

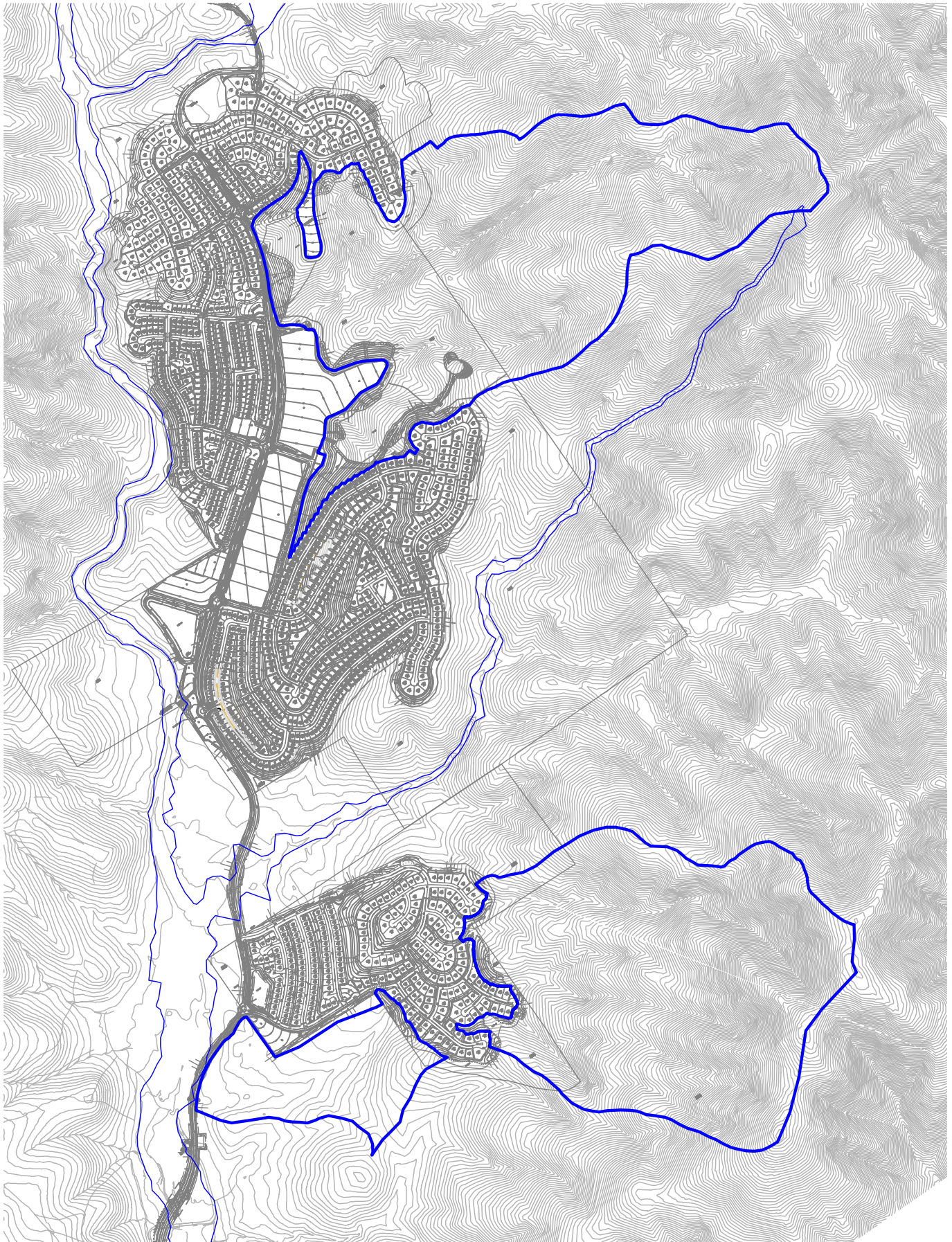
CHAPTER 4

4.1.3 – Rational Method Hydrologic Analysis (AES 2015)

Eastern Slopes Drainage Area bypassing WQ Basins

LAND EXCHANGE ALTERNATIVE

EASTERN SLOPES DRAINAGE AREA ROUTED THROUGH SITE (NOT TRIBUTARY TO ANY WQ BASIN)



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
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***** DESCRIPTION OF STUDY *****
* VILLAGE 14 TM HYDROLOGY ANALYSIS *
* OFFSITE SLOPES CONVEYED THROUGH SITE BUT NOT THROUGH WQ BASINS. *
* 100- YEAR RETURN INTERVAL. W.O. 2421-31. *

FILE NAME: R:\1235\HYD\CALCS\AES\TM\OFF.DAT
TIME/DATE OF STUDY: 16:41 06/01/2015

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.100
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	16.0	8.0	0.020/0.020/0.020	0.50	2.00 0.0313 0.125	0.0150
2	12.0	6.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0130

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 850.00 TO NODE 851.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1890.00
DOWNSTREAM ELEVATION(FEET) = 1880.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.061
SUBAREA RUNOFF(CFS) = 1.61
TOTAL AREA(ACRES) = 0.65 TOTAL RUNOFF(CFS) = 1.61

FLOW PROCESS FROM NODE 851.00 TO NODE 852.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1880.00 DOWNSTREAM(FEET) = 1425.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1052.00 CHANNEL SLOPE = 0.4325
CHANNEL FLOW THRU SUBAREA(CFS) = 1.61
FLOW VELOCITY(FEET/SEC) = 4.31 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.07 Tc(MIN.) = 10.33
LONGEST FLOWPATH FROM NODE 850.00 TO NODE 852.00 = 1152.00 FEET.

FLOW PROCESS FROM NODE 851.00 TO NODE 852.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.114
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0

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AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 18.66 SUBAREA RUNOFF(CFS) = 33.40
TOTAL AREA(ACRES) = 19.3 TOTAL RUNOFF(CFS) = 34.56
TC(MIN.) = 10.33

*****
FLOW PROCESS FROM NODE 852.00 TO NODE 853.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1425.00 DOWNSTREAM(FEET) = 1260.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1057.00 CHANNEL SLOPE = 0.1561
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 34.56
FLOW VELOCITY(FEET/SEC) = 11.02 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.60 Tc(MIN.) = 11.93
LONGEST FLOWPATH FROM NODE 850.00 TO NODE 853.00 = 2209.00 FEET.

*****
FLOW PROCESS FROM NODE 852.00 TO NODE 853.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.661
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 36.90 SUBAREA RUNOFF(CFS) = 60.20
TOTAL AREA(ACRES) = 56.2 TOTAL RUNOFF(CFS) = 91.70
TC(MIN.) = 11.93

*****
FLOW PROCESS FROM NODE 853.00 TO NODE 854.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1260.00 DOWNSTREAM(FEET) = 1150.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1048.00 CHANNEL SLOPE = 0.1050
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 91.70
FLOW VELOCITY(FEET/SEC) = 14.63 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.19 Tc(MIN.) = 13.13
LONGEST FLOWPATH FROM NODE 850.00 TO NODE 854.00 = 3257.00 FEET.

*****
FLOW PROCESS FROM NODE 853.00 TO NODE 854.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.383
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 31.63 SUBAREA RUNOFF(CFS) = 48.52
TOTAL AREA(ACRES) = 87.8 TOTAL RUNOFF(CFS) = 134.74
TC(MIN.) = 13.13

*****
FLOW PROCESS FROM NODE 854.00 TO NODE 855.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1150.00 DOWNSTREAM(FEET) = 1040.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 992.00 CHANNEL SLOPE = 0.1109
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 134.74
FLOW VELOCITY(FEET/SEC) = 16.43 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.01 Tc(MIN.) = 14.13
LONGEST FLOWPATH FROM NODE 850.00 TO NODE 855.00 = 4249.00 FEET.

*****
FLOW PROCESS FROM NODE 854.00 TO NODE 855.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.179
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 32.36 SUBAREA RUNOFF(CFS) = 47.33
TOTAL AREA(ACRES) = 120.2 TOTAL RUNOFF(CFS) = 175.80
TC(MIN.) = 14.13

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FLOW PROCESS FROM NODE      855.00 TO NODE      856.00 IS CODE =   52
-----
>>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1040.00 DOWNSTREAM(FEET) =    880.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  1077.00 CHANNEL SLOPE =   0.1486
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =    175.80
FLOW VELOCITY(FEET/SEC) =   17.82 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =    1.01 Tc(MIN.) =   15.14
LONGEST FLOWPATH FROM NODE      850.00 TO NODE      856.00 =   5326.00 FEET.

*****
FLOW PROCESS FROM NODE      855.00 TO NODE      856.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   3.997
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =   37.32 SUBAREA RUNOFF(CFS) =   52.21
TOTAL AREA(ACRES) =   157.5 TOTAL RUNOFF(CFS) =   220.38
TC(MIN.) =   15.14

*****
FLOW PROCESS FROM NODE      856.00 TO NODE      857.00 IS CODE =   52
-----
>>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    880.00 DOWNSTREAM(FEET) =   750.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  1297.00 CHANNEL SLOPE =   0.1002
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =    220.38
FLOW VELOCITY(FEET/SEC) =   19.11 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =    1.13 Tc(MIN.) =   16.27
LONGEST FLOWPATH FROM NODE      850.00 TO NODE      857.00 =   6623.00 FEET.

*****
FLOW PROCESS FROM NODE      856.00 TO NODE      857.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   3.816
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =   42.96 SUBAREA RUNOFF(CFS) =   57.37
TOTAL AREA(ACRES) =   200.5 TOTAL RUNOFF(CFS) =   267.75
TC(MIN.) =   16.27

*****
FLOW PROCESS FROM NODE      858.00 TO NODE      857.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   3.816
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =    5.02 SUBAREA RUNOFF(CFS) =    6.70
TOTAL AREA(ACRES) =   205.5 TOTAL RUNOFF(CFS) =   274.45
TC(MIN.) =   16.27

*****
FLOW PROCESS FROM NODE      857.00 TO NODE      859.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    750.00 DOWNSTREAM(FEET) =   740.00
FLOW LENGTH(FEET) =   400.00 MANNING'S N =   0.013
DEPTH OF FLOW IN 54.0 INCH PIPE IS 40.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   21.58
ESTIMATED PIPE DIAMETER(INCH) =  54.00 NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =    274.45
PIPE TRAVEL TIME(MIN.) =    0.31 Tc(MIN.) =   16.58
LONGEST FLOWPATH FROM NODE      850.00 TO NODE      859.00 =   7023.00 FEET.

*****
FLOW PROCESS FROM NODE      859.00 TO NODE      859.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =    2

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CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.58
RAINFALL INTENSITY(INCH/HR) = 3.77
TOTAL STREAM AREA(ACRES) = 205.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 274.45

*****
FLOW PROCESS FROM NODE 860.00 TO NODE 861.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 915.00
DOWNSTREAM ELEVATION(FEET) = 905.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.061
SUBAREA RUNOFF(CFS) = 0.82
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 0.82

*****
FLOW PROCESS FROM NODE 861.00 TO NODE 862.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 905.00 DOWNSTREAM(FEET) = 800.00
FLOW LENGTH(FEET) = 1115.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.62
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.82
PIPE TRAVEL TIME(MIN.) = 2.44 Tc(MIN.) = 8.70
LONGEST FLOWPATH FROM NODE 860.00 TO NODE 862.00 = 1215.00 FEET.

*****
FLOW PROCESS FROM NODE 861.00 TO NODE 862.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.712
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 9.02 SUBAREA RUNOFF(CFS) = 18.03
TOTAL AREA(ACRES) = 9.4 TOTAL RUNOFF(CFS) = 18.69
Tc(MIN.) = 8.70

*****
FLOW PROCESS FROM NODE 862.00 TO NODE 859.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 800.00 DOWNSTREAM(FEET) = 740.00
FLOW LENGTH(FEET) = 986.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.64
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 18.69
PIPE TRAVEL TIME(MIN.) = 1.05 Tc(MIN.) = 9.75
LONGEST FLOWPATH FROM NODE 860.00 TO NODE 859.00 = 2201.00 FEET.

*****
FLOW PROCESS FROM NODE 859.00 TO NODE 859.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.75
RAINFALL INTENSITY(INCH/HR) = 5.31
TOTAL STREAM AREA(ACRES) = 9.35
PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.69

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 274.45 16.58 3.770 205.50
2 18.69 9.75 5.307 9.35

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

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** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
  1         180.18      9.75      5.307
  2         287.73     16.58      3.770

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =      287.73   Tc(MIN.) =    16.58
TOTAL AREA(ACRES) =      214.8
LONGEST FLOWPATH FROM NODE      850.00 TO NODE      859.00 =    7023.00 FEET.

*****
FLOW PROCESS FROM NODE      859.00 TO NODE      863.00 IS CODE =   31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    740.00  DOWNSTREAM(FEET) =    705.00
FLOW LENGTH(FEET) =    1318.00  MANNING'S N =    0.013
DEPTH OF FLOW IN  54.0 INCH PIPE IS  40.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    22.28
ESTIMATED PIPE DIAMETER(INCH) =    54.00    NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =      287.73
PIPE TRAVEL TIME(MIN.) =    0.99    Tc(MIN.) =    17.56
LONGEST FLOWPATH FROM NODE      850.00 TO NODE      863.00 =    8341.00 FEET.

*****
FLOW PROCESS FROM NODE      863.00 TO NODE      863.00 IS CODE =   10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====

*****
FLOW PROCESS FROM NODE      865.00 TO NODE      866.00 IS CODE =   21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =    100.00
UPSTREAM ELEVATION(FEET) =    1540.00
DOWNSTREAM ELEVATION(FEET) =    1530.00
ELEVATION DIFFERENCE(FEET) =    10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    7.061
SUBAREA RUNOFF(CFS) =    0.49
TOTAL AREA(ACRES) =    0.20    TOTAL RUNOFF(CFS) =    0.49

*****
FLOW PROCESS FROM NODE      866.00 TO NODE      867.00 IS CODE =   53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    1530.00  DOWNSTREAM(FEET) =    1175.00
CHANNEL LENGTH THRU SUBAREA(FEET) =    1014.00  CHANNEL SLOPE =    0.3501
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =    0.49
FLOW VELOCITY(FEET/SEC) =    3.31 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =    5.10    Tc(MIN.) =    11.37
LONGEST FLOWPATH FROM NODE      865.00 TO NODE      867.00 =    1114.00 FEET.

*****
FLOW PROCESS FROM NODE      866.00 TO NODE      867.00 IS CODE =   81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.809
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =    12.73  SUBAREA RUNOFF(CFS) =    21.43
TOTAL AREA(ACRES) =    12.9    TOTAL RUNOFF(CFS) =    21.76
TC(MIN.) =    11.37

*****
FLOW PROCESS FROM NODE      867.00 TO NODE      868.00 IS CODE =   52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    1175.00  DOWNSTREAM(FEET) =    930.00
CHANNEL LENGTH THRU SUBAREA(FEET) =    1050.00  CHANNEL SLOPE =    0.2333
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =    21.76
FLOW VELOCITY(FEET/SEC) =    9.69 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

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TRAVEL TIME(MIN.) = 1.81    Tc(MIN.) = 13.17
LONGEST FLOWPATH FROM NODE 865.00 TO NODE 868.00 = 2164.00 FEET.

*****
FLOW PROCESS FROM NODE 867.00 TO NODE 868.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.373
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 22.59 SUBAREA RUNOFF(CFS) = 34.57
TOTAL AREA(ACRES) = 35.5 TOTAL RUNOFF(CFS) = 54.36
TC(MIN.) = 13.17

*****
FLOW PROCESS FROM NODE 868.00 TO NODE 869.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 930.00 DOWNSTREAM(FEET) = 780.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1086.00 CHANNEL SLOPE = 0.1381
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 54.36
FLOW VELOCITY(FEET/SEC) = 12.54 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.44 Tc(MIN.) = 14.62
LONGEST FLOWPATH FROM NODE 865.00 TO NODE 869.00 = 3250.00 FEET.

*****
FLOW PROCESS FROM NODE 868.00 TO NODE 869.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.089
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 44.20 SUBAREA RUNOFF(CFS) = 63.26
TOTAL AREA(ACRES) = 79.7 TOTAL RUNOFF(CFS) = 114.09
TC(MIN.) = 14.62

*****
FLOW PROCESS FROM NODE 869.00 TO NODE 872.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 780.00 DOWNSTREAM(FEET) = 755.00
FLOW LENGTH(FEET) = 730.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 28.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.36
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 114.09
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 15.24
LONGEST FLOWPATH FROM NODE 865.00 TO NODE 872.00 = 3980.00 FEET.

*****
FLOW PROCESS FROM NODE 872.00 TO NODE 872.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 15.24
RAINFALL INTENSITY(INCH/HR) = 3.98
TOTAL STREAM AREA(ACRES) = 79.72
PEAK FLOW RATE(CFS) AT CONFLUENCE = 114.09

*****
FLOW PROCESS FROM NODE 870.00 TO NODE 871.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 950.00
DOWNSTREAM ELEVATION(FEET) = 940.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.061
SUBAREA RUNOFF(CFS) = 0.79
TOTAL AREA(ACRES) = 0.32 TOTAL RUNOFF(CFS) = 0.79

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*****
FLOW PROCESS FROM NODE      871.00 TO NODE      872.00 IS CODE =   52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    930.00 DOWNSTREAM(FEET) =    755.00
CHANNEL LENGTH THRU SUBAREA(FEET) =    864.00 CHANNEL SLOPE =    0.2025
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =          0.79
FLOW VELOCITY(FEET/SEC) =    4.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =    3.04 Tc(MIN.) =    9.30
LONGEST FLOWPATH FROM NODE      870.00 TO NODE      872.00 =    964.00 FEET.

