

Appendix C –
Proposed Hydrology
(Un-Mitigated Peak Flow)

Hydrologic Work Maps
AES Output



DRAINAGE BOUNDARY
FLOW PATH → → → →
DRAINAGE NODE (100)

185614 - STARLIGHT SOLAR

PROPOSED DRAINAGE MAP ON-SITE AREA A

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
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Ver. 23.0 Release Date: 07/01/2016 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* 185614 STARLIGHT SOLAR *
* PR Q100 ON-SITE AREA A *
* 2024-02-27 *

FILE NAME: 614PRA.DAT
TIME/DATE OF STUDY: 17:33 02/27/2024

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 24.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

+-----+
| BEGIN AREA DRAINING TO NODE 106 |
| |
+-----+

FLOW PROCESS FROM NODE 100.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
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*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 96.00
UPSTREAM ELEVATION(FEET) = 3720.00
DOWNSTREAM ELEVATION(FEET) = 3710.00
ELEVATION DIFFERENCE(FEET) = 10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.122
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.291
SUBAREA RUNOFF(CFS) = 0.14
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.14

FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
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ELEVATION DATA: UPSTREAM(FEET) = 3710.00 DOWNSTREAM(FEET) = 3690.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 363.00 CHANNEL SLOPE = 0.0551
CHANNEL BASE(FEET) = 60.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.006
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.94
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.84
AVERAGE FLOW DEPTH(FEET) = 0.02 TRAVEL TIME(MIN.) = 7.22
Tc(MIN.) = 14.34
SUBAREA AREA(ACRES) = 1.71 SUBAREA RUNOFF(CFS) = 1.58
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 1.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.03 FLOW VELOCITY(FEET/SEC.) = 1.04
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 459.00 FEET.

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 3690.00 DOWNSTREAM(FEET) = 3670.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1099.00 CHANNEL SLOPE = 0.0182
CHANNEL BASE(FEET) = 50.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.493
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.98
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.18
AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 15.58
Tc(MIN.) = 29.92
SUBAREA AREA(ACRES) = 14.45 SUBAREA RUNOFF(CFS) = 8.29
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 16.3 PEAK FLOW RATE(CFS) = 9.32

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.11 FLOW VELOCITY(FEET/SEC.) = 1.37
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 1558.00 FEET.

FLOW PROCESS FROM NODE 104.00 TO NODE 106.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 3660.00 DOWNSTREAM(FEET) = 3554.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1371.00 CHANNEL SLOPE = 0.0773
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 7.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.301
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.31
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.77
AVERAGE FLOW DEPTH(FEET) = 0.55 TRAVEL TIME(MIN.) = 3.96
Tc(MIN.) = 33.88
SUBAREA AREA(ACRES) = 11.27 SUBAREA RUNOFF(CFS) = 5.96
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 27.5 PEAK FLOW RATE(CFS) = 14.57

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.58 FLOW VELOCITY(FEET/SEC.) = 6.09
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 2929.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.301
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2300
SUBAREA AREA(ACRES) = 45.90 SUBAREA RUNOFF(CFS) = 24.29
TOTAL AREA(ACRES) = 73.4 TOTAL RUNOFF(CFS) = 38.86
TC(MIN.) = 33.88

+-----+
| BEGIN AREA DRAINING TO NODE 118 |
| |
+-----+

FLOW PROCESS FROM NODE 110.00 TO NODE 112.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
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*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 91.00
UPSTREAM ELEVATION(FEET) = 3720.00
DOWNSTREAM ELEVATION(FEET) = 3710.00
ELEVATION DIFFERENCE(FEET) = 10.00

Results here used to
developed 100yr inflow
hydrograph for storage
analysis.

NODE 106

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.174
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.262
SUBAREA RUNOFF(CFS) = 0.13
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.13

FLOW PROCESS FROM NODE 112.00 TO NODE 113.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) =	3710.00	DOWNSTREAM(FEET) =	3655.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	313.00	CHANNEL SLOPE =	0.1757
CHANNEL BASE(FEET) =	50.00	"Z" FACTOR =	99.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	4.483		
*USER SPECIFIED(SUBAREA):			
USER-SPECIFIED RUNOFF COEFFICIENT =	.2000		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	1.01		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	1.07		
AVERAGE FLOW DEPTH(FEET) =	0.02	TRAVEL TIME(MIN.) =	4.87
Tc(MIN.) =	12.04		
SUBAREA AREA(ACRES) =	1.85	SUBAREA RUNOFF(CFS) =	1.66
AREA-AVERAGE RUNOFF COEFFICIENT =	0.200		
TOTAL AREA(ACRES) =	2.0	PEAK FLOW RATE(CFS) =	1.75

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.02 FLOW VELOCITY(FEET/SEC.) = 1.68
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 113.00 = 404.00 FEET.

FLOW PROCESS FROM NODE 113.00 TO NODE 114.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) =	3655.00	DOWNSTREAM(FEET) =	3650.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	772.00	CHANNEL SLOPE =	0.0065
CHANNEL BASE(FEET) =	23.00	"Z" FACTOR =	15.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.011		
*USER SPECIFIED(SUBAREA):			
USER-SPECIFIED RUNOFF COEFFICIENT =	.2000		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	6.28		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	1.25		
AVERAGE FLOW DEPTH(FEET) =	0.19	TRAVEL TIME(MIN.) =	10.28
Tc(MIN.) =	22.32		
SUBAREA AREA(ACRES) =	14.69	SUBAREA RUNOFF(CFS) =	8.85
AREA-AVERAGE RUNOFF COEFFICIENT =	0.200		
TOTAL AREA(ACRES) =	16.6	PEAK FLOW RATE(CFS) =	10.02

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.25 FLOW VELOCITY(FEET/SEC.) = 1.47
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 114.00 = 1176.00 FEET.

FLOW PROCESS FROM NODE 114.00 TO NODE 116.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3650.00 DOWNSTREAM(FEET) = 3610.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 489.00 CHANNEL SLOPE = 0.0818
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 14.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.879
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.13
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.07
AVERAGE FLOW DEPTH(FEET) = 0.43 TRAVEL TIME(MIN.) = 1.61
Tc(MIN.) = 23.93
SUBAREA AREA(ACRES) = 10.78 SUBAREA RUNOFF(CFS) = 6.21
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 27.4 PEAK FLOW RATE(CFS) = 15.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.46 FLOW VELOCITY(FEET/SEC.) = 5.32
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 116.00 = 1665.00 FEET.

FLOW PROCESS FROM NODE 116.00 TO NODE 118.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3610.00 DOWNSTREAM(FEET) = 3570.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1110.00 CHANNEL SLOPE = 0.0360
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 20.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.561
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.89
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.88
AVERAGE FLOW DEPTH(FEET) = 0.53 TRAVEL TIME(MIN.) = 4.77
Tc(MIN.) = 28.70

SUBAREA AREA(ACRES) = 23.78 SUBAREA RUNOFF(CFS) = 12.18
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 51.2 PEAK FLOW RATE(CFS) = 26.22

NODE 118

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.57 FLOW VELOCITY(FEET/SEC.) = 4.07
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 118.00 = 2775.00 FEET.

+-----+
| BEGIN AREA DRAINING TO NODE 128 |
| |
+-----+

FLOW PROCESS FROM NODE 120.00 TO NODE 122.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

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*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 3694.00
DOWNSTREAM ELEVATION(FEET) = 3690.00
ELEVATION DIFFERENCE(FEET) = 4.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.866
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.099
SUBAREA RUNOFF(CFS) = 0.13
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.13

FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3690.00 DOWNSTREAM(FEET) = 3674.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 251.00 CHANNEL SLOPE = 0.0637
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.158
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.95
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.14
AVERAGE FLOW DEPTH(FEET) = 0.03 TRAVEL TIME(MIN.) = 3.67
Tc(MIN.) = 13.53
SUBAREA AREA(ACRES) = 1.73 SUBAREA RUNOFF(CFS) = 1.65
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 1.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 1.41
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 123.00 = 351.00 FEET.

FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3674.00 DOWNSTREAM(FEET) = 3616.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 657.00 CHANNEL SLOPE = 0.0883
CHANNEL BASE(FEET) = 35.00 "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.361
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.14
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.07
AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 5.29
Tc(MIN.) = 18.82
SUBAREA AREA(ACRES) = 6.07 SUBAREA RUNOFF(CFS) = 4.69
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 7.9 PEAK FLOW RATE(CFS) = 6.12

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 2.39

LONGEST FLOWPATH FROM NODE 120.00 TO NODE 124.00 = 1008.00 FEET.

FLOW PROCESS FROM NODE 124.00 TO NODE 128.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3616.00	DOWNSTREAM(FEET) =	3560.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	576.00	CHANNEL SLOPE =	0.0972
CHANNEL BASE(FEET) =	13.00	"Z" FACTOR =	14.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.129		

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.00

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.34

AVERAGE FLOW DEPTH(FEET) = 0.18 TRAVEL TIME(MIN.) = 2.21

Tc(MIN.) = 21.04

SUBAREA AREA(ACRES) = 16.34 SUBAREA RUNOFF(CFS) = 11.76

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230

TOTAL AREA(ACRES) = 24.2 PEAK FLOW RATE(CFS) = 17.45

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 4.98

LONGEST FLOWPATH FROM NODE 120.00 TO NODE 128.00 = 1584.00 FEET.

Results here used to
developed 100yr inflow
hydrograph for storage
analysis.

NODE 128

+-----+
| BEGIN AREA DRAINING TO NODE 138 |
| |
+-----+

FLOW PROCESS FROM NODE 130.00 TO NODE 132.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 96.00

UPSTREAM ELEVATION(FEET) = 3688.00

DOWNSTREAM ELEVATION(FEET) = 3684.00

ELEVATION DIFFERENCE(FEET) = 4.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.865

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.099

SUBAREA RUNOFF(CFS) = 0.19

TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.19

FLOW PROCESS FROM NODE 132.00 TO NODE 133.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

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ELEVATION DATA: UPSTREAM(FEET) =	3684.00	DOWNSTREAM(FEET) =	3660.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	396.00	CHANNEL SLOPE =	0.0606
CHANNEL BASE(FEET) =	0.00	"Z" FACTOR =	6.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.464
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.00
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.92
AVERAGE FLOW DEPTH(FEET) = 0.24 TRAVEL TIME(MIN.) = 2.26
Tc(MIN.) = 12.12
SUBAREA AREA(ACRES) = 1.81 SUBAREA RUNOFF(CFS) = 1.62
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 1.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 3.43
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 133.00 = 492.00 FEET.

FLOW PROCESS FROM NODE 133.00 TO NODE 134.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3660.00 DOWNSTREAM(FEET) = 3638.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 510.00 CHANNEL SLOPE = 0.0431
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 14.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.904
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.28
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.03
AVERAGE FLOW DEPTH(FEET) = 0.32 TRAVEL TIME(MIN.) = 2.80
Tc(MIN.) = 14.93
SUBAREA AREA(ACRES) = 6.37 SUBAREA RUNOFF(CFS) = 4.97
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 8.4 PEAK FLOW RATE(CFS) = 6.54

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 FLOW VELOCITY(FEET/SEC.) = 3.39
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 134.00 = 1002.00 FEET.

FLOW PROCESS FROM NODE 134.00 TO NODE 136.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3638.00 DOWNSTREAM(FEET) = 3590.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1409.00 CHANNEL SLOPE = 0.0341
CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 20.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.054
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 15.01
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.40
AVERAGE FLOW DEPTH(FEET) = 0.36 TRAVEL TIME(MIN.) = 6.91
Tc(MIN.) = 21.84
SUBAREA AREA(ACRES) = 27.56 SUBAREA RUNOFF(CFS) = 16.83

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 35.9 PEAK FLOW RATE(CFS) = 21.95

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.43 FLOW VELOCITY(FEET/SEC.) = 3.75
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 136.00 = 2411.00 FEET.

FLOW PROCESS FROM NODE 136.00 TO NODE 138.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 3590.00 DOWNSTREAM(FEET) = 3512.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1556.00 CHANNEL SLOPE = 0.0501
CHANNEL BASE(FEET) = 40.00 "Z" FACTOR = 25.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.555

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 35.53

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.72

AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 6.96

Tc(MIN.) = 28.80

SUBAREA AREA(ACRES) = 53.16 SUBAREA RUNOFF(CFS) = 27.16

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 89.1 PEAK FLOW RATE(CFS) = 45.52

NODE 138

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 FLOW VELOCITY(FEET/SEC.) = 3.99
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 138.00 = 3967.00 FEET.

+-----+
| BEGIN AREA DRAINING TO NODE 149 |
| |
+-----+

FLOW PROCESS FROM NODE 140.00 TO NODE 142.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 3698.00

DOWNSTREAM ELEVATION(FEET) = 3690.00

ELEVATION DIFFERENCE(FEET) = 8.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.101

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.790

SUBAREA RUNOFF(CFS) = 0.50

TOTAL AREA(ACRES) = 0.43 TOTAL RUNOFF(CFS) = 0.50

FLOW PROCESS FROM NODE 142.00 TO NODE 143.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<


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=====
ELEVATION DATA: UPSTREAM(FEET) = 3690.00 DOWNSTREAM(FEET) = 3680.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 169.00 CHANNEL SLOPE = 0.0592
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 7.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.932
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.03
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.23
AVERAGE FLOW DEPTH(FEET) = 0.03 TRAVEL TIME(MIN.) = 2.29
Tc(MIN.) = 10.39
SUBAREA AREA(ACRES) = 1.09 SUBAREA RUNOFF(CFS) = 1.08
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 1.50

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 1.40
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 143.00 = 269.00 FEET.

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FLOW PROCESS FROM NODE 143.00 TO NODE 144.00 IS CODE = 51
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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

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=====
ELEVATION DATA: UPSTREAM(FEET) = 3680.00 DOWNSTREAM(FEET) = 3640.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 409.00 CHANNEL SLOPE = 0.0978
CHANNEL BASE(FEET) = 12.00 "Z" FACTOR = 6.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.368
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.84
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.17
AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 2.15
Tc(MIN.) = 12.54
SUBAREA AREA(ACRES) = 5.35 SUBAREA RUNOFF(CFS) = 4.67
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 6.9 PEAK FLOW RATE(CFS) = 6.00

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 3.77
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 144.00 = 678.00 FEET.

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*****
FLOW PROCESS FROM NODE 144.00 TO NODE 146.00 IS CODE = 51
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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

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=====
ELEVATION DATA: UPSTREAM(FEET) = 3640.00 DOWNSTREAM(FEET) = 3564.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 872.00 CHANNEL SLOPE = 0.0872
CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 14.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.746
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0

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TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.23
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.31
AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 3.37
Tc(MIN.) = 15.91
SUBAREA AREA(ACRES) = 11.26 SUBAREA RUNOFF(CFS) = 8.44
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 18.1 PEAK FLOW RATE(CFS) = 13.58

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 4.61
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 146.00 = 1550.00 FEET.

FLOW PROCESS FROM NODE 146.00 TO NODE 148.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3564.00 DOWNSTREAM(FEET) = 3516.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 774.00 CHANNEL SLOPE = 0.0620
CHANNEL BASE(FEET) = 18.00 "Z" FACTOR = 9.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.361

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.33

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.42

AVERAGE FLOW DEPTH(FEET) = 0.24 TRAVEL TIME(MIN.) = 2.92

Tc(MIN.) = 18.83

SUBAREA AREA(ACRES) = 23.02 SUBAREA RUNOFF(CFS) = 15.47

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 41.2 PEAK FLOW RATE(CFS) = 27.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.28 FLOW VELOCITY(FEET/SEC.) = 4.86

LONGEST FLOWPATH FROM NODE 140.00 TO NODE 148.00 = 2324.00 FEET.

FLOW PROCESS FROM NODE 148.00 TO NODE 149.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3516.00 DOWNSTREAM(FEET) = 3490.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 742.00 CHANNEL SLOPE = 0.0350
CHANNEL BASE(FEET) = 9.00 "Z" FACTOR = 20.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.062

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 35.44

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.22

AVERAGE FLOW DEPTH(FEET) = 0.46 TRAVEL TIME(MIN.) = 2.93

Tc(MIN.) = 21.76

SUBAREA AREA(ACRES) = 25.43 SUBAREA RUNOFF(CFS) = 15.57

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 66.6 PEAK FLOW RATE(CFS) = 40.77

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 FLOW VELOCITY(FEET/SEC.) = 4.38
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 149.00 = 3066.00 FEET.

FLOW PROCESS FROM NODE 149.00 TO NODE 149.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.062

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.2000

SUBAREA AREA(ACRES) = 42.04 SUBAREA RUNOFF(CFS) = 25.74

TOTAL AREA(ACRES) = 108.6 TOTAL RUNOFF(CFS) = 66.51

TC(MIN.) = 21.76

NODE 149

+-----+
| BEGIN AREA DRAINING TO NODE 156 |
+-----+

FLOW PROCESS FROM NODE 150.00 TO NODE 152.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 3690.00

DOWNSTREAM ELEVATION(FEET) = 3680.00

ELEVATION DIFFERENCE(FEET) = 10.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.269

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.209

SUBAREA RUNOFF(CFS) = 1.43

TOTAL AREA(ACRES) = 1.00 TOTAL RUNOFF(CFS) = 1.43

FLOW PROCESS FROM NODE 152.00 TO NODE 153.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3680.00 DOWNSTREAM(FEET) = 3668.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 431.00 CHANNEL SLOPE = 0.0278

CHANNEL BASE(FEET) = 14.00 "Z" FACTOR = 9.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.561

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.26

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.61

AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 4.46

Tc(MIN.) = 11.73

SUBAREA AREA(ACRES) = 1.57 SUBAREA RUNOFF(CFS) = 1.65

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230

TOTAL AREA(ACRES) = 2.6 PEAK FLOW RATE(CFS) = 2.70

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 1.74

LONGEST FLOWPATH FROM NODE 150.00 TO NODE 153.00 = 531.00 FEET.

FLOW PROCESS FROM NODE 153.00 TO NODE 154.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3668.00 DOWNSTREAM(FEET) = 3616.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 723.00 CHANNEL SLOPE = 0.0719

CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 15.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.645

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.71

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.47

AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 4.88

Tc(MIN.) = 16.60

SUBAREA AREA(ACRES) = 9.50 SUBAREA RUNOFF(CFS) = 7.96

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230

TOTAL AREA(ACRES) = 12.1 PEAK FLOW RATE(CFS) = 10.12

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.11 FLOW VELOCITY(FEET/SEC.) = 2.92

LONGEST FLOWPATH FROM NODE 150.00 TO NODE 154.00 = 1254.00 FEET.

FLOW PROCESS FROM NODE 154.00 TO NODE 156.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3616.00 DOWNSTREAM(FEET) = 3570.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 591.00 CHANNEL SLOPE = 0.0778

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 10.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.411

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.61

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.47

AVERAGE FLOW DEPTH(FEET) = 0.50 TRAVEL TIME(MIN.) = 1.80

Tc(MIN.) = 18.40

SUBAREA AREA(ACRES) = 8.89 SUBAREA RUNOFF(CFS) = 6.97

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230

TOTAL AREA(ACRES) = 21.0 PEAK FLOW RATE(CFS) = 16.44

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.54 FLOW VELOCITY(FEET/SEC.) = 5.70

LONGEST FLOWPATH FROM NODE 150.00 TO NODE 156.00 = 1845.00 FEET.

+-----+

BEGIN AREA DRAINING TO NODE 166

|-----|

Results here used to
developed 100yr inflow
hydrograph for storage
analysis.

NODE 156


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|-----|
+-----+

*****
FLOW PROCESS FROM NODE    160.00 TO NODE    162.00 IS CODE =  21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) =  0
INITIAL SUBAREA FLOW-LENGTH(FEET) =   93.00
UPSTREAM ELEVATION(FEET) =  3644.00
DOWNSTREAM ELEVATION(FEET) =  3630.00
ELEVATION DIFFERENCE(FEET) =   14.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =   7.010
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  6.356
SUBAREA RUNOFF(CFS) =      0.92
TOTAL AREA(ACRES) =      0.63  TOTAL RUNOFF(CFS) =      0.92

*****
FLOW PROCESS FROM NODE    162.00 TO NODE    163.00 IS CODE =  51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  3630.00  DOWNSTREAM(FEET) =  3610.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  213.00  CHANNEL SLOPE =  0.0939
CHANNEL BASE(FEET) =   0.00  "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.030  MAXIMUM DEPTH(FEET) =  2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.860
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) =  0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =      2.34
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =  3.77
AVERAGE FLOW DEPTH(FEET) =  0.25  TRAVEL TIME(MIN.) =  0.94
Tc(MIN.) =  7.95
SUBAREA AREA(ACRES) =      2.10  SUBAREA RUNOFF(CFS) =      2.83
AREA-AVERAGE RUNOFF COEFFICIENT =  0.230
TOTAL AREA(ACRES) =      2.7  PEAK FLOW RATE(CFS) =      3.68

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.29  FLOW VELOCITY(FEET/SEC.) =  4.24
LONGEST FLOWPATH FROM NODE    160.00 TO NODE    163.00 =  306.00 FEET.

*****
FLOW PROCESS FROM NODE    163.00 TO NODE    164.00 IS CODE =  51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  3610.00  DOWNSTREAM(FEET) =  3560.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  562.00  CHANNEL SLOPE =  0.0890
CHANNEL BASE(FEET) =   0.00  "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.030  MAXIMUM DEPTH(FEET) =  2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.158
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) =  0

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TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.41
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.38
AVERAGE FLOW DEPTH(FEET) = 0.44 TRAVEL TIME(MIN.) = 1.74
Tc(MIN.) = 9.69
SUBAREA AREA(ACRES) = 11.32 SUBAREA RUNOFF(CFS) = 13.43
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 14.0 PEAK FLOW RATE(CFS) = 16.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.52 FLOW VELOCITY(FEET/SEC.) = 6.08
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 164.00 = 868.00 FEET.

FLOW PROCESS FROM NODE 164.00 TO NODE 165.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3560.00 DOWNSTREAM(FEET) = 3550.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 539.00 CHANNEL SLOPE = 0.0186
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 17.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.393

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 26.49

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.28

AVERAGE FLOW DEPTH(FEET) = 0.69 TRAVEL TIME(MIN.) = 2.74

Tc(MIN.) = 12.43

SUBAREA AREA(ACRES) = 19.40 SUBAREA RUNOFF(CFS) = 19.60

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230

TOTAL AREA(ACRES) = 33.4 PEAK FLOW RATE(CFS) = 33.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.75 FLOW VELOCITY(FEET/SEC.) = 3.51

LONGEST FLOWPATH FROM NODE 160.00 TO NODE 165.00 = 1407.00 FEET.

FLOW PROCESS FROM NODE 165.00 TO NODE 166.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3550.00 DOWNSTREAM(FEET) = 3524.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 285.00 CHANNEL SLOPE = 0.0912
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.253

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 35.47

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.42

AVERAGE FLOW DEPTH(FEET) = 0.69 TRAVEL TIME(MIN.) = 0.64

Tc(MIN.) = 13.07

SUBAREA AREA(ACRES) = 3.43 SUBAREA RUNOFF(CFS) = 3.35

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230

TOTAL AREA(ACRES) = 36.9 PEAK FLOW RATE(CFS) = 36.07

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

Results here used to
developed 100yr inflow
hydrograph for storage
analysis.

NODE 165

DEPTH(FEET) = 0.70 FLOW VELOCITY(FEET/SEC.) = 7.38
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 166.00 = 1692.00 FEET.

