH/HR) = 7.92  
TOTAL STREAM AREA(ACRES) = 6.21  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.10

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FLOW PROCESS FROM NODE 2914.30 TO NODE 2914.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00

UPSTREAM ELEVATION(FEET) = 1484.00

DOWNSTREAM ELEVATION(FEET) = 1477.00

ELEVATION DIFFERENCE(FEET) = 7.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.398

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.50

TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 2914.20 TO NODE 2914.10 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 1477.00 DOWNSTREAM ELEVATION(FEET) = 1408.00

STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 8.0

STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.018

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.12

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.20

HALFSTREET FLOOD WIDTH(FEET) = 2.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.75

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.73

STREET FLOW TRAVEL TIME(MIN.) = 0.81 Tc(MIN.) = 2.21

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.222

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .9000

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S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 3.24  
TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 3.73

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.20 HALFSTREET FLOOD WIDTH(FEET) = 2.00  
FLOW VELOCITY(FEET/SEC.) = 8.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.73  
LONGEST FLOWPATH FROM NODE 2914.30 TO NODE 2914.10 = 495.00 FEET.

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FLOW PROCESS FROM NODE 2914.10 TO NODE 2914.00 IS CODE = 31

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1406.00 DOWNSTREAM(FEET) = 1405.00  
FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.30  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.73  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 2.30  
LONGEST FLOWPATH FROM NODE 2914.30 TO NODE 2914.00 = 535.00 FEET.

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FLOW PROCESS FROM NODE 2914.00 TO NODE 2914.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

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TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 2.30  
RAINFALL INTENSITY(INCH/HR) = 9.22  
TOTAL STREAM AREA(ACRES) = 0.45  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.73

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 12.10        | 6.33      | 7.918                 | 6.21        |
| 2             | 3.73         | 2.30      | 9.222                 | 0.45        |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 14.13        | 2.30      | 9.222                 |
| 2             | 15.31        | 6.33      | 7.918                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.31 Tc(MIN.) = 6.33  
TOTAL AREA(ACRES) = 6.7  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2914.00 = 870.00 FEET.

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FLOW PROCESS FROM NODE 2914.00 TO NODE 2913.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1399.00 DOWNSTREAM(FEET) = 1398.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.62  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.31  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 6.42  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2913.00 = 920.00 FEET.

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FLOW PROCESS FROM NODE 2913.00 TO NODE 2912.00 IS CODE = 53

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>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 1398.00 DOWNSTREAM(FEET) = 1290.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 575.00 CHANNEL SLOPE = 0.1878  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1539 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 15.31  
FLOW VELOCITY(FEET/SEC) = 5.45 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 8.18  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2912.00 = 1495.00 FEET.

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FLOW PROCESS FROM NODE 2913.00 TO NODE 2912.00 IS CODE = 81

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.714  
\*USER SPECIFIED(SUBAREA):

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RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3562  
SUBAREA AREA(ACRES) = 4.69 SUBAREA RUNOFF(CFS) = 11.02  
TOTAL AREA(ACRES) = 11.4 TOTAL RUNOFF(CFS) = 27.14  
TC(MIN.) = 8.18

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FLOW PROCESS FROM NODE 2912.00 TO NODE 2911.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1290.00 DOWNSTREAM(FEET) = 1025.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1175.00 CHANNEL SLOPE = 0.2255  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1718 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 27.14  
FLOW VELOCITY(FEET/SEC) = 6.97 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.81 Tc(MIN.) = 10.99  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2911.00 = 2670.00 FEET.