*****
FLOW PROCESS FROM NODE      871.00 TO NODE      872.00 IS CODE =   81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    5.473
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT =    0.3500
SUBAREA AREA(ACRES) =    9.68 SUBAREA RUNOFF(CFS) =    18.54
TOTAL AREA(ACRES) =    10.0 TOTAL RUNOFF(CFS) =    19.15
TC(MIN.) =    9.30

*****
FLOW PROCESS FROM NODE      872.00 TO NODE      872.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =    9.30
RAINFALL INTENSITY(INCH/HR) =    5.47
TOTAL STREAM AREA(ACRES) =    10.00
PEAK FLOW RATE(CFS) AT CONFLUENCE =    19.15

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
1          114.09    15.24      3.980      79.72
2          19.15     9.30      5.473     10.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR  2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
1          88.78     9.30      5.473
2         128.02    15.24      3.980

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =    128.02 Tc(MIN.) =    15.24
TOTAL AREA(ACRES) =    89.7
LONGEST FLOWPATH FROM NODE      865.00 TO NODE      872.00 =    3980.00 FEET.

*****
FLOW PROCESS FROM NODE      872.00 TO NODE      877.00 IS CODE =   31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    755.00 DOWNSTREAM(FEET) =    730.00
FLOW LENGTH(FEET) =    460.00 MANNING'S N =    0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    24.04
ESTIMATED PIPE DIAMETER(INCH) =    36.00 NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =    128.02
PIPE TRAVEL TIME(MIN.) =    0.32 Tc(MIN.) =    15.56
LONGEST FLOWPATH FROM NODE      865.00 TO NODE      877.00 =    4440.00 FEET.

*****
FLOW PROCESS FROM NODE      877.00 TO NODE      877.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    15.56
RAINFALL INTENSITY(INCH/HR) =    3.93
TOTAL STREAM AREA(ACRES) =    89.72
PEAK FLOW RATE(CFS) AT CONFLUENCE =    128.02

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FLOW PROCESS FROM NODE      875.00 TO NODE      876.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(Feet) = 100.00
UPSTREAM ELEVATION(Feet) = 895.00
DOWNSTREAM ELEVATION(Feet) = 885.00
ELEVATION DIFFERENCE(Feet) = 10.00
SUBAREA OVERLAND TIME OF FLOW(Min.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.061
SUBAREA RUNOFF(CFS) = 0.72
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.72

*****
FLOW PROCESS FROM NODE      876.00 TO NODE      877.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(Feet) = 885.00 DOWNSTREAM(Feet) = 735.00
FLOW LENGTH(Feet) = 587.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.5 INCHES
PIPE-FLOW VELOCITY(Feet/Sec.) = 10.40
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.72
PIPE TRAVEL TIME(Min.) = 0.94 Tc(Min.) = 7.21
LONGEST FLOWPATH FROM NODE 875.00 TO NODE 877.00 = 687.00 FEET.

*****
FLOW PROCESS FROM NODE      876.00 TO NODE      877.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.451
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 2.92 SUBAREA RUNOFF(CFS) = 6.59
TOTAL AREA(ACRES) = 3.2 TOTAL RUNOFF(CFS) = 7.25
Tc(Min.) = 7.21

*****
FLOW PROCESS FROM NODE      877.00 TO NODE      877.00 IS CODE =  1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(Min.) = 7.21
RAINFALL INTENSITY(INCH/HR) = 6.45
TOTAL STREAM AREA(ACRES) = 3.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.25

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (Min.) (INCH/HOUR) (ACRE)
1 128.02 15.56 3.927 89.72
2 7.25 7.21 6.451 3.21

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (Min.) (INCH/HOUR)
1 85.17 7.21 6.451
2 132.43 15.56 3.927

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 132.43 Tc(Min.) = 15.56
TOTAL AREA(ACRES) = 92.9
LONGEST FLOWPATH FROM NODE 865.00 TO NODE 877.00 = 4440.00 FEET.

*****
FLOW PROCESS FROM NODE      877.00 TO NODE      878.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(Feet) = 730.00 DOWNSTREAM(Feet) = 720.00
FLOW LENGTH(Feet) = 288.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 28.5 INCHES
PIPE-FLOW VELOCITY(Feet/Sec.) = 20.41

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ESTIMATED PIPE DIAMETER(INCH) = 39.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 132.43
PIPE TRAVEL TIME(MIN.) = 0.24    Tc(MIN.) = 15.80
LONGEST FLOWPATH FROM NODE 865.00 TO NODE 878.00 = 4728.00 FEET.

*****
FLOW PROCESS FROM NODE 878.00 TO NODE 878.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 15.80
RAINFALL INTENSITY(INCH/HR) = 3.89
TOTAL STREAM AREA(ACRES) = 92.93
PEAK FLOW RATE(CFS) AT CONFLUENCE = 132.43

*****
FLOW PROCESS FROM NODE 880.00 TO NODE 881.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 880.00
DOWNSTREAM ELEVATION(FEET) = 870.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.061
SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) = 0.14    TOTAL RUNOFF(CFS) = 0.35

*****
FLOW PROCESS FROM NODE 881.00 TO NODE 882.00 IS CODE = 53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 870.00    DOWNSTREAM(FEET) = 725.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 650.00    CHANNEL SLOPE = 0.2231
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.35
FLOW VELOCITY(FEET/SEC) = 2.64 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.10    Tc(MIN.) = 10.36
LONGEST FLOWPATH FROM NODE 880.00 TO NODE 882.00 = 750.00 FEET.

*****
FLOW PROCESS FROM NODE 881.00 TO NODE 882.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.105
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 5.76    SUBAREA RUNOFF(CFS) = 10.29
TOTAL AREA(ACRES) = 5.9    TOTAL RUNOFF(CFS) = 10.54
TC(MIN.) = 10.36

*****
FLOW PROCESS FROM NODE 882.00 TO NODE 878.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 725.00    DOWNSTREAM(FEET) = 720.00
FLOW LENGTH(FEET) = 300.00    MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.31
ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.54
PIPE TRAVEL TIME(MIN.) = 0.60    Tc(MIN.) = 10.96
LONGEST FLOWPATH FROM NODE 880.00 TO NODE 878.00 = 1050.00 FEET.

*****
FLOW PROCESS FROM NODE 878.00 TO NODE 878.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.96
RAINFALL INTENSITY(INCH/HR) = 4.92
TOTAL STREAM AREA(ACRES) = 5.90
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.54

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** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
  1         132.43      15.80      3.889         92.93
  2          10.54      10.96      4.922          5.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
  1         115.18      10.96      4.922
  2         140.76      15.80      3.889

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =      140.76   Tc(MIN.) =      15.80
TOTAL AREA(ACRES) =           98.8
LONGEST FLOWPATH FROM NODE      865.00 TO NODE      878.00 =      4728.00 FEET.

*****
FLOW PROCESS FROM NODE      878.00 TO NODE      863.00 IS CODE =      31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =      720.00  DOWNSTREAM(FEET) =      705.00
FLOW LENGTH(FEET) =      478.00  MANNING'S N =      0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 31.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =      19.59
ESTIMATED PIPE DIAMETER(INCH) =      39.00  NUMBER OF PIPES =      1
PIPE-FLOW(CFS) =      140.76
PIPE TRAVEL TIME(MIN.) =      0.41   Tc(MIN.) =      16.20
LONGEST FLOWPATH FROM NODE      865.00 TO NODE      863.00 =      5206.00 FEET.

*****
FLOW PROCESS FROM NODE      863.00 TO NODE      863.00 IS CODE =      11
-----
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<
=====

** MAIN STREAM CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
  1         140.76      16.20      3.826         98.83
LONGEST FLOWPATH FROM NODE      865.00 TO NODE      863.00 =      5206.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
  1         287.73      17.56      3.632         214.85
LONGEST FLOWPATH FROM NODE      850.00 TO NODE      863.00 =      8341.00 FEET.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
  1         406.21      16.20      3.826
  2         421.36      17.56      3.632

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =      421.36   Tc(MIN.) =      17.56
TOTAL AREA(ACRES) =      313.7

*****
FLOW PROCESS FROM NODE      863.00 TO NODE      863.00 IS CODE =      12
-----
>>>>CLEAR MEMORY BANK # 1 <<<<
=====

*****
FLOW PROCESS FROM NODE      863.00 TO NODE      883.00 IS CODE =      31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =      705.00  DOWNSTREAM(FEET) =      618.00
FLOW LENGTH(FEET) =      3114.00  MANNING'S N =      0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 48.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =      24.63
ESTIMATED PIPE DIAMETER(INCH) =      60.00  NUMBER OF PIPES =      1
PIPE-FLOW(CFS) =      421.36
PIPE TRAVEL TIME(MIN.) =      2.11   Tc(MIN.) =      19.67
LONGEST FLOWPATH FROM NODE      850.00 TO NODE      883.00 =      11455.00 FEET.

+-----+
|                                             |
|                                             |
|                                             |
+-----+

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*****
FLOW PROCESS FROM NODE      900.00 TO NODE      901.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 1870.00
DOWNSTREAM ELEVATION(FEET) = 1860.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.061
SUBAREA RUNOFF(CFS) = 0.67
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 0.67

*****
FLOW PROCESS FROM NODE      901.00 TO NODE      902.00 IS CODE =  53
-----
>>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1860.00 DOWNSTREAM(FEET) = 1350.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1045.00 CHANNEL SLOPE = 0.4880
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.67
FLOW VELOCITY(FEET/SEC) = 3.91 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.45 Tc(MIN.) = 10.72
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 902.00 = 1145.00 FEET.

*****
FLOW PROCESS FROM NODE      901.00 TO NODE      902.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.995
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 21.52 SUBAREA RUNOFF(CFS) = 37.62
TOTAL AREA(ACRES) = 21.8 TOTAL RUNOFF(CFS) = 38.09
TC(MIN.) = 10.72

*****
FLOW PROCESS FROM NODE      902.00 TO NODE      903.00 IS CODE =  52
-----
>>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1350.00 DOWNSTREAM(FEET) = 960.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1672.00 CHANNEL SLOPE = 0.2333
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 38.09
FLOW VELOCITY(FEET/SEC) = 11.32 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.46 Tc(MIN.) = 13.18
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 903.00 = 2817.00 FEET.

*****
FLOW PROCESS FROM NODE      902.00 TO NODE      903.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.371
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 43.96 SUBAREA RUNOFF(CFS) = 67.26
TOTAL AREA(ACRES) = 65.8 TOTAL RUNOFF(CFS) = 100.59
TC(MIN.) = 13.18

*****
FLOW PROCESS FROM NODE      903.00 TO NODE      904.00 IS CODE =  52
-----
>>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 960.00 DOWNSTREAM(FEET) = 730.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 2069.00 CHANNEL SLOPE = 0.1112
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 100.59
FLOW VELOCITY(FEET/SEC) = 15.04 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 15.47
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 904.00 = 4886.00 FEET.

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FLOW PROCESS FROM NODE      903.00 TO NODE      904.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.942
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =  44.48  SUBAREA RUNOFF(CFS) =  61.36
TOTAL AREA(ACRES) =  110.2  TOTAL RUNOFF(CFS) =  152.07
TC(MIN.) =  15.47

*****
FLOW PROCESS FROM NODE      904.00 TO NODE      905.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  730.00  DOWNSTREAM(FEET) =  715.00
FLOW LENGTH(FEET) =  546.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 42.0 INCH PIPE IS 32.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  19.20
ESTIMATED PIPE DIAMETER(INCH) = 42.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  152.07
PIPE TRAVEL TIME(MIN.) =  0.47  Tc(MIN.) =  15.95
LONGEST FLOWPATH FROM NODE      900.00 TO NODE      905.00 =  5432.00 FEET.

*****
FLOW PROCESS FROM NODE      905.00 TO NODE      905.00 IS CODE =  10
-----
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====

*****
FLOW PROCESS FROM NODE      910.00 TO NODE      911.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =  0
INITIAL SUBAREA FLOW-LENGTH(FEET) =  100.00
UPSTREAM ELEVATION(FEET) =  1780.00
DOWNSTREAM ELEVATION(FEET) =  1770.00
ELEVATION DIFFERENCE(FEET) =  10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =  6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  7.061
SUBAREA RUNOFF(CFS) =  0.67
TOTAL AREA(ACRES) =  0.27  TOTAL RUNOFF(CFS) =  0.67

*****
FLOW PROCESS FROM NODE      911.00 TO NODE      912.00 IS CODE =  53
-----
>>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  1770.00  DOWNSTREAM(FEET) =  1240.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1025.00  CHANNEL SLOPE =  0.5171
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
NOTE: CHANNEL SLOPE OF .5 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =  0.67
FLOW VELOCITY(FEET/SEC) =  3.96 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =  4.31  Tc(MIN.) =  10.58
LONGEST FLOWPATH FROM NODE      910.00 TO NODE      912.00 =  1125.00 FEET.

*****
FLOW PROCESS FROM NODE      911.00 TO NODE      912.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.036
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =  11.69  SUBAREA RUNOFF(CFS) =  20.61
TOTAL AREA(ACRES) =  12.0  TOTAL RUNOFF(CFS) =  21.08
TC(MIN.) =  10.58

*****
FLOW PROCESS FROM NODE      912.00 TO NODE      913.00 IS CODE =  52
-----
>>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  1240.00  DOWNSTREAM(FEET) =  990.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1000.00  CHANNEL SLOPE =  0.2500
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION

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CHANNEL FLOW THRU SUBAREA(CFS) =      21.08
FLOW VELOCITY(FEET/SEC) =      9.61 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =      1.73   Tc(MIN.) =      12.31
LONGEST FLOWPATH FROM NODE      910.00 TO NODE      913.00 =      2125.00 FEET.

*****
FLOW PROCESS FROM NODE      912.00 TO NODE      913.00 IS CODE =      81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =      4.567
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =      0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =      19.69   SUBAREA RUNOFF(CFS) =      31.47
TOTAL AREA(ACRES) =      31.7   TOTAL RUNOFF(CFS) =      50.59
TC(MIN.) =      12.31

*****
FLOW PROCESS FROM NODE      913.00 TO NODE      914.00 IS CODE =      52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =      990.00   DOWNSTREAM(FEET) =      740.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1297.00   CHANNEL SLOPE =      0.1928
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =      50.59
FLOW VELOCITY(FEET/SEC) =      12.28 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =      1.76   Tc(MIN.) =      14.08
LONGEST FLOWPATH FROM NODE      910.00 TO NODE      914.00 =      3422.00 FEET.

*****
FLOW PROCESS FROM NODE      913.00 TO NODE      914.00 IS CODE =      81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =      4.190
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =      0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =      37.07   SUBAREA RUNOFF(CFS) =      54.36
TOTAL AREA(ACRES) =      68.7   TOTAL RUNOFF(CFS) =      100.77
TC(MIN.) =      14.08

*****
FLOW PROCESS FROM NODE      914.00 TO NODE      915.00 IS CODE =      31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =      740.00   DOWNSTREAM(FEET) =      739.00
FLOW LENGTH(FEET) =      200.00   MANNING'S N =      0.013
DEPTH OF FLOW IN 51.0 INCH PIPE IS 36.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =      9.23
ESTIMATED PIPE DIAMETER(INCH) = 51.00   NUMBER OF PIPES =      1
PIPE-FLOW(CFS) =      100.77
PIPE TRAVEL TIME(MIN.) =      0.36   Tc(MIN.) =      14.44
LONGEST FLOWPATH FROM NODE      910.00 TO NODE      915.00 =      3622.00 FEET.

*****
FLOW PROCESS FROM NODE      915.00 TO NODE      915.00 IS CODE =      1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =      2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =      14.44
RAINFALL INTENSITY(INCH/HR) =      4.12
TOTAL STREAM AREA(ACRES) =      68.72
PEAK FLOW RATE(CFS) AT CONFLUENCE =      100.77

*****
FLOW PROCESS FROM NODE      920.00 TO NODE      921.00 IS CODE =      21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =      0
INITIAL SUBAREA FLOW-LENGTH(FEET) =      100.00
UPSTREAM ELEVATION(FEET) =      1770.00
DOWNSTREAM ELEVATION(FEET) =      1760.00
ELEVATION DIFFERENCE(FEET) =      10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =      6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =      7.061
SUBAREA RUNOFF(CFS) =      0.59

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TOTAL AREA(ACRES) =      0.24  TOTAL RUNOFF(CFS) =      0.59

*****
FLOW PROCESS FROM NODE    921.00 TO NODE    922.00 IS CODE =  53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1760.00 DOWNSTREAM(FEET) =   1330.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  1171.00 CHANNEL SLOPE =  0.3672
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =         0.59
FLOW VELOCITY(FEET/SEC) =    3.39 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =    5.75 Tc(MIN.) =   12.02
LONGEST FLOWPATH FROM NODE    920.00 TO NODE    922.00 =   1271.00 FEET.