FLOW PROCESS FROM NODE 166.00 TO NODE 166.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.07
RAINFALL INTENSITY(INCH/HR) = 4.25
TOTAL STREAM AREA(ACRES) = 36.88
PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.07

FLOW PROCESS FROM NODE 161.00 TO NODE 161.10 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 3654.00
DOWNSTREAM ELEVATION(FEET) = 3640.00
ELEVATION DIFFERENCE(FEET) = 14.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.269
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.209
SUBAREA RUNOFF(CFS) = 0.61
TOTAL AREA(ACRES) = 0.43 TOTAL RUNOFF(CFS) = 0.61

FLOW PROCESS FROM NODE 161.10 TO NODE 161.20 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3640.00 DOWNSTREAM(FEET) = 3580.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 475.00 CHANNEL SLOPE = 0.1263
CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.240
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.15
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.62
AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 2.19
Tc(MIN.) = 9.46
SUBAREA AREA(ACRES) = 5.82 SUBAREA RUNOFF(CFS) = 7.01
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 6.2 PEAK FLOW RATE(CFS) = 7.53

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.15 FLOW VELOCITY(FEET/SEC.) = 4.44
LONGEST FLOWPATH FROM NODE 161.00 TO NODE 161.20 = 575.00 FEET.

FLOW PROCESS FROM NODE 161.20 TO NODE 161.30 IS CODE = 51

```

-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 3580.00 DOWNSTREAM(FEET) = 3556.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 481.00 CHANNEL SLOPE = 0.0499
CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 3.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 5.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.561
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.66
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.53
AVERAGE FLOW DEPTH(FEET) = 0.19 TRAVEL TIME(MIN.) = 2.27
Tc(MIN.) = 11.73
SUBAREA AREA(ACRES) = 5.93 SUBAREA RUNOFF(CFS) = 6.22
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 12.2 PEAK FLOW RATE(CFS) = 12.78

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.21 FLOW VELOCITY(FEET/SEC.) = 3.88
LONGEST FLOWPATH FROM NODE 161.00 TO NODE 161.30 = 1056.00 FEET.

*****
FLOW PROCESS FROM NODE 161.30 TO NODE 166.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 3556.00 DOWNSTREAM(FEET) = 3524.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 530.00 CHANNEL SLOPE = 0.0604
CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 5.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 5.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.120
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2300
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.66
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.41
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 2.00
Tc(MIN.) = 13.73
SUBAREA AREA(ACRES) = 8.20 SUBAREA RUNOFF(CFS) = 7.77
AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 20.4 PEAK FLOW RATE(CFS) = 19.31

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.25 FLOW VELOCITY(FEET/SEC.) = 4.66
LONGEST FLOWPATH FROM NODE 161.00 TO NODE 166.00 = 1586.00 FEET.

*****
FLOW PROCESS FROM NODE 166.00 TO NODE 166.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 13.73
RAINFALL INTENSITY(INCH/HR) = 4.12
TOTAL STREAM AREA(ACRES) = 20.38

```


PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.31

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	36.07	13.07	4.253	36.88
2	19.31	13.73	4.120	20.38

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	54.46	13.07	4.253
2	54.26	13.73	4.120

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 54.46 Tc(MIN.) = 13.07

TOTAL AREA(ACRES) = 57.3

LONGEST FLOWPATH FROM NODE 160.00 TO NODE 166.00 = 1692.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 57.3 TC(MIN.) = 13.07

PEAK FLOW RATE(CFS) = 54.46

NODE 166
(Unmitigated)

END OF RATIONAL METHOD ANALYSIS



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1264

Analysis prepared by:

Mitigated Analysis for Node 166

***** DESCRIPTION OF STUDY *****

* 185614 STARLIGHT SOLAR *
* PR MITIGATED ON-SITE AREA A - NODES 165 AND 166 *
* 2024-02-27 *

FILE NAME: 614PRAM.DAT
TIME/DATE OF STUDY: 18:38 02/27/2024

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 24.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS
USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
 HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
 WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

+-----+
| BEGIN AREA DRAINING TO NODE 166 |
| Use HydraFlow Hydrograph Output for Node 165 Basin Outflow |
| |
+-----+

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 264.00 RAIN INTENSITY(INCH/HOUR) = 0.61

TOTAL AREA(ACRES) = 33.40 TOTAL RUNOFF(CFS) = 9.00

FLOW PROCESS FROM NODE 165.00 TO NODE 166.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3550.00 DOWNSTREAM(FEET) = 3524.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 285.00 CHANNEL SLOPE = 0.0912

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 10.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 0.611

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.24

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.32

AVERAGE FLOW DEPTH(FEET) = 0.42 TRAVEL TIME(MIN.) = 0.89

Tc(MIN.) = 264.89

SUBAREA AREA(ACRES) = 3.43 SUBAREA RUNOFF(CFS) = 0.48

AREA-AVERAGE RUNOFF COEFFICIENT = 0.421

TOTAL AREA(ACRES) = 36.8 PEAK FLOW RATE(CFS) = 9.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 FLOW VELOCITY(FEET/SEC.) = 5.30

LONGEST FLOWPATH FROM NODE 0.00 TO NODE 166.00 = 285.00 FEET.

FLOW PROCESS FROM NODE 166.00 TO NODE 166.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 264.89

RAINFALL INTENSITY(INCH/HR) = 0.61

TOTAL STREAM AREA(ACRES) = 36.83

PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.46

FLOW PROCESS FROM NODE 161.00 TO NODE 161.10 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 3654.00
DOWNSTREAM ELEVATION(FEET) = 3640.00
ELEVATION DIFFERENCE(FEET) = 14.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.269
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.209
SUBAREA RUNOFF(CFS) = 0.61
TOTAL AREA(ACRES) = 0.43 TOTAL RUNOFF(CFS) = 0.61

FLOW PROCESS FROM NODE 161.10 TO NODE 161.20 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3640.00	DOWNSTREAM(FEET) =	3580.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	475.00	CHANNEL SLOPE =	0.1263
CHANNEL BASE(FEET) =	10.00	"Z" FACTOR =	10.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	5.240		
*USER SPECIFIED(SUBAREA):			
USER-SPECIFIED RUNOFF COEFFICIENT =	.2300		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	4.15		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	3.62		
AVERAGE FLOW DEPTH(FEET) =	0.10	TRAVEL TIME(MIN.) =	2.19
Tc(MIN.) =	9.46		
SUBAREA AREA(ACRES) =	5.82	SUBAREA RUNOFF(CFS) =	7.01
AREA-AVERAGE RUNOFF COEFFICIENT =	0.230		
TOTAL AREA(ACRES) =	6.2	PEAK FLOW RATE(CFS) =	7.53

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.15 FLOW VELOCITY(FEET/SEC.) = 4.44
LONGEST FLOWPATH FROM NODE 161.00 TO NODE 161.20 = 575.00 FEET.

FLOW PROCESS FROM NODE 161.20 TO NODE 161.30 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3580.00	DOWNSTREAM(FEET) =	3556.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	481.00	CHANNEL SLOPE =	0.0499
CHANNEL BASE(FEET) =	15.00	"Z" FACTOR =	3.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	5.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	4.561		
*USER SPECIFIED(SUBAREA):			
USER-SPECIFIED RUNOFF COEFFICIENT =	.2300		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	10.66		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	3.53		
AVERAGE FLOW DEPTH(FEET) =	0.19	TRAVEL TIME(MIN.) =	2.27
Tc(MIN.) =	11.73		
SUBAREA AREA(ACRES) =	5.93	SUBAREA RUNOFF(CFS) =	6.22

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230
TOTAL AREA(ACRES) = 12.2 PEAK FLOW RATE(CFS) = 12.78

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.21 FLOW VELOCITY(FEET/SEC.) = 3.88
LONGEST FLOWPATH FROM NODE 161.00 TO NODE 161.30 = 1056.00 FEET.

FLOW PROCESS FROM NODE 161.30 TO NODE 166.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3556.00 DOWNSTREAM(FEET) = 3524.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 530.00 CHANNEL SLOPE = 0.0604

CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 5.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 5.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.120

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2300

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.66

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.41

AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 2.00

Tc(MIN.) = 13.73

SUBAREA AREA(ACRES) = 8.20 SUBAREA RUNOFF(CFS) = 7.77

AREA-AVERAGE RUNOFF COEFFICIENT = 0.230

TOTAL AREA(ACRES) = 20.4 PEAK FLOW RATE(CFS) = 19.31

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.25 FLOW VELOCITY(FEET/SEC.) = 4.66

LONGEST FLOWPATH FROM NODE 161.00 TO NODE 166.00 = 1586.00 FEET.

FLOW PROCESS FROM NODE 166.00 TO NODE 166.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 13.73

RAINFALL INTENSITY(INCH/HR) = 4.12

TOTAL STREAM AREA(ACRES) = 20.38

PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.31

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.46	264.89	0.611	36.83
2	19.31	13.73	4.120	20.38

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	19.80	13.73	4.120
2	12.32	264.89	0.611

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 19.80 Tc(MIN.) = 13.73

TOTAL AREA(ACRES) = 57.2

LONGEST FLOWPATH FROM NODE 161.00 TO NODE 166.00 = 1586.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 57.2 TC(MIN.) = 13.73

PEAK FLOW RATE(CFS) = 19.80

NODE 166
(Mitigated)

=====

END OF RATIONAL METHOD ANALYSIS



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
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Ver. 23.0 Release Date: 07/01/2016 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* 185614 STARLIGHT SOLAR *
* PR Q100 ON-SITE AREA B *
* 2024-03-01 *

FILE NAME: 614PRB.DAT
TIME/DATE OF STUDY: 08:31 03/02/2024

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 24.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS
USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
 HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
 WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 200.00 TO NODE 202.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000
 S.C.S. CURVE NUMBER (AMC II) = 0
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
 UPSTREAM ELEVATION(FEET) = 3626.00
 DOWNSTREAM ELEVATION(FEET) = 3590.00
 ELEVATION DIFFERENCE(FEET) = 36.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.520
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.075
 SUBAREA RUNOFF(CFS) = 0.12
 TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.12

FLOW PROCESS FROM NODE 202.00 TO NODE 204.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3590.00 DOWNSTREAM(FEET) = 3526.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 262.00 CHANNEL SLOPE = 0.2443
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 8.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.285

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000
 S.C.S. CURVE NUMBER (AMC II) = 0
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.63
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.41
 AVERAGE FLOW DEPTH(FEET) = 0.03 TRAVEL TIME(MIN.) = 1.81
 Tc(MIN.) = 9.33
 SUBAREA AREA(ACRES) = 2.83 SUBAREA RUNOFF(CFS) = 2.99
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
 TOTAL AREA(ACRES) = 2.9 PEAK FLOW RATE(CFS) = 3.10

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 3.12
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 204.00 = 362.00 FEET.

FLOW PROCESS FROM NODE 204.00 TO NODE 216.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3526.00 DOWNSTREAM(FEET) = 3500.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 933.00 CHANNEL SLOPE = 0.0279
 CHANNEL BASE(FEET) = 25.00 "Z" FACTOR = 15.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.425

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000
 S.C.S. CURVE NUMBER (AMC II) = 0
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.80
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.74
 AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 8.95

Tc(MIN.) = 18.28
SUBAREA AREA(ACRES) = 4.83 SUBAREA RUNOFF(CFS) = 3.31
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 7.8 PEAK FLOW RATE(CFS) = 5.32

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.11 FLOW VELOCITY(FEET/SEC.) = 1.82
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 216.00 = 1295.00 FEET.

FLOW PROCESS FROM NODE 204.00 TO NODE 216.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 18.28
RAINFALL INTENSITY(INCH/HR) = 3.43
TOTAL STREAM AREA(ACRES) = 7.76
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.32

FLOW PROCESS FROM NODE 210.00 TO NODE 212.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 98.00
UPSTREAM ELEVATION(FEET) = 3530.00
DOWNSTREAM ELEVATION(FEET) = 3514.00
ELEVATION DIFFERENCE(FEET) = 16.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.444
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.115
SUBAREA RUNOFF(CFS) = 0.20
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.20

FLOW PROCESS FROM NODE 212.00 TO NODE 214.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3514.00 DOWNSTREAM(FEET) = 3510.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 306.00 CHANNEL SLOPE = 0.0131
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 45.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.852
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.90
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.65

AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 7.79
Tc(MIN.) = 15.24
SUBAREA AREA(ACRES) = 1.73 SUBAREA RUNOFF(CFS) = 1.33
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 1.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 0.80
LONGEST FLOWPATH FROM NODE 210.00 TO NODE 214.00 = 404.00 FEET.

FLOW PROCESS FROM NODE 214.00 TO NODE 216.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3510.00 DOWNSTREAM(FEET) = 3500.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 513.00 CHANNEL SLOPE = 0.0195
CHANNEL BASE(FEET) = 55.00 "Z" FACTOR = 35.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.817

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.48

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.90

AVERAGE FLOW DEPTH(FEET) = 0.05 TRAVEL TIME(MIN.) = 9.51

Tc(MIN.) = 24.75

SUBAREA AREA(ACRES) = 3.55 SUBAREA RUNOFF(CFS) = 2.00

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 5.4 PEAK FLOW RATE(CFS) = 3.07

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 0.96
LONGEST FLOWPATH FROM NODE 210.00 TO NODE 216.00 = 917.00 FEET.

FLOW PROCESS FROM NODE 214.00 TO NODE 216.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 24.75

RAINFALL INTENSITY(INCH/HR) = 2.82

TOTAL STREAM AREA(ACRES) = 5.44

PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.07

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.32	18.28	3.425	7.76
2	3.07	24.75	2.817	5.44

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

**** PEAK FLOW RATE TABLE ****

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	7.58	18.28	3.425
2	7.44	24.75	2.817

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.58 Tc(MIN.) = 18.28
TOTAL AREA(ACRES) = 13.2

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 216.00 = 1295.00 FEET.

NODE 216

END NODE 216
BEGIN NODE 220

FLOW PROCESS FROM NODE 220.00 TO NODE 222.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 3516.00
DOWNSTREAM ELEVATION(FEET) = 3510.00
ELEVATION DIFFERENCE(FEET) = 6.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 8.166
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.760
SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.35

FLOW PROCESS FROM NODE 222.00 TO NODE 224.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3510.00 DOWNSTREAM(FEET) = 3500.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 282.00 CHANNEL SLOPE = 0.0355
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 30.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.370
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.18
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.08
AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 4.36
Tc(MIN.) = 12.53

SUBAREA AREA(ACRES) = 1.91 SUBAREA RUNOFF(CFS) = 1.67
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 1.93

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 1.21
LONGEST FLOWPATH FROM NODE 220.00 TO NODE 224.00 = 372.00 FEET.

FLOW PROCESS FROM NODE 224.00 TO NODE 226.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3500.00 DOWNSTREAM(FEET) = 3482.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 525.00 CHANNEL SLOPE = 0.0343

CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 30.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.409

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.13

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.49

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 5.89

Tc(MIN.) = 18.42

SUBAREA AREA(ACRES) = 3.50 SUBAREA RUNOFF(CFS) = 2.39

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 5.7 PEAK FLOW RATE(CFS) = 3.89

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 1.52

LONGEST FLOWPATH FROM NODE 220.00 TO NODE 226.00 = 897.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 5.7 TC(MIN.) = 18.42

PEAK FLOW RATE(CFS) = 3.89

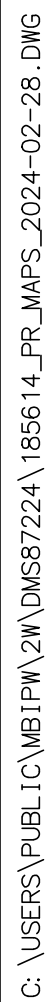
NODE 226

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END OF RATIONAL METHOD ANALYSIS

↑



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* 185614 STARLIGHT SOLAR *
* PR Q100 ONSITE & OFFSITE AREA C *
* 2024-03-01 *

FILE NAME: 614PRC.DAT
TIME/DATE OF STUDY: 08:42 03/02/2024

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 24.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS
USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
 HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
 WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 300.00 TO NODE 302.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 83.00
UPSTREAM ELEVATION(FEET) = 3560.00
DOWNSTREAM ELEVATION(FEET) = 3540.00
ELEVATION DIFFERENCE(FEET) = 20.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.851
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.451
SUBAREA RUNOFF(CFS) = 0.12
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.12

FLOW PROCESS FROM NODE 302.00 TO NODE 304.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3540.00	DOWNSTREAM(FEET) =	3528.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	201.00	CHANNEL SLOPE =	0.0597
CHANNEL BASE(FEET) =	18.00	"Z" FACTOR =	6.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	5.005		

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2000
S.C.S. CURVE NUMBER (AMC II) =	0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	0.47
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	1.01
AVERAGE FLOW DEPTH(FEET) =	0.03
TRAVEL TIME(MIN.) =	3.30
Tc(MIN.) =	10.15
SUBAREA AREA(ACRES) =	0.70
SUBAREA RUNOFF(CFS) =	0.70
AREA-AVERAGE RUNOFF COEFFICIENT =	0.200
TOTAL AREA(ACRES) =	0.8
PEAK FLOW RATE(CFS) =	0.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) =	0.03	FLOW VELOCITY(FEET/SEC.) =	1.30
LONGEST FLOWPATH FROM NODE	300.00	TO NODE	304.00 =
			284.00 FEET.

FLOW PROCESS FROM NODE 304.00 TO NODE 312.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3528.00	DOWNSTREAM(FEET) =	3510.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	250.00	CHANNEL SLOPE =	0.0720
CHANNEL BASE(FEET) =	17.00	"Z" FACTOR =	24.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	4.451		

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2000
S.C.S. CURVE NUMBER (AMC II) =	0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	2.20
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	2.05
AVERAGE FLOW DEPTH(FEET) =	0.06
TRAVEL TIME(MIN.) =	2.03

Tc(MIN.) = 12.18
SUBAREA AREA(ACRES) = 3.17 SUBAREA RUNOFF(CFS) = 2.82
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 3.52

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 2.30
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 312.00 = 534.00 FEET.

FLOW PROCESS FROM NODE 304.00 TO NODE 312.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.18
RAINFALL INTENSITY(INCH/HR) = 4.45
TOTAL STREAM AREA(ACRES) = 3.96
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.52

FLOW PROCESS FROM NODE 306.00 TO NODE 308.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.00
UPSTREAM ELEVATION(FEET) = 3630.00
DOWNSTREAM ELEVATION(FEET) = 3610.00
ELEVATION DIFFERENCE(FEET) = 20.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.406
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.135
SUBAREA RUNOFF(CFS) = 0.15
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.15

FLOW PROCESS FROM NODE 308.00 TO NODE 310.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3610.00 DOWNSTREAM(FEET) = 3584.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 595.00 CHANNEL SLOPE = 0.0437
CHANNEL BASE(FEET) = 9.00 "Z" FACTOR = 5.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.691
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.38
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.60

AVERAGE FLOW DEPTH(FEET) = 0.13 TRAVEL TIME(MIN.) = 3.82
Tc(MIN.) = 11.23
SUBAREA AREA(ACRES) = 6.76 SUBAREA RUNOFF(CFS) = 6.34
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 6.9 PEAK FLOW RATE(CFS) = 6.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.20 FLOW VELOCITY(FEET/SEC.) = 3.31
LONGEST FLOWPATH FROM NODE 306.00 TO NODE 310.00 = 692.00 FEET.

FLOW PROCESS FROM NODE 310.00 TO NODE 311.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3584.00 DOWNSTREAM(FEET) = 3530.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 619.00 CHANNEL SLOPE = 0.0872
CHANNEL BASE(FEET) = 35.00 "Z" FACTOR = 4.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.941

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.29

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.96

AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 3.48

Tc(MIN.) = 14.71

SUBAREA AREA(ACRES) = 7.19 SUBAREA RUNOFF(CFS) = 5.67

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 14.1 PEAK FLOW RATE(CFS) = 11.09

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 3.07
LONGEST FLOWPATH FROM NODE 306.00 TO NODE 311.00 = 1311.00 FEET.

FLOW PROCESS FROM NODE 311.00 TO NODE 312.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3530.00 DOWNSTREAM(FEET) = 3510.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 501.00 CHANNEL SLOPE = 0.0399
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 4.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.688

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.30

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.24

AVERAGE FLOW DEPTH(FEET) = 0.80 TRAVEL TIME(MIN.) = 1.59

Tc(MIN.) = 16.30

SUBAREA AREA(ACRES) = 6.00 SUBAREA RUNOFF(CFS) = 4.43

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 20.1 PEAK FLOW RATE(CFS) = 14.80

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.83 FLOW VELOCITY(FEET/SEC.) = 5.39
LONGEST FLOWPATH FROM NODE 306.00 TO NODE 312.00 = 1812.00 FEET.

FLOW PROCESS FROM NODE 311.00 TO NODE 312.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 16.30
RAINFALL INTENSITY(INCH/HR) = 3.69
TOTAL STREAM AREA(ACRES) = 20.07
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.80

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.52	12.18	4.451	3.96
2	14.80	16.30	3.688	20.07

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	14.59	12.18	4.451
2	17.72	16.30	3.688

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 17.72 Tc(MIN.) = 16.30
TOTAL AREA(ACRES) = 24.0
LONGEST FLOWPATH FROM NODE 306.00 TO NODE 312.00 = 1812.00 FEET.

FLOW PROCESS FROM NODE 312.00 TO NODE 314.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3510.00 DOWNSTREAM(FEET) = 3488.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 645.00 CHANNEL SLOPE = 0.0341
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 25.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.297
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.68

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.48
AVERAGE FLOW DEPTH(FEET) = 0.48 TRAVEL TIME(MIN.) = 3.09
Tc(MIN.) = 19.39
SUBAREA AREA(ACRES) = 5.93 SUBAREA RUNOFF(CFS) = 3.91
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 30.0 PEAK FLOW RATE(CFS) = 19.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.48 FLOW VELOCITY(FEET/SEC.) = 3.49
LONGEST FLOWPATH FROM NODE 306.00 TO NODE 314.00 = 2457.00 FEET.

FLOW PROCESS FROM NODE 314.00 TO NODE 330.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3488.00 DOWNSTREAM(FEET) = 3472.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 476.00 CHANNEL SLOPE = 0.0336
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 36.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.019

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 20.89

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.79

AVERAGE FLOW DEPTH(FEET) = 0.20 TRAVEL TIME(MIN.) = 2.85

Tc(MIN.) = 22.24

SUBAREA AREA(ACRES) = 3.77 SUBAREA RUNOFF(CFS) = 2.28

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 33.7 PEAK FLOW RATE(CFS) = 20.36

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.20 FLOW VELOCITY(FEET/SEC.) = 2.72
LONGEST FLOWPATH FROM NODE 306.00 TO NODE 330.00 = 2933.00 FEET.

FLOW PROCESS FROM NODE 314.00 TO NODE 330.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 22.24
RAINFALL INTENSITY(INCH/HR) = 3.02
TOTAL STREAM AREA(ACRES) = 33.73
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.36

FLOW PROCESS FROM NODE 316.00 TO NODE 318.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 99.00
UPSTREAM ELEVATION(FEET) = 3580.00
DOWNSTREAM ELEVATION(FEET) = 3578.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 11.836
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 85.30
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN T_c CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.534
SUBAREA RUNOFF(CFS) = 0.64
TOTAL AREA(ACRES) = 0.71 TOTAL RUNOFF(CFS) = 0.64

FLOW PROCESS FROM NODE 318.00 TO NODE 320.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3578.00	DOWNSTREAM(FEET) =	3540.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	363.00	CHANNEL SLOPE =	0.1047
CHANNEL BASE(FEET) =	30.00	"Z" FACTOR =	99.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.770		

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2000		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	1.72		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	1.54		
AVERAGE FLOW DEPTH(FEET) =	0.03	TRAVEL TIME(MIN.) =	3.92
T_c (MIN.) =	15.76		
SUBAREA AREA(ACRES) =	2.82	SUBAREA RUNOFF(CFS) =	2.13
AREA-AVERAGE RUNOFF COEFFICIENT =	0.200		
TOTAL AREA(ACRES) =	3.5	PEAK FLOW RATE(CFS) =	2.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) =	0.04	FLOW VELOCITY(FEET/SEC.) =	1.81
LONGEST FLOWPATH FROM NODE	316.00	TO NODE	320.00 =
			462.00 FEET.