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FLOW PROCESS FROM NODE 2912.00 TO NODE 2911.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.549  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .4300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4025  
SUBAREA AREA(ACRES) = 19.17 SUBAREA RUNOFF(CFS) = 45.74  
TOTAL AREA(ACRES) = 30.5 TOTAL RUNOFF(CFS) = 68.18  
TC(MIN.) = 10.99

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FLOW PROCESS FROM NODE 2911.00 TO NODE 2910.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1025.00 DOWNSTREAM(FEET) = 835.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 830.00 CHANNEL SLOPE = 0.2289  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1730 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 68.18  
FLOW VELOCITY(FEET/SEC) = 9.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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TRAVEL TIME(MIN.) = 1.46 Tc(MIN.) = 12.44  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 2910.00 = 3500.00 FEET.

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FLOW PROCESS FROM NODE 2911.00 TO NODE 2910.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.121  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .4300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4146  
SUBAREA AREA(ACRES) = 23.79 SUBAREA RUNOFF(CFS) = 52.39  
TOTAL AREA(ACRES) = 54.3 TOTAL RUNOFF(CFS) = 115.31  
TC(MIN.) = 12.44

\*\*\*\*\*

FLOW PROCESS FROM NODE 2910.00 TO NODE 29.00 IS CODE = 52

-----  
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 835.00 DOWNSTREAM(FEET) = 800.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 455.00 CHANNEL SLOPE = 0.0769  
CHANNEL FLOW THRU SUBAREA(CFS) = 115.31  
FLOW VELOCITY(FEET/SEC) = 13.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 13.00  
LONGEST FLOWPATH FROM NODE 2919.50 TO NODE 29.00 = 3955.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 29.00 TO NODE 29.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 13.00  
RAINFALL INTENSITY(INCH/HR) = 4.98  
TOTAL STREAM AREA(ACRES) = 54.31  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 115.31

\*\*\*\*\*

FLOW PROCESS FROM NODE 2927.00 TO NODE 2926.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

P-29d.TXT

RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 1603.00  
DOWNSTREAM ELEVATION(FEET) = 1570.00  
ELEVATION DIFFERENCE(FEET) = 33.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.972  
SUBAREA RUNOFF(CFS) = 0.53  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 2926.00 TO NODE 2925.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1570.00 DOWNSTREAM(FEET) = 1470.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 307.00 CHANNEL SLOPE = 0.3257  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .2010 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.53  
FLOW VELOCITY(FEET/SEC) = 2.51 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.04 Tc(MIN.) = 8.30  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2925.00 = 407.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2926.00 TO NODE 2925.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.648  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 1.15 SUBAREA RUNOFF(CFS) = 2.68  
TOTAL AREA(ACRES) = 1.3 TOTAL RUNOFF(CFS) = 3.12  
TC(MIN.) = 8.30

\*\*\*\*\*

FLOW PROCESS FROM NODE 2925.00 TO NODE 2924.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

P-29d.TXT

ELEVATION DATA: UPSTREAM(FEET) = 1470.00 DOWNSTREAM(FEET) = 1390.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 520.00 CHANNEL SLOPE = 0.1538  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1369 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 3.12  
FLOW VELOCITY(FEET/SEC) = 3.03 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.86 Tc(MIN.) = 11.17  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2924.00 = 927.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2925.00 TO NODE 2924.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.491  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500  
SUBAREA AREA(ACRES) = 6.88 SUBAREA RUNOFF(CFS) = 13.22  
TOTAL AREA(ACRES) = 8.2 TOTAL RUNOFF(CFS) = 15.80  
TC(MIN.) = 11.17

\*\*\*\*\*

FLOW PROCESS FROM NODE 2924.00 TO NODE 2922.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1390.00 DOWNSTREAM(FEET) = 1370.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 361.00 CHANNEL SLOPE = 0.0554  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0554 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 15.80  
FLOW VELOCITY(FEET/SEC) = 3.30 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 1.82 Tc(MIN.) = 12.99  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2922.00 = 1288.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2924.00 TO NODE 2922.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.982  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500