*****
FLOW PROCESS FROM NODE    921.00 TO NODE    922.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   4.639
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =   12.01 SUBAREA RUNOFF(CFS) =   19.50
TOTAL AREA(ACRES) =   12.2 TOTAL RUNOFF(CFS) =   19.89
TC(MIN.) =   12.02

*****
FLOW PROCESS FROM NODE    922.00 TO NODE    923.00 IS CODE =  52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1330.00 DOWNSTREAM(FEET) =   1080.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  1050.00 CHANNEL SLOPE =  0.2381
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =         19.89
FLOW VELOCITY(FEET/SEC) =    9.46 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =    1.85 Tc(MIN.) =   13.87
LONGEST FLOWPATH FROM NODE    920.00 TO NODE    923.00 =   2321.00 FEET.

*****
FLOW PROCESS FROM NODE    922.00 TO NODE    923.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   4.230
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =   26.58 SUBAREA RUNOFF(CFS) =   39.35
TOTAL AREA(ACRES) =   38.8 TOTAL RUNOFF(CFS) =   57.49
TC(MIN.) =   13.87

*****
FLOW PROCESS FROM NODE    923.00 TO NODE    924.00 IS CODE =  52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   1080.00 DOWNSTREAM(FEET) =    740.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  1722.00 CHANNEL SLOPE =  0.1974
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) =         57.49
FLOW VELOCITY(FEET/SEC) =   12.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =    2.25 Tc(MIN.) =   16.12
LONGEST FLOWPATH FROM NODE    920.00 TO NODE    924.00 =   4043.00 FEET.

*****
FLOW PROCESS FROM NODE    923.00 TO NODE    924.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   3.839
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =   33.93 SUBAREA RUNOFF(CFS) =   45.59
TOTAL AREA(ACRES) =   72.8 TOTAL RUNOFF(CFS) =   97.76
TC(MIN.) =   16.12

*****
FLOW PROCESS FROM NODE    924.00 TO NODE    915.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

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>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 740.00 DOWNSTREAM(FEET) = 739.00
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.94
ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 97.76
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 16.39
LONGEST FLOWPATH FROM NODE 920.00 TO NODE 915.00 = 4203.00 FEET.

*****
FLOW PROCESS FROM NODE 915.00 TO NODE 915.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 16.39
RAINFALL INTENSITY(INCH/HR) = 3.80
TOTAL STREAM AREA(ACRES) = 72.76
PEAK FLOW RATE(CFS) AT CONFLUENCE = 97.76

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HR) (ACRE)
1 100.77 14.44 4.122 68.72
2 97.76 16.39 3.798 72.76

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HR)
1 186.89 14.44 4.122
2 190.62 16.39 3.798

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 190.62 Tc(MIN.) = 16.39
TOTAL AREA(ACRES) = 141.5
LONGEST FLOWPATH FROM NODE 920.00 TO NODE 915.00 = 4203.00 FEET.

*****
FLOW PROCESS FROM NODE 915.00 TO NODE 925.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 739.00 DOWNSTREAM(FEET) = 735.00
FLOW LENGTH(FEET) = 310.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 54.0 INCH PIPE IS 39.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.43
ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 190.62
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 16.72
LONGEST FLOWPATH FROM NODE 920.00 TO NODE 925.00 = 4513.00 FEET.

*****
FLOW PROCESS FROM NODE 925.00 TO NODE 925.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.72
RAINFALL INTENSITY(INCH/HR) = 3.75
TOTAL STREAM AREA(ACRES) = 141.48
PEAK FLOW RATE(CFS) AT CONFLUENCE = 190.62

*****
FLOW PROCESS FROM NODE 930.00 TO NODE 931.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 850.00
DOWNSTREAM ELEVATION(FEET) = 840.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HR) = 7.061
SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.27

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FLOW PROCESS FROM NODE      931.00 TO NODE      932.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   840.00  DOWNSTREAM(FEET) =   740.00
FLOW LENGTH(FEET) =   463.00  MANNING'S N =   0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   1.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   7.35
ESTIMATED PIPE DIAMETER(INCH) =  18.00  NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =         0.27
PIPE TRAVEL TIME(MIN.) =   1.05  Tc(MIN.) =   7.32
LONGEST FLOWPATH FROM NODE      930.00 TO NODE      932.00 =   563.00 FEET.

*****
FLOW PROCESS FROM NODE      931.00 TO NODE      932.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   6.390
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) =   0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) =   2.76  SUBAREA RUNOFF(CFS) =   6.17
TOTAL AREA(ACRES) =   2.9  TOTAL RUNOFF(CFS) =   6.42
TC(MIN.) =   7.32

*****
FLOW PROCESS FROM NODE      932.00 TO NODE      925.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   735.00  DOWNSTREAM(FEET) =   730.00
FLOW LENGTH(FEET) =   348.00  MANNING'S N =   0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   9.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   7.02
ESTIMATED PIPE DIAMETER(INCH) =  18.00  NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =         6.42
PIPE TRAVEL TIME(MIN.) =   0.83  Tc(MIN.) =   8.14
LONGEST FLOWPATH FROM NODE      930.00 TO NODE      925.00 =   911.00 FEET.

*****
FLOW PROCESS FROM NODE      925.00 TO NODE      925.00 IS CODE =   1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) =   8.14
RAINFALL INTENSITY(INCH/HR) =   5.96
TOTAL STREAM AREA(ACRES) =   2.87
PEAK FLOW RATE(CFS) AT CONFLUENCE =   6.42

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)      (INCH/HOUR)      (ACRE)
1          190.62      16.72      3.749          141.48
2           6.42       8.14       5.964           2.87

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)      (INCH/HOUR)
1          126.24       8.14       5.964
2          194.65      16.72      3.749

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =   194.65  Tc(MIN.) =   16.72
TOTAL AREA(ACRES) =   144.4
LONGEST FLOWPATH FROM NODE      920.00 TO NODE      925.00 =   4513.00 FEET.

*****
FLOW PROCESS FROM NODE      925.00 TO NODE      905.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   730.00  DOWNSTREAM(FEET) =   720.00
FLOW LENGTH(FEET) =   286.00  MANNING'S N =   0.013
DEPTH OF FLOW IN  45.0 INCH PIPE IS  32.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  22.53
ESTIMATED PIPE DIAMETER(INCH) =  45.00  NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =   194.65

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PIPE TRAVEL TIME(MIN.) = 0.21    Tc(MIN.) = 16.93
LONGEST FLOWPATH FROM NODE 920.00 TO NODE 905.00 = 4799.00 FEET.

*****
FLOW PROCESS FROM NODE 905.00 TO NODE 905.00 IS CODE = 11
-----
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<
=====

** MAIN STREAM CONFLUENCE DATA **
STREAM    RUNOFF    Tc    INTENSITY    AREA
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)    (ACRE)
1         194.65    16.93    3.719    144.35
LONGEST FLOWPATH FROM NODE 920.00 TO NODE 905.00 = 4799.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **
STREAM    RUNOFF    Tc    INTENSITY    AREA
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)    (ACRE)
1         152.07    15.95    3.866    110.23
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 905.00 = 5432.00 FEET.

** PEAK FLOW RATE TABLE **
STREAM    RUNOFF    Tc    INTENSITY
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)
1         335.37    15.95    3.866
2         340.94    16.93    3.719

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 340.94    Tc(MIN.) = 16.93
TOTAL AREA(ACRES) = 254.6

*****
FLOW PROCESS FROM NODE 905.00 TO NODE 905.00 IS CODE = 12
-----
>>>>CLEAR MEMORY BANK # 1 <<<<
=====

*****
FLOW PROCESS FROM NODE 905.00 TO NODE 933.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 720.00    DOWNSTREAM(FEET) = 650.00
FLOW LENGTH(FEET) = 1281.00    MANNING'S N = 0.013
DEPTH OF FLOW IN 51.0 INCH PIPE IS 37.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 30.63
ESTIMATED PIPE DIAMETER(INCH) = 51.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 340.94
PIPE TRAVEL TIME(MIN.) = 0.70    Tc(MIN.) = 17.63
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 933.00 = 6713.00 FEET.

*****
FLOW PROCESS FROM NODE 933.00 TO NODE 934.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 650.00    DOWNSTREAM(FEET) = 615.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1105.00    CHANNEL SLOPE = 0.0317
CHANNEL FLOW THRU SUBAREA(CFS) = 340.94
FLOW VELOCITY(FEET/SEC) = 12.34 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.49    Tc(MIN.) = 19.12
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 934.00 = 7818.00 FEET.

*****
FLOW PROCESS FROM NODE 933.00 TO NODE 934.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.438
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 24.30    SUBAREA RUNOFF(CFS) = 29.24
TOTAL AREA(ACRES) = 278.9    TOTAL RUNOFF(CFS) = 340.94
TC(MIN.) = 19.12
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

*****
FLOW PROCESS FROM NODE 934.00 TO NODE 935.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 615.00    DOWNSTREAM(FEET) = 575.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1385.00    CHANNEL SLOPE = 0.0289
CHANNEL FLOW THRU SUBAREA(CFS) = 340.94
FLOW VELOCITY(FEET/SEC) = 11.78 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

```

```

TRAVEL TIME(MIN.) = 1.96   Tc(MIN.) = 21.08
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 935.00 = 9203.00 FEET.

*****
FLOW PROCESS FROM NODE 934.00 TO NODE 935.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.228
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 33.04 SUBAREA RUNOFF(CFS) = 37.33
TOTAL AREA(ACRES) = 311.9 TOTAL RUNOFF(CFS) = 352.45
TC(MIN.) = 21.08

*****
FLOW PROCESS FROM NODE 935.00 TO NODE 936.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 575.00 DOWNSTREAM(FEET) = 574.00
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 63.0 INCH PIPE IS 48.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.61
ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 352.45
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 21.13
LONGEST FLOWPATH FROM NODE 900.00 TO NODE 936.00 = 9263.00 FEET.

*****
FLOW PROCESS FROM NODE 936.00 TO NODE 936.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====

*****
FLOW PROCESS FROM NODE 940.00 TO NODE 941.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00
UPSTREAM ELEVATION(FEET) = 622.00
DOWNSTREAM ELEVATION(FEET) = 618.00
ELEVATION DIFFERENCE(FEET) = 4.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.428
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.328
SUBAREA RUNOFF(CFS) = 0.33
TOTAL AREA(ACRES) = 0.15 TOTAL RUNOFF(CFS) = 0.33

*****
FLOW PROCESS FROM NODE 941.00 TO NODE 942.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 618.00 DOWNSTREAM(FEET) = 600.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 406.00 CHANNEL SLOPE = 0.0443
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.33
FLOW VELOCITY(FEET/SEC) = 3.16 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.14 Tc(MIN.) = 9.57
LONGEST FLOWPATH FROM NODE 940.00 TO NODE 942.00 = 491.00 FEET.

*****
FLOW PROCESS FROM NODE 941.00 TO NODE 942.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.373
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 2.03 SUBAREA RUNOFF(CFS) = 3.82
TOTAL AREA(ACRES) = 2.2 TOTAL RUNOFF(CFS) = 4.10
TC(MIN.) = 9.57

*****
FLOW PROCESS FROM NODE 942.00 TO NODE 943.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

```

TIME OF CONCENTRATION(MIN.) = 9.57
 RAINFALL INTENSITY(INCH/HR) = 5.37
 TOTAL STREAM AREA(ACRES) = 2.18
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.10

The following input data taken from South hydrology model and is
 the discharge from the South WQ basin.

 FLOW PROCESS FROM NODE 208.00 TO NODE 208.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:
 TC(MIN) = 14.42 RAIN INTENSITY(INCH/HOUR) = 4.12
 TOTAL AREA(ACRES) = 140.97 TOTAL RUNOFF(CFS) = 306.69

 FLOW PROCESS FROM NODE 208.00 TO NODE 943.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 585.00 DOWNSTREAM(FEET) = 580.00
 FLOW LENGTH(FEET) = 294.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 45.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.14
 ESTIMATED PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 306.69
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 14.68
 LONGEST FLOWPATH FROM NODE 930.00 TO NODE 943.00 = 1205.00 FEET.

 FLOW PROCESS FROM NODE 943.00 TO NODE 943.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 14.68
 RAINFALL INTENSITY(INCH/HR) = 4.08
 TOTAL STREAM AREA(ACRES) = 140.97
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 306.69

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.10	9.57	5.373	2.18
2	306.69	14.68	4.078	140.97

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	204.09	9.57	5.373
2	309.80	14.68	4.078

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 309.80 Tc(MIN.) = 14.68
 TOTAL AREA(ACRES) = 143.1
 LONGEST FLOWPATH FROM NODE 930.00 TO NODE 943.00 = 1205.00 FEET.

 FLOW PROCESS FROM NODE 943.00 TO NODE 936.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 575.00 DOWNSTREAM(FEET) = 570.00
 FLOW LENGTH(FEET) = 294.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 46.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.16
 ESTIMATED PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 309.80
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 14.93
 LONGEST FLOWPATH FROM NODE 930.00 TO NODE 936.00 = 1499.00 FEET.

 FLOW PROCESS FROM NODE 936.00 TO NODE 936.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	309.80	14.93	4.033	143.15

LONGEST FLOWPATH FROM NODE 930.00 TO NODE 936.00 = 1499.00 FEET.

**** MEMORY BANK # 1 CONFLUENCE DATA ****

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	352.45	21.13	3.223	311.92

LONGEST FLOWPATH FROM NODE 900.00 TO NODE 936.00 = 9263.00 FEET.

**** PEAK FLOW RATE TABLE ****

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	558.81	14.93	4.033
2	600.06	21.13	3.223

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 600.06 Tc(MIN.) = 21.13
 TOTAL AREA(ACRES) = 455.1

 FLOW PROCESS FROM NODE 936.00 TO NODE 936.00 IS CODE = 12

 >>>>CLEAR MEMORY BANK # 1 <<<<
 =====

 FLOW PROCESS FROM NODE 936.00 TO NODE 944.00 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 570.00 DOWNSTREAM(FEET) = 569.00
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 75.0 INCH PIPE IS 56.8 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 24.08
 ESTIMATED PIPE DIAMETER(INCH) = 75.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 600.06
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 21.17
 LONGEST FLOWPATH FROM NODE 900.00 TO NODE 944.00 = 9313.00 FEET.
 =====
 END OF STUDY SUMMARY:
 TOTAL AREA(ACRES) = 455.1 TC(MIN.) = 21.17
 PEAK FLOW RATE(CFS) = 600.06
 =====
 END OF RATIONAL METHOD ANALYSIS

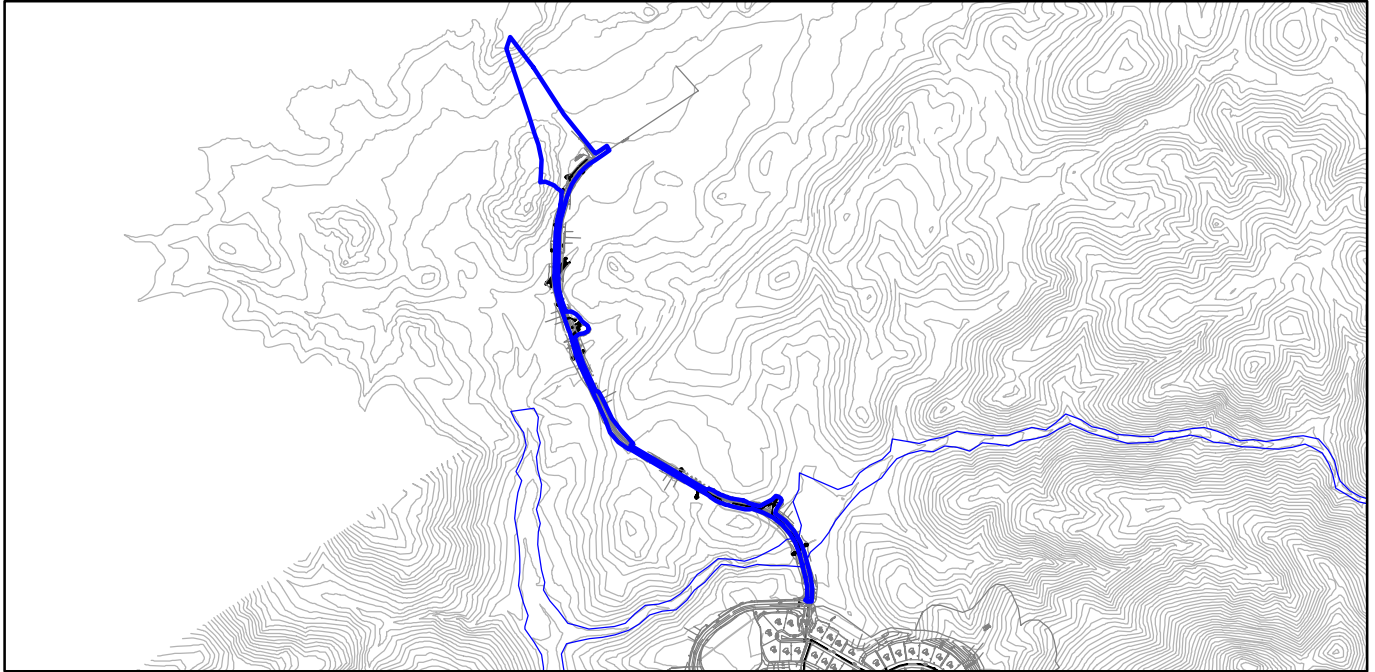
CHAPTER 4

4.1.4 – Rational Method Hydrologic Analysis (AES 2015)

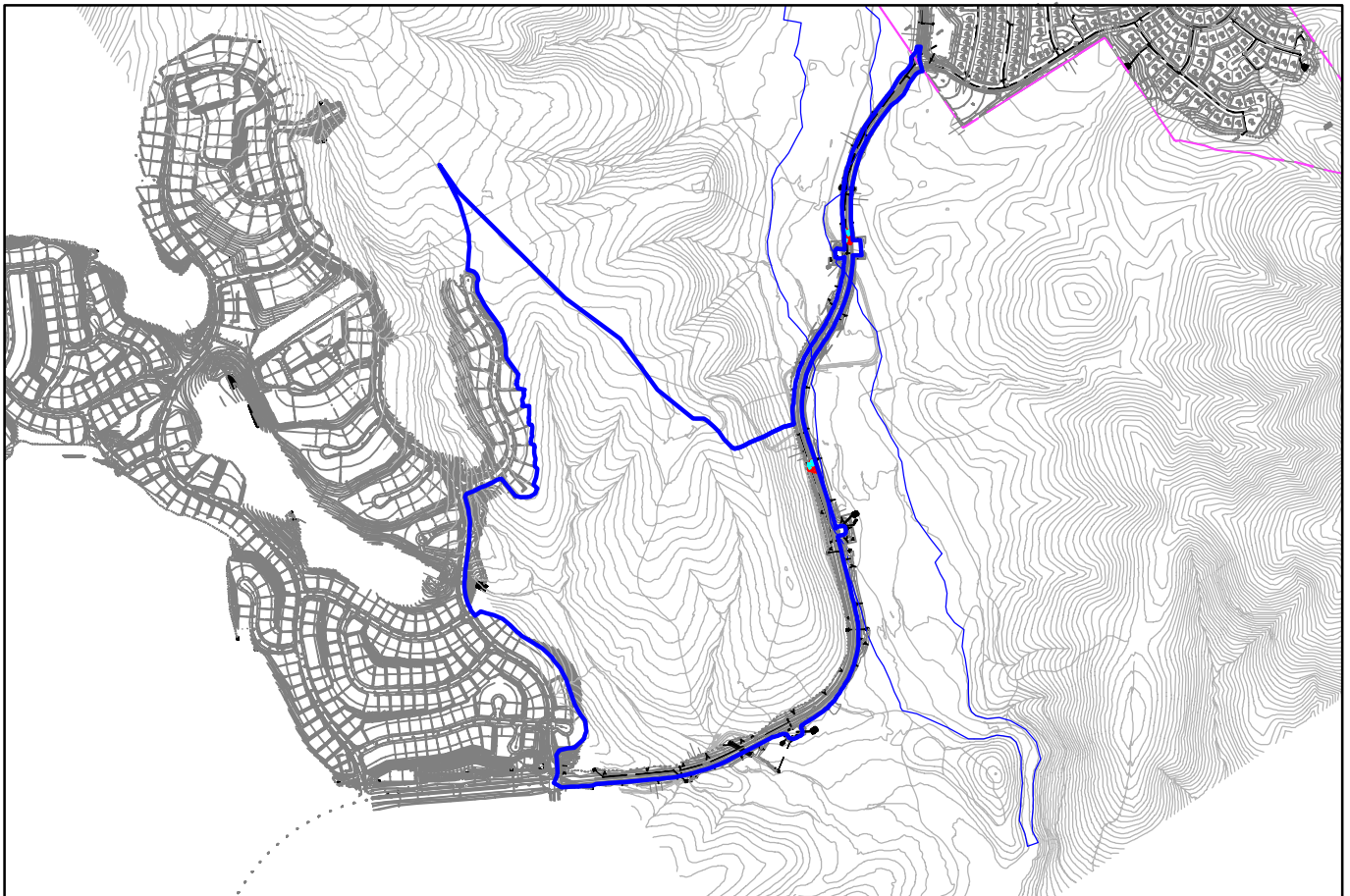
Drainage Areas Along Proctor Valley Road (North and South)

LAND EXCHANGE ALTERNATIVE DRAINAGE AREAS ALONG PROCTOR VALLEY ROAD

NORTHERN PORTION



SOUTHERN PORTION



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2015 Advanced Engineering Software (aes)
Ver. 22.0 Release Date: 07/01/2015 License ID 1239

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* VILLAGE 14 TM HYDROLOGY ANALYSIS *
* PVR-SOUTH *
* 100-YEAR RETURN INTERVAL. W.O. 2421-31 *

FILE NAME: R:\1235\HYD\CALCS\AES\TM\PVR-S.DAT
TIME/DATE OF STUDY: 16:32 10/25/2017

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.100
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS
USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
 HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
 WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 16.0 8.0 0.020/0.020/0.020 0.50 2.00 0.0313 0.125 0.0150
2 12.0 6.0 0.020/0.020/0.020 0.50 1.50 0.0313 0.125 0.0130

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .4100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 970.00
DOWNSTREAM ELEVATION(FEET) = 960.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.765
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.451
SUBAREA RUNOFF(CFS) = 0.61
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.61

FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STANDARD CURB SECTION USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 960.00 DOWNSTREAM ELEVATION(FEET) = 890.00
STREET LENGTH(FEET) = 1062.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