FLOW PROCESS FROM NODE 320.00 TO NODE 322.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3540.00	DOWNSTREAM(FEET) =	3496.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	699.00	CHANNEL SLOPE =	0.0629
CHANNEL BASE(FEET) =	7.00	"Z" FACTOR =	5.000
MANNING'S FACTOR =	0.030	MAXIMUM DEPTH(FEET) =	2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.332		

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2000		
S.C.S. CURVE NUMBER (AMC II) =	0		

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.70
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.51
 AVERAGE FLOW DEPTH(FEET) = 0.17 TRAVEL TIME(MIN.) = 3.32
 Tc(MIN.) = 19.08
 SUBAREA AREA(ACRES) = 6.09 SUBAREA RUNOFF(CFS) = 4.06
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
 TOTAL AREA(ACRES) = 9.6 PEAK FLOW RATE(CFS) = 6.41

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.20 FLOW VELOCITY(FEET/SEC.) = 3.94
 LONGEST FLOWPATH FROM NODE 316.00 TO NODE 322.00 = 1161.00 FEET.

FLOW PROCESS FROM NODE 322.00 TO NODE 330.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3496.00 DOWNSTREAM(FEET) = 3472.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 686.00 CHANNEL SLOPE = 0.0350
 CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 22.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.890

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.05

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.43

AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 4.71

Tc(MIN.) = 23.79

SUBAREA AREA(ACRES) = 2.19 SUBAREA RUNOFF(CFS) = 1.27

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 11.8 PEAK FLOW RATE(CFS) = 6.83

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 2.38
 LONGEST FLOWPATH FROM NODE 316.00 TO NODE 330.00 = 1847.00 FEET.

FLOW PROCESS FROM NODE 322.00 TO NODE 330.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 23.79
 RAINFALL INTENSITY(INCH/HR) = 2.89
 TOTAL STREAM AREA(ACRES) = 11.81
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.83

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	20.36	22.24	3.019	33.73

2 6.83 23.79 2.890 11.81

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	26.74	22.24	3.019
2	26.32	23.79	2.890

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.74 Tc(MIN.) = 22.24

TOTAL AREA(ACRES) = 45.5

LONGEST FLOWPATH FROM NODE 306.00 TO NODE 330.00 = 2933.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 45.5 TC(MIN.) = 22.24

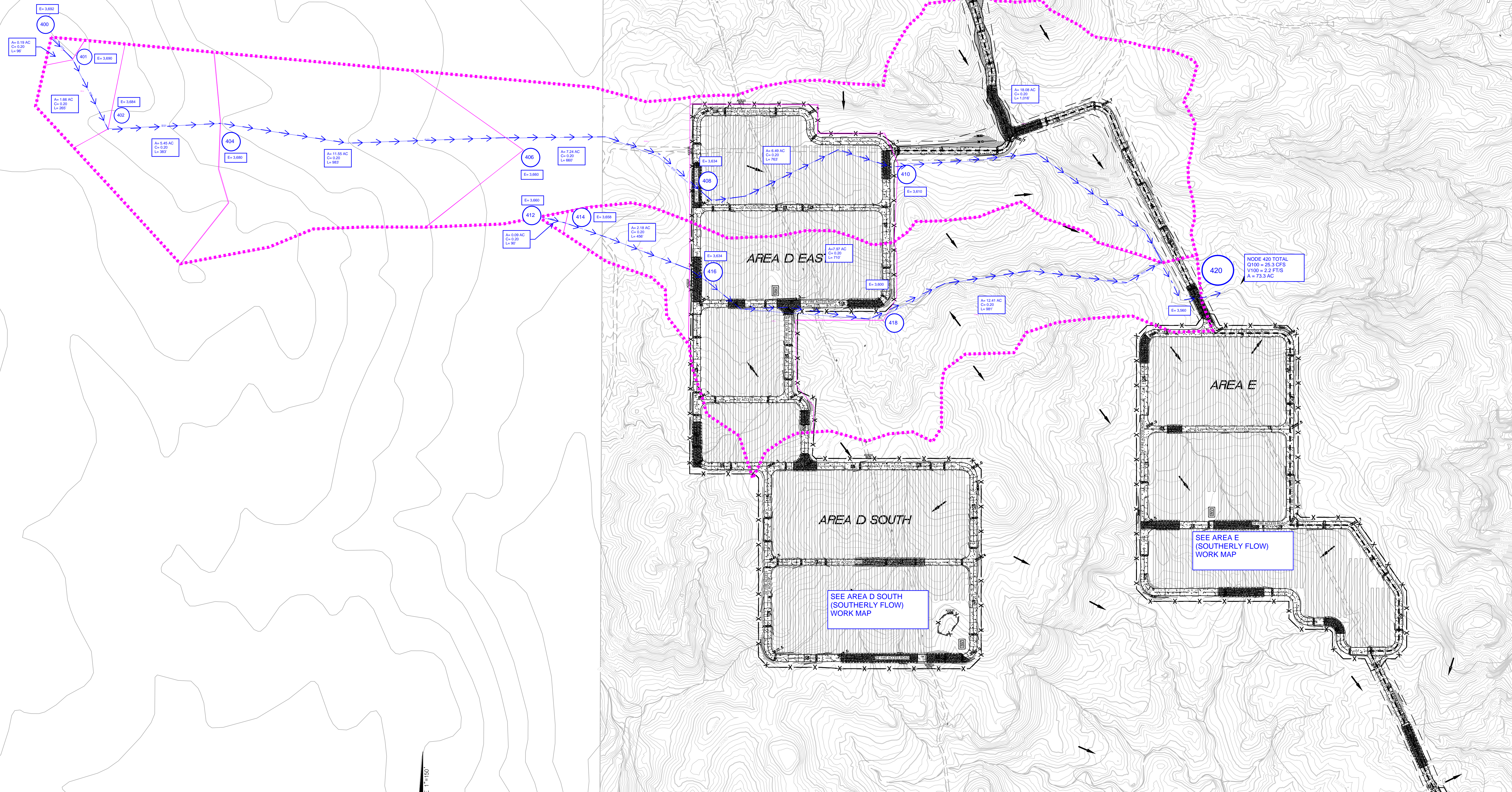
PEAK FLOW RATE(CFS) = 26.74

=====

END OF RATIONAL METHOD ANALYSIS

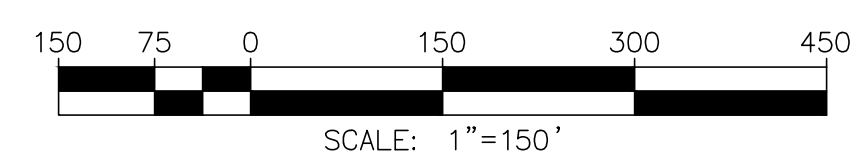


SEE AREA C WORK MAP



C:\USERS\PUBLIC\BIPW\2W\DNS87224\185614_PR_MAPS_2024-02-28.DWG 3/14/2024 8:15 AM

Michael Baker
INTERNATIONAL
9755 Clairemont Mesa Boulevard
San Diego, CA 92124
Phone: (858) 614-5000 ·
MBAKERINTL.COM



SCALE 1"=150'

185614 - STARLIGHT SOLAR
PROPOSED DRAINAGE MAP
ON-SITE AREA D (EASTERLY FLOW)

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* 185614 STARLIGHT SOLAR *
* PR Q100 AREA D (EASTERLY FLOW) *
* 2024-03-01 *

FILE NAME: 614PRD.DAT
TIME/DATE OF STUDY: 08:47 03/02/2024

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 24.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: CONSIDER ALL CONFLUENCE STREAM COMBINATIONS
FOR ALL DOWNSTREAM ANALYSES

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL								
	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)						
===	=====	=====	=====	=====	=====	=====	=====	=====
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====

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*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 96.00
UPSTREAM ELEVATION(FEET) = 3692.00
DOWNSTREAM ELEVATION(FEET) = 3690.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 11.780
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 86.25
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.548
SUBAREA RUNOFF(CFS) = 0.17
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.17

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FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 51
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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====

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ELEVATION DATA: UPSTREAM(FEET) = 3690.00 DOWNSTREAM(FEET) = 3684.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 265.00 CHANNEL SLOPE = 0.0226
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.430
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.76
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.68
AVERAGE FLOW DEPTH(FEET) = 0.03 TRAVEL TIME(MIN.) = 6.46
Tc(MIN.) = 18.24
SUBAREA AREA(ACRES) = 1.66 SUBAREA RUNOFF(CFS) = 1.14
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 1.27

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END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 0.86
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 402.00 = 361.00 FEET.

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FLOW PROCESS FROM NODE 402.00 TO NODE 404.00 IS CODE = 51
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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====

```

```

ELEVATION DATA: UPSTREAM(FEET) = 3684.00 DOWNSTREAM(FEET) = 3680.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 383.00 CHANNEL SLOPE = 0.0104
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.735
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000

```

S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.79
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 0.83
AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 7.68
Tc(MIN.) = 25.92
SUBAREA AREA(ACRES) = 5.45 SUBAREA RUNOFF(CFS) = 2.98
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 7.3 PEAK FLOW RATE(CFS) = 3.99

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 0.95
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 404.00 = 744.00 FEET.

FLOW PROCESS FROM NODE 404.00 TO NODE 406.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3680.00 DOWNSTREAM(FEET) = 3660.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 983.00 CHANNEL SLOPE = 0.0203
CHANNEL BASE(FEET) = 43.00 "Z" FACTOR = 99.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.119

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.45

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.30

AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 12.56

Tc(MIN.) = 38.48

SUBAREA AREA(ACRES) = 11.55 SUBAREA RUNOFF(CFS) = 4.90

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 18.9 PEAK FLOW RATE(CFS) = 7.99

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 1.44
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 406.00 = 1727.00 FEET.

FLOW PROCESS FROM NODE 406.00 TO NODE 408.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3660.00 DOWNSTREAM(FEET) = 3634.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 660.00 CHANNEL SLOPE = 0.0394
CHANNEL BASE(FEET) = 17.00 "Z" FACTOR = 16.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 1.991

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.43

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.80

AVERAGE FLOW DEPTH(FEET) = 0.17 TRAVEL TIME(MIN.) = 3.93
Tc(MIN.) = 42.41
SUBAREA AREA(ACRES) = 7.24 SUBAREA RUNOFF(CFS) = 2.88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 26.1 PEAK FLOW RATE(CFS) = 10.39

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.18 FLOW VELOCITY(FEET/SEC.) = 2.90
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 408.00 = 2387.00 FEET.

FLOW PROCESS FROM NODE 408.00 TO NODE 410.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3634.00 DOWNSTREAM(FEET) = 3610.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 763.00 CHANNEL SLOPE = 0.0315
CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 30.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 1.856

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.59

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.61

AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 4.87

Tc(MIN.) = 47.28

SUBAREA AREA(ACRES) = 6.49 SUBAREA RUNOFF(CFS) = 2.41

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 32.6 PEAK FLOW RATE(CFS) = 12.09

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.22 FLOW VELOCITY(FEET/SEC.) = 2.60

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 410.00 = 3150.00 FEET.

FLOW PROCESS FROM NODE 410.00 TO NODE 420.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3610.00 DOWNSTREAM(FEET) = 3580.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1016.00 CHANNEL SLOPE = 0.0295
CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 25.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 1.724

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 15.21

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.97

AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 5.70

Tc(MIN.) = 52.98

SUBAREA AREA(ACRES) = 18.08 SUBAREA RUNOFF(CFS) = 6.24

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 50.7 PEAK FLOW RATE(CFS) = 17.47

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 FLOW VELOCITY(FEET/SEC.) = 3.09
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 420.00 = 4166.00 FEET.

FLOW PROCESS FROM NODE 410.00 TO NODE 420.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 52.98
RAINFALL INTENSITY(INCH/HR) = 1.72
TOTAL STREAM AREA(ACRES) = 50.66
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.47

FLOW PROCESS FROM NODE 412.00 TO NODE 414.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 3660.00
DOWNSTREAM ELEVATION(FEET) = 3658.00
ELEVATION DIFFERENCE(FEET) = 2.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 11.668
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 88.33
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.576
SUBAREA RUNOFF(CFS) = 0.18
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.18

FLOW PROCESS FROM NODE 414.00 TO NODE 416.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3658.00 DOWNSTREAM(FEET) = 3634.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 456.00 CHANNEL SLOPE = 0.0526
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 20.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.350
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.89

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.05
AVERAGE FLOW DEPTH(FEET) = 0.03 TRAVEL TIME(MIN.) = 7.25
Tc(MIN.) = 18.92
SUBAREA AREA(ACRES) = 2.07 SUBAREA RUNOFF(CFS) = 1.39
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 2.3 PEAK FLOW RATE(CFS) = 1.52

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.04 FLOW VELOCITY(FEET/SEC.) = 1.20
LONGEST FLOWPATH FROM NODE 412.00 TO NODE 416.00 = 546.00 FEET.

FLOW PROCESS FROM NODE 416.00 TO NODE 418.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3634.00 DOWNSTREAM(FEET) = 3600.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 710.00 CHANNEL SLOPE = 0.0479
CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 20.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.810

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.77

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.00

AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 5.93

Tc(MIN.) = 24.85

SUBAREA AREA(ACRES) = 7.97 SUBAREA RUNOFF(CFS) = 4.48

AREA-AVERAGE RUNOFF COEFFICIENT = 0.200

TOTAL AREA(ACRES) = 10.2 PEAK FLOW RATE(CFS) = 5.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.11 FLOW VELOCITY(FEET/SEC.) = 2.36
LONGEST FLOWPATH FROM NODE 412.00 TO NODE 418.00 = 1256.00 FEET.

FLOW PROCESS FROM NODE 418.00 TO NODE 420.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3600.00 DOWNSTREAM(FEET) = 3580.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 981.00 CHANNEL SLOPE = 0.0204
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 30.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.377

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.71

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.22

AVERAGE FLOW DEPTH(FEET) = 0.36 TRAVEL TIME(MIN.) = 7.35

Tc(MIN.) = 32.20

SUBAREA AREA(ACRES) = 12.41 SUBAREA RUNOFF(CFS) = 5.90
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 22.6 PEAK FLOW RATE(CFS) = 10.77

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.39 FLOW VELOCITY(FEET/SEC.) = 2.41
LONGEST FLOWPATH FROM NODE 412.00 TO NODE 420.00 = 2237.00 FEET.

FLOW PROCESS FROM NODE 418.00 TO NODE 420.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 32.20
RAINFALL INTENSITY(INCH/HR) = 2.38
TOTAL STREAM AREA(ACRES) = 22.65
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.77

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	17.47	52.98	1.724	50.66
2	10.77	32.20	2.377	22.65

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	21.39	32.20	2.377
2	25.28	52.98	1.724

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 25.28 Tc(MIN.) = 52.98
TOTAL AREA(ACRES) = 73.3
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 420.00 = 4166.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)	=	73.3	TC(MIN.) =	52.98
PEAK FLOW RATE(CFS)	=	25.28		

NODE 420

*** PEAK FLOW RATE TABLE ***

	Q(CFS)	Tc(MIN.)
1	21.39	32.20
2	25.28	52.98

=====

=====

END OF RATIONAL METHOD ANALYSIS



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* 185614 STARLIGHT SOLAR *
* PR Q100 ONSITE AREAS D (SOUTHERLY FLOW) - H *
* 2024-03-01 *

FILE NAME: 614PRDH.DAT
TIME/DATE OF STUDY: 08:53 03/02/2024

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 3.000
SPECIFIED MINIMUM PIPE SIZE(INCH) = 24.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS
USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
 HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
 WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 500.00 TO NODE 502.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 86.00
UPSTREAM ELEVATION(FEET) = 3646.00
DOWNSTREAM ELEVATION(FEET) = 3640.00
ELEVATION DIFFERENCE(FEET) = 6.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.863
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.903
SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.31 TOTAL RUNOFF(CFS) = 0.37

FLOW PROCESS FROM NODE 502.00 TO NODE 504.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3640.00	DOWNSTREAM(FEET) =	3590.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	808.00	CHANNEL SLOPE =	0.0619
CHANNEL BASE(FEET) =	8.00	"Z" FACTOR =	15.000
MANNING'S FACTOR = 0.030	MAXIMUM DEPTH(FEET) =	2.00	
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	4.505		

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2000		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	5.69		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	3.29		
AVERAGE FLOW DEPTH(FEET) =	0.16	TRAVEL TIME(MIN.) =	4.09
Tc(MIN.) =	11.95		
SUBAREA AREA(ACRES) =	11.62	SUBAREA RUNOFF(CFS) =	10.47
AREA-AVERAGE RUNOFF COEFFICIENT =	0.200		
TOTAL AREA(ACRES) =	11.9	PEAK FLOW RATE(CFS) =	10.75

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) =	0.23	FLOW VELOCITY(FEET/SEC.) =	4.00
LONGEST FLOWPATH FROM NODE	500.00	TO NODE	504.00 =
			894.00 FEET.

FLOW PROCESS FROM NODE 504.00 TO NODE 520.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	3590.00	DOWNSTREAM(FEET) =	3500.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1505.00	CHANNEL SLOPE =	0.0598
CHANNEL BASE(FEET) =	0.00	"Z" FACTOR =	10.000
MANNING'S FACTOR = 0.030	MAXIMUM DEPTH(FEET) =	2.00	
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.618		

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2000		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	16.35		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	5.18		
AVERAGE FLOW DEPTH(FEET) =	0.56	TRAVEL TIME(MIN.) =	4.84
Tc(MIN.) =	16.79		

SUBAREA AREA(ACRES) = 15.42 SUBAREA RUNOFF(CFS) = 11.16
AREA-AVERAGE RUNOFF COEFFICIENT = 0.200
TOTAL AREA(ACRES) = 27.4 PEAK FLOW RATE(CFS) = 19.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.61 FLOW VELOCITY(FEET/SEC.) = 5.40
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 520.00 = 2399.00 FEET.

FLOW PROCESS FROM NODE 504.00 TO NODE 520.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.79
RAINFALL INTENSITY(INCH/HR) = 3.62
TOTAL STREAM AREA(ACRES) = 27.35
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.79

FLOW PROCESS FROM NODE 510.00 TO NODE 512.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 98.00
UPSTREAM ELEVATION(FEET) = 3624.00
DOWNSTREAM ELEVATION(FEET) = 3606.00
ELEVATION DIFFERENCE(FEET) = 18.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.444
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.115
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.13 TOTAL RUNOFF(CFS) = 0.16

FLOW PROCESS FROM NODE 512.00 TO NODE 514.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3606.00 DOWNSTREAM(FEET) = 3524.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 959.00 CHANNEL SLOPE = 0.0855
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 20.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.784
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.24
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.64
AVERAGE FLOW DEPTH(FEET) = 0.36 TRAVEL TIME(MIN.) = 3.45

Tc(MIN.) = 10.89
SUBAREA AREA(ACRES) = 20.24 SUBAREA RUNOFF(CFS) = 24.21
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250
TOTAL AREA(ACRES) = 20.4 PEAK FLOW RATE(CFS) = 24.33

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.47 FLOW VELOCITY(FEET/SEC.) = 5.50
LONGEST FLOWPATH FROM NODE 510.00 TO NODE 514.00 = 1057.00 FEET.

FLOW PROCESS FROM NODE 514.00 TO NODE 520.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3524.00 DOWNSTREAM(FEET) = 3500.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 671.00 CHANNEL SLOPE = 0.0358
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 40.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.079

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 34.51
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.66
AVERAGE FLOW DEPTH(FEET) = 0.49 TRAVEL TIME(MIN.) = 3.05
Tc(MIN.) = 13.95
SUBAREA AREA(ACRES) = 19.92 SUBAREA RUNOFF(CFS) = 20.31
AREA-AVERAGE RUNOFF COEFFICIENT = 0.250
TOTAL AREA(ACRES) = 40.3 PEAK FLOW RATE(CFS) = 41.06

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.52 FLOW VELOCITY(FEET/SEC.) = 3.77
LONGEST FLOWPATH FROM NODE 510.00 TO NODE 520.00 = 1728.00 FEET.

FLOW PROCESS FROM NODE 514.00 TO NODE 520.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 13.95
RAINFALL INTENSITY(INCH/HR) = 4.08
TOTAL STREAM AREA(ACRES) = 40.29
PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.06

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	19.79	16.79	3.618	27.35
2	41.06	13.95	4.079	40.29

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	57.49	13.95	4.079
2	56.21	16.79	3.618

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 57.49 Tc(MIN.) = 13.95

TOTAL AREA(ACRES) = 67.6

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 520.00 = 2399.00 FEET.

FLOW PROCESS FROM NODE 520.00 TO NODE 522.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3500.00 DOWNSTREAM(FEET) = 3484.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1157.00 CHANNEL SLOPE = 0.0138

CHANNEL BASE(FEET) = 13.00 "Z" FACTOR = 10.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.386

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2600

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 74.51

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.13

AVERAGE FLOW DEPTH(FEET) = 0.84 TRAVEL TIME(MIN.) = 4.67

Tc(MIN.) = 18.61

SUBAREA AREA(ACRES) = 38.66 SUBAREA RUNOFF(CFS) = 34.03

AREA-AVERAGE RUNOFF COEFFICIENT = 0.241

TOTAL AREA(ACRES) = 106.3 PEAK FLOW RATE(CFS) = 86.63

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.91 FLOW VELOCITY(FEET/SEC.) = 4.34

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 522.00 = 3556.00 FEET.

FLOW PROCESS FROM NODE 522.00 TO NODE 524.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3484.00 DOWNSTREAM(FEET) = 3450.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1621.00 CHANNEL SLOPE = 0.0210

CHANNEL BASE(FEET) = 11.00 "Z" FACTOR = 16.000

MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.846

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 93.06

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.70

AVERAGE FLOW DEPTH(FEET) = 0.82 TRAVEL TIME(MIN.) = 5.75
Tc(MIN.) = 24.37
SUBAREA AREA(ACRES) = 22.59 SUBAREA RUNOFF(CFS) = 12.86
AREA-AVERAGE RUNOFF COEFFICIENT = 0.234
TOTAL AREA(ACRES) = 128.9 PEAK FLOW RATE(CFS) = 86.63

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.79 FLOW VELOCITY(FEET/SEC.) = 4.63
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 524.00 = 5177.00 FEET.

FLOW PROCESS FROM NODE 524.00 TO NODE 524.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.846
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2285
SUBAREA AREA(ACRES) = 22.73 SUBAREA RUNOFF(CFS) = 12.94
TOTAL AREA(ACRES) = 151.6 TOTAL RUNOFF(CFS) = 98.61
TC(MIN.) = 24.37

FLOW PROCESS FROM NODE 524.00 TO NODE 526.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3450.00 DOWNSTREAM(FEET) = 3430.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1313.00 CHANNEL SLOPE = 0.0152
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 50.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.440
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 106.28
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.34
AVERAGE FLOW DEPTH(FEET) = 0.80 TRAVEL TIME(MIN.) = 6.56
Tc(MIN.) = 30.93
SUBAREA AREA(ACRES) = 31.42 SUBAREA RUNOFF(CFS) = 15.33
AREA-AVERAGE RUNOFF COEFFICIENT = 0.224
TOTAL AREA(ACRES) = 183.0 PEAK FLOW RATE(CFS) = 99.89

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.78 FLOW VELOCITY(FEET/SEC.) = 3.27
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 526.00 = 6490.00 FEET.

FLOW PROCESS FROM NODE 526.00 TO NODE 550.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 3430.00 DOWNSTREAM(FEET) = 3420.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1665.00 CHANNEL SLOPE = 0.0060
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 40.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.000
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 108.10
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.49
AVERAGE FLOW DEPTH(FEET) = 1.04 TRAVEL TIME(MIN.) = 11.16
Tc(MIN.) = 42.08
SUBAREA AREA(ACRES) = 41.01 SUBAREA RUNOFF(CFS) = 16.41
AREA-AVERAGE RUNOFF COEFFICIENT = 0.219
TOTAL AREA(ACRES) = 224.0 PEAK FLOW RATE(CFS) = 99.89

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 1.01 FLOW VELOCITY(FEET/SEC.) = 2.44
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 550.00 = 8155.00 FEET.

*****
FLOW PROCESS FROM NODE 526.00 TO NODE 550.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 42.08
RAINFALL INTENSITY(INCH/HR) = 2.00
TOTAL STREAM AREA(ACRES) = 224.05
PEAK FLOW RATE(CFS) AT CONFLUENCE = 99.89

*****
FLOW PROCESS FROM NODE 530.00 TO NODE 532.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2600
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 3552.00
DOWNSTREAM ELEVATION(FEET) = 3518.00
ELEVATION DIFFERENCE(FEET) = 34.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.019
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.351
SUBAREA RUNOFF(CFS) = 1.87
TOTAL AREA(ACRES) = 1.13 TOTAL RUNOFF(CFS) = 1.87

*****
FLOW PROCESS FROM NODE 532.00 TO NODE 534.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

```


>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3518.00 DOWNSTREAM(FEET) = 3480.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 794.00 CHANNEL SLOPE = 0.0479
CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 20.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.805

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2600

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.94

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.48

AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 3.80

Tc(MIN.) = 10.82

SUBAREA AREA(ACRES) = 15.90 SUBAREA RUNOFF(CFS) = 19.86

AREA-AVERAGE RUNOFF COEFFICIENT = 0.260

TOTAL AREA(ACRES) = 17.0 PEAK FLOW RATE(CFS) = 21.27

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 FLOW VELOCITY(FEET/SEC.) = 4.10

LONGEST FLOWPATH FROM NODE 530.00 TO NODE 534.00 = 894.00 FEET.