P-29d.TXT

SUBAREA AREA(ACRES) = 9.30 SUBAREA RUNOFF(CFS) = 16.22  
TOTAL AREA(ACRES) = 17.5 TOTAL RUNOFF(CFS) = 30.55  
TC(MIN.) = 12.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 2922.00 TO NODE 2921.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1370.00 DOWNSTREAM(FEET) = 1300.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1235.00 CHANNEL SLOPE = 0.0567  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .0567 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 30.55  
FLOW VELOCITY(FEET/SEC) = 4.16 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 4.94 Tc(MIN.) = 17.93  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2921.00 = 2523.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2922.00 TO NODE 2921.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.046  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .4300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4002  
SUBAREA AREA(ACRES) = 29.57 SUBAREA RUNOFF(CFS) = 51.44  
TOTAL AREA(ACRES) = 47.1 TOTAL RUNOFF(CFS) = 76.25  
TC(MIN.) = 17.93

\*\*\*\*\*

FLOW PROCESS FROM NODE 2921.00 TO NODE 2920.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1300.00 DOWNSTREAM(FEET) = 893.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1300.00 CHANNEL SLOPE = 0.3131  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1983 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 76.25  
FLOW VELOCITY(FEET/SEC) = 10.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.05 Tc(MIN.) = 19.99  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 2920.00 = 3823.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2921.00 TO NODE 2920.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.773  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .4400  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4099  
SUBAREA AREA(ACRES) = 15.07 SUBAREA RUNOFF(CFS) = 25.02  
TOTAL AREA(ACRES) = 62.2 TOTAL RUNOFF(CFS) = 96.13  
TC(MIN.) = 19.99

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2920.00 TO NODE 29.00 IS CODE = 53

-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 893.00 DOWNSTREAM(FEET) = 800.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 335.00 CHANNEL SLOPE = 0.2776  
SLOPE ADJUSTMENT CURVE USED:  
EFFECTIVE SLOPE = .1892 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
CHANNEL FLOW THRU SUBAREA(CFS) = 96.13  
FLOW VELOCITY(FEET/SEC) = 11.14 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 20.49  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 29.00 = 4158.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2920.00 TO NODE 29.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.713  
\*USER SPECIFIED(SUBAREA):  
RESIDENTIAL (7.3 DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4251  
SUBAREA AREA(ACRES) = 27.04 SUBAREA RUNOFF(CFS) = 46.19  
TOTAL AREA(ACRES) = 89.2 TOTAL RUNOFF(CFS) = 140.79  
TC(MIN.) = 20.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 29.00 TO NODE 29.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 20.49  
RAINFALL INTENSITY(INCH/HR) = 3.71  
TOTAL STREAM AREA(ACRES) = 89.20  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 140.79

\*\* CONFLUENCE DATA \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) | AREA (ACRE) |
|---------------|--------------|-----------|-----------------------|-------------|
| 1             | 115.31       | 13.00     | 4.980                 | 54.31       |
| 2             | 140.79       | 20.49     | 3.713                 | 89.20       |

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

| STREAM NUMBER | RUNOFF (CFS) | Tc (MIN.) | INTENSITY (INCH/HOUR) |
|---------------|--------------|-----------|-----------------------|
| 1             | 204.62       | 13.00     | 4.980                 |
| 2             | 226.76       | 20.49     | 3.713                 |

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 226.76 Tc(MIN.) = 20.49  
TOTAL AREA(ACRES) = 143.5  
LONGEST FLOWPATH FROM NODE 2927.00 TO NODE 29.00 = 4158.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 143.5 TC(MIN.) = 20.49  
PEAK FLOW RATE(CFS) = 226.76

=====

END OF RATIONAL METHOD ANALYSIS



# APPENDIX A

AES  
Rational Method Hydrology

Proposed Condition

BASIN E

THE FOLLOWING SUBBASINS OF MAJOR BASIN E  
HAVE NO GRADING, THUS THERE IS NO CHANGE IN HYDROLOGY FOR  
THE PROPOSED CONDITION.

32

33

34

35