```

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.01
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 8.09
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.18
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.49
STREET FLOW TRAVEL TIME(MIN.) = 3.42 Tc(MIN.) = 9.18
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.518
*USER SPECIFIED(SUBAREA):
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .4200
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.420
SUBAREA AREA(ACRES) = 6.30 SUBAREA RUNOFF(CFS) = 14.60
TOTAL AREA(ACRES) = 6.5 PEAK FLOW RATE(CFS) = 15.05

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.66
FLOW VELOCITY(FEET/SEC.) = 6.00 DEPTH*VELOCITY(FT*FT/SEC.) = 2.04
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 12.00 = 1162.00 FEET.

*****
FLOW PROCESS FROM NODE 13.00 TO NODE 12.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.518
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4476
SUBAREA AREA(ACRES) = 0.45 SUBAREA RUNOFF(CFS) = 2.11
TOTAL AREA(ACRES) = 6.9 TOTAL RUNOFF(CFS) = 17.17
TC(MIN.) = 9.18

+-----+
| 0 |
| |
| |
+-----+

*****
FLOW PROCESS FROM NODE 20.00 TO NODE 21.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 901.00
DOWNSTREAM ELEVATION(FEET) = 900.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.789
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 60.00
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.74
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.74

*****
FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 900.00 DOWNSTREAM ELEVATION(FEET) = 896.00
STREET LENGTH(FEET) = 897.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 14.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.90
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

```

```

STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 7.74
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.33
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.37
STREET FLOW TRAVEL TIME(MIN.) = 11.27 Tc(MIN.) = 14.06
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.193
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 0.59 SUBAREA RUNOFF(CFS) = 2.23
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.60

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.94
FLOW VELOCITY(FEET/SEC.) = 1.42 DEPTH*VELOCITY(FT*FT/SEC.) = 0.43
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 22.00 = 997.00 FEET.

*****
FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 890.00 DOWNSTREAM(FEET) = 884.00
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.40
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.60
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 14.17
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 23.00 = 1067.00 FEET.

*****
FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.172
*USER SPECIFIED(SUBAREA):
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6950
SUBAREA AREA(ACRES) = 0.41 SUBAREA RUNOFF(CFS) = 0.60
TOTAL AREA(ACRES) = 1.1 TOTAL RUNOFF(CFS) = 3.19
TC(MIN.) = 14.17

*****
FLOW PROCESS FROM NODE 23.00 TO NODE 24.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 884.00 DOWNSTREAM(FEET) = 882.00
FLOW LENGTH(FEET) = 219.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.95
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.19
PIPE TRAVEL TIME(MIN.) = 0.74 Tc(MIN.) = 14.91
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 24.00 = 1286.00 FEET.

*****
FLOW PROCESS FROM NODE 24.00 TO NODE 24.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.91
RAINFALL INTENSITY(INCH/HR) = 4.04
TOTAL STREAM AREA(ACRES) = 1.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.19

*****
FLOW PROCESS FROM NODE 25.00 TO NODE 26.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00

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UPSTREAM ELEVATION(FEET) = 920.00
DOWNSTREAM ELEVATION(FEET) = 914.00
ELEVATION DIFFERENCE(FEET) = 6.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.618
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.53
TOTAL AREA(ACRES) = 0.22 TOTAL RUNOFF(CFS) = 1.53

*****
FLOW PROCESS FROM NODE 26.00 TO NODE 24.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 914.00 DOWNSTREAM ELEVATION(FEET) = 898.00
STREET LENGTH(FEET) = 681.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 14.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.46
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 7.85
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.03
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.86
STREET FLOW TRAVEL TIME(MIN.) = 3.74 Tc(MIN.) = 5.36
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.812
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.850
SUBAREA AREA(ACRES) = 0.88 SUBAREA RUNOFF(CFS) = 5.84
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 7.30

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.76
FLOW VELOCITY(FEET/SEC.) = 3.41 DEPTH*VELOCITY(FT*FT/SEC.) = 1.10
LONGEST FLOWPATH FROM NODE 25.00 TO NODE 24.00 = 741.00 FEET.

*****
FLOW PROCESS FROM NODE 24.00 TO NODE 24.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.36
RAINFALL INTENSITY(INCH/HR) = 7.81
TOTAL STREAM AREA(ACRES) = 1.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.30

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 3.19 14.91 4.037 1.10
2 7.30 5.36 7.812 1.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 8.45 5.36 7.812
2 6.96 14.91 4.037

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 8.45 Tc(MIN.) = 5.36
TOTAL AREA(ACRES) = 2.2
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 24.00 = 1286.00 FEET.

*****
FLOW PROCESS FROM NODE 24.00 TO NODE 27.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 882.00 DOWNSTREAM(FEET) = 880.00
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.65
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.45
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.44
LONGEST FLOWPATH FROM NODE 20.00 TO NODE 27.00 = 1341.00 FEET.

+-----+
| 0 |
+-----+

*****
FLOW PROCESS FROM NODE 30.00 TO NODE 31.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 920.00
DOWNSTREAM ELEVATION(FEET) = 911.00
ELEVATION DIFFERENCE(FEET) = 9.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.585
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.51
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.51

*****
FLOW PROCESS FROM NODE 31.00 TO NODE 32.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 911.00 DOWNSTREAM ELEVATION(FEET) = 908.00
STREET LENGTH(FEET) = 600.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 14.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.61
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 8.72
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.45
STREET FLOW TRAVEL TIME(MIN.) = 6.75 Tc(MIN.) = 8.33
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.876
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 0.77 SUBAREA RUNOFF(CFS) = 4.07
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 4.44

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.02
FLOW VELOCITY(FEET/SEC.) = 1.67 DEPTH*VELOCITY(FT*FT/SEC.) = 0.58
LONGEST FLOWPATH FROM NODE 30.00 TO NODE 32.00 = 690.00 FEET.

*****
FLOW PROCESS FROM NODE 32.00 TO NODE 33.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 903.00 DOWNSTREAM(FEET) = 890.00
FLOW LENGTH(FEET) = 530.00 MANNING'S N = 0.013

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ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.76
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.44
PIPE TRAVEL TIME(MIN.) = 1.14 Tc(MIN.) = 9.47
LONGEST FLOWPATH FROM NODE 30.00 TO NODE 33.00 = 1220.00 FEET.

*****
FLOW PROCESS FROM NODE 32.00 TO NODE 33.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.410
*USER SPECIFIED(SUBAREA):
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7778
SUBAREA AREA(ACRES) = 0.24 SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 1.1 TOTAL RUNOFF(CFS) = 4.54
TC(MIN.) = 9.47

*****
FLOW PROCESS FROM NODE 33.00 TO NODE 34.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 890.00 DOWNSTREAM(FEET) = 885.00
FLOW LENGTH(FEET) = 430.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.94
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.54
PIPE TRAVEL TIME(MIN.) = 1.21 Tc(MIN.) = 10.68
LONGEST FLOWPATH FROM NODE 30.00 TO NODE 34.00 = 1650.00 FEET.

*****
FLOW PROCESS FROM NODE 34.00 TO NODE 34.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.68
RAINFALL INTENSITY(INCH/HR) = 5.01
TOTAL STREAM AREA(ACRES) = 1.08
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.54

*****
FLOW PROCESS FROM NODE 35.00 TO NODE 36.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 911.00
DOWNSTREAM ELEVATION(FEET) = 908.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.301
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 85.00
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.96
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.96

*****
FLOW PROCESS FROM NODE 36.00 TO NODE 34.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 908.00 DOWNSTREAM ELEVATION(FEET) = 905.00
STREET LENGTH(FEET) = 474.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 14.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

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SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.41
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.31
HALFSTREET FLOOD WIDTH(FEET) = 9.32
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.73
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.54
STREET FLOW TRAVEL TIME(MIN.) = 4.57 Tc(MIN.) = 6.87
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.652
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900
SUBAREA AREA(ACRES) = 0.81 SUBAREA RUNOFF(CFS) = 4.85
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 5.63

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.57
FLOW VELOCITY(FEET/SEC.) = 1.93 DEPTH*VELOCITY(FT*FT/SEC.) = 0.69
LONGEST FLOWPATH FROM NODE 35.00 TO NODE 34.00 = 574.00 FEET.

*****
FLOW PROCESS FROM NODE 34.00 TO NODE 34.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.87
RAINFALL INTENSITY(INCH/HR) = 6.65
TOTAL STREAM AREA(ACRES) = 0.94
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.63

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 4.54 10.68 5.007 1.08
2 5.63 6.87 6.652 0.94

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 8.55 6.87 6.652
2 8.78 10.68 5.007

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 8.78 Tc(MIN.) = 10.68
TOTAL AREA(ACRES) = 2.0
LONGEST FLOWPATH FROM NODE 30.00 TO NODE 34.00 = 1650.00 FEET.

+-----+
| 0 |
| |
+-----+

*****
FLOW PROCESS FROM NODE 950.00 TO NODE 951.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8200
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 595.00
DOWNSTREAM ELEVATION(FEET) = 593.50
ELEVATION DIFFERENCE(FEET) = 1.50
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.617
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 67.50
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.00

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TOTAL AREA(ACRES) =      0.15  TOTAL RUNOFF(CFS) =      1.00

*****
FLOW PROCESS FROM NODE      951.00 TO NODE      952.00 IS CODE =  61
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STANDARD CURB SECTION USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =  593.50  DOWNSTREAM ELEVATION(FEET) =  587.00
STREET LENGTH(FEET) =  701.00  CURB HEIGHT(INCHES) =  6.0
STREET HALFWIDTH(FEET) =  22.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =  11.00
INSIDE STREET CROSSFALL(DECIMAL) =  0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =  0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =  2
STREET PARKWAY CROSSFALL(DECIMAL) =  0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =  0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =  0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =      3.90
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =  0.31
HALFSTREET FLOOD WIDTH(FEET) =  9.11
AVERAGE FLOW VELOCITY(FT/SEC.) =  2.06
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =  0.63
STREET FLOW TRAVEL TIME(MIN.) =  5.68  Tc(MIN.) =  9.30
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.475
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT =  0.793
SUBAREA AREA(ACRES) =  1.30  SUBAREA RUNOFF(CFS) =  5.62
TOTAL AREA(ACRES) =  1.4  PEAK FLOW RATE(CFS) =  6.30

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =  0.35  HALFSTREET FLOOD WIDTH(FEET) =  11.21
FLOW VELOCITY(FT/SEC.) =  2.29  DEPTH*VELOCITY(FT*FT/SEC.) =  0.80
LONGEST FLOWPATH FROM NODE      950.00 TO NODE      952.00 =  801.00 FEET.

*****
FLOW PROCESS FROM NODE      953.00 TO NODE      957.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  582.00  DOWNSTREAM(FEET) =  577.00
FLOW LENGTH(FEET) =  504.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.2 INCHES
PIPE-FLOW VELOCITY(FT/SEC.) =  6.07
ESTIMATED PIPE DIAMETER(INCH) =  18.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  6.30
PIPE TRAVEL TIME(MIN.) =  1.38  Tc(MIN.) =  10.68
LONGEST FLOWPATH FROM NODE      950.00 TO NODE      957.00 =  1305.00 FEET.

*****
FLOW PROCESS FROM NODE      957.00 TO NODE      957.00 IS CODE =  1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =  10.68
RAINFALL INTENSITY(INCH/HR) =  5.01
TOTAL STREAM AREA(ACRES) =  1.45
PEAK FLOW RATE(CFS) AT CONFLUENCE =  6.30

*****
FLOW PROCESS FROM NODE      955.00 TO NODE      956.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) =  0
INITIAL SUBAREA FLOW-LENGTH(FT) =  100.00
UPSTREAM ELEVATION(FT) =  586.75
DOWNSTREAM ELEVATION(FT) =  585.75
ELEVATION DIFFERENCE(FT) =  1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =  4.322
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH =  60.00
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

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100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.03
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 1.03

*****
FLOW PROCESS FROM NODE 956.00 TO NODE 957.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 585.75 DOWNSTREAM ELEVATION(FEET) = 581.75
STREET LENGTH(FEET) = 394.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 22.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 11.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.59
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 7.40
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.94
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.53
STREET FLOW TRAVEL TIME(MIN.) = 3.38 Tc(MIN.) = 7.70
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.182
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.790
SUBAREA AREA(ACRES) = 0.63 SUBAREA RUNOFF(CFS) = 3.08
TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 3.86

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 8.88
FLOW VELOCITY(FEET/SEC.) = 2.13 DEPTH*VELOCITY(FT*FT/SEC.) = 0.65
LONGEST FLOWPATH FROM NODE 955.00 TO NODE 957.00 = 494.00 FEET.