FLOW PROCESS FROM NODE 534.00 TO NODE 536.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3480.00 DOWNSTREAM(FEET) = 3456.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 831.00 CHANNEL SLOPE = 0.0289
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 35.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.909

*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 31.08

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.40

AVERAGE FLOW DEPTH(FEET) = 0.47 TRAVEL TIME(MIN.) = 4.08

Tc(MIN.) = 14.89

SUBAREA AREA(ACRES) = 24.94 SUBAREA RUNOFF(CFS) = 19.50

AREA-AVERAGE RUNOFF COEFFICIENT = 0.224

TOTAL AREA(ACRES) = 42.0 PEAK FLOW RATE(CFS) = 36.81

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.51 FLOW VELOCITY(FEET/SEC.) = 3.51

LONGEST FLOWPATH FROM NODE 530.00 TO NODE 536.00 = 1725.00 FEET.

FLOW PROCESS FROM NODE 536.00 TO NODE 538.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3456.00 DOWNSTREAM(FEET) = 3440.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1314.00 CHANNEL SLOPE = 0.0122
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 80.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.814
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .2000
 S.C.S. CURVE NUMBER (AMC II) = 0
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 47.76
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.21
 AVERAGE FLOW DEPTH(FEET) = 0.46 TRAVEL TIME(MIN.) = 9.89
 Tc(MIN.) = 24.79
 SUBAREA AREA(ACRES) = 38.62 SUBAREA RUNOFF(CFS) = 21.74
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.213
 TOTAL AREA(ACRES) = 80.6 PEAK FLOW RATE(CFS) = 48.24

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.46 FLOW VELOCITY(FEET/SEC.) = 2.22
 LONGEST FLOWPATH FROM NODE 530.00 TO NODE 538.00 = 3039.00 FEET.

FLOW PROCESS FROM NODE 538.00 TO NODE 550.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3440.00 DOWNSTREAM(FEET) = 3420.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 940.00 CHANNEL SLOPE = 0.0213
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 60.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.490
 *USER SPECIFIED(SUBAREA):
 USER-SPECIFIED RUNOFF COEFFICIENT = .2000
 S.C.S. CURVE NUMBER (AMC II) = 0
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 52.80
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.02
 AVERAGE FLOW DEPTH(FEET) = 0.46 TRAVEL TIME(MIN.) = 5.18
 Tc(MIN.) = 29.97
 SUBAREA AREA(ACRES) = 18.34 SUBAREA RUNOFF(CFS) = 9.13
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.210
 TOTAL AREA(ACRES) = 98.9 PEAK FLOW RATE(CFS) = 51.82

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.46 FLOW VELOCITY(FEET/SEC.) = 2.99
 LONGEST FLOWPATH FROM NODE 530.00 TO NODE 550.00 = 3979.00 FEET.

FLOW PROCESS FROM NODE 538.00 TO NODE 550.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 29.97
 RAINFALL INTENSITY(INCH/HR) = 2.49

TOTAL STREAM AREA(ACRES) = 98.93
PEAK FLOW RATE(CFS) AT CONFLUENCE = 51.82

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	99.89	42.08	2.000	224.05
2	51.82	29.97	2.490	98.93

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	132.06	29.97	2.490
2	141.52	42.08	2.000

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 141.52 Tc(MIN.) = 42.08

TOTAL AREA(ACRES) = 323.0

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 550.00 = 8155.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 323.0 TC(MIN.) = 42.08

PEAK FLOW RATE(CFS) = 141.52

=====

=====

END OF RATIONAL METHOD ANALYSIS



Appendix D –
Proposed Detention Basin
(Mitigated Peak Flow)

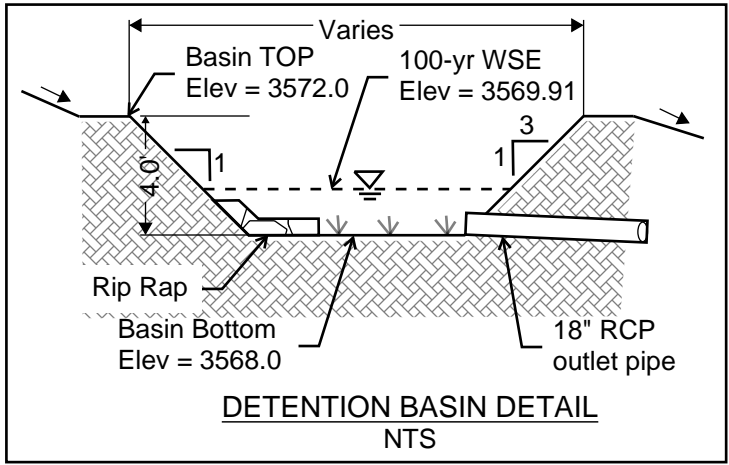
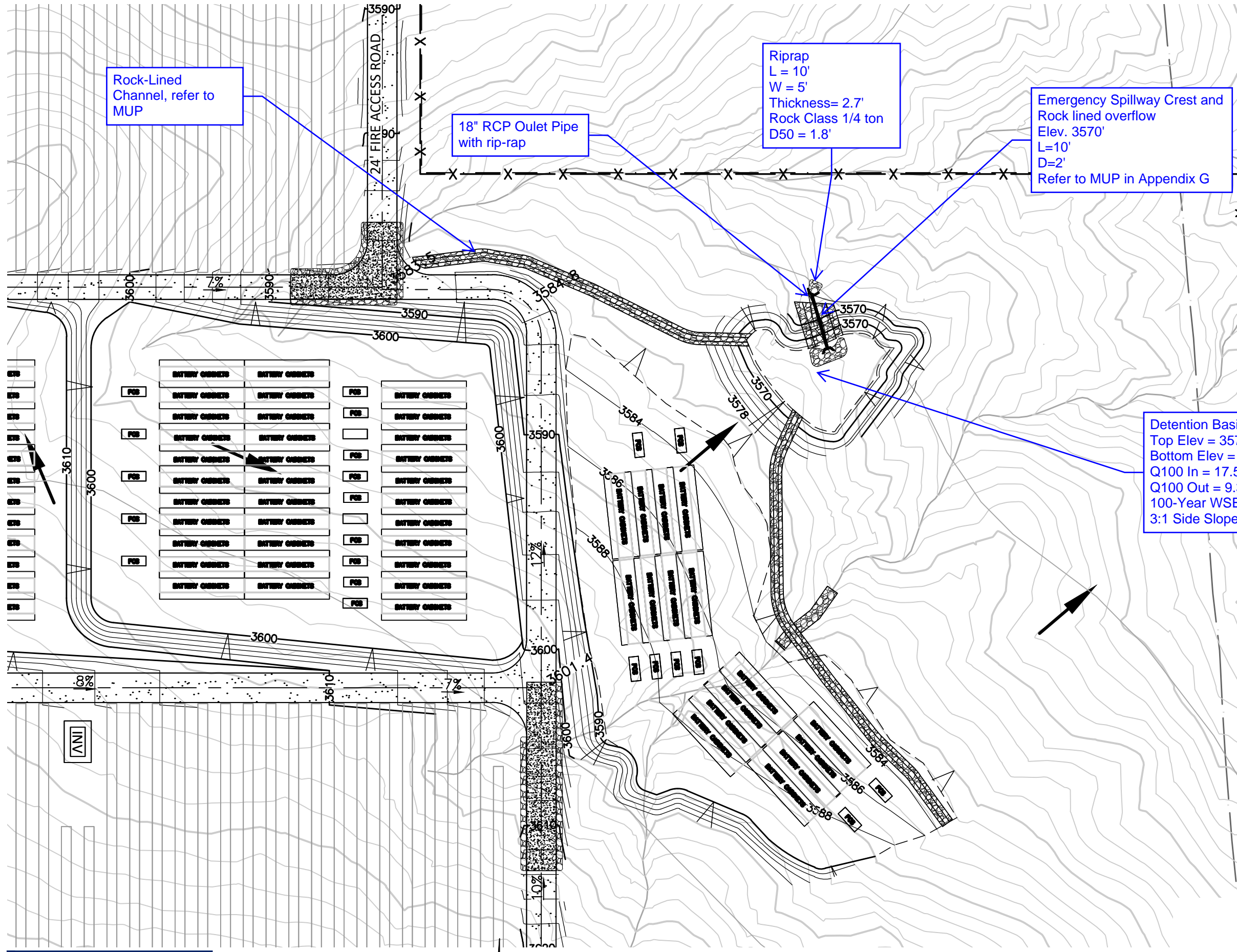
Exhibits
Hydraflow Hydrographs Input/Output



MBI 185614
March 2024

Node 128

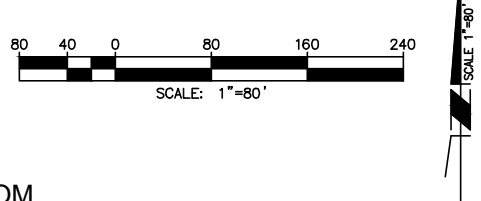
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Detention Basin
Top Elev = 3572'
Bottom Elev = 3568'
Q100 In = 17.5 cfs
Q100 Out = 9.3 cfs
100-Year WSE = 3569.91'
3:1 Side Slopes

Michael Baker

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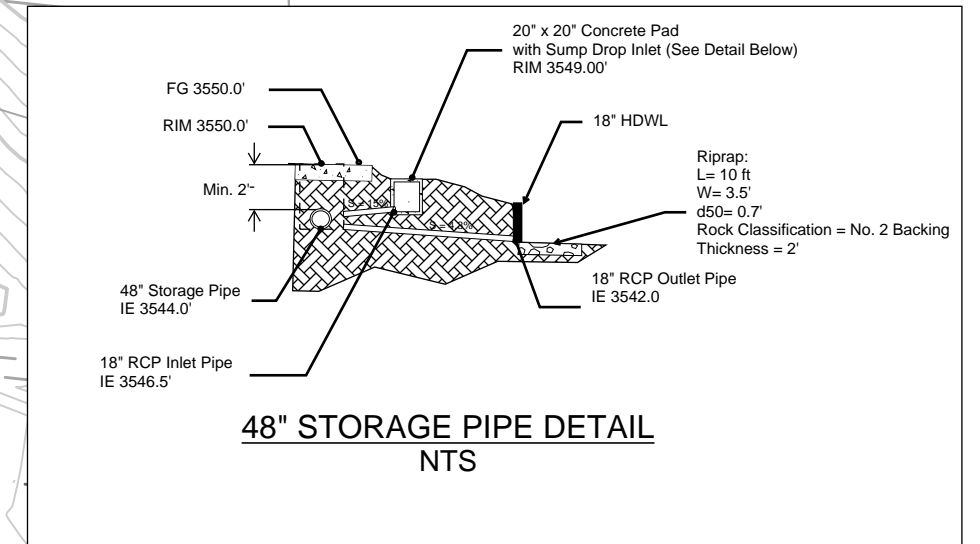
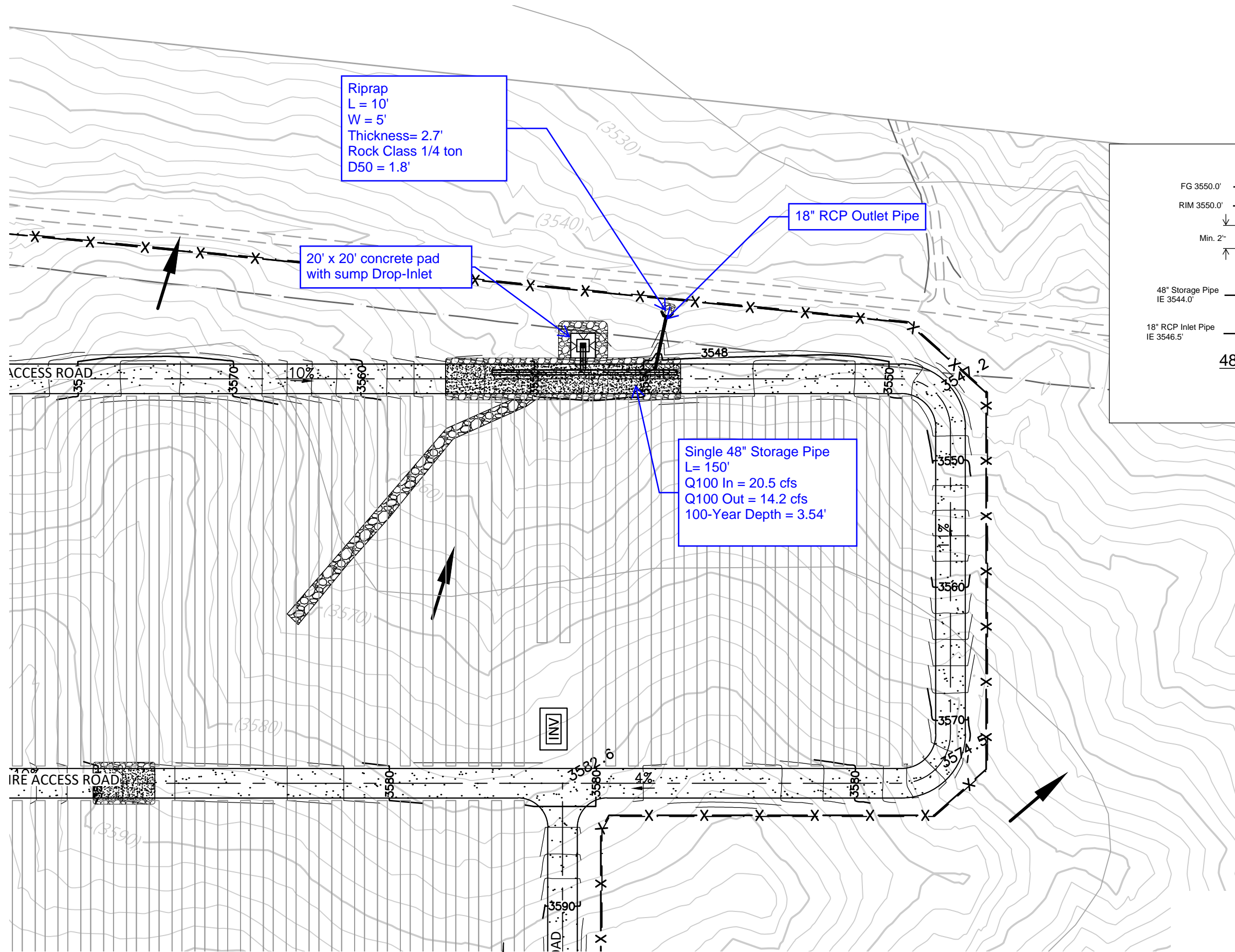


STARLIGHT SOLAR
PROPOSED DETENTION BASIN

MBI 185614
March 2024

Node 129

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STARLIGHT SOLAR
PROPOSED STORAGE PIPE

Michael Baker

INTERNATIONAL

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San Diego, CA 92124

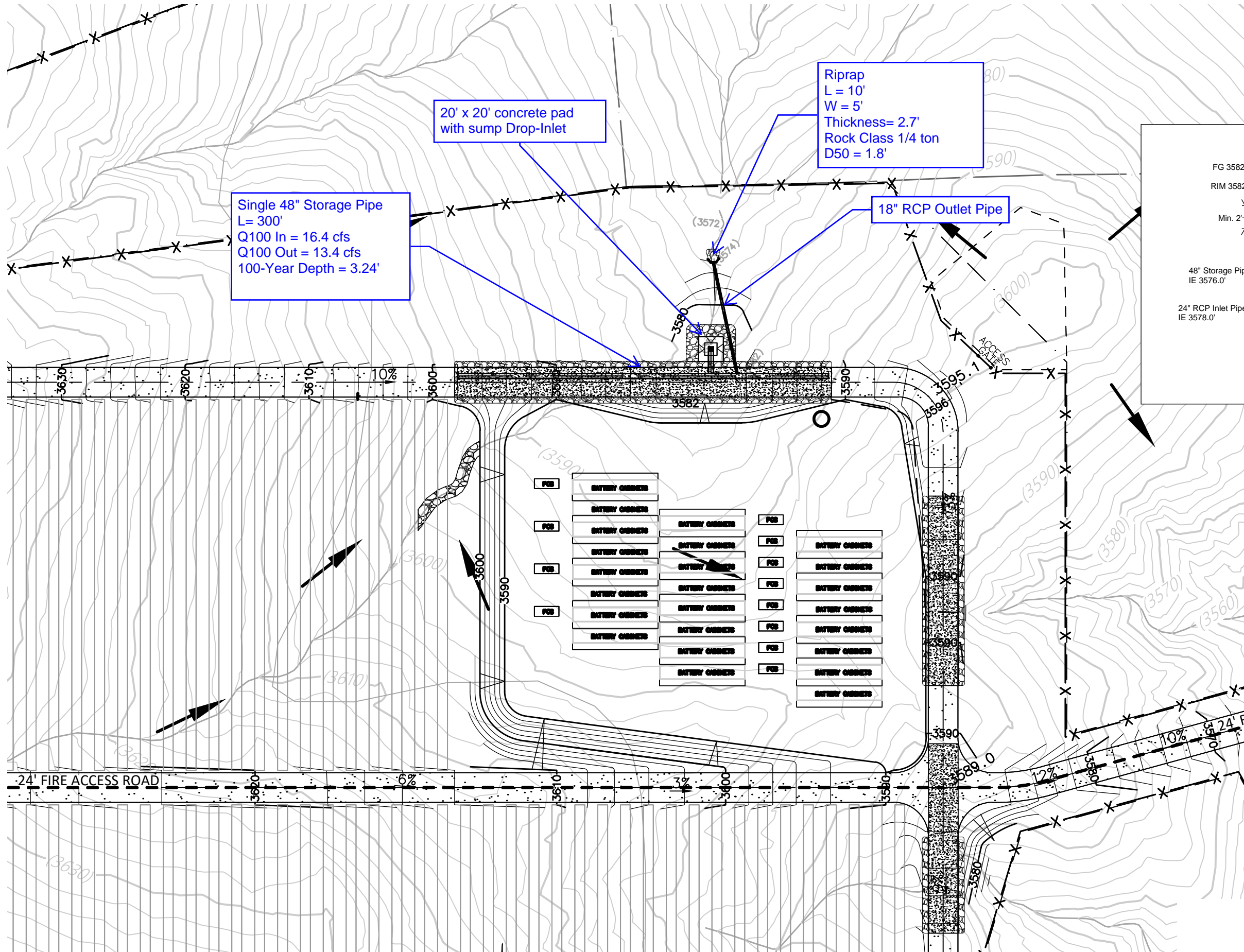
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MBI 185614

March 2024

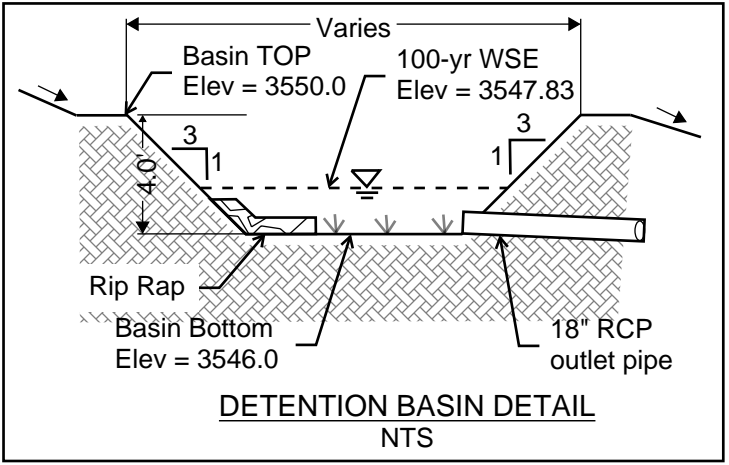
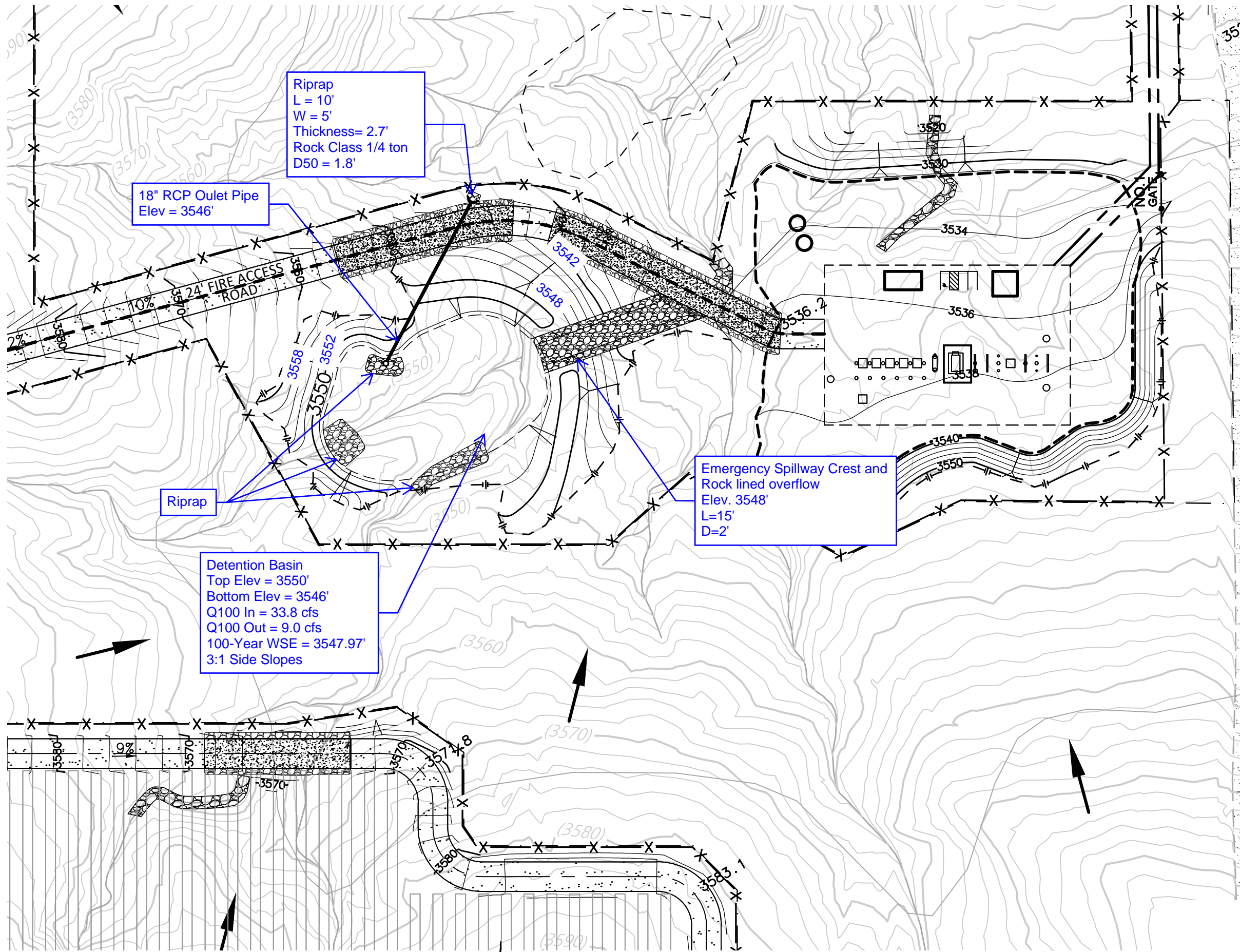
Node 156