*****
FLOW PROCESS FROM NODE 957.00 TO NODE 957.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.70
RAINFALL INTENSITY(INCH/HR) = 6.18
TOTAL STREAM AREA(ACRES) = 0.79
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.86

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 6.30 10.68 5.006 1.45
2 3.86 7.70 6.182 0.79

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 8.40 7.70 6.182
2 9.42 10.68 5.006

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 9.42 Tc(MIN.) = 10.68
TOTAL AREA(ACRES) = 2.2
LONGEST FLOWPATH FROM NODE 950.00 TO NODE 957.00 = 1305.00 FEET.

*****
FLOW PROCESS FROM NODE 957.00 TO NODE 962.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 577.00 DOWNSTREAM(FEET) = 572.00
FLOW LENGTH(FEET) = 470.00 MANNING'S N = 0.013

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DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.75
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.42
PIPE TRAVEL TIME(MIN.) = 1.16 Tc(MIN.) = 11.84
LONGEST FLOWPATH FROM NODE 950.00 TO NODE 962.00 = 1775.00 FEET.

*****
FLOW PROCESS FROM NODE 962.00 TO NODE 962.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.84
RAINFALL INTENSITY(INCH/HR) = 4.68
TOTAL STREAM AREA(ACRES) = 2.24
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.42

*****
FLOW PROCESS FROM NODE 960.00 TO NODE 961.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 585.40
DOWNSTREAM ELEVATION(FEET) = 584.60
ELEVATION DIFFERENCE(FEET) = 0.80
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.411
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 57.78
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.03
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 1.03

*****
FLOW PROCESS FROM NODE 961.00 TO NODE 962.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 584.60 DOWNSTREAM ELEVATION(FEET) = 577.10
STREET LENGTH(FEET) = 751.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 22.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 11.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.73
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.34
HALFSTREET FLOOD WIDTH(FEET) = 10.59
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.31
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 5.42 Tc(MIN.) = 9.83
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.282
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.790
SUBAREA AREA(ACRES) = 2.19 SUBAREA RUNOFF(CFS) = 9.14
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 9.81

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.19
FLOW VELOCITY(FEET/SEC.) = 2.64 DEPTH*VELOCITY(FT*FT/SEC.) = 1.03
LONGEST FLOWPATH FROM NODE 960.00 TO NODE 962.00 = 841.00 FEET.

*****
FLOW PROCESS FROM NODE 962.00 TO NODE 962.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.83
RAINFALL INTENSITY(INCH/HR) = 5.28
TOTAL STREAM AREA(ACRES) = 2.35
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.81

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HR)      (ACRE)
1           9.42      11.84    4.684          2.24
2           9.81      9.83     5.282          2.35

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HR)
1           18.16     9.83     5.282
2           18.12    11.84     4.684

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 18.16 Tc(MIN.) = 9.83
TOTAL AREA(ACRES) = 4.6
LONGEST FLOWPATH FROM NODE 950.00 TO NODE 962.00 = 1775.00 FEET.

*****
FLOW PROCESS FROM NODE 962.00 TO NODE 963.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 572.00 DOWNSTREAM(FEET) = 570.00
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.39
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 18.16
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 10.04
LONGEST FLOWPATH FROM NODE 950.00 TO NODE 963.00 = 1895.00 FEET.

+-----+
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|                                             |
|                                             |
+-----+

*****
FLOW PROCESS FROM NODE 965.00 TO NODE 966.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 585.40
DOWNSTREAM ELEVATION(FEET) = 584.36
ELEVATION DIFFERENCE(FEET) = 1.04
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.106
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
         THE MAXIMUM OVERLAND FLOW LENGTH = 64.50
         (Reference: Table 3-1B of Hydrology Manual)
         THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.03
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 1.03

*****
FLOW PROCESS FROM NODE 966.00 TO NODE 967.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 584.35 DOWNSTREAM ELEVATION(FEET) = 579.00
STREET LENGTH(FEET) = 558.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 22.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 11.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

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SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.19
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 8.22
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.01
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.58
STREET FLOW TRAVEL TIME(MIN.) = 4.63 Tc(MIN.) = 8.74
100 YEAR RAINFALL INTENSITY(INCH/ HOUR) = 5.698
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.790
SUBAREA AREA(ACRES) = 0.94 SUBAREA RUNOFF(CFS) = 4.23
TOTAL AREA(ACRES) = 1.1 PEAK FLOW RATE(CFS) = 4.95

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.00
FLOW VELOCITY(FEET/SEC.) = 2.21 DEPTH*VELOCITY(FT*FT/SEC.) = 0.72
LONGEST FLOWPATH FROM NODE 965.00 TO NODE 967.00 = 638.00 FEET.

*****
FLOW PROCESS FROM NODE 967.00 TO NODE 972.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 575.00 DOWNSTREAM(FEET) = 565.00
FLOW LENGTH(FEET) = 900.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.98
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.95
PIPE TRAVEL TIME(MIN.) = 2.51 Tc(MIN.) = 11.25
LONGEST FLOWPATH FROM NODE 965.00 TO NODE 972.00 = 1538.00 FEET.

*****
FLOW PROCESS FROM NODE 972.00 TO NODE 972.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.25
RAINFALL INTENSITY(INCH/HR) = 4.84
TOTAL STREAM AREA(ACRES) = 1.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.95

*****
FLOW PROCESS FROM NODE 970.00 TO NODE 971.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 578.90
DOWNSTREAM ELEVATION(FEET) = 577.90
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.322
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 60.00
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.23
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 1.23

*****
FLOW PROCESS FROM NODE 971.00 TO NODE 972.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 577.90 DOWNSTREAM ELEVATION(FEET) = 570.00
STREET LENGTH(FEET) = 782.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 22.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 11.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.75
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.34
HALFSTREET FLOOD WIDTH(FEET) = 10.59
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.32
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 5.62 Tc(MIN.) = 9.94
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.243
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.790
SUBAREA AREA(ACRES) = 2.12 SUBAREA RUNOFF(CFS) = 8.78
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 9.57

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.02
FLOW VELOCITY(FEET/SEC.) = 2.64 DEPTH*VELOCITY(FT*FT/SEC.) = 1.02
LONGEST FLOWPATH FROM NODE 970.00 TO NODE 972.00 = 882.00 FEET.

*****
FLOW PROCESS FROM NODE 972.00 TO NODE 972.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.94
RAINFALL INTENSITY(INCH/HR) = 5.24
TOTAL STREAM AREA(ACRES) = 2.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.57

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 4.95 11.25 4.842 1.10
2 9.57 9.94 5.243 2.31

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 13.94 9.94 5.243
2 13.79 11.25 4.842

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 13.94 Tc(MIN.) = 9.94
TOTAL AREA(ACRES) = 3.4
LONGEST FLOWPATH FROM NODE 965.00 TO NODE 972.00 = 1538.00 FEET.

*****
FLOW PROCESS FROM NODE 972.00 TO NODE 973.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 565.00 DOWNSTREAM(FEET) = 560.00
FLOW LENGTH(FEET) = 195.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.41
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 13.94
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 10.25
LONGEST FLOWPATH FROM NODE 965.00 TO NODE 973.00 = 1733.00 FEET.

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+-----+

*****
FLOW PROCESS FROM NODE 975.00 TO NODE 976.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 574.80
DOWNSTREAM ELEVATION(FEET) = 573.90
ELEVATION DIFFERENCE(FEET) = 0.90
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.402
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 58.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
          100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.03
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 1.03

*****
FLOW PROCESS FROM NODE 976.00 TO NODE 977.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 573.90 DOWNSTREAM ELEVATION(FEET) = 563.40
STREET LENGTH(FEET) = 1089.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 22.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 11.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.86
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 13.36
AVERAGE FLOW VELOCITY(FT/SEC.) = 2.59
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.02
STREET FLOW TRAVEL TIME(MIN.) = 7.01 Tc(MIN.) = 11.41
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.797
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.790
SUBAREA AREA(ACRES) = 4.46 SUBAREA RUNOFF(CFS) = 16.90
TOTAL AREA(ACRES) = 4.6 PEAK FLOW RATE(CFS) = 17.51

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.46 HALFSTREET FLOOD WIDTH(FEET) = 16.80
FLOW VELOCITY(FT/SEC.) = 2.98 DEPTH*VELOCITY(FT*FT/SEC.) = 1.38
*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,
AND L = 1089.0 FT WITH ELEVATION-DROP = 10.5 FT, IS 28.8 CFS,
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 977.00
LONGEST FLOWPATH FROM NODE 975.00 TO NODE 977.00 = 1189.00 FEET.

*****
FLOW PROCESS FROM NODE 977.00 TO NODE 977.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.41
RAINFALL INTENSITY(INCH/HR) = 4.80
TOTAL STREAM AREA(ACRES) = 4.62
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.51

*****
FLOW PROCESS FROM NODE 980.00 TO NODE 981.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 98.00
UPSTREAM ELEVATION(FEET) = 626.00
DOWNSTREAM ELEVATION(FEET) = 624.00

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ELEVATION DIFFERENCE(FEET) =      2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =      3.820
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
        THE MAXIMUM OVERLAND FLOW LENGTH =      75.41
        (Reference: Table 3-1B of Hydrology Manual)
        THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =      8.168
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) =      1.16
TOTAL AREA(ACRES) =      0.18    TOTAL RUNOFF(CFS) =      1.16

*****
FLOW PROCESS FROM NODE      981.00 TO NODE      982.00 IS CODE =  61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) =  624.00  DOWNSTREAM ELEVATION(FEET) =  592.00
STREET LENGTH(FEET) =  910.00    CURB HEIGHT(INCHES) =  6.0
STREET HALFWIDTH(FEET) =  22.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =  11.00
INSIDE STREET CROSSFALL(DECIMAL) =  0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =  0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =  2
STREET PARKWAY CROSSFALL(DECIMAL) =  0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =  0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =  0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =      5.58
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =  0.28
HALFSTREET FLOOD WIDTH(FEET) =  7.92
AVERAGE FLOW VELOCITY(FEET/SEC.) =  3.75
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =  1.07
STREET FLOW TRAVEL TIME(MIN.) =  4.05    Tc(MIN.) =  7.87
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  6.096
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7900
S.C.S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT =  0.790
SUBAREA AREA(ACRES) =  1.81    SUBAREA RUNOFF(CFS) =  8.72
TOTAL AREA(ACRES) =  2.0    PEAK FLOW RATE(CFS) =  9.58

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =  0.33    HALFSTREET FLOOD WIDTH(FEET) =  10.07
FLOW VELOCITY(FEET/SEC.) =  4.23    DEPTH*VELOCITY(FT*FT/SEC.) =  1.39
LONGEST FLOWPATH FROM NODE      980.00 TO NODE      982.00 =  1008.00 FEET.

*****
FLOW PROCESS FROM NODE      982.00 TO NODE      977.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  585.00  DOWNSTREAM(FEET) =  560.00
FLOW LENGTH(FEET) =  948.00    MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS  9.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  9.74
ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  9.58
PIPE TRAVEL TIME(MIN.) =  1.62    Tc(MIN.) =  9.49
LONGEST FLOWPATH FROM NODE      980.00 TO NODE      977.00 =  1956.00 FEET.

*****
FLOW PROCESS FROM NODE      977.00 TO NODE      977.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =  9.49
RAINFALL INTENSITY(INCH/HR) =  5.40
TOTAL STREAM AREA(ACRES) =  1.99
PEAK FLOW RATE(CFS) AT CONFLUENCE =  9.58

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
1          17.51      11.41      4.797      4.62
2           9.58       9.49      5.402      1.99

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	24.15	9.49	5.402
2	26.02	11.41	4.797

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.02 Tc(MIN.) = 11.41
TOTAL AREA(ACRES) = 6.6
LONGEST FLOWPATH FROM NODE 980.00 TO NODE 977.00 = 1956.00 FEET.

FLOW PROCESS FROM NODE 977.00 TO NODE 984.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) =	560.00	DOWNSTREAM(FEET) =	550.00
FLOW LENGTH(FEET) =	295.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS	15.8 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	13.41		
ESTIMATED PIPE DIAMETER(INCH) =	21.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	26.02		
PIPE TRAVEL TIME(MIN.) =	0.37	Tc(MIN.) =	11.78
LONGEST FLOWPATH FROM NODE	980.00	TO NODE	984.00 = 2251.00 FEET.

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FLOW PROCESS FROM NODE 985.00 TO NODE 986.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====

*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 715.00
DOWNSTREAM ELEVATION(FEET) = 705.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.061
SUBAREA RUNOFF(CFS) = 0.47
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.47

FLOW PROCESS FROM NODE 986.00 TO NODE 987.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) =	700.00	DOWNSTREAM(FEET) =	560.00
FLOW LENGTH(FEET) =	1154.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO	18.000		
DEPTH OF FLOW IN 18.0 INCH PIPE IS	1.4 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	7.04		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.47		
PIPE TRAVEL TIME(MIN.) =	2.73	Tc(MIN.) =	9.00
LONGEST FLOWPATH FROM NODE	985.00	TO NODE	987.00 = 1254.00 FEET.

FLOW PROCESS FROM NODE 986.00 TO NODE 987.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.591
*USER SPECIFIED(SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 14.04 SUBAREA RUNOFF(CFS) = 27.47
TOTAL AREA(ACRES) = 14.2 TOTAL RUNOFF(CFS) = 27.85
TC(MIN.) = 9.00

FLOW PROCESS FROM NODE 987.00 TO NODE 988.00 IS CODE = 31

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-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 560.00 DOWNSTREAM(FEET) = 550.00
FLOW LENGTH(FEET) = 177.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.79
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 27.85
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 9.17
LONGEST FLOWPATH FROM NODE 985.00 TO NODE 988.00 = 1431.00 FEET.

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*****
FLOW PROCESS FROM NODE 990.00 TO NODE 991.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 677.00
DOWNSTREAM ELEVATION(FEET) = 670.00
ELEVATION DIFFERENCE(FEET) = 7.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.058
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.540
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.16

*****
FLOW PROCESS FROM NODE 991.00 TO NODE 992.00 IS CODE = 53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 670.00 DOWNSTREAM(FEET) = 570.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 513.00 CHANNEL SLOPE = 0.1949
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.16
FLOW VELOCITY(FEET/SEC) = 2.47 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.46 Tc(MIN.) = 10.52
LONGEST FLOWPATH FROM NODE 990.00 TO NODE 992.00 = 613.00 FEET.

*****
FLOW PROCESS FROM NODE 991.00 TO NODE 992.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.056
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 7.79 SUBAREA RUNOFF(CFS) = 13.79
TOTAL AREA(ACRES) = 7.9 TOTAL RUNOFF(CFS) = 13.91
TC(MIN.) = 10.52

*****
FLOW PROCESS FROM NODE 992.00 TO NODE 993.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 570.00 DOWNSTREAM(FEET) = 545.00
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.78
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 13.91
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 10.64
LONGEST FLOWPATH FROM NODE 990.00 TO NODE 993.00 = 773.00 FEET.

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| The following input information is per the Hydrology Study for Rolling |
| Hills Ranch Neighborhoods 9-12 (Oct 2003)                             |
+-----+

*****
FLOW PROCESS FROM NODE      994.00 TO NODE      994.00 IS CODE =   7
-----
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<
=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN) = 22.29  RAIN INTENSITY(INCH/HOUR) = 3.11
TOTAL AREA(ACRES) = 261.03  TOTAL RUNOFF(CFS) = 469.76

*****
FLOW PROCESS FROM NODE      994.00 TO NODE      995.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 605.00  DOWNSTREAM(FEET) = 600.00
FLOW LENGTH(FEET) = 233.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 66.0 INCH PIPE IS 52.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.00
ESTIMATED PIPE DIAMETER(INCH) = 66.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 469.76
PIPE TRAVEL TIME(MIN.) = 0.17  Tc(MIN.) = 22.46
LONGEST FLOWPATH FROM NODE      990.00 TO NODE      995.00 = 1006.00 FEET.

*****
FLOW PROCESS FROM NODE      994.00 TO NODE      995.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.099
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5754
SUBAREA AREA(ACRES) = 2.78  SUBAREA RUNOFF(CFS) = 3.02
TOTAL AREA(ACRES) = 263.8  TOTAL RUNOFF(CFS) = 470.50
TC(MIN.) = 22.46

*****
FLOW PROCESS FROM NODE      995.00 TO NODE      996.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 600.00  DOWNSTREAM(FEET) = 575.00
FLOW LENGTH(FEET) = 771.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 63.0 INCH PIPE IS 46.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 27.23
ESTIMATED PIPE DIAMETER(INCH) = 63.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 470.50
PIPE TRAVEL TIME(MIN.) = 0.47  Tc(MIN.) = 22.93
LONGEST FLOWPATH FROM NODE      990.00 TO NODE      996.00 = 1777.00 FEET.

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| The following information is per the Hydrology Study for Rolling Hills |
| Ranch Neighborhoods 9-12 (October 2003).                             |
+-----+

*****
FLOW PROCESS FROM NODE      997.00 TO NODE      997.00 IS CODE =   7
-----
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<
=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN) = 20.04  RAIN INTENSITY(INCH/HOUR) = 3.34
TOTAL AREA(ACRES) = 718.66  TOTAL RUNOFF(CFS) = 1373.90

*****
FLOW PROCESS FROM NODE      997.00 TO NODE      998.00 IS CODE =  52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<

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```

>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =      600.00  DOWNSTREAM(FEET) =      559.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1925.00  CHANNEL SLOPE = 0.0213
CHANNEL FLOW THRU SUBAREA(CFS) = 1373.90
FLOW VELOCITY(FEET/SEC) = 15.88 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.02  Tc(MIN.) = 22.06
LONGEST FLOWPATH FROM NODE 990.00 TO NODE 998.00 = 3702.00 FEET.

*****
FLOW PROCESS FROM NODE 997.00 TO NODE 998.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.135
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.5634
SUBAREA AREA(ACRES) = 32.59  SUBAREA RUNOFF(CFS) = 35.76
TOTAL AREA(ACRES) = 751.2  TOTAL RUNOFF(CFS) = 1373.90
TC(MIN.) = 22.06
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

*****
FLOW PROCESS FROM NODE 998.00 TO NODE 998.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 22.06
RAINFALL INTENSITY(INCH/HR) = 3.14
TOTAL STREAM AREA(ACRES) = 751.25
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1373.90

*****
FLOW PROCESS FROM NODE 998.10 TO NODE 998.20 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 745.00
DOWNSTREAM ELEVATION(FEET) = 742.00
ELEVATION DIFFERENCE(FEET) = 3.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.361
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.451
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.09  TOTAL RUNOFF(CFS) = 0.17

*****
FLOW PROCESS FROM NODE 998.20 TO NODE 998.30 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 742.00  DOWNSTREAM(FEET) = 650.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1153.00  CHANNEL SLOPE = 0.0798
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.17
FLOW VELOCITY(FEET/SEC) = 4.24 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.54  Tc(MIN.) = 13.90
LONGEST FLOWPATH FROM NODE 998.10 TO NODE 998.30 = 1253.00 FEET.

*****
FLOW PROCESS FROM NODE 998.20 TO NODE 998.30 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.224
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 10.82  SUBAREA RUNOFF(CFS) = 16.00
TOTAL AREA(ACRES) = 10.9  TOTAL RUNOFF(CFS) = 16.13
TC(MIN.) = 13.90

*****
FLOW PROCESS FROM NODE 998.30 TO NODE 998.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<

```

```

>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 650.00 DOWNSTREAM(FEET) = 559.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1816.00 CHANNEL SLOPE = 0.0501
CHANNEL FLOW THRU SUBAREA(CFS) = 16.13
FLOW VELOCITY(FEET/SEC) = 6.33 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.78 Tc(MIN.) = 18.68
LONGEST FLOWPATH FROM NODE 998.10 TO NODE 998.00 = 3069.00 FEET.

*****
FLOW PROCESS FROM NODE 998.30 TO NODE 998.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.491
*USER SPECIFIED(SUBAREA):
NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3500
SUBAREA AREA(ACRES) = 36.38 SUBAREA RUNOFF(CFS) = 44.45
TOTAL AREA(ACRES) = 47.3 TOTAL RUNOFF(CFS) = 57.78
TC(MIN.) = 18.68

*****
FLOW PROCESS FROM NODE 998.00 TO NODE 998.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 18.68
RAINFALL INTENSITY(INCH/HR) = 3.49
TOTAL STREAM AREA(ACRES) = 47.29
PEAK FLOW RATE(CFS) AT CONFLUENCE = 57.78

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 1373.90 22.06 3.135 751.25
2 57.78 18.68 3.491 47.29

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 1220.83 18.68 3.491
2 1425.80 22.06 3.135

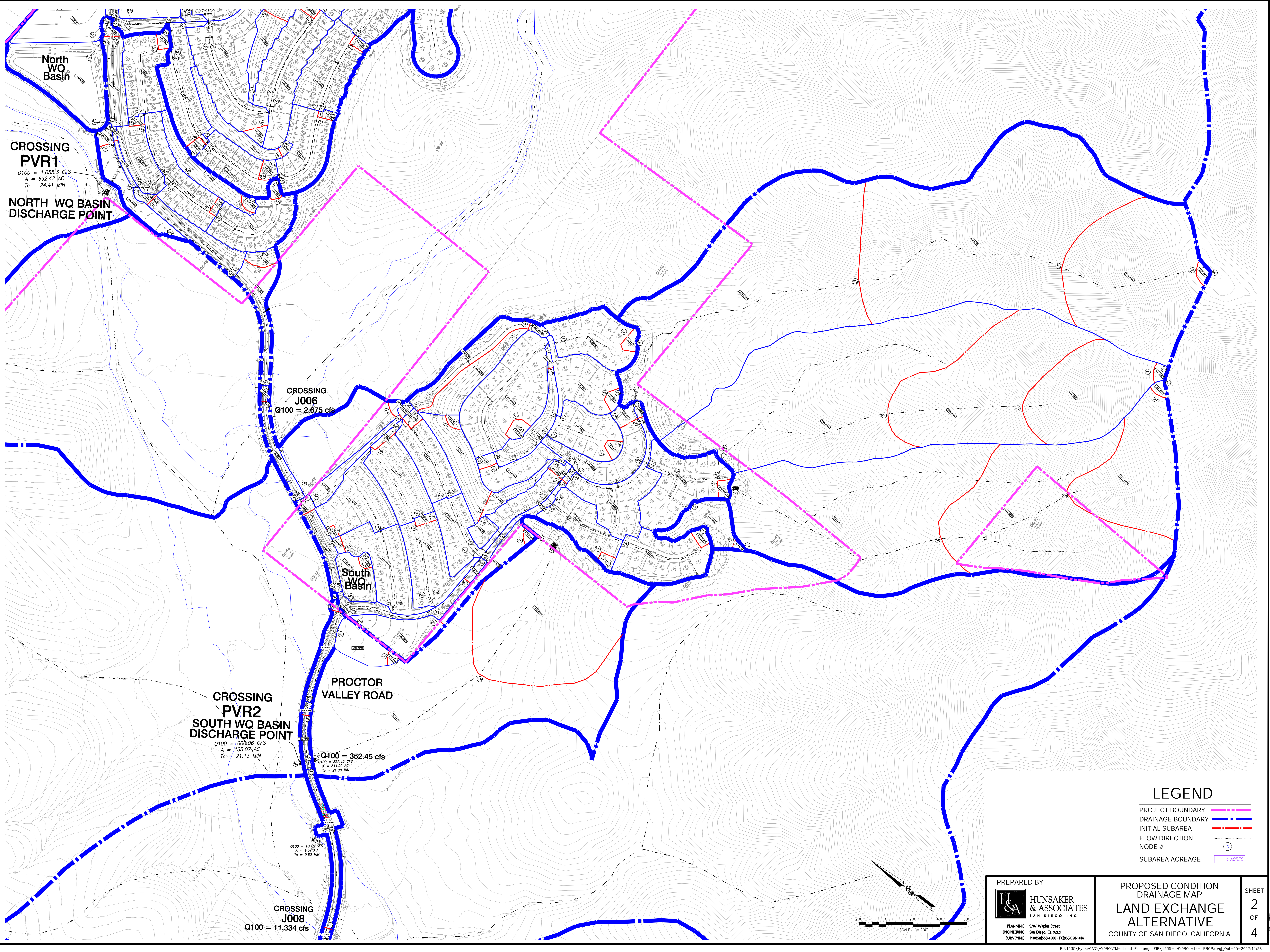
COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 1425.80 Tc(MIN.) = 22.06
TOTAL AREA(ACRES) = 798.5
LONGEST FLOWPATH FROM NODE 990.00 TO NODE 998.00 = 3702.00 FEET.