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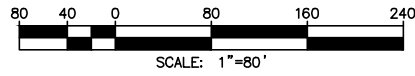
Node 165

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Michael Baker

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STARLIGHT SOLAR
PROPOSED DETENTION BASIN

MBI 185614
March 2024

RUN DATE 2/27/2024
HYDROGRAPH FILE NAME Text1
TIME OF CONCENTRATION 34 MIN.
6 HOUR RAINFALL 3 INCHES
BASIN AREA 73.4 ACRES
RUNOFF COEFFICIENT 0.23
PEAK DISCHARGE 38.86 CFS

Area A (NE)
Proposed Condition
Node 106

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 34	DISCHARGE (CFS) = 3
TIME (MIN) = 68	DISCHARGE (CFS) = 3.5
TIME (MIN) = 102	DISCHARGE (CFS) = 3.8
TIME (MIN) = 136	DISCHARGE (CFS) = 4.6
TIME (MIN) = 170	DISCHARGE (CFS) = 5.2
TIME (MIN) = 204	DISCHARGE (CFS) = 7.7
TIME (MIN) = 238	DISCHARGE (CFS) = 10.7
TIME (MIN) = 272	DISCHARGE (CFS) = 38.86
TIME (MIN) = 306	DISCHARGE (CFS) = 6.2
TIME (MIN) = 340	DISCHARGE (CFS) = 4.1
TIME (MIN) = 374	DISCHARGE (CFS) = 3.2
TIME (MIN) = 408	DISCHARGE (CFS) = 0

RUN DATE 2/27/2024
HYDROGRAPH FILE NAME Text1
TIME OF CONCENTRATION 21 MIN.
6 HOUR RAINFALL 3 INCHES
BASIN AREA 24.2 ACRES
RUNOFF COEFFICIENT 0.23
PEAK DISCHARGE 17.45 CFS

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 21	DISCHARGE (CFS) = 1
TIME (MIN) = 42	DISCHARGE (CFS) = 1.1
TIME (MIN) = 63	DISCHARGE (CFS) = 1.2
TIME (MIN) = 84	DISCHARGE (CFS) = 1.3
TIME (MIN) = 105	DISCHARGE (CFS) = 1.4
TIME (MIN) = 126	DISCHARGE (CFS) = 1.6
TIME (MIN) = 147	DISCHARGE (CFS) = 1.7
TIME (MIN) = 168	DISCHARGE (CFS) = 2.1
TIME (MIN) = 189	DISCHARGE (CFS) = 2.4
TIME (MIN) = 210	DISCHARGE (CFS) = 3.5
TIME (MIN) = 231	DISCHARGE (CFS) = 4.8
TIME (MIN) = 252	DISCHARGE (CFS) = 17.45
TIME (MIN) = 273	DISCHARGE (CFS) = 2.8
TIME (MIN) = 294	DISCHARGE (CFS) = 1.9
TIME (MIN) = 315	DISCHARGE (CFS) = 1.4
TIME (MIN) = 336	DISCHARGE (CFS) = 1.2
TIME (MIN) = 357	DISCHARGE (CFS) = 1.1
TIME (MIN) = 378	DISCHARGE (CFS) = 0

Area A (NE)
Proposed Condition
Node 128

RUN DATE 2/27/2024
HYDROGRAPH FILE NAME Text1
TIME OF CONCENTRATION 5 MIN.
6 HOUR RAINFALL 3 INCHES
BASIN AREA 11.32 ACRES
RUNOFF COEFFICIENT 0.23
PEAK DISCHARGE 20.5 CFS

Area A (NE)
Proposed Condition
Node 129

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 5	DISCHARGE (CFS) = 0.5
TIME (MIN) = 10	DISCHARGE (CFS) = 0.5
TIME (MIN) = 15	DISCHARGE (CFS) = 0.5
TIME (MIN) = 20	DISCHARGE (CFS) = 0.5
TIME (MIN) = 25	DISCHARGE (CFS) = 0.5
TIME (MIN) = 30	DISCHARGE (CFS) = 0.5
TIME (MIN) = 35	DISCHARGE (CFS) = 0.5
TIME (MIN) = 40	DISCHARGE (CFS) = 0.5
TIME (MIN) = 45	DISCHARGE (CFS) = 0.5
TIME (MIN) = 50	DISCHARGE (CFS) = 0.5
TIME (MIN) = 55	DISCHARGE (CFS) = 0.5
TIME (MIN) = 60	DISCHARGE (CFS) = 0.5
TIME (MIN) = 65	DISCHARGE (CFS) = 0.6
TIME (MIN) = 70	DISCHARGE (CFS) = 0.6
TIME (MIN) = 75	DISCHARGE (CFS) = 0.6
TIME (MIN) = 80	DISCHARGE (CFS) = 0.6
TIME (MIN) = 85	DISCHARGE (CFS) = 0.6
TIME (MIN) = 90	DISCHARGE (CFS) = 0.6
TIME (MIN) = 95	DISCHARGE (CFS) = 0.6
TIME (MIN) = 100	DISCHARGE (CFS) = 0.6
TIME (MIN) = 105	DISCHARGE (CFS) = 0.7
TIME (MIN) = 110	DISCHARGE (CFS) = 0.7
TIME (MIN) = 115	DISCHARGE (CFS) = 0.7
TIME (MIN) = 120	DISCHARGE (CFS) = 0.7
TIME (MIN) = 125	DISCHARGE (CFS) = 0.7
TIME (MIN) = 130	DISCHARGE (CFS) = 0.7
TIME (MIN) = 135	DISCHARGE (CFS) = 0.8
TIME (MIN) = 140	DISCHARGE (CFS) = 0.8
TIME (MIN) = 145	DISCHARGE (CFS) = 0.8
TIME (MIN) = 150	DISCHARGE (CFS) = 0.8
TIME (MIN) = 155	DISCHARGE (CFS) = 0.9
TIME (MIN) = 160	DISCHARGE (CFS) = 0.9
TIME (MIN) = 165	DISCHARGE (CFS) = 1
TIME (MIN) = 170	DISCHARGE (CFS) = 1
TIME (MIN) = 175	DISCHARGE (CFS) = 1
TIME (MIN) = 180	DISCHARGE (CFS) = 1.1
TIME (MIN) = 185	DISCHARGE (CFS) = 1.2
TIME (MIN) = 190	DISCHARGE (CFS) = 1.2
TIME (MIN) = 195	DISCHARGE (CFS) = 1.3
TIME (MIN) = 200	DISCHARGE (CFS) = 1.4
TIME (MIN) = 205	DISCHARGE (CFS) = 1.5
TIME (MIN) = 210	DISCHARGE (CFS) = 1.6
TIME (MIN) = 215	DISCHARGE (CFS) = 1.8
TIME (MIN) = 220	DISCHARGE (CFS) = 2
TIME (MIN) = 225	DISCHARGE (CFS) = 2.4
TIME (MIN) = 230	DISCHARGE (CFS) = 2.8
TIME (MIN) = 235	DISCHARGE (CFS) = 4.1
TIME (MIN) = 240	DISCHARGE (CFS) = 5.8
TIME (MIN) = 245	DISCHARGE (CFS) = 20.5
TIME (MIN) = 250	DISCHARGE (CFS) = 3.3
TIME (MIN) = 255	DISCHARGE (CFS) = 2.2
TIME (MIN) = 260	DISCHARGE (CFS) = 1.7
TIME (MIN) = 265	DISCHARGE (CFS) = 1.4
TIME (MIN) = 270	DISCHARGE (CFS) = 1.2
TIME (MIN) = 275	DISCHARGE (CFS) = 1.1
TIME (MIN) = 280	DISCHARGE (CFS) = 1
TIME (MIN) = 285	DISCHARGE (CFS) = 0.9
TIME (MIN) = 290	DISCHARGE (CFS) = 0.9
TIME (MIN) = 295	DISCHARGE (CFS) = 0.8
TIME (MIN) = 300	DISCHARGE (CFS) = 0.8
TIME (MIN) = 305	DISCHARGE (CFS) = 0.7
TIME (MIN) = 310	DISCHARGE (CFS) = 0.7
TIME (MIN) = 315	DISCHARGE (CFS) = 0.7
TIME (MIN) = 320	DISCHARGE (CFS) = 0.6
TIME (MIN) = 325	DISCHARGE (CFS) = 0.6
TIME (MIN) = 330	DISCHARGE (CFS) = 0.6
TIME (MIN) = 335	DISCHARGE (CFS) = 0.6
TIME (MIN) = 340	DISCHARGE (CFS) = 0.5
TIME (MIN) = 345	DISCHARGE (CFS) = 0.5
TIME (MIN) = 350	DISCHARGE (CFS) = 0.5
TIME (MIN) = 355	DISCHARGE (CFS) = 0.5
TIME (MIN) = 360	DISCHARGE (CFS) = 0.5
TIME (MIN) = 365	DISCHARGE (CFS) = 0

RUN DATE 2/27/2024
HYDROGRAPH FILE NAME Text1
TIME OF CONCENTRATION 18 MIN.
6 HOUR RAINFALL 3 INCHES
BASIN AREA 21 ACRES
RUNOFF COEFFICIENT 0.23
PEAK DISCHARGE 16.44 CFS

Area A (NE)
Proposed Condition
Node 156

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 18	DISCHARGE (CFS) = 0.9
TIME (MIN) = 36	DISCHARGE (CFS) = 0.9
TIME (MIN) = 54	DISCHARGE (CFS) = 1
TIME (MIN) = 72	DISCHARGE (CFS) = 1.1
TIME (MIN) = 90	DISCHARGE (CFS) = 1.1
TIME (MIN) = 108	DISCHARGE (CFS) = 1.2
TIME (MIN) = 126	DISCHARGE (CFS) = 1.3
TIME (MIN) = 144	DISCHARGE (CFS) = 1.5
TIME (MIN) = 162	DISCHARGE (CFS) = 1.6
TIME (MIN) = 180	DISCHARGE (CFS) = 2
TIME (MIN) = 198	DISCHARGE (CFS) = 2.3
TIME (MIN) = 216	DISCHARGE (CFS) = 3.3
TIME (MIN) = 234	DISCHARGE (CFS) = 4.9
TIME (MIN) = 252	DISCHARGE (CFS) = 16.44
TIME (MIN) = 270	DISCHARGE (CFS) = 2.7
TIME (MIN) = 288	DISCHARGE (CFS) = 1.8
TIME (MIN) = 306	DISCHARGE (CFS) = 1.4
TIME (MIN) = 324	DISCHARGE (CFS) = 1.2
TIME (MIN) = 342	DISCHARGE (CFS) = 1
TIME (MIN) = 360	DISCHARGE (CFS) = 0.9
TIME (MIN) = 378	DISCHARGE (CFS) = 0

RUN DATE 2/27/2024
HYDROGRAPH FILE NAME Text1
TIME OF CONCENTRATION 12 MIN.
6 HOUR RAINFALL 3 INCHES
BASIN AREA 33.4 ACRES
RUNOFF COEFFICIENT 0.23
PEAK DISCHARGE 33.8 CFS

Area A (NE)
Proposed Condition
Node 165

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 12	DISCHARGE (CFS) = 1.4
TIME (MIN) = 24	DISCHARGE (CFS) = 1.4
TIME (MIN) = 36	DISCHARGE (CFS) = 1.5
TIME (MIN) = 48	DISCHARGE (CFS) = 1.5
TIME (MIN) = 60	DISCHARGE (CFS) = 1.6
TIME (MIN) = 72	DISCHARGE (CFS) = 1.6
TIME (MIN) = 84	DISCHARGE (CFS) = 1.7
TIME (MIN) = 96	DISCHARGE (CFS) = 1.8
TIME (MIN) = 108	DISCHARGE (CFS) = 1.9
TIME (MIN) = 120	DISCHARGE (CFS) = 2
TIME (MIN) = 132	DISCHARGE (CFS) = 2.2
TIME (MIN) = 144	DISCHARGE (CFS) = 2.3
TIME (MIN) = 156	DISCHARGE (CFS) = 2.5
TIME (MIN) = 168	DISCHARGE (CFS) = 2.7
TIME (MIN) = 180	DISCHARGE (CFS) = 3.1
TIME (MIN) = 192	DISCHARGE (CFS) = 3.3
TIME (MIN) = 204	DISCHARGE (CFS) = 4.1
TIME (MIN) = 216	DISCHARGE (CFS) = 4.7
TIME (MIN) = 228	DISCHARGE (CFS) = 6.8
TIME (MIN) = 240	DISCHARGE (CFS) = 10.4
TIME (MIN) = 252	DISCHARGE (CFS) = 33.8
TIME (MIN) = 264	DISCHARGE (CFS) = 5.5
TIME (MIN) = 276	DISCHARGE (CFS) = 3.7
TIME (MIN) = 288	DISCHARGE (CFS) = 2.9
TIME (MIN) = 300	DISCHARGE (CFS) = 2.4
TIME (MIN) = 312	DISCHARGE (CFS) = 2.1
TIME (MIN) = 324	DISCHARGE (CFS) = 1.9
TIME (MIN) = 336	DISCHARGE (CFS) = 1.7
TIME (MIN) = 348	DISCHARGE (CFS) = 1.6
TIME (MIN) = 360	DISCHARGE (CFS) = 1.4
TIME (MIN) = 372	DISCHARGE (CFS) = 0

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

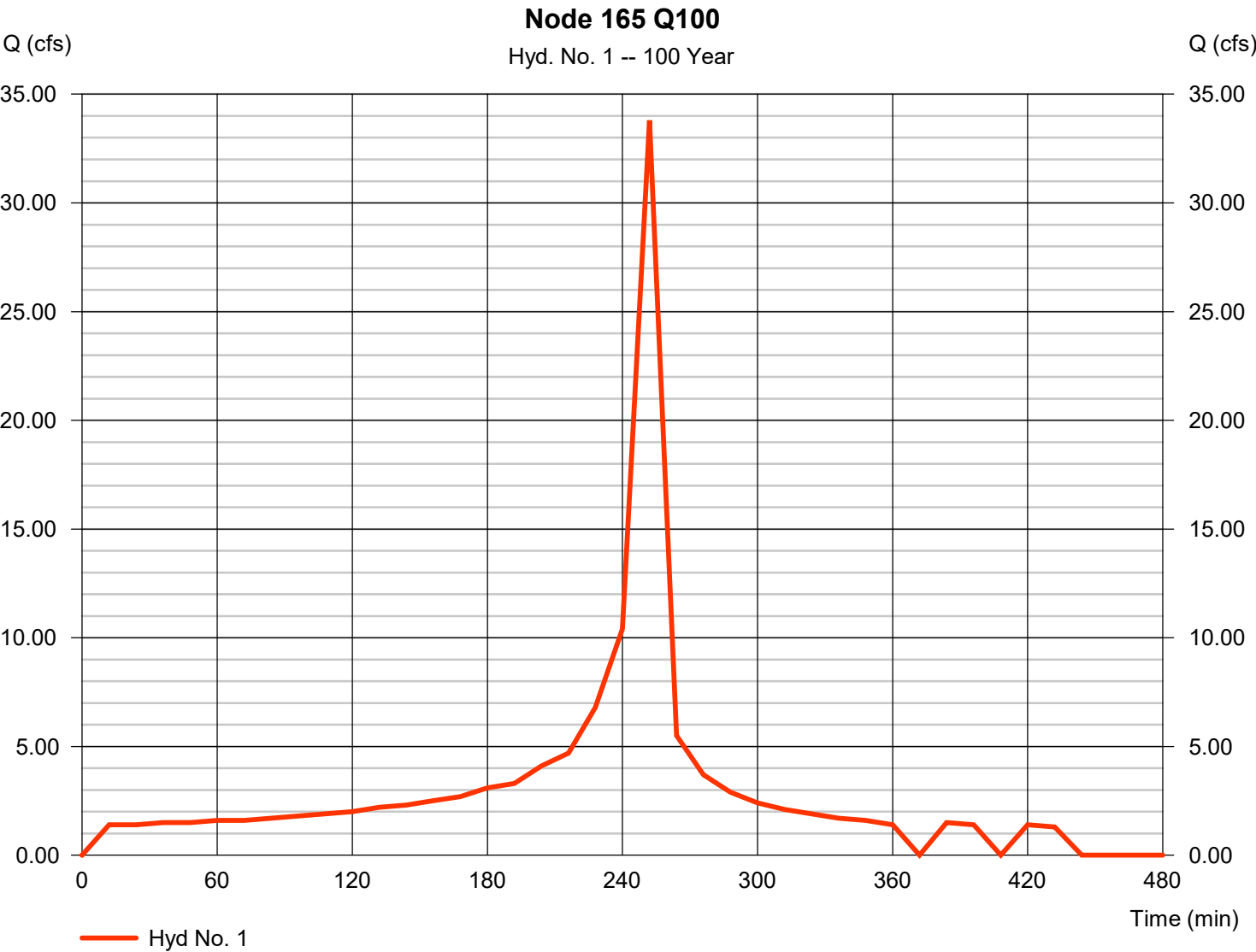
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Manual	33.80	12	252	87,192	-----	-----	-----	Node 165 Q100
2	Reservoir	8.985	12	264	87,160	1	101.97	39,117	Mitigated Q100
4	Manual	16.44	18	252	55,663	-----	-----	-----	Node 156 Q100
5	Reservoir	13.44	18	252	55,922	4	103.24	3,271	Mitigated Q100
7	Manual	17.45	21	252	63,063	-----	-----	-----	Node 128 Q100
8	Reservoir	9.346	21	273	63,050	7	101.91	15,236	Mitigated Q100
10	Manual	38.86	34	272	199,226	-----	-----	-----	Node 106 Q100
11	Reservoir	30.22	34	272	200,132	10	104.99	16,093	Mitigated Q100
13	Manual	20.50	5	245	28,200	-----	-----	-----	Node 129 Q100
14	Reservoir	14.21	5	245	28,199	13	103.54	1,762	Mitigated Q100

Hydrograph Report

Hyd. No. 1

Node 165 Q100

Hydrograph type	= Manual	Peak discharge	= 33.80 cfs
Storm frequency	= 100 yrs	Time to peak	= 252 min
Time interval	= 12 min	Hyd. volume	= 87,192 cuft



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

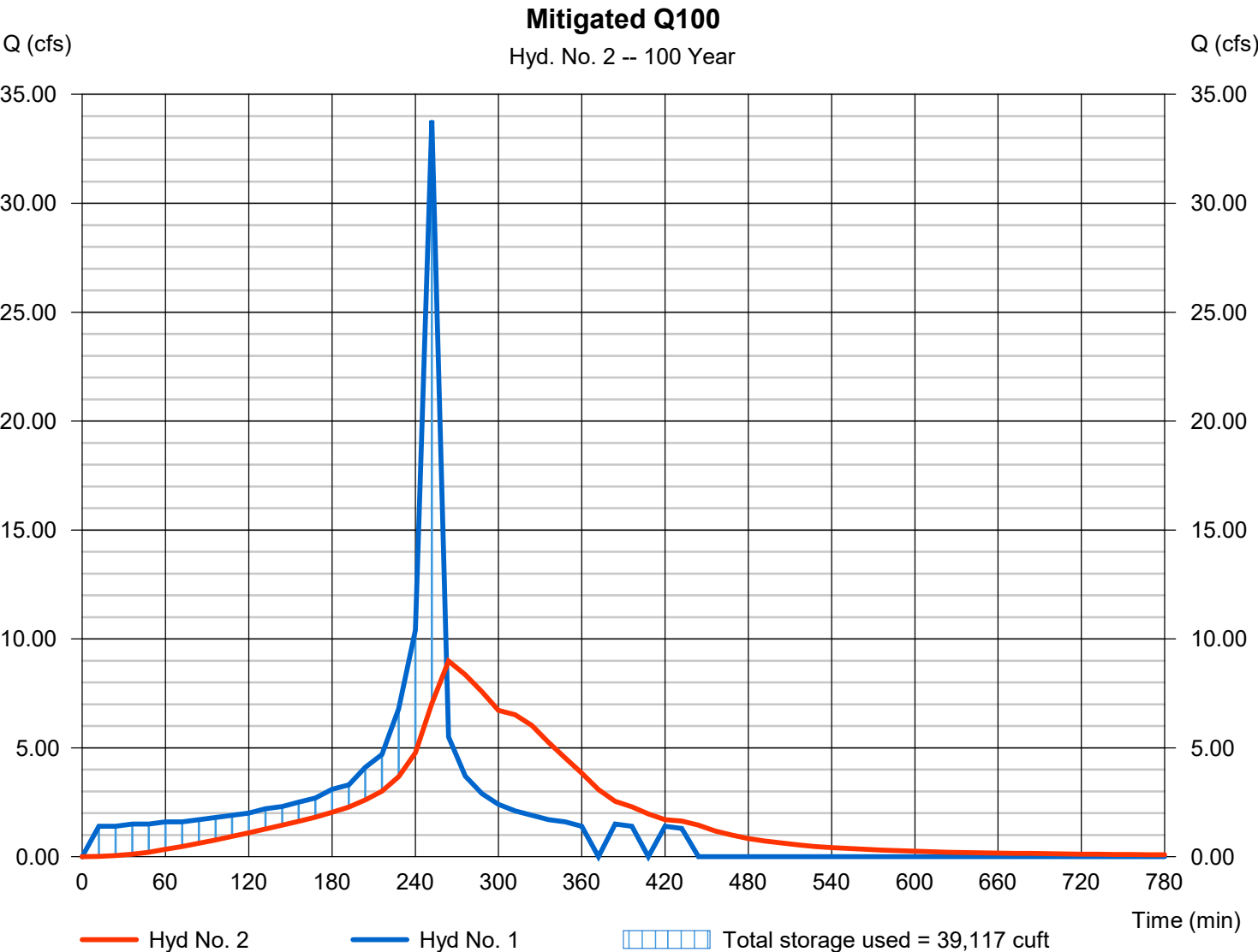
Saturday, 03 / 2 / 2024

Hyd. No. 2

Mitigated Q100

Hydrograph type	= Reservoir	Peak discharge	= 8.985 cfs
Storm frequency	= 100 yrs	Time to peak	= 264 min
Time interval	= 12 min	Hyd. volume	= 87,160 cuft
Inflow hyd. No.	= 1 - Node 165 Q100	Max. Elevation	= 101.97 ft
Reservoir name	= Node 165 Det. Basin	Max. Storage	= 39,117 cuft

Storage Indication method used.