*****
FLOW PROCESS FROM NODE 998.00 TO NODE 999.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 559.00 DOWNSTREAM(FEET) = 550.00
FLOW LENGTH(FEET) = 210.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 90.0 INCH PIPE IS 68.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 39.79
ESTIMATED PIPE DIAMETER(INCH) = 90.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1425.80
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 22.15
LONGEST FLOWPATH FROM NODE 990.00 TO NODE 999.00 = 3912.00 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 798.5 TC(MIN.) = 22.15
PEAK FLOW RATE(CFS) = 1425.80
=====
END OF RATIONAL METHOD ANALYSIS

```

CHAPTER 4

4.1.5 – Rational Method Proposed Condition Hydrology Maps



CROSSING PVR1
Q100 = 1,055.3 CFS
A = 692.42 AC
Tc = 24.41 MIN

NORTH WQ BASIN DISCHARGE POINT

CROSSING J006
Q100 = 2,675 cfs

South WQ Basin

CROSSING PVR2
SOUTH WQ BASIN DISCHARGE POINT
Q100 = 600.06 CFS
A = 455.07 AC
Tc = 21.13 MIN

PROCTOR VALLEY ROAD

Q100 = 352.45 cfs
Q100 = 352.45 CFS
A = 311.92 AC
Tc = 21.08 MIN

CROSSING J008
Q100 = 11,334 cfs

Q100 = 18.16 CFS
A = 4.59 AC
Tc = 9.83 MIN

LEGEND

- PROJECT BOUNDARY
- DRAINAGE BOUNDARY
- INITIAL SUBAREA
- FLOW DIRECTION
- NODE #
- SUBAREA ACREAGE

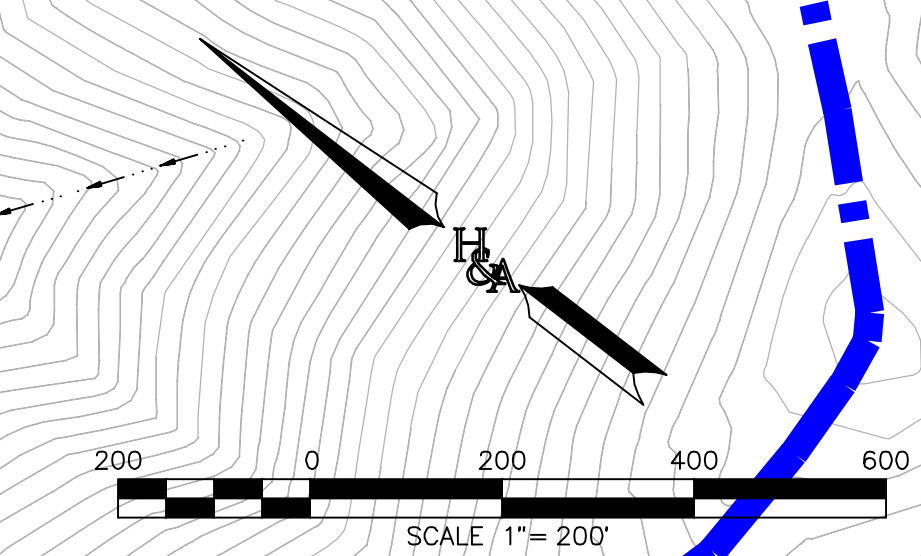
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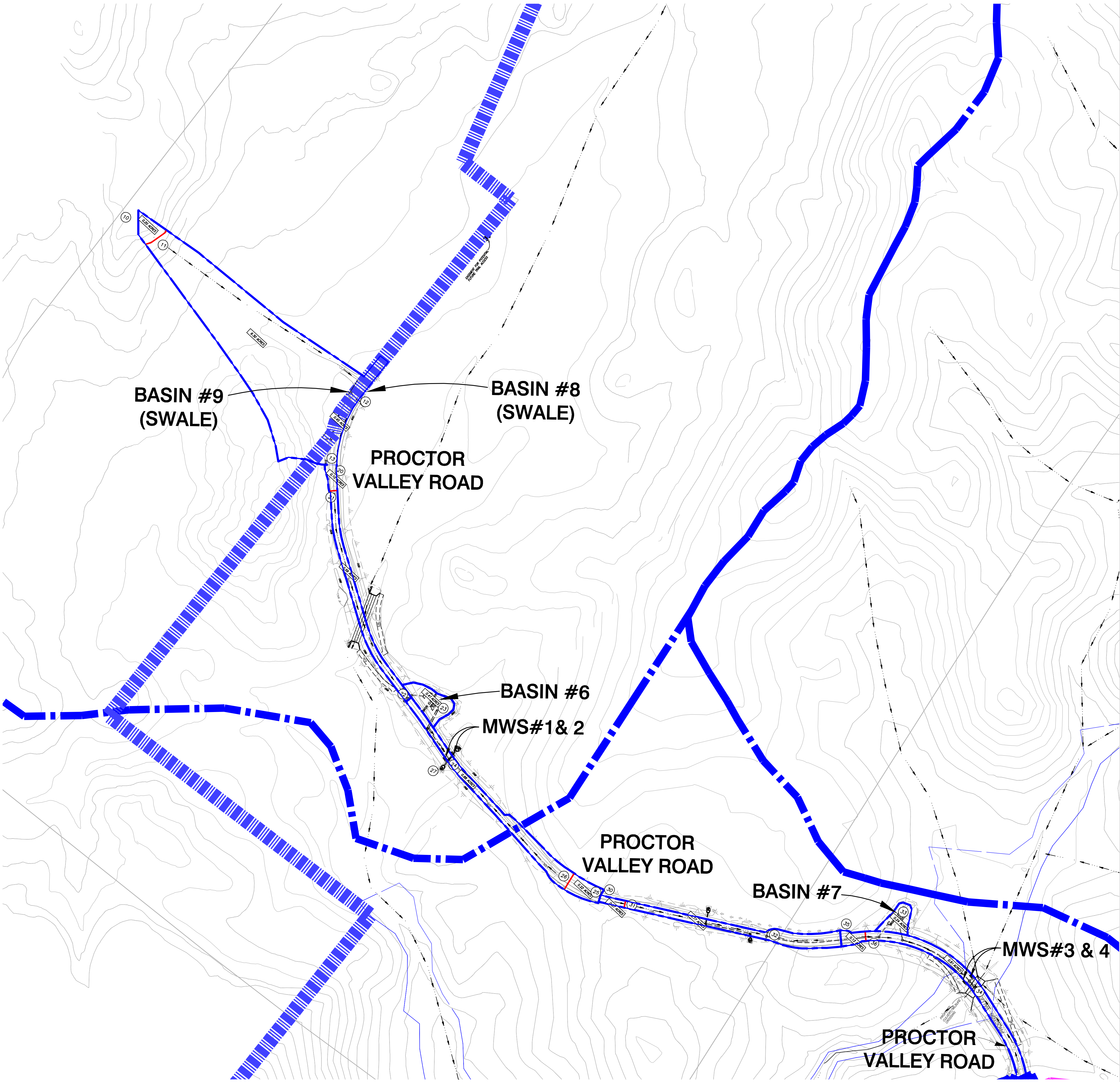
H & A
HUNSAKER & ASSOCIATES
SAN DIEGO, INC.

PLANNING 9707 Waples Street
ENGINEERING San Diego, CA 92121
SURVEYING PH(619)558-4500 - FX(619)558-1414

PROPOSED CONDITION
DRAINAGE MAP
**LAND EXCHANGE
ALTERNATIVE**
COUNTY OF SAN DIEGO, CALIFORNIA

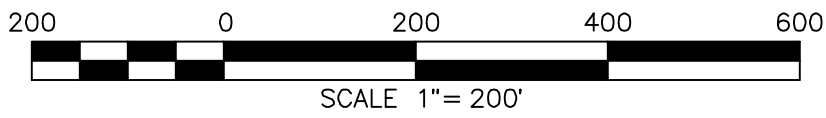
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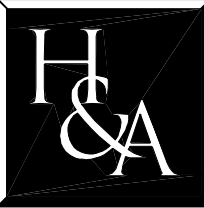


LEGEND

- PROJECT BOUNDARY
- DRAINAGE BOUNDARY
- INITIAL SUBAREA
- FLOW DIRECTION
- NODE #
- SUBAREA ACREAGE



PREPARED BY:

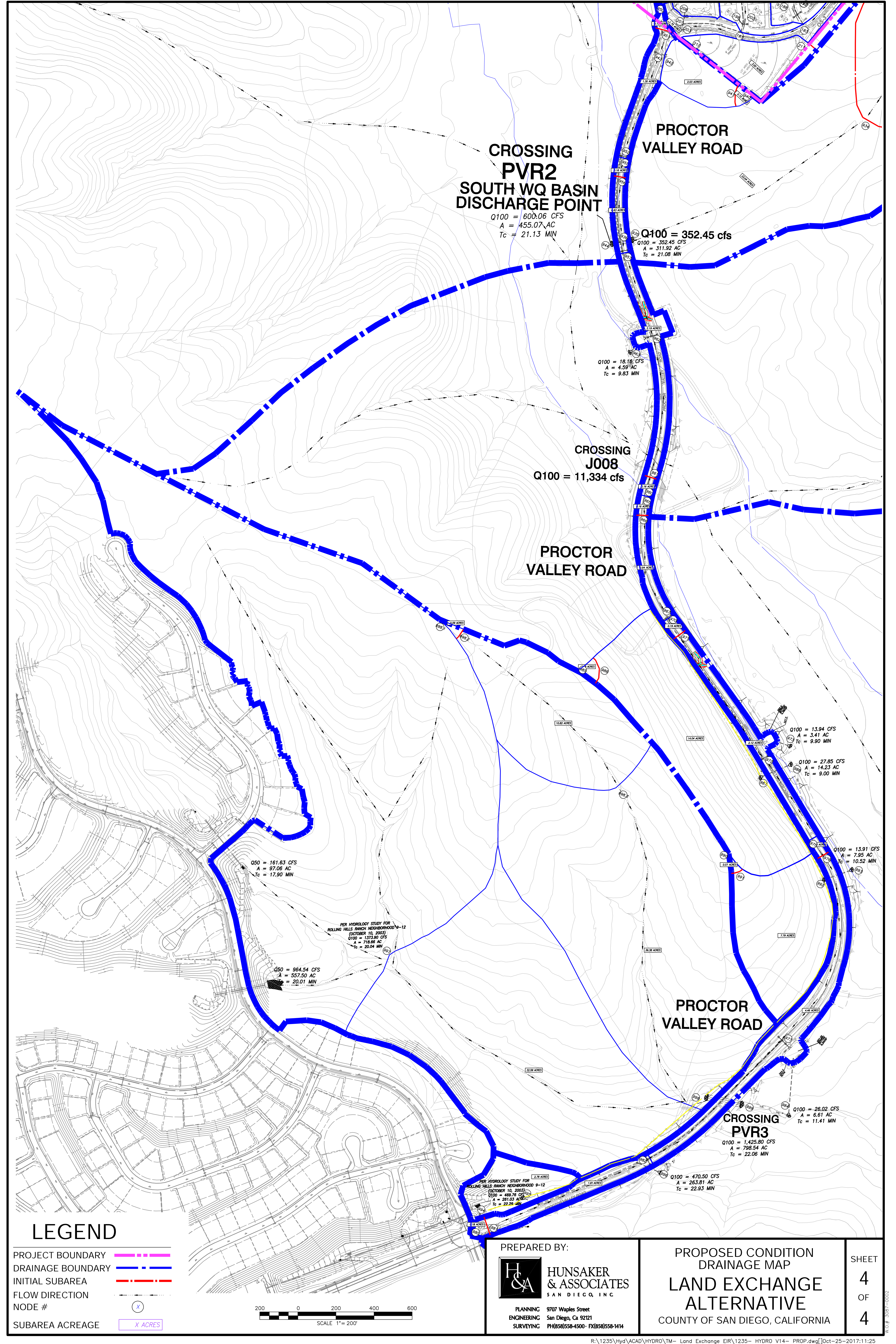


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PLANNING 9707 Waples Street
ENGINEERING San Diego, Ca 92121
SURVEYING PH(858)558-4500 • FX(858)558-1414

PROPOSED CONDITION
DRAINAGE MAP
LAND EXCHANGE
ALTERNATIVE
COUNTY OF SAN DIEGO, CALIFORNIA

SHEET
3
OF
4



LEGEND

- PROJECT BOUNDARY
- DRAINAGE BOUNDARY
- INITIAL SUBAREA
- FLOW DIRECTION
- NODE #
- SUBAREA ACREAGE



PREPARED BY:



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ENGINEERING San Diego, Ca 92121
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PROPOSED CONDITION
DRAINAGE MAP
LAND EXCHANGE
ALTERNATIVE
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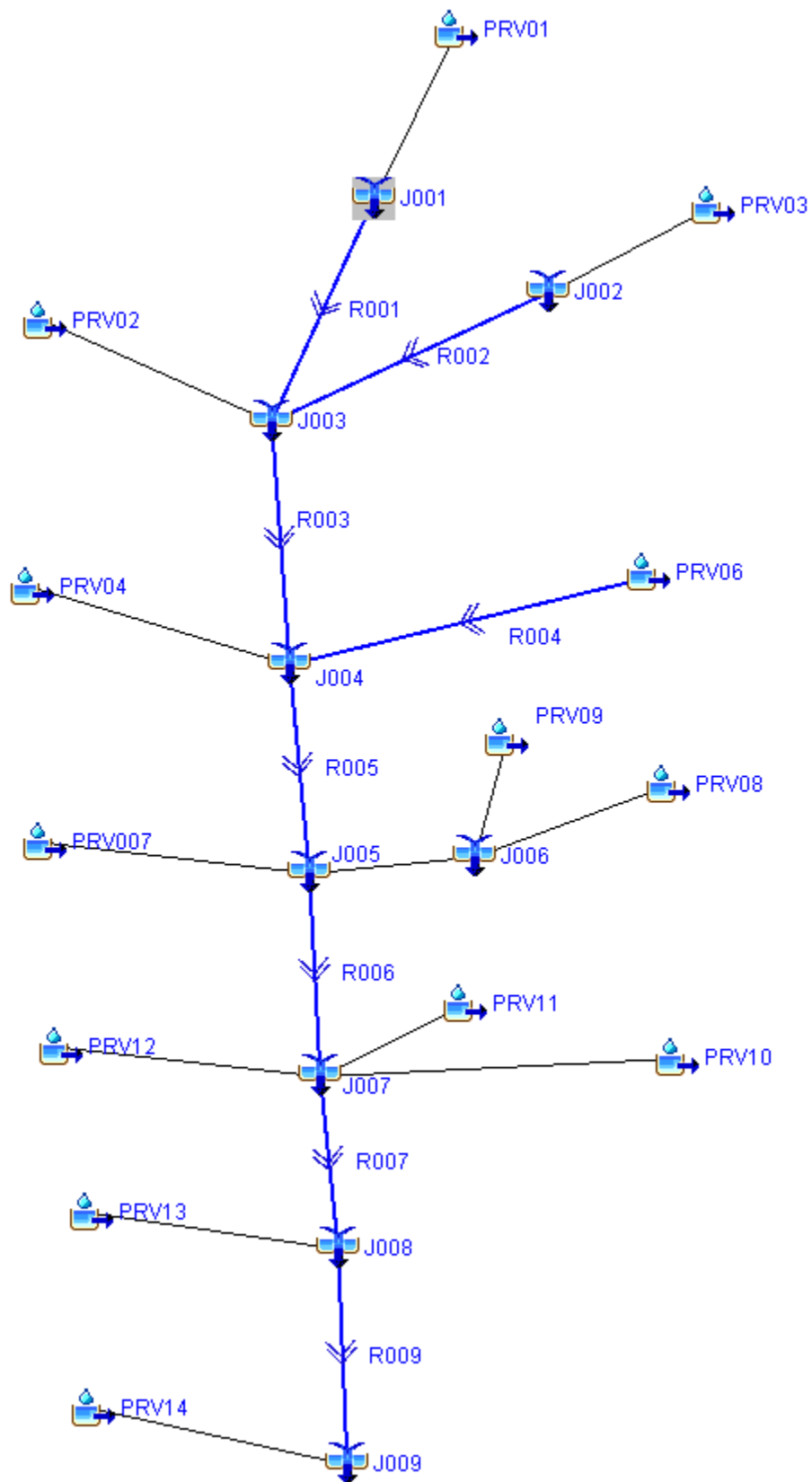
SHEET
4
OF
4

CHAPTER 5

100-Year Unit Hydrograph Hydrologic Model for Proposed Conditions

CHAPTER 5

5.1 – Unit Hydrograph Hydrologic Analysis (HEC HMS)



HEC-HMS Basin Input-Proposed Conditions

Subarea	Area (ft ²)	Area (mi ²)	"n" value	L (ft)	L _c (ft)	L (miles)	L _c (miles)	Elev ₁ (ft)	Elev ₂ (ft)	Elev ₍₁₋₂₎ (ft)	Slope (ft/mile)	Corps T ₁ (hrs)	NRCS T ₁ (hrs)	NRCS T ₁ (min)
PRV01	41547092.4	1.490	0.050	10200	5571	1.932	1.055	1148.0	868.0	280	144.941	0.61	0.52	31.10
PRV02	45198362.1	1.621	0.050	8232	3865	1.559	0.732	2510.0	820.0	1690	1083.965	0.33	0.28	16.80
PRV03	33654203.7	1.207	0.050	10119	5744	1.916	1.088	1620.0	890.0	730	380.907	0.51	0.43	26.03
PRV04	25073572.8	0.899	0.050	7749	3323	1.468	0.629	2060.0	618.0	1442	982.547	0.31	0.26	15.76
PRV06	13664384.9	0.490	0.050	6623	3953	1.254	0.749	1910.0	750.0	1160	924.777	0.32	0.27	16.05
PRV07	18068957.3	0.648	0.050	11593	6021	2.196	1.140	2560.0	588.0	1972	898.142	0.47	0.39	23.66
PRV08	38388604.6	1.377	0.050	10817	4868	2.049	0.922	1910.0	610.0	1300	634.557	0.45	0.38	22.69
PRV09	16497871.7	0.592	0.018	9559	4996	1.810	0.946	1340.0	647.0	693	382.785	0.17	0.14	8.36
PRV10	13686799.8	0.491	0.050	8973	5061	1.699	0.959	1870.0	580.0	1290	759.077	0.41	0.34	20.69
PRV11	6141025.1	0.220	0.018	4950	2506	0.938	0.475	770.0	580.0	190	202.667	0.12	0.09	5.49
PRV12	14223154.7	0.510	0.050	6658	3964	1.261	0.751	1095.0	568.0	527	417.927	0.37	0.31	18.81
PRV13	3517726.8	0.126	0.050	2752	1823	0.521	0.345	774.0	558.0	216	414.419	0.20	0.16	9.79
PRV14	30059449.2	1.078	0.050	11978	8327	2.269	1.577	1720.0	515.0	1205	531.174	0.59	0.50	30.08
Total Check	299721205.090	10.751												

Lag Equations from SD County Manual (2003)

$$\text{Corps } T_1 = 24n((L \times L_c)/(s^{0.5}))^m$$

$$\text{NRCS } T_1 = T_p - 0.5D$$

$$T_p = 0.862 * \text{Corps } T_1$$

HEC-HMS Routing Input-Proposed Conditions

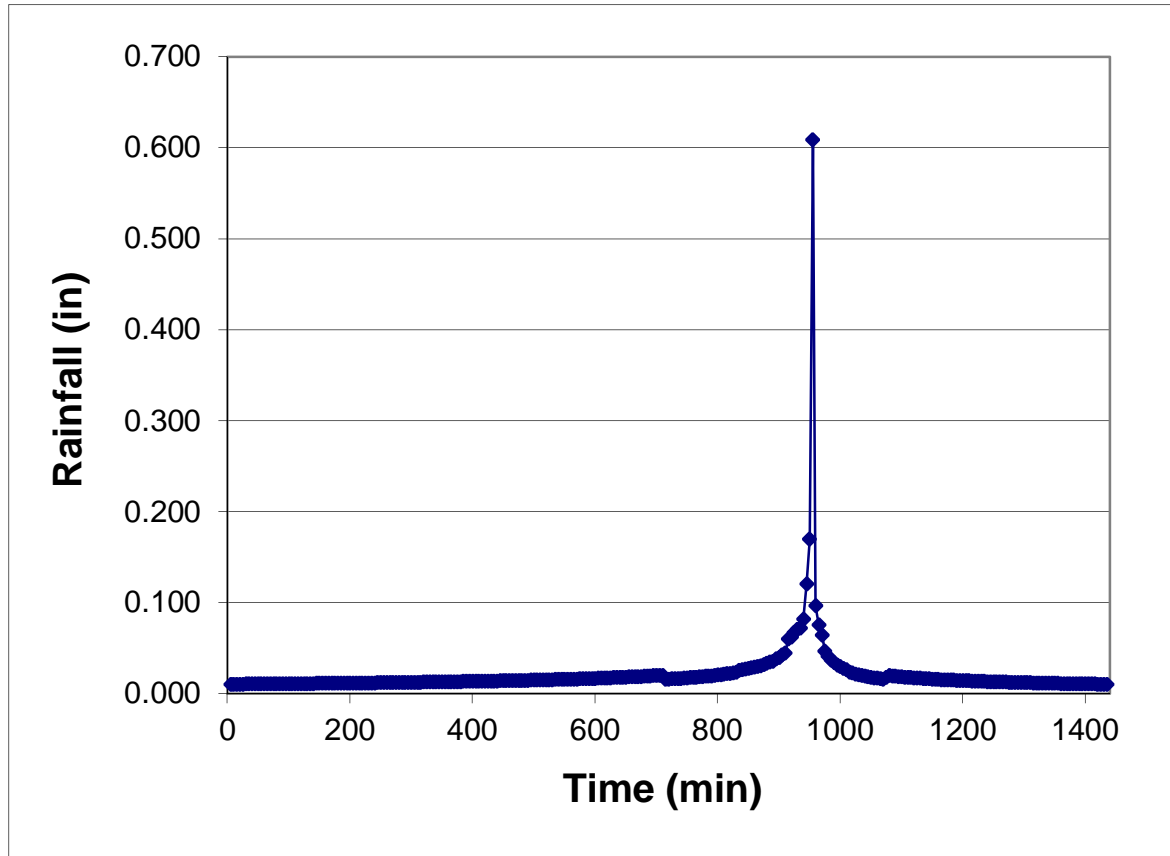
Subarea	Reach	U/S Node	D/S Node	Length (ft)	U/S Elev (ft)	D/S Elev (ft)	Slope (ft/ft)	Slope (ft/mi)	"n" value	Channel Type	Dimensions
PRV01	R001	J001	J003	2189	868.0	818.0	0.02284	120.60302	0.05	Trap	50' (W), 3H:1V
PRV03	R002	J002	J003	2563	885.0	818.0	0.02614	138.02575	0.05	Trap	30' (W), 3H:1V
PRV04	R003	J003	J004	8454	818.0	615.0	0.02401	126.78495	0.018	Trap	30' (W), 3H:1V
PRV06	R004	PRV06	J004	4976	750.0	615.0	0.02713	143.24759	0.05	Trap	30' (W), 3H:1V
PRV07	R005	J004	J005	2399	615.0	587.0	0.01167	61.62568	0.05	Trap	50' (W), 8H:1V
PRV12	R006	J005	J007	2125	587.0	568.0	0.00894	47.20941	0.05	Trap	50' (W), 8H:1V
PRV13	R007	J007	J008	1429	568.0	558.0	0.00700	36.94892	0.05	Trap	20' (W), 3H:1V
PRV14	R008	J008	J009	4448	558.0	515.0	0.00967	51.04317	0.05	Trap	20' (W), 3H:1V

Proposed Conditions

Subarea	Total Acres	Soil Type	Acreage	CN	Soil Type	Acreage	CN	Soil Type	Acreage	CN	Soil Type	Acreage	CN	CN _{2.0}	CN _{2.7}
PRV01	953.79	A	155.7	41	B	71.7	64	C	591.5	75	D	134.89	85	70	81
PRV02	1037.61	A	0	0	B	0	62	C	0	74	D	1037.61	85	85	91
PRV03	772.59	A	0	0	B	0	62	C	0	74	D	772.59	85	85	91
PRV04	575.61	A	0	0	B	0	62	C	0	74	D	575.61	85	85	91
PRV06	313.69	A	0	0	B	0	62	C	0	74	D	313.69	85	85	91
PRV07	414.81	A	0	0	B	0	62	C	0	74	D	414.81	85	85	91
PRV08	881.28	A	0	0	B	0	62	C	0	74	D	881.28	85	85	91
PRV09	378.74	A	0	61	B	0	75	C	0	83	D	378.74	87	87	93
PRV10	314.21	A	0	0	B	0	62	C	0	74	D	314.21	85	85	91
PRV11	140.98	A	0	61	B	0	75	C	0	83	D	140.98	87	87	93
PRV12	326.52	A	0	0	B	0	62	C	0	74	D	326.52	85	85	91
PRV13	80.76	A	0	0	B	0	62	C	0	74	D	80.76	85	85	91
PRV14	690.07	A	0	0	B	0	62	C	0	74	D	690.07	85	85	91

OTAY RANCH VILLAGE 14
HEC HMS HYETOGRAPH CALCULATIONS

CALCULATED RAINFALL SORTED IN (2/3,1/3) DISTRIBUTION



OTAY RANCH VILLAGE 14

HEC HMS HYETOGRAPH CALCULATIONS

SD COUNTY HYETOGRAPH CALCULATIONS

Area	(sq ft)	(sq mi)	
PRV01	41547092.4	1.49	953.79
PRV02	45198362.07	1.62	1037.61
PRV03	33654203.68	1.21	772.59
PRV04	25073572.81	0.90	575.61
PRV06	13664384.94	0.49	313.69
PRV07	18068957.34	0.65	414.81
PRV08	38388604.64	1.38	881.28
PRV09	16497871.65	0.59	378.74
PRV10	13686799.82	0.49	314.21
PRV11	6141025.13	0.22	140.98
PRV12	14223154.66	0.51	326.52
PRV13	3517726.75	0.13	80.76
PRV14	30059449.2	1.08	690.07

Total 299721205.1 10.75 6880.65

Watershed area		Rainfall Depth-Area Adjustment Data Points				
(sq mi)		30	60	180	360	1440
10		0.9	0.947	0.97	0.98	0.985 Taken from Table 4-1
10.75		0.895	0.943	0.969	0.979	0.984 Interpolated
20		0.834	0.9	0.952	0.963	0.975 Taken from Table 4-1

P(6)= 3.1 in

CALCULATED RAINFALL SORTED IN (2/3,1/3) DISTRIBUTION

RAINFALL DISTRIBUTION SORTED IN ORDER OF INCREASING DURATION

Duration (min)	Rainfall Precipitation for Duration (in)	Depth Area Adjustment for Duration	Depth-Area Adjusted Precipitation (in)	Hyetograph Ordinate (in)	Sorted Hyetograph Ordinate (in)
5	0.681	0.895	0.609	0.609	1 0.010
10	0.871	0.895	0.779	0.170	2 0.010
15	1.005	0.895	0.900	0.121	3 0.010
20	1.113	0.895	0.997	0.097	4 0.011
25	1.205	0.895	1.079	0.082	5 0.011
30	1.286	0.895	1.151	0.072	6 0.011
35	1.358	0.903	1.227	0.076	7 0.011
40	1.424	0.911	1.298	0.071	8 0.011
45	1.485	0.919	1.365	0.067	9 0.011
50	1.541	0.927	1.429	0.064	10 0.011
55	1.594	0.935	1.491	0.062	11 0.011
60	1.644	0.943	1.552	0.060	12 0.011
65	1.692	0.945	1.598	0.046	13 0.011
70	1.737	0.946	1.642	0.044	14 0.011
75	1.780	0.947	1.685	0.043	15 0.011
80	1.821	0.948	1.726	0.041	16 0.011
85	1.861	0.949	1.765	0.040	17 0.011
90	1.899	0.950	1.804	0.038	18 0.011
95	1.936	0.951	1.841	0.037	19 0.011
100	1.971	0.952	1.877	0.036	20 0.011
105	2.006	0.953	1.911	0.035	21 0.011
110	2.039	0.954	1.945	0.034	22 0.011
115	2.072	0.955	1.979	0.033	23 0.011
120	2.103	0.956	2.011	0.032	24 0.011
125	2.134	0.957	2.042	0.032	25 0.011
130	2.164	0.958	2.073	0.031	26 0.011
135	2.193	0.959	2.104	0.030	27 0.011

OTAY RANCH VILLAGE 14
HEC HMS HYETOGRAPH CALCULATIONS

140	2.222	0.960	2.133	0.030	28	0.011
145	2.249	0.961	2.162	0.029	29	0.011
150	2.277	0.962	2.191	0.029	30	0.011
155	2.303	0.963	2.219	0.028	31	0.011
160	2.329	0.964	2.247	0.028	32	0.011
165	2.355	0.966	2.274	0.027	33	0.011
170	2.380	0.967	2.300	0.027	34	0.011
175	2.405	0.968	2.327	0.026	35	0.011
180	2.429	0.969	2.353	0.026	36	0.012
185	2.453	0.969	2.376	0.024	37	0.012
190	2.476	0.969	2.400	0.023	38	0.012
195	2.499	0.969	2.423	0.023	39	0.012
200	2.521	0.970	2.445	0.023	40	0.012
205	2.544	0.970	2.467	0.022	41	0.012
210	2.565	0.970	2.489	0.022	42	0.012
215	2.587	0.971	2.511	0.022	43	0.012
220	2.608	0.971	2.532	0.021	44	0.012
225	2.629	0.971	2.553	0.021	45	0.012
230	2.650	0.971	2.574	0.021	46	0.012
235	2.670	0.972	2.595	0.020	47	0.012
240	2.690	0.972	2.615	0.020	48	0.012
245	2.710	0.972	2.635	0.020	49	0.012
250	2.729	0.973	2.654	0.020	50	0.012
255	2.749	0.973	2.674	0.019	51	0.012
260	2.768	0.973	2.693	0.019	52	0.012