Pond Report

4

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Pond No. 1 - Node 165 Det. Basin

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 100.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	15,000	0	0
1.00	101.00	20,000	17,438	17,438
2.00	102.00	25,000	22,451	39,890
3.00	103.00	50,000	36,781	76,671

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 18.00	0.00	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 100.00	0.00	0.00	0.00
Length (ft)	= 50.00	0.00	0.00	0.00
Slope (%)	= 1.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 100.00	0.00	0.00	0.00
Crest El. (ft)	= 102.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= Rect	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000 (by Contour)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	100.00	0.00	---	---	---	0.00	---	---	---	---	---	0.000
0.10	1,744	100.10	0.05 ic	---	---	---	0.00	---	---	---	---	---	0.055
0.20	3,488	100.20	0.21 ic	---	---	---	0.00	---	---	---	---	---	0.213
0.30	5,232	100.30	0.47 ic	---	---	---	0.00	---	---	---	---	---	0.471
0.40	6,975	100.40	0.81 ic	---	---	---	0.00	---	---	---	---	---	0.815
0.50	8,719	100.50	1.24 ic	---	---	---	0.00	---	---	---	---	---	1.243
0.60	10,463	100.60	1.74 ic	---	---	---	0.00	---	---	---	---	---	1.742
0.70	12,207	100.70	2.31 ic	---	---	---	0.00	---	---	---	---	---	2.306
0.80	13,951	100.80	2.92 ic	---	---	---	0.00	---	---	---	---	---	2.922
0.90	15,695	100.90	3.58 ic	---	---	---	0.00	---	---	---	---	---	3.580
1.00	17,438	101.00	4.26 ic	---	---	---	0.00	---	---	---	---	---	4.265
1.10	19,684	101.10	4.96 ic	---	---	---	0.00	---	---	---	---	---	4.964
1.20	21,929	101.20	5.65 ic	---	---	---	0.00	---	---	---	---	---	5.654
1.30	24,174	101.30	6.22 oc	---	---	---	0.00	---	---	---	---	---	6.224
1.40	26,419	101.40	6.51 oc	---	---	---	0.00	---	---	---	---	---	6.513
1.50	28,664	101.50	6.47 oc	---	---	---	0.00	---	---	---	---	---	6.470
1.60	30,909	101.60	7.08 oc	---	---	---	0.00	---	---	---	---	---	7.085
1.70	33,154	101.70	7.65 oc	---	---	---	0.00	---	---	---	---	---	7.652
1.80	35,399	101.80	8.18 oc	---	---	---	0.00	---	---	---	---	---	8.181
1.90	37,645	101.90	8.68 oc	---	---	---	0.00	---	---	---	---	---	8.677
2.00	39,890	102.00	9.15 oc	---	---	---	0.00	---	---	---	---	---	9.146
2.10	43,568	102.10	9.59 oc	---	---	---	10.53	---	---	---	---	---	20.12
2.20	47,246	102.20	10.02 oc	---	---	---	29.78	---	---	---	---	---	39.80
2.30	50,924	102.30	10.43 oc	---	---	---	54.72	---	---	---	---	---	65.14
2.40	54,602	102.40	10.82 oc	---	---	---	84.24	---	---	---	---	---	95.06
2.50	58,280	102.50	11.20 oc	---	---	---	117.73	---	---	---	---	---	128.93
2.60	61,959	102.60	11.57 oc	---	---	---	154.76	---	---	---	---	---	166.33
2.70	65,637	102.70	11.88 ic	---	---	---	195.02	---	---	---	---	---	206.90
2.80	69,315	102.80	12.18 ic	---	---	---	238.27	---	---	---	---	---	250.45
2.90	72,993	102.90	12.47 ic	---	---	---	284.31	---	---	---	---	---	296.79
3.00	76,671	103.00	12.76 ic	---	---	---	333.00	---	---	---	---	---	345.76

Hydrograph Report

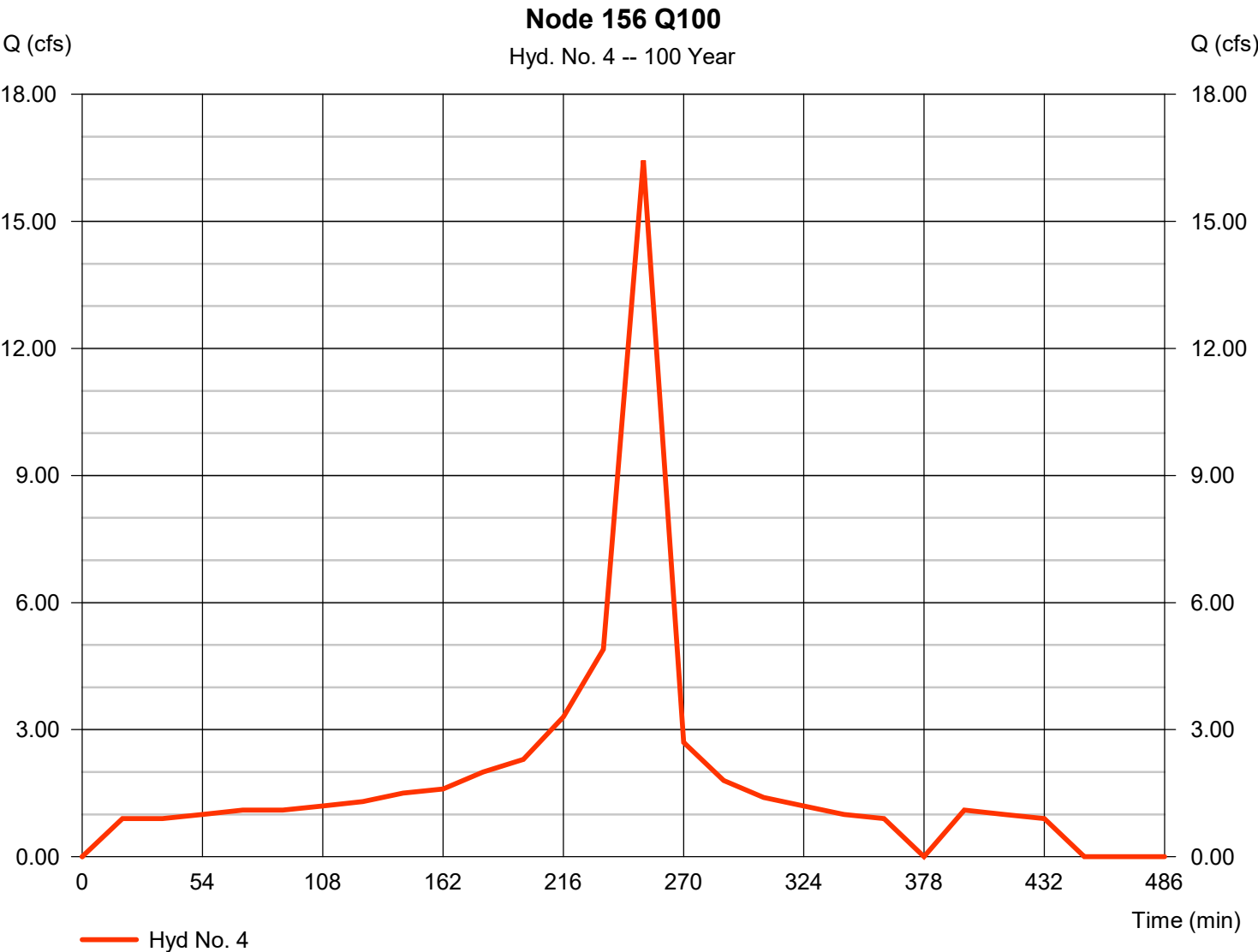
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Hyd. No. 4

Node 156 Q100

Hydrograph type	= Manual	Peak discharge	= 16.44 cfs
Storm frequency	= 100 yrs	Time to peak	= 252 min
Time interval	= 18 min	Hyd. volume	= 55,663 cuft



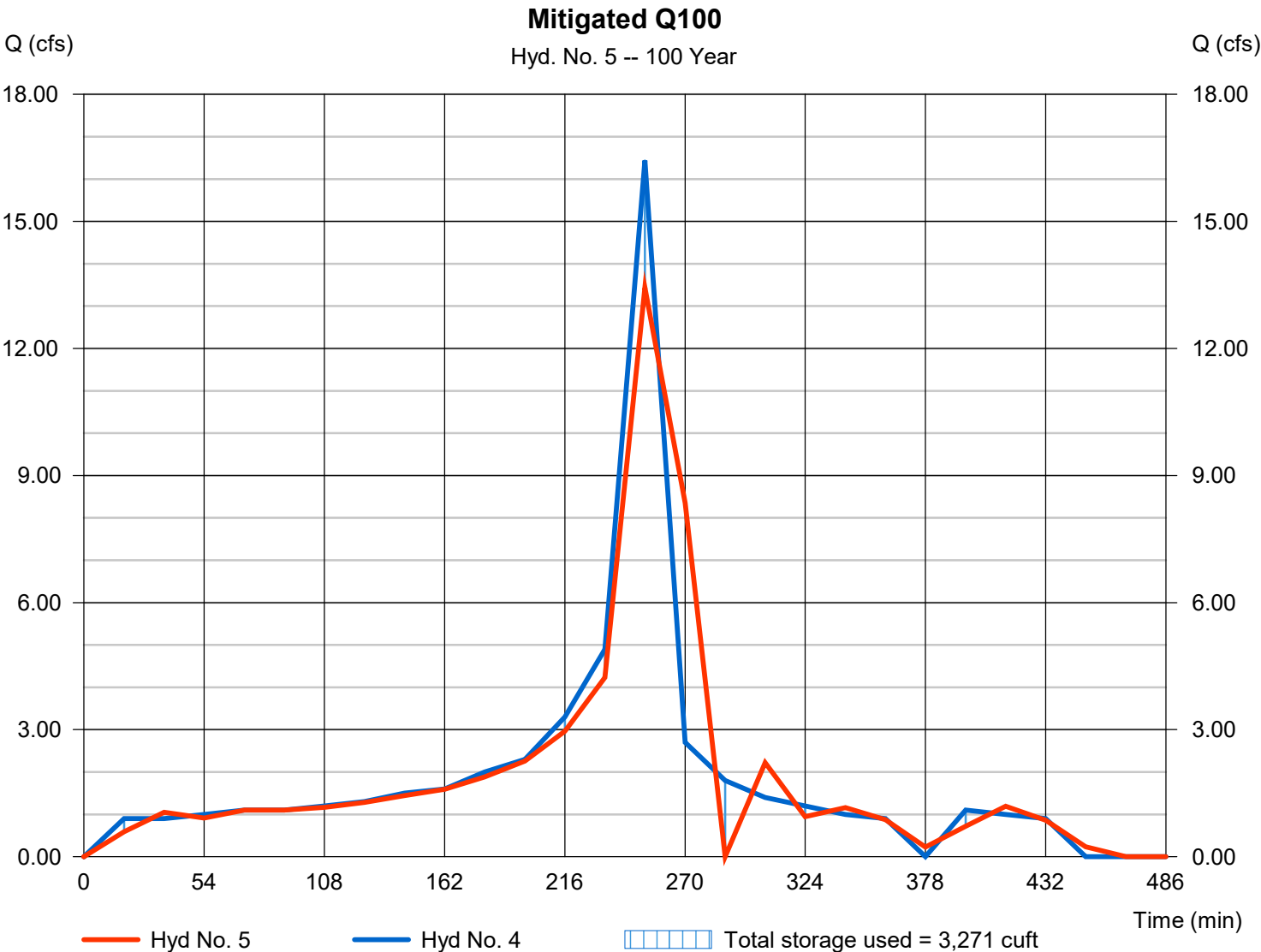
Hydrograph Report

Hyd. No. 5

Mitigated Q100

Hydrograph type	= Reservoir	Peak discharge	= 13.44 cfs
Storm frequency	= 100 yrs	Time to peak	= 252 min
Time interval	= 18 min	Hyd. volume	= 55,922 cuft
Inflow hyd. No.	= 4 - Node 156 Q100	Max. Elevation	= 103.24 ft
Reservoir name	= Node 156 Pipe Storage	Max. Storage	= 3,271 cuft

Storage Indication method used.



Pond Report

7

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Pond No. 3 - Node 156 Pipe Storage

Pond Data

UG Chambers -Invert elev. = 100.00 ft, Rise x Span = 4.00 x 4.00 ft, Barrel Len = 300.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	n/a	0	0
0.40	100.40	n/a	197	197
0.80	100.80	n/a	341	537
1.20	101.20	n/a	415	952
1.60	101.60	n/a	457	1,409
2.00	102.00	n/a	477	1,886
2.40	102.40	n/a	477	2,363
2.80	102.80	n/a	457	2,820
3.20	103.20	n/a	414	3,234
3.60	103.60	n/a	341	3,575
4.00	104.00	n/a	196	3,771

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 18.00	0.00	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 100.00	0.00	0.00	0.00
Length (ft)	= 15.00	0.00	0.00	0.00
Slope (%)	= 1.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 0.00	0.00	0.00	0.00
Crest El. (ft)	= 0.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= ---	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	100.00	0.00	---	---	---	---	---	---	---	---	---	0.000
0.04	20	100.04	0.01 ic	---	---	---	---	---	---	---	---	---	0.009
0.08	39	100.08	0.04 ic	---	---	---	---	---	---	---	---	---	0.035
0.12	59	100.12	0.08 ic	---	---	---	---	---	---	---	---	---	0.079
0.16	79	100.16	0.14 ic	---	---	---	---	---	---	---	---	---	0.138
0.20	98	100.20	0.21 ic	---	---	---	---	---	---	---	---	---	0.213
0.24	118	100.24	0.30 ic	---	---	---	---	---	---	---	---	---	0.304
0.28	138	100.28	0.41 ic	---	---	---	---	---	---	---	---	---	0.411
0.32	157	100.32	0.53 ic	---	---	---	---	---	---	---	---	---	0.533
0.36	177	100.36	0.67 ic	---	---	---	---	---	---	---	---	---	0.667
0.40	197	100.40	0.81 ic	---	---	---	---	---	---	---	---	---	0.815
0.44	231	100.44	0.96 oc	---	---	---	---	---	---	---	---	---	0.960
0.48	265	100.48	1.10 oc	---	---	---	---	---	---	---	---	---	1.095
0.52	299	100.52	1.23 oc	---	---	---	---	---	---	---	---	---	1.233
0.56	333	100.56	1.37 oc	---	---	---	---	---	---	---	---	---	1.373
0.60	367	100.60	1.52 oc	---	---	---	---	---	---	---	---	---	1.516
0.64	401	100.64	1.66 oc	---	---	---	---	---	---	---	---	---	1.663
0.68	435	100.68	1.81 oc	---	---	---	---	---	---	---	---	---	1.808
0.72	469	100.72	1.96 oc	---	---	---	---	---	---	---	---	---	1.955
0.76	503	100.76	2.10 oc	---	---	---	---	---	---	---	---	---	2.103
0.80	537	100.80	2.25 oc	---	---	---	---	---	---	---	---	---	2.250
0.84	579	100.84	2.40 oc	---	---	---	---	---	---	---	---	---	2.396
0.88	620	100.88	2.54 oc	---	---	---	---	---	---	---	---	---	2.540
0.92	662	100.92	2.69 oc	---	---	---	---	---	---	---	---	---	2.685
0.96	703	100.96	2.83 oc	---	---	---	---	---	---	---	---	---	2.827
1.00	745	101.00	2.97 oc	---	---	---	---	---	---	---	---	---	2.967
1.04	786	101.04	3.10 oc	---	---	---	---	---	---	---	---	---	3.102
1.08	827	101.08	3.24 oc	---	---	---	---	---	---	---	---	---	3.237
1.12	869	101.12	3.36 oc	---	---	---	---	---	---	---	---	---	3.364
1.16	910	101.16	3.49 oc	---	---	---	---	---	---	---	---	---	3.488
1.20	952	101.20	3.60 oc	---	---	---	---	---	---	---	---	---	3.604
1.24	998	101.24	3.72 oc	---	---	---	---	---	---	---	---	---	3.716

Continues on next page...

Node 156 Pipe Storage

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
1.28	1,043	101.28	3.82 oc	---	---	---	---	---	---	---	---	---	3.819
1.32	1,089	101.32	3.91 oc	---	---	---	---	---	---	---	---	---	3.913
1.36	1,135	101.36	4.00 oc	---	---	---	---	---	---	---	---	---	3.997
1.40	1,180	101.40	4.07 oc	---	---	---	---	---	---	---	---	---	4.067
1.44	1,226	101.44	4.12 oc	---	---	---	---	---	---	---	---	---	4.120
1.48	1,272	101.48	4.15 oc	---	---	---	---	---	---	---	---	---	4.146
1.52	1,317	101.52	4.39 oc	---	---	---	---	---	---	---	---	---	4.393
1.56	1,363	101.56	4.88 oc	---	---	---	---	---	---	---	---	---	4.883
1.60	1,409	101.60	5.33 oc	---	---	---	---	---	---	---	---	---	5.327
1.64	1,456	101.64	5.74 oc	---	---	---	---	---	---	---	---	---	5.738
1.68	1,504	101.68	6.12 oc	---	---	---	---	---	---	---	---	---	6.121
1.72	1,552	101.72	6.48 oc	---	---	---	---	---	---	---	---	---	6.481
1.76	1,599	101.76	6.82 oc	---	---	---	---	---	---	---	---	---	6.823
1.80	1,647	101.80	7.15 oc	---	---	---	---	---	---	---	---	---	7.148
1.84	1,695	101.84	7.46 oc	---	---	---	---	---	---	---	---	---	7.458
1.88	1,743	101.88	7.76 oc	---	---	---	---	---	---	---	---	---	7.757
1.92	1,790	101.92	8.04 oc	---	---	---	---	---	---	---	---	---	8.044
1.96	1,838	101.96	8.32 oc	---	---	---	---	---	---	---	---	---	8.322
2.00	1,886	102.00	8.59 oc	---	---	---	---	---	---	---	---	---	8.590
2.04	1,933	102.04	8.85 oc	---	---	---	---	---	---	---	---	---	8.851
2.08	1,981	102.08	9.10 oc	---	---	---	---	---	---	---	---	---	9.104
2.12	2,029	102.12	9.35 oc	---	---	---	---	---	---	---	---	---	9.350
2.16	2,077	102.16	9.59 oc	---	---	---	---	---	---	---	---	---	9.589
2.20	2,124	102.20	9.82 oc	---	---	---	---	---	---	---	---	---	9.823
2.24	2,172	102.24	10.05 oc	---	---	---	---	---	---	---	---	---	10.05
2.28	2,220	102.28	10.28 oc	---	---	---	---	---	---	---	---	---	10.28
2.32	2,267	102.32	10.49 oc	---	---	---	---	---	---	---	---	---	10.49
2.36	2,315	102.36	10.71 oc	---	---	---	---	---	---	---	---	---	10.71
2.40	2,363	102.40	10.92 oc	---	---	---	---	---	---	---	---	---	10.92
2.44	2,409	102.44	11.06 ic	---	---	---	---	---	---	---	---	---	11.06
2.48	2,454	102.48	11.19 ic	---	---	---	---	---	---	---	---	---	11.19
2.52	2,500	102.52	11.32 ic	---	---	---	---	---	---	---	---	---	11.32
2.56	2,546	102.56	11.45 ic	---	---	---	---	---	---	---	---	---	11.45
2.60	2,591	102.60	11.57 ic	---	---	---	---	---	---	---	---	---	11.57
2.64	2,637	102.64	11.70 ic	---	---	---	---	---	---	---	---	---	11.70
2.68	2,683	102.68	11.82 ic	---	---	---	---	---	---	---	---	---	11.82
2.72	2,728	102.72	11.94 ic	---	---	---	---	---	---	---	---	---	11.94
2.76	2,774	102.76	12.06 ic	---	---	---	---	---	---	---	---	---	12.06
2.80	2,820	102.80	12.18 ic	---	---	---	---	---	---	---	---	---	12.18
2.84	2,861	102.84	12.30 ic	---	---	---	---	---	---	---	---	---	12.30
2.88	2,902	102.88	12.42 ic	---	---	---	---	---	---	---	---	---	12.42
2.92	2,944	102.92	12.53 ic	---	---	---	---	---	---	---	---	---	12.53
2.96	2,985	102.96	12.65 ic	---	---	---	---	---	---	---	---	---	12.65
3.00	3,027	103.00	12.76 ic	---	---	---	---	---	---	---	---	---	12.76
3.04	3,068	103.04	12.87 ic	---	---	---	---	---	---	---	---	---	12.87
3.08	3,110	103.08	12.99 ic	---	---	---	---	---	---	---	---	---	12.99
3.12	3,151	103.12	13.10 ic	---	---	---	---	---	---	---	---	---	13.10
3.16	3,193	103.16	13.21 ic	---	---	---	---	---	---	---	---	---	13.21
3.20	3,234	103.20	13.32 ic	---	---	---	---	---	---	---	---	---	13.32
3.24	3,268	103.24	13.42 ic	---	---	---	---	---	---	---	---	---	13.42
3.28	3,302	103.28	13.53 ic	---	---	---	---	---	---	---	---	---	13.53
3.32	3,336	103.32	13.64 ic	---	---	---	---	---	---	---	---	---	13.64
3.36	3,370	103.36	13.74 ic	---	---	---	---	---	---	---	---	---	13.74
3.40	3,404	103.40	13.85 ic	---	---	---	---	---	---	---	---	---	13.85
3.44	3,438	103.44	13.95 ic	---	---	---	---	---	---	---	---	---	13.95
3.48	3,472	103.48	14.06 ic	---	---	---	---	---	---	---	---	---	14.06
3.52	3,507	103.52	14.16 ic	---	---	---	---	---	---	---	---	---	14.16
3.56	3,541	103.56	14.26 ic	---	---	---	---	---	---	---	---	---	14.26
3.60	3,575	103.60	14.36 ic	---	---	---	---	---	---	---	---	---	14.36
3.64	3,594	103.64	14.46 ic	---	---	---	---	---	---	---	---	---	14.46
3.68	3,614	103.68	14.56 ic	---	---	---	---	---	---	---	---	---	14.56
3.72	3,633	103.72	14.66 ic	---	---	---	---	---	---	---	---	---	14.66
3.76	3,653	103.76	14.76 ic	---	---	---	---	---	---	---	---	---	14.76
3.80	3,673	103.80	14.86 ic	---	---	---	---	---	---	---	---	---	14.86
3.84	3,692	103.84	14.96 ic	---	---	---	---	---	---	---	---	---	14.96
3.88	3,712	103.88	15.05 ic	---	---	---	---	---	---	---	---	---	15.05
3.92	3,731	103.92	15.15 ic	---	---	---	---	---	---	---	---	---	15.15
3.96	3,751	103.96	15.24 ic	---	---	---	---	---	---	---	---	---	15.24
4.00	3,771	104.00	15.34 ic	---	---	---	---	---	---	---	---	---	15.34

...End

Hydrograph Report

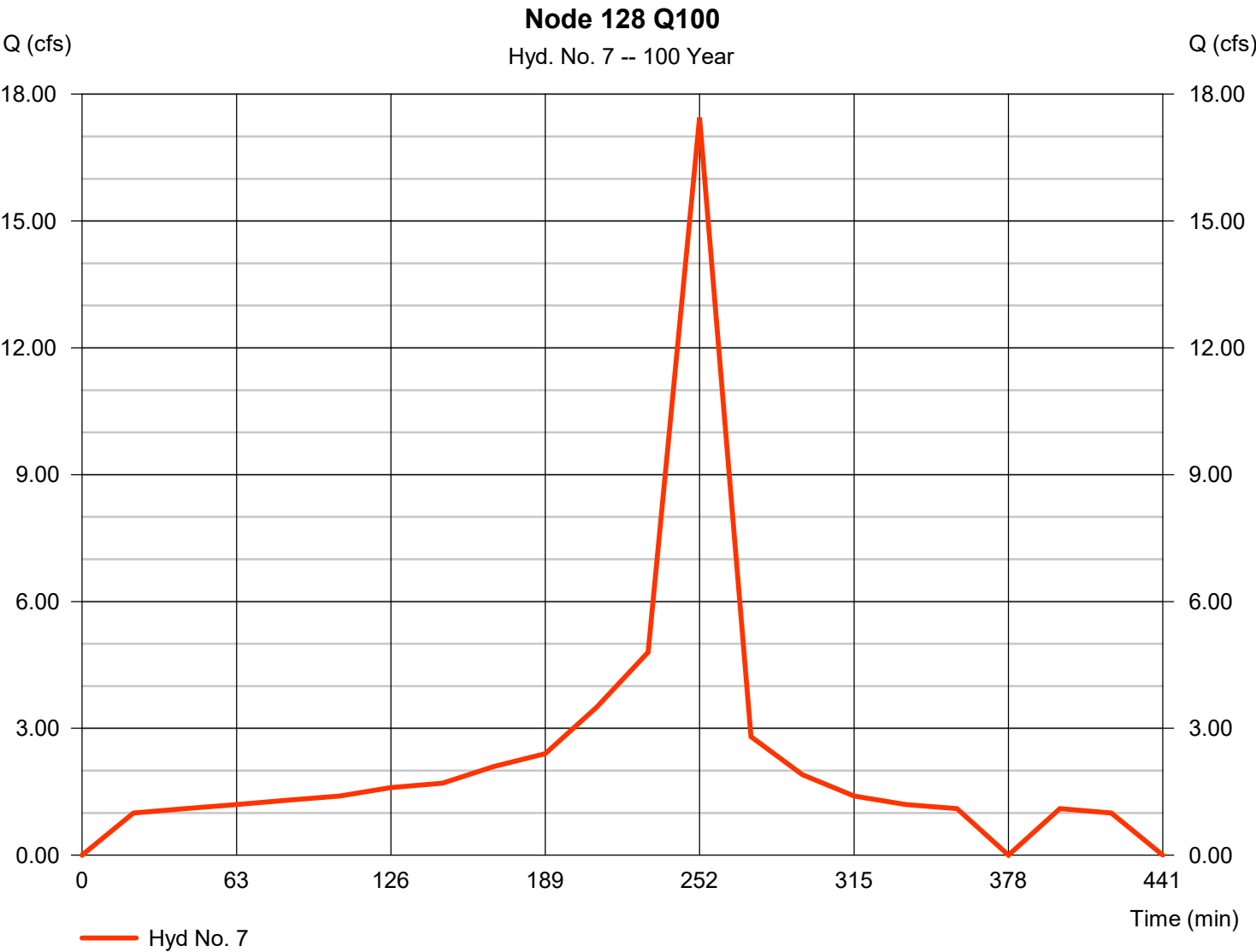
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Hyd. No. 7

Node 128 Q100

Hydrograph type	= Manual	Peak discharge	= 17.45 cfs
Storm frequency	= 100 yrs	Time to peak	= 252 min
Time interval	= 21 min	Hyd. volume	= 63,063 cuft



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

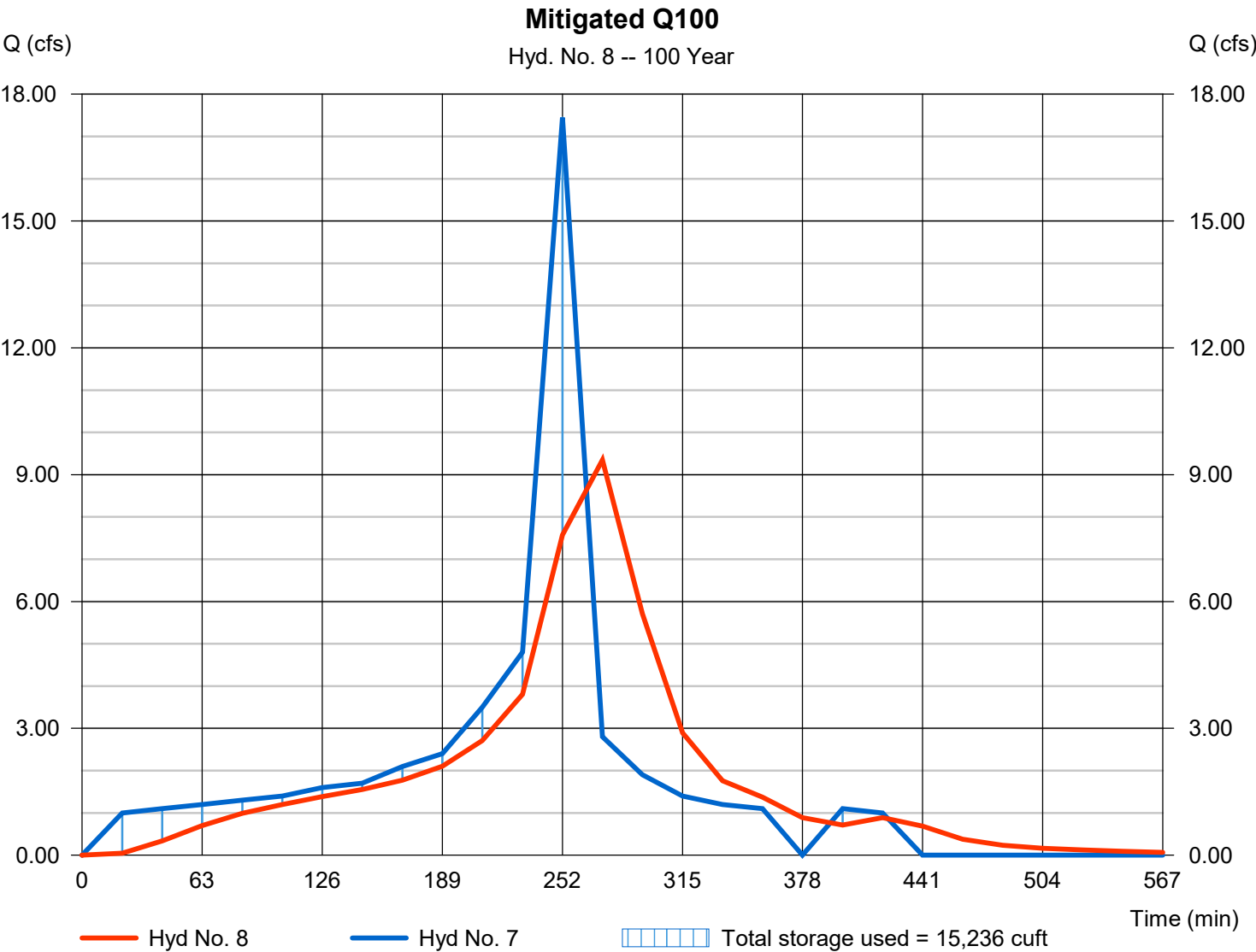
Saturday, 03 / 2 / 2024

Hyd. No. 8

Mitigated Q100

Hydrograph type	= Reservoir	Peak discharge	= 9.346 cfs
Storm frequency	= 100 yrs	Time to peak	= 273 min
Time interval	= 21 min	Hyd. volume	= 63,050 cuft
Inflow hyd. No.	= 7 - Node 128 Q100	Max. Elevation	= 101.91 ft
Reservoir name	= Node 128 Det. Basin	Max. Storage	= 15,236 cuft

Storage Indication method used.



Pond Report

11

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Pond No. 5 - Node 128 Det. Basin

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 100.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	5,542	0	0
1.00	101.00	8,028	6,746	6,746
2.00	102.00	10,662	9,313	16,059
3.00	103.00	12,987	11,804	27,863
4.00	104.00	50,000	29,487	57,350

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 18.00	0.00	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 100.00	0.00	0.00	0.00
Length (ft)	= 50.00	0.00	0.00	0.00
Slope (%)	= 1.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 50.00	0.00	0.00	0.00
Crest El. (ft)	= 101.90	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= Rect	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	100.00	0.00	---	---	---	0.00	---	---	---	---	---	0.000
0.10	675	100.10	0.05 ic	---	---	---	0.00	---	---	---	---	---	0.055
0.20	1,349	100.20	0.21 ic	---	---	---	0.00	---	---	---	---	---	0.213
0.30	2,024	100.30	0.47 ic	---	---	---	0.00	---	---	---	---	---	0.471
0.40	2,698	100.40	0.81 ic	---	---	---	0.00	---	---	---	---	---	0.815
0.50	3,373	100.50	1.24 ic	---	---	---	0.00	---	---	---	---	---	1.243
0.60	4,048	100.60	1.74 ic	---	---	---	0.00	---	---	---	---	---	1.742
0.70	4,722	100.70	2.31 ic	---	---	---	0.00	---	---	---	---	---	2.306
0.80	5,397	100.80	2.92 ic	---	---	---	0.00	---	---	---	---	---	2.922
0.90	6,071	100.90	3.58 ic	---	---	---	0.00	---	---	---	---	---	3.580
1.00	6,746	101.00	4.26 ic	---	---	---	0.00	---	---	---	---	---	4.265
1.10	7,677	101.10	4.96 ic	---	---	---	0.00	---	---	---	---	---	4.964
1.20	8,609	101.20	5.65 ic	---	---	---	0.00	---	---	---	---	---	5.654
1.30	9,540	101.30	6.22 oc	---	---	---	0.00	---	---	---	---	---	6.224
1.40	10,471	101.40	6.51 oc	---	---	---	0.00	---	---	---	---	---	6.513
1.50	11,403	101.50	6.47 oc	---	---	---	0.00	---	---	---	---	---	6.470
1.60	12,334	101.60	7.08 oc	---	---	---	0.00	---	---	---	---	---	7.085
1.70	13,265	101.70	7.65 oc	---	---	---	0.00	---	---	---	---	---	7.652
1.80	14,196	101.80	8.18 oc	---	---	---	0.00	---	---	---	---	---	8.181
1.90	15,128	101.90	8.68 oc	---	---	---	0.00	---	---	---	---	---	8.677
2.00	16,059	102.00	9.15 oc	---	---	---	5.27	---	---	---	---	---	14.41
2.10	17,239	102.10	9.59 oc	---	---	---	14.89	---	---	---	---	---	24.48
2.20	18,420	102.20	10.02 oc	---	---	---	27.36	---	---	---	---	---	37.38
2.30	19,600	102.30	10.43 oc	---	---	---	42.12	---	---	---	---	---	52.55
2.40	20,781	102.40	10.82 oc	---	---	---	58.87	---	---	---	---	---	69.69
2.50	21,961	102.50	11.20 oc	---	---	---	77.38	---	---	---	---	---	88.58
2.60	23,142	102.60	11.57 oc	---	---	---	97.51	---	---	---	---	---	109.08
2.70	24,322	102.70	11.88 ic	---	---	---	119.14	---	---	---	---	---	131.02
2.80	25,502	102.80	12.18 ic	---	---	---	142.16	---	---	---	---	---	154.34
2.90	26,683	102.90	12.47 ic	---	---	---	166.50	---	---	---	---	---	178.97
3.00	27,863	103.00	12.76 ic	---	---	---	192.09	---	---	---	---	---	204.85
3.10	30,812	103.10	13.04 ic	---	---	---	218.87	---	---	---	---	---	231.91
3.20	33,761	103.20	13.32 ic	---	---	---	246.79	---	---	---	---	---	260.11
3.30	36,709	103.30	13.59 ic	---	---	---	275.81	---	---	---	---	---	289.39
3.40	39,658	103.40	13.85 ic	---	---	---	305.88	---	---	---	---	---	319.73
3.50	42,607	103.50	14.11 ic	---	---	---	336.97	---	---	---	---	---	351.08
3.60	45,555	103.60	14.36 ic	---	---	---	369.05	---	---	---	---	---	383.41
3.70	48,504	103.70	14.61 ic	---	---	---	402.09	---	---	---	---	---	416.70

Continues on next page...

Node 128 Det. Basin

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
3.80	51,453	103.80	14.86 ic	---	---	---	436.05	---	---	---	---	---	450.91
3.90	54,401	103.90	15.10 ic	---	---	---	470.93	---	---	---	---	---	486.03
4.00	57,350	104.00	15.34 ic	---	---	---	506.69	---	---	---	---	---	522.03

...End

Hydrograph Report

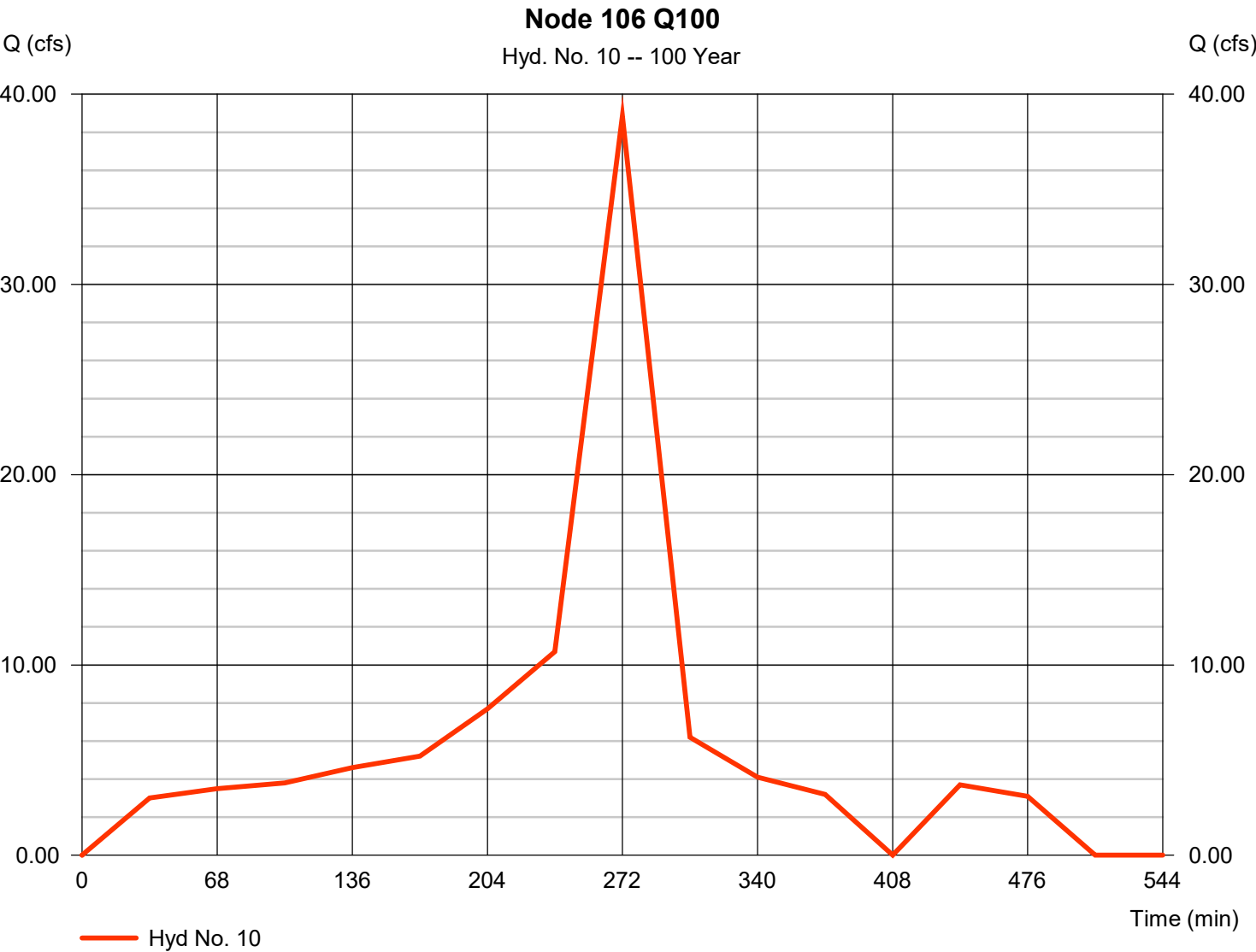
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Hyd. No. 10

Node 106 Q100

Hydrograph type	= Manual	Peak discharge	= 38.86 cfs
Storm frequency	= 100 yrs	Time to peak	= 272 min
Time interval	= 34 min	Hyd. volume	= 199,226 cuft



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

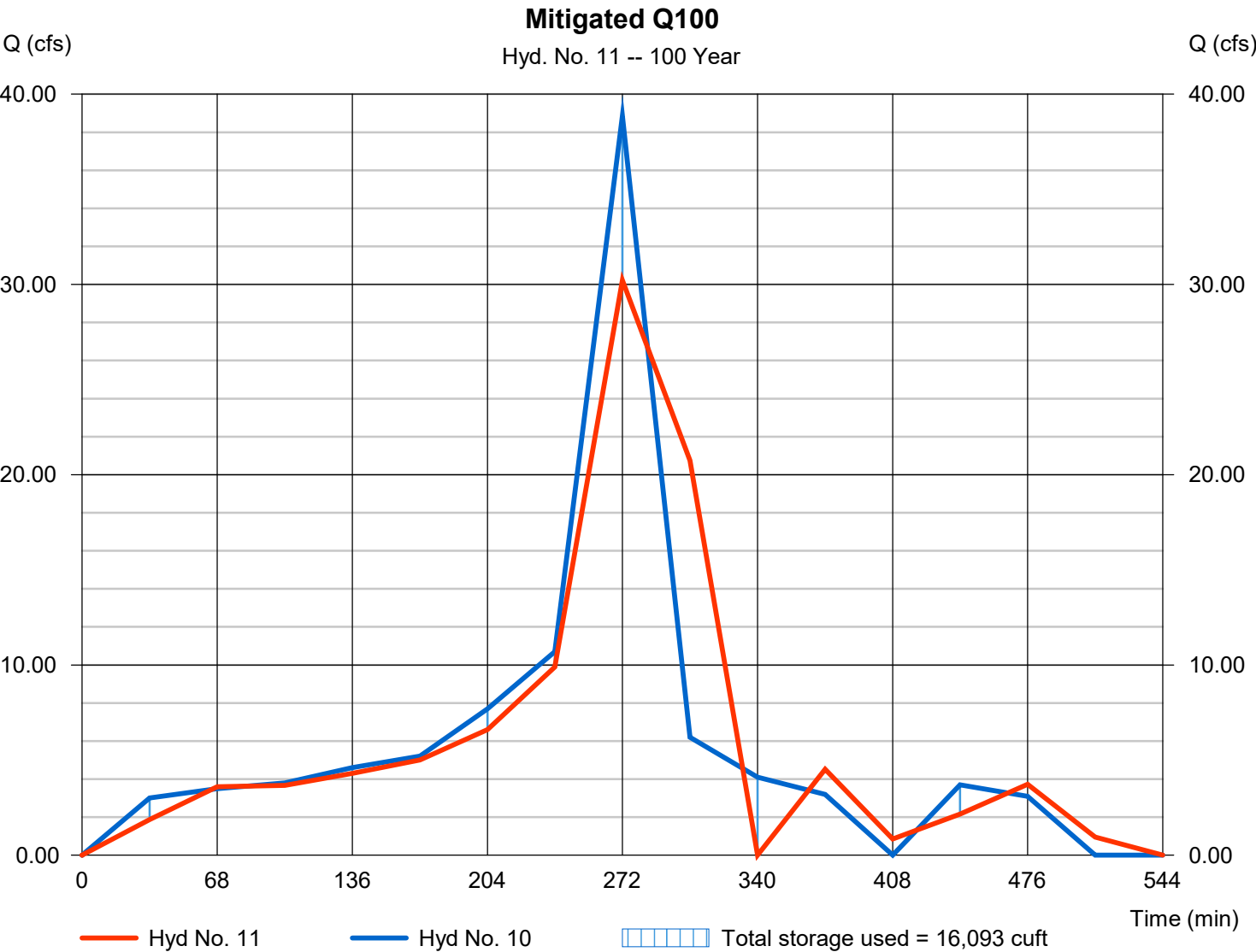
Saturday, 03 / 2 / 2024

Hyd. No. 11

Mitigated Q100

Hydrograph type	= Reservoir	Peak discharge	= 30.22 cfs
Storm frequency	= 100 yrs	Time to peak	= 272 min
Time interval	= 34 min	Hyd. volume	= 200,132 cuft
Inflow hyd. No.	= 10 - Node 106 Q100	Max. Elevation	= 104.99 ft
Reservoir name	= Node 106 Pipe Storage	Max. Storage	= 16,093 cuft

Storage Indication method used.



Pond Report

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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Pond No. 7 - Node 106 Pipe Storage

Pond Data

UG Chambers -Invert elev. = 100.00 ft, Rise x Span = 5.00 x 5.00 ft, Barrel Len = 410.00 ft, No. Barrels = 2, Slope = 0.00%, Headers = No

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	n/a	0	0
0.50	100.50	n/a	838	838
1.00	101.00	n/a	1,456	2,294
1.50	101.50	n/a	1,771	4,065
2.00	102.00	n/a	1,951	6,016
2.50	102.50	n/a	2,038	8,054
3.00	103.00	n/a	2,038	10,092
3.50	103.50	n/a	1,950	12,042
4.00	104.00	n/a	1,770	13,812
4.50	104.50	n/a	1,455	15,267
5.00	105.00	n/a	837	16,104

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 24.00	0.00	0.00	0.00
Span (in)	= 24.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 100.00	0.00	0.00	0.00
Length (ft)	= 15.00	0.00	0.00	0.00
Slope (%)	= 1.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 0.00	0.00	0.00	0.00
Crest El. (ft)	= 0.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= ---	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	100.00	0.00	---	---	---	---	---	---	---	---	---	0.000
0.05	84	100.05	0.02 ic	---	---	---	---	---	---	---	---	---	0.016
0.10	168	100.10	0.06 ic	---	---	---	---	---	---	---	---	---	0.064
0.15	251	100.15	0.14 ic	---	---	---	---	---	---	---	---	---	0.142
0.20	335	100.20	0.25 ic	---	---	---	---	---	---	---	---	---	0.250
0.25	419	100.25	0.39 ic	---	---	---	---	---	---	---	---	---	0.388
0.30	503	100.30	0.55 ic	---	---	---	---	---	---	---	---	---	0.553
0.35	587	100.35	0.75 ic	---	---	---	---	---	---	---	---	---	0.745
0.40	670	100.40	0.97 ic	---	---	---	---	---	---	---	---	---	0.966
0.45	754	100.45	1.19 oc	---	---	---	---	---	---	---	---	---	1.189
0.50	838	100.50	1.40 oc	---	---	---	---	---	---	---	---	---	1.396
0.55	984	100.55	1.61 oc	---	---	---	---	---	---	---	---	---	1.611
0.60	1,129	100.60	1.84 oc	---	---	---	---	---	---	---	---	---	1.839
0.65	1,275	100.65	2.07 oc	---	---	---	---	---	---	---	---	---	2.066
0.70	1,421	100.70	2.30 oc	---	---	---	---	---	---	---	---	---	2.303
0.75	1,566	100.75	2.54 oc	---	---	---	---	---	---	---	---	---	2.540
0.80	1,712	100.80	2.78 oc	---	---	---	---	---	---	---	---	---	2.777
0.85	1,857	100.85	3.03 oc	---	---	---	---	---	---	---	---	---	3.026
0.90	2,003	100.90	3.27 oc	---	---	---	---	---	---	---	---	---	3.272
0.95	2,149	100.95	3.52 oc	---	---	---	---	---	---	---	---	---	3.520
1.00	2,294	101.00	3.77 oc	---	---	---	---	---	---	---	---	---	3.769
1.05	2,471	101.05	4.01 oc	---	---	---	---	---	---	---	---	---	4.011
1.10	2,648	101.10	4.26 oc	---	---	---	---	---	---	---	---	---	4.258
1.15	2,826	101.15	4.50 oc	---	---	---	---	---	---	---	---	---	4.504
1.20	3,003	101.20	4.75 oc	---	---	---	---	---	---	---	---	---	4.753
1.25	3,180	101.25	4.99 oc	---	---	---	---	---	---	---	---	---	4.989
1.30	3,357	101.30	5.23 oc	---	---	---	---	---	---	---	---	---	5.226
1.35	3,534	101.35	5.46 oc	---	---	---	---	---	---	---	---	---	5.462
1.40	3,711	101.40	5.69 oc	---	---	---	---	---	---	---	---	---	5.688
1.45	3,888	101.45	5.92 oc	---	---	---	---	---	---	---	---	---	5.916
1.50	4,065	101.50	6.13 oc	---	---	---	---	---	---	---	---	---	6.130
1.55	4,260	101.55	6.34 oc	---	---	---	---	---	---	---	---	---	6.336

Continues on next page...