265	2.786	0.973	2.712	0.019	53	0.012
270	2.805	0.974	2.731	0.019	54	0.012
275	2.823	0.974	2.750	0.019	55	0.012
280	2.841	0.974	2.768	0.018	56	0.012
285	2.859	0.975	2.786	0.018	57	0.012
290	2.877	0.975	2.804	0.018	58	0.012
295	2.894	0.975	2.822	0.018	59	0.012
300	2.912	0.975	2.840	0.018	60	0.012
305	2.929	0.976	2.858	0.018	61	0.013
310	2.946	0.976	2.875	0.017	62	0.013
315	2.963	0.976	2.892	0.017	63	0.013
320	2.979	0.976	2.909	0.017	64	0.013
325	2.996	0.977	2.926	0.017	65	0.013
330	3.012	0.977	2.943	0.017	66	0.013
335	3.028	0.977	2.959	0.017	67	0.013
340	3.044	0.978	2.976	0.016	68	0.013
345	3.060	0.978	2.992	0.016	69	0.013
350	3.076	0.978	3.008	0.016	70	0.013
355	3.091	0.978	3.024	0.016	71	0.013
360	3.106	0.979	3.040	0.016	72	0.013
365	3.021	0.979	2.957	0.018	73	0.013
370	3.041	0.979	2.977	0.020	74	0.013
375	3.062	0.979	2.997	0.020	75	0.013
380	3.082	0.979	3.017	0.020	76	0.013
385	3.102	0.979	3.037	0.020	77	0.013
390	3.122	0.979	3.057	0.020	78	0.013
395	3.142	0.979	3.076	0.020	79	0.013
400	3.162	0.979	3.096	0.019	80	0.014
405	3.182	0.979	3.115	0.019	81	0.014
410	3.202	0.979	3.134	0.019	82	0.014
415	3.221	0.979	3.153	0.019	83	0.014
420	3.240	0.979	3.172	0.019	84	0.014
425	3.260	0.979	3.191	0.019	85	0.014
430	3.279	0.979	3.210	0.019	86	0.014

OTAY RANCH VILLAGE 14
HEC HMS HYETOGRAPH CALCULATIONS

435	3.298	0.979	3.229	0.019	87	0.014
440	3.317	0.979	3.247	0.019	88	0.014
445	3.335	0.979	3.266	0.018	89	0.014
450	3.354	0.979	3.284	0.018	90	0.014
455	3.373	0.979	3.303	0.018	91	0.014
460	3.391	0.979	3.321	0.018	92	0.014
465	3.410	0.979	3.339	0.018	93	0.014
470	3.428	0.979	3.357	0.018	94	0.014
475	3.446	0.979	3.375	0.018	95	0.014
480	3.464	0.979	3.393	0.018	96	0.015
485	3.482	0.979	3.410	0.018	97	0.015
490	3.500	0.979	3.428	0.018	98	0.015
495	3.518	0.979	3.445	0.018	99	0.015
500	3.536	0.979	3.463	0.017	100	0.015
505	3.553	0.979	3.480	0.017	101	0.015
510	3.571	0.979	3.497	0.017	102	0.015
515	3.588	0.980	3.515	0.017	103	0.015
520	3.606	0.980	3.532	0.017	104	0.015
525	3.623	0.980	3.549	0.017	105	0.015
530	3.640	0.980	3.566	0.017	106	0.015
535	3.657	0.980	3.583	0.017	107	0.015
540	3.674	0.980	3.599	0.017	108	0.016
545	3.691	0.980	3.616	0.017	109	0.016
550	3.708	0.980	3.633	0.017	110	0.016
555	3.725	0.980	3.649	0.017	111	0.016
560	3.742	0.980	3.666	0.016	112	0.016
565	3.758	0.980	3.682	0.016	113	0.016
570	3.775	0.980	3.699	0.016	114	0.016
575	3.791	0.980	3.715	0.016	115	0.016
580	3.808	0.980	3.731	0.016	116	0.016
585	3.824	0.980	3.747	0.016	117	0.016
590	3.841	0.980	3.763	0.016	118	0.017
595	3.857	0.980	3.779	0.016	119	0.017
600	3.873	0.980	3.795	0.016	120	0.017
605	3.889	0.980	3.811	0.016	121	0.017
610	3.905	0.980	3.827	0.016	122	0.017
615	3.921	0.980	3.843	0.016	123	0.017
620	3.937	0.980	3.858	0.016	124	0.017
625	3.953	0.980	3.874	0.016	125	0.017
630	3.969	0.980	3.890	0.016	126	0.018
635	3.984	0.980	3.905	0.016	127	0.018
640	4.000	0.980	3.921	0.015	128	0.018
645	4.016	0.980	3.936	0.015	129	0.018
650	4.031	0.980	3.951	0.015	130	0.018
655	4.047	0.980	3.967	0.015	131	0.018
660	4.062	0.980	3.982	0.015	132	0.018
665	4.077	0.980	3.997	0.015	133	0.018
670	4.093	0.980	4.012	0.015	134	0.019
675	4.108	0.980	4.027	0.015	135	0.019
680	4.123	0.980	4.042	0.015	136	0.019
685	4.138	0.980	4.057	0.015	137	0.019
690	4.153	0.980	4.072	0.015	138	0.019
695	4.168	0.980	4.087	0.015	139	0.019
700	4.183	0.980	4.102	0.015	140	0.020
705	4.198	0.980	4.116	0.015	141	0.020
710	4.213	0.981	4.131	0.015	142	0.020
715	4.228	0.981	4.146	0.015	143	0.020
720	4.243	0.981	4.160	0.015	144	0.016
725	4.257	0.981	4.175	0.015	145	0.016

OTAY RANCH VILLAGE 14
HEC HMS HYETOGRAPH CALCULATIONS

730	4.272	0.981	4.189	0.014	146	0.016
735	4.287	0.981	4.204	0.014	147	0.016
740	4.301	0.981	4.218	0.014	148	0.017
745	4.316	0.981	4.232	0.014	149	0.017
750	4.330	0.981	4.247	0.014	150	0.017
755	4.345	0.981	4.261	0.014	151	0.017
760	4.359	0.981	4.275	0.014	152	0.018
765	4.373	0.981	4.289	0.014	153	0.018
770	4.387	0.981	4.303	0.014	154	0.018
775	4.402	0.981	4.317	0.014	155	0.018
780	4.416	0.981	4.331	0.014	156	0.019
785	4.430	0.981	4.345	0.014	157	0.019
790	4.444	0.981	4.359	0.014	158	0.019
795	4.458	0.981	4.373	0.014	159	0.020
800	4.472	0.981	4.387	0.014	160	0.020
805	4.486	0.981	4.401	0.014	161	0.020
810	4.500	0.981	4.415	0.014	162	0.021
815	4.514	0.981	4.428	0.014	163	0.021
820	4.528	0.981	4.442	0.014	164	0.022
825	4.541	0.981	4.456	0.014	165	0.022
830	4.555	0.981	4.469	0.014	166	0.023
835	4.569	0.981	4.483	0.014	167	0.023
840	4.583	0.981	4.496	0.014	168	0.026
845	4.596	0.981	4.510	0.013	169	0.026
850	4.610	0.981	4.523	0.013	170	0.027
855	4.623	0.981	4.537	0.013	171	0.028
860	4.637	0.981	4.550	0.013	172	0.029
865	4.650	0.981	4.563	0.013	173	0.029
870	4.664	0.981	4.577	0.013	174	0.030
875	4.677	0.981	4.590	0.013	175	0.031
880	4.690	0.981	4.603	0.013	176	0.032
885	4.704	0.981	4.616	0.013	177	0.033
890	4.717	0.981	4.629	0.013	178	0.035
895	4.730	0.981	4.643	0.013	179	0.036
900	4.743	0.981	4.656	0.013	180	0.038
905	4.757	0.982	4.669	0.013	181	0.040
910	4.770	0.982	4.682	0.013	182	0.043
915	4.783	0.982	4.695	0.013	183	0.044
920	4.796	0.982	4.708	0.013	184	0.060
925	4.809	0.982	4.720	0.013	185	0.062
930	4.822	0.982	4.733	0.013	186	0.067
935	4.835	0.982	4.746	0.013	187	0.071
940	4.848	0.982	4.759	0.013	188	0.072
945	4.861	0.982	4.772	0.013	189	0.082
950	4.873	0.982	4.784	0.013	190	0.121
955	4.886	0.982	4.797	0.013	191	0.170
960	4.899	0.982	4.810	0.013	192	0.609
965	4.912	0.982	4.822	0.013	193	0.097
970	4.924	0.982	4.835	0.013	194	0.076
975	4.937	0.982	4.848	0.013	195	0.064
980	4.950	0.982	4.860	0.013	196	0.046
985	4.962	0.982	4.873	0.013	197	0.041
990	4.975	0.982	4.885	0.012	198	0.037
995	4.987	0.982	4.898	0.012	199	0.034
1000	5.000	0.982	4.910	0.012	200	0.032
1005	5.012	0.982	4.922	0.012	201	0.030
1010	5.025	0.982	4.935	0.012	202	0.028
1015	5.037	0.982	4.947	0.012	203	0.027
1020	5.050	0.982	4.959	0.012	204	0.024

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1025	5.062	0.982	4.972	0.012	205	0.023
1030	5.074	0.982	4.984	0.012	206	0.022
1035	5.087	0.982	4.996	0.012	207	0.021
1040	5.099	0.982	5.008	0.012	208	0.020
1045	5.111	0.982	5.020	0.012	209	0.019
1050	5.123	0.982	5.033	0.012	210	0.019
1055	5.136	0.982	5.045	0.012	211	0.018
1060	5.148	0.982	5.057	0.012	212	0.018
1065	5.160	0.982	5.069	0.012	213	0.017
1070	5.172	0.982	5.081	0.012	214	0.017
1075	5.184	0.982	5.093	0.012	215	0.016
1080	5.196	0.982	5.105	0.012	216	0.018
1085	5.208	0.982	5.117	0.012	217	0.020
1090	5.220	0.982	5.129	0.012	218	0.020
1095	5.232	0.982	5.140	0.012	219	0.019
1100	5.244	0.983	5.152	0.012	220	0.019
1105	5.256	0.983	5.164	0.012	221	0.019
1110	5.268	0.983	5.176	0.012	222	0.018
1115	5.280	0.983	5.188	0.012	223	0.018
1120	5.292	0.983	5.199	0.012	224	0.018
1125	5.303	0.983	5.211	0.012	225	0.017
1130	5.315	0.983	5.223	0.012	226	0.017
1135	5.327	0.983	5.235	0.012	227	0.017
1140	5.339	0.983	5.246	0.012	228	0.017
1145	5.350	0.983	5.258	0.012	229	0.016
1150	5.362	0.983	5.269	0.012	230	0.016
1155	5.374	0.983	5.281	0.012	231	0.016
1160	5.385	0.983	5.293	0.012	232	0.016
1165	5.397	0.983	5.304	0.012	233	0.016
1170	5.408	0.983	5.316	0.012	234	0.016
1175	5.420	0.983	5.327	0.011	235	0.015
1180	5.431	0.983	5.339	0.011	236	0.015
1185	5.443	0.983	5.350	0.011	237	0.015
1190	5.454	0.983	5.361	0.011	238	0.015
1195	5.466	0.983	5.373	0.011	239	0.015
1200	5.477	0.983	5.384	0.011	240	0.015
1205	5.489	0.983	5.396	0.011	241	0.014
1210	5.500	0.983	5.407	0.011	242	0.014
1215	5.511	0.983	5.418	0.011	243	0.014
1220	5.523	0.983	5.429	0.011	244	0.014
1225	5.534	0.983	5.441	0.011	245	0.014
1230	5.545	0.983	5.452	0.011	246	0.014
1235	5.557	0.983	5.463	0.011	247	0.014
1240	5.568	0.983	5.474	0.011	248	0.013
1245	5.579	0.983	5.486	0.011	249	0.013
1250	5.590	0.983	5.497	0.011	250	0.013
1255	5.601	0.983	5.508	0.011	251	0.013
1260	5.612	0.983	5.519	0.011	252	0.013
1265	5.624	0.983	5.530	0.011	253	0.013
1270	5.635	0.983	5.541	0.011	254	0.013
1275	5.646	0.983	5.552	0.011	255	0.013
1280	5.657	0.983	5.563	0.011	256	0.013
1285	5.668	0.983	5.574	0.011	257	0.013
1290	5.679	0.983	5.585	0.011	258	0.012
1295	5.690	0.984	5.596	0.011	259	0.012
1300	5.701	0.984	5.607	0.011	260	0.012
1305	5.712	0.984	5.618	0.011	261	0.012
1310	5.723	0.984	5.629	0.011	262	0.012
1315	5.734	0.984	5.640	0.011	263	0.012

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1320	5.745	0.984	5.651	0.011	264	0.012
1325	5.755	0.984	5.661	0.011	265	0.012
1330	5.766	0.984	5.672	0.011	266	0.012
1335	5.777	0.984	5.683	0.011	267	0.012
1340	5.788	0.984	5.694	0.011	268	0.012
1345	5.799	0.984	5.705	0.011	269	0.012
1350	5.809	0.984	5.715	0.011	270	0.011
1355	5.820	0.984	5.726	0.011	271	0.011
1360	5.831	0.984	5.737	0.011	272	0.011
1365	5.842	0.984	5.747	0.011	273	0.011
1370	5.852	0.984	5.758	0.011	274	0.011
1375	5.863	0.984	5.769	0.011	275	0.011
1380	5.874	0.984	5.779	0.011	276	0.011
1385	5.884	0.984	5.790	0.011	277	0.011
1390	5.895	0.984	5.801	0.011	278	0.011
1395	5.906	0.984	5.811	0.011	279	0.011
1400	5.916	0.984	5.822	0.011	280	0.011
1405	5.927	0.984	5.832	0.011	281	0.011
1410	5.937	0.984	5.843	0.011	282	0.011
1415	5.948	0.984	5.853	0.011	283	0.011
1420	5.958	0.984	5.864	0.010	284	0.011
1425	5.969	0.984	5.874	0.010	285	0.011
1430	5.979	0.984	5.885	0.010	286	0.011
1435	5.990	0.984	5.895	0.010	287	0.010
1440	6.000	0.984	5.905	0.010	288	0.010

CHAPTER 5

5.2 – Proposed Condition Hydrology Map (HEC HMS)