Node 106 Pipe Storage

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
1.60	4,455	101.60	6.54 oc	---	---	---	---	---	---	---	---	---	6.536
1.65	4,650	101.65	6.73 oc	---	---	---	---	---	---	---	---	---	6.726
1.70	4,845	101.70	6.90 oc	---	---	---	---	---	---	---	---	---	6.903
1.75	5,041	101.75	7.07 oc	---	---	---	---	---	---	---	---	---	7.066
1.80	5,236	101.80	7.22 oc	---	---	---	---	---	---	---	---	---	7.216
1.85	5,431	101.85	7.34 oc	---	---	---	---	---	---	---	---	---	7.344
1.90	5,626	101.90	7.45 oc	---	---	---	---	---	---	---	---	---	7.450
1.95	5,821	101.95	7.52 oc	---	---	---	---	---	---	---	---	---	7.524
2.00	6,016	102.00	7.52 oc	---	---	---	---	---	---	---	---	---	7.522
2.05	6,220	102.05	8.69 oc	---	---	---	---	---	---	---	---	---	8.685
2.10	6,423	102.10	9.71 oc	---	---	---	---	---	---	---	---	---	9.710
2.15	6,627	102.15	10.64 oc	---	---	---	---	---	---	---	---	---	10.64
2.20	6,831	102.20	11.49 oc	---	---	---	---	---	---	---	---	---	11.49
2.25	7,035	102.25	12.28 oc	---	---	---	---	---	---	---	---	---	12.28
2.30	7,239	102.30	13.03 oc	---	---	---	---	---	---	---	---	---	13.03
2.35	7,442	102.35	13.73 oc	---	---	---	---	---	---	---	---	---	13.73
2.40	7,646	102.40	14.40 oc	---	---	---	---	---	---	---	---	---	14.40
2.45	7,850	102.45	15.04 oc	---	---	---	---	---	---	---	---	---	15.04
2.50	8,054	102.50	15.66 oc	---	---	---	---	---	---	---	---	---	15.66
2.55	8,258	102.55	16.25 oc	---	---	---	---	---	---	---	---	---	16.25
2.60	8,461	102.60	16.82 oc	---	---	---	---	---	---	---	---	---	16.82
2.65	8,665	102.65	17.37 oc	---	---	---	---	---	---	---	---	---	17.37
2.70	8,869	102.70	17.90 oc	---	---	---	---	---	---	---	---	---	17.90
2.75	9,073	102.75	18.42 oc	---	---	---	---	---	---	---	---	---	18.42
2.80	9,277	102.80	18.93 oc	---	---	---	---	---	---	---	---	---	18.93
2.85	9,480	102.85	19.42 oc	---	---	---	---	---	---	---	---	---	19.42
2.90	9,684	102.90	19.90 oc	---	---	---	---	---	---	---	---	---	19.90
2.95	9,888	102.95	20.37 oc	---	---	---	---	---	---	---	---	---	20.37
3.00	10,092	103.00	20.83 oc	---	---	---	---	---	---	---	---	---	20.83
3.05	10,287	103.05	21.27 oc	---	---	---	---	---	---	---	---	---	21.27
3.10	10,482	103.10	21.71 oc	---	---	---	---	---	---	---	---	---	21.71
3.15	10,677	103.15	22.14 oc	---	---	---	---	---	---	---	---	---	22.14
3.20	10,872	103.20	22.43 ic	---	---	---	---	---	---	---	---	---	22.43
3.25	11,067	103.25	22.69 ic	---	---	---	---	---	---	---	---	---	22.69
3.30	11,262	103.30	22.94 ic	---	---	---	---	---	---	---	---	---	22.94
3.35	11,457	103.35	23.19 ic	---	---	---	---	---	---	---	---	---	23.19
3.40	11,652	103.40	23.43 ic	---	---	---	---	---	---	---	---	---	23.43
3.45	11,847	103.45	23.67 ic	---	---	---	---	---	---	---	---	---	23.67
3.50	12,042	103.50	23.91 ic	---	---	---	---	---	---	---	---	---	23.91
3.55	12,219	103.55	24.15 ic	---	---	---	---	---	---	---	---	---	24.15
3.60	12,396	103.60	24.39 ic	---	---	---	---	---	---	---	---	---	24.39
3.65	12,573	103.65	24.62 ic	---	---	---	---	---	---	---	---	---	24.62
3.70	12,750	103.70	24.85 ic	---	---	---	---	---	---	---	---	---	24.85
3.75	12,927	103.75	25.08 ic	---	---	---	---	---	---	---	---	---	25.08
3.80	13,104	103.80	25.31 ic	---	---	---	---	---	---	---	---	---	25.31
3.85	13,281	103.85	25.53 ic	---	---	---	---	---	---	---	---	---	25.53
3.90	13,458	103.90	25.76 ic	---	---	---	---	---	---	---	---	---	25.76
3.95	13,635	103.95	25.98 ic	---	---	---	---	---	---	---	---	---	25.98
4.00	13,812	104.00	26.20 ic	---	---	---	---	---	---	---	---	---	26.20
4.05	13,957	104.05	26.41 ic	---	---	---	---	---	---	---	---	---	26.41
4.10	14,103	104.10	26.63 ic	---	---	---	---	---	---	---	---	---	26.63
4.15	14,248	104.15	26.84 ic	---	---	---	---	---	---	---	---	---	26.84
4.20	14,394	104.20	27.06 ic	---	---	---	---	---	---	---	---	---	27.06
4.25	14,539	104.25	27.27 ic	---	---	---	---	---	---	---	---	---	27.27
4.30	14,685	104.30	27.48 ic	---	---	---	---	---	---	---	---	---	27.48
4.35	14,830	104.35	27.68 ic	---	---	---	---	---	---	---	---	---	27.68
4.40	14,976	104.40	27.89 ic	---	---	---	---	---	---	---	---	---	27.89
4.45	15,121	104.45	28.09 ic	---	---	---	---	---	---	---	---	---	28.09
4.50	15,267	104.50	28.30 ic	---	---	---	---	---	---	---	---	---	28.30
4.55	15,351	104.55	28.50 ic	---	---	---	---	---	---	---	---	---	28.50
4.60	15,434	104.60	28.70 ic	---	---	---	---	---	---	---	---	---	28.70
4.65	15,518	104.65	28.90 ic	---	---	---	---	---	---	---	---	---	28.90
4.70	15,602	104.70	29.09 ic	---	---	---	---	---	---	---	---	---	29.09
4.75	15,685	104.75	29.29 ic	---	---	---	---	---	---	---	---	---	29.29
4.80	15,769	104.80	29.48 ic	---	---	---	---	---	---	---	---	---	29.48
4.85	15,853	104.85	29.68 ic	---	---	---	---	---	---	---	---	---	29.68
4.90	15,936	104.90	29.87 ic	---	---	---	---	---	---	---	---	---	29.87
4.95	16,020	104.95	30.06 ic	---	---	---	---	---	---	---	---	---	30.06
5.00	16,104	105.00	30.25 ic	---	---	---	---	---	---	---	---	---	30.25

...End

Hydrograph Report

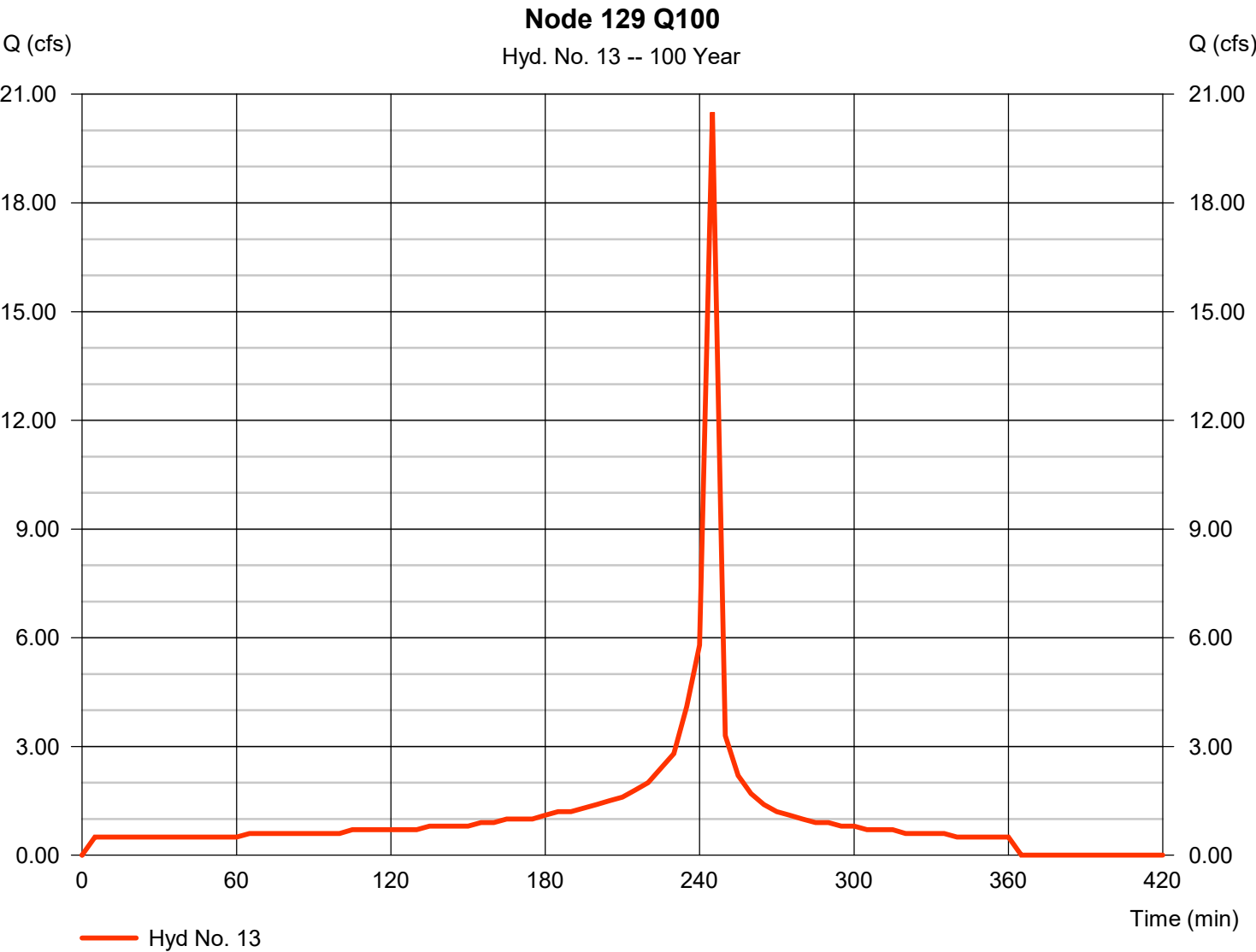
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

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Hyd. No. 13

Node 129 Q100

Hydrograph type	= Manual	Peak discharge	= 20.50 cfs
Storm frequency	= 100 yrs	Time to peak	= 245 min
Time interval	= 5 min	Hyd. volume	= 28,200 cuft



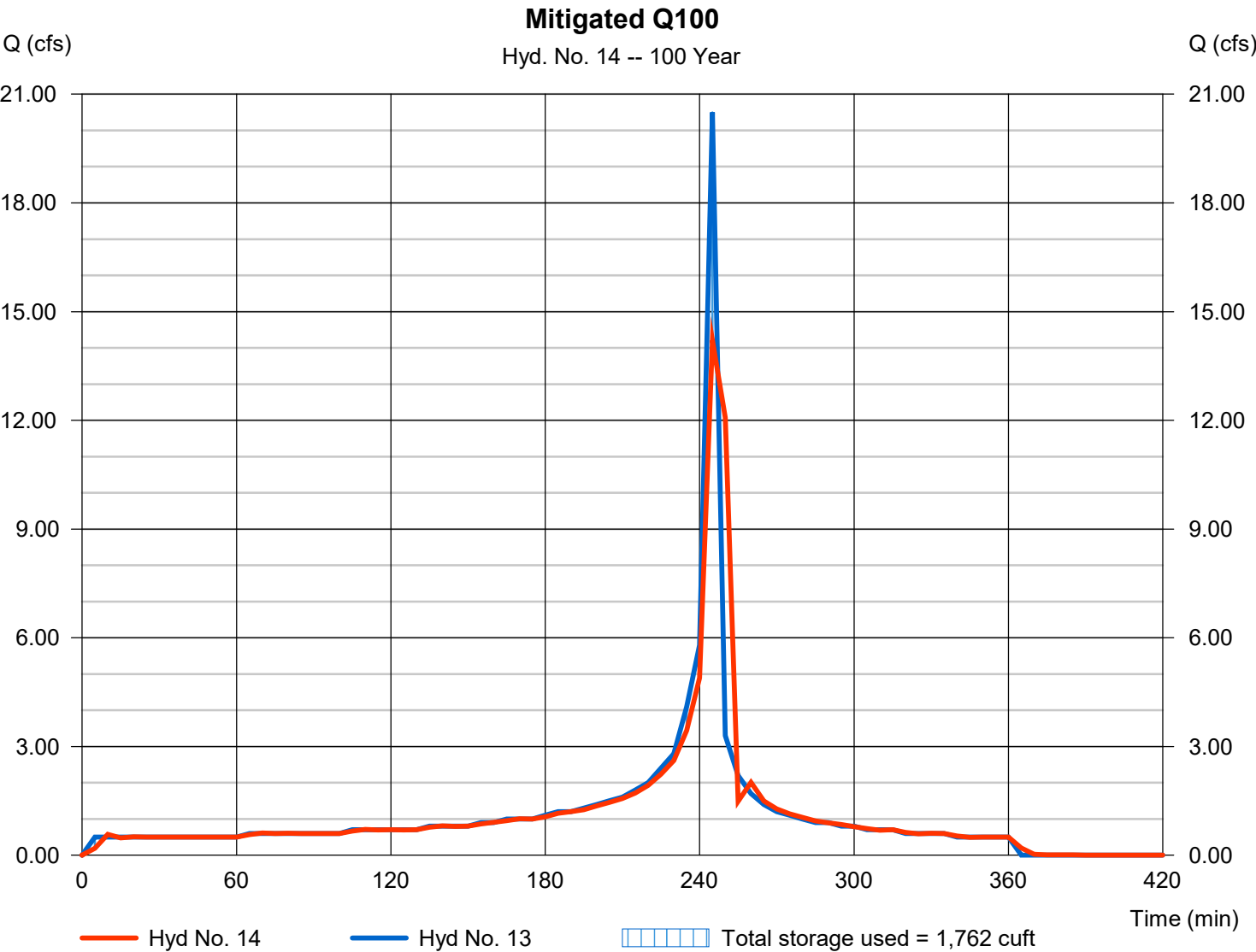
Hydrograph Report

Hyd. No. 14

Mitigated Q100

Hydrograph type	= Reservoir	Peak discharge	= 14.21 cfs
Storm frequency	= 100 yrs	Time to peak	= 245 min
Time interval	= 5 min	Hyd. volume	= 28,199 cuft
Inflow hyd. No.	= 13 - Node 129 Q100	Max. Elevation	= 103.54 ft
Reservoir name	= Node 129 Pipe Storage	Max. Storage	= 1,762 cuft

Storage Indication method used.



Pond Report

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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Saturday, 03 / 2 / 2024

Pond No. 9 - Node 129 Pipe Storage

Pond Data

UG Chambers -Invert elev. = 100.00 ft, Rise x Span = 4.00 x 4.00 ft, Barrel Len = 150.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	n/a	0	0
0.40	100.40	n/a	98	98
0.80	100.80	n/a	170	269
1.20	101.20	n/a	207	476
1.60	101.60	n/a	228	704
2.00	102.00	n/a	239	943
2.40	102.40	n/a	239	1,181
2.80	102.80	n/a	228	1,410
3.20	103.20	n/a	207	1,617
3.60	103.60	n/a	170	1,787
4.00	104.00	n/a	98	1,885

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 18.00	0.00	0.00	0.00
Span (in)	= 18.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 100.00	0.00	0.00	0.00
Length (ft)	= 15.00	0.00	0.00	0.00
Slope (%)	= 1.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 0.00	0.00	0.00	0.00
Crest El. (ft)	= 0.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= ---	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	100.00	0.00	---	---	---	---	---	---	---	---	---	0.000
0.04	10	100.04	0.01 ic	---	---	---	---	---	---	---	---	---	0.009
0.08	20	100.08	0.04 ic	---	---	---	---	---	---	---	---	---	0.035
0.12	30	100.12	0.08 ic	---	---	---	---	---	---	---	---	---	0.079
0.16	39	100.16	0.14 ic	---	---	---	---	---	---	---	---	---	0.138
0.20	49	100.20	0.21 ic	---	---	---	---	---	---	---	---	---	0.213
0.24	59	100.24	0.30 ic	---	---	---	---	---	---	---	---	---	0.304
0.28	69	100.28	0.41 ic	---	---	---	---	---	---	---	---	---	0.411
0.32	79	100.32	0.53 ic	---	---	---	---	---	---	---	---	---	0.533
0.36	89	100.36	0.67 ic	---	---	---	---	---	---	---	---	---	0.667
0.40	98	100.40	0.81 ic	---	---	---	---	---	---	---	---	---	0.815
0.44	115	100.44	0.96 oc	---	---	---	---	---	---	---	---	---	0.960
0.48	132	100.48	1.10 oc	---	---	---	---	---	---	---	---	---	1.095
0.52	149	100.52	1.23 oc	---	---	---	---	---	---	---	---	---	1.233
0.56	166	100.56	1.37 oc	---	---	---	---	---	---	---	---	---	1.373
0.60	183	100.60	1.52 oc	---	---	---	---	---	---	---	---	---	1.516
0.64	200	100.64	1.66 oc	---	---	---	---	---	---	---	---	---	1.663
0.68	218	100.68	1.81 oc	---	---	---	---	---	---	---	---	---	1.808
0.72	235	100.72	1.96 oc	---	---	---	---	---	---	---	---	---	1.955
0.76	252	100.76	2.10 oc	---	---	---	---	---	---	---	---	---	2.103
0.80	269	100.80	2.25 oc	---	---	---	---	---	---	---	---	---	2.250
0.84	289	100.84	2.40 oc	---	---	---	---	---	---	---	---	---	2.396
0.88	310	100.88	2.54 oc	---	---	---	---	---	---	---	---	---	2.540
0.92	331	100.92	2.69 oc	---	---	---	---	---	---	---	---	---	2.685
0.96	352	100.96	2.83 oc	---	---	---	---	---	---	---	---	---	2.827
1.00	372	101.00	2.97 oc	---	---	---	---	---	---	---	---	---	2.967
1.04	393	101.04	3.10 oc	---	---	---	---	---	---	---	---	---	3.102
1.08	414	101.08	3.24 oc	---	---	---	---	---	---	---	---	---	3.237
1.12	434	101.12	3.36 oc	---	---	---	---	---	---	---	---	---	3.364
1.16	455	101.16	3.49 oc	---	---	---	---	---	---	---	---	---	3.488
1.20	476	101.20	3.60 oc	---	---	---	---	---	---	---	---	---	3.604
1.24	499	101.24	3.72 oc	---	---	---	---	---	---	---	---	---	3.716

Continues on next page...

Node 129 Pipe Storage

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
1.28	522	101.28	3.82 oc	---	---	---	---	---	---	---	---	---	3.819
1.32	544	101.32	3.91 oc	---	---	---	---	---	---	---	---	---	3.913
1.36	567	101.36	4.00 oc	---	---	---	---	---	---	---	---	---	3.997
1.40	590	101.40	4.07 oc	---	---	---	---	---	---	---	---	---	4.067
1.44	613	101.44	4.12 oc	---	---	---	---	---	---	---	---	---	4.120
1.48	636	101.48	4.15 oc	---	---	---	---	---	---	---	---	---	4.146
1.52	659	101.52	4.39 oc	---	---	---	---	---	---	---	---	---	4.393
1.56	681	101.56	4.88 oc	---	---	---	---	---	---	---	---	---	4.883
1.60	704	101.60	5.33 oc	---	---	---	---	---	---	---	---	---	5.327
1.64	728	101.64	5.74 oc	---	---	---	---	---	---	---	---	---	5.738
1.68	752	101.68	6.12 oc	---	---	---	---	---	---	---	---	---	6.121
1.72	776	101.72	6.48 oc	---	---	---	---	---	---	---	---	---	6.481
1.76	800	101.76	6.82 oc	---	---	---	---	---	---	---	---	---	6.823
1.80	824	101.80	7.15 oc	---	---	---	---	---	---	---	---	---	7.148
1.84	847	101.84	7.46 oc	---	---	---	---	---	---	---	---	---	7.458
1.88	871	101.88	7.76 oc	---	---	---	---	---	---	---	---	---	7.757
1.92	895	101.92	8.04 oc	---	---	---	---	---	---	---	---	---	8.044
1.96	919	101.96	8.32 oc	---	---	---	---	---	---	---	---	---	8.322
2.00	943	102.00	8.59 oc	---	---	---	---	---	---	---	---	---	8.590
2.04	967	102.04	8.85 oc	---	---	---	---	---	---	---	---	---	8.851
2.08	991	102.08	9.10 oc	---	---	---	---	---	---	---	---	---	9.104
2.12	1,014	102.12	9.35 oc	---	---	---	---	---	---	---	---	---	9.350
2.16	1,038	102.16	9.59 oc	---	---	---	---	---	---	---	---	---	9.589
2.20	1,062	102.20	9.82 oc	---	---	---	---	---	---	---	---	---	9.823
2.24	1,086	102.24	10.05 oc	---	---	---	---	---	---	---	---	---	10.05
2.28	1,110	102.28	10.28 oc	---	---	---	---	---	---	---	---	---	10.28
2.32	1,134	102.32	10.49 oc	---	---	---	---	---	---	---	---	---	10.49
2.36	1,158	102.36	10.71 oc	---	---	---	---	---	---	---	---	---	10.71
2.40	1,181	102.40	10.92 oc	---	---	---	---	---	---	---	---	---	10.92
2.44	1,204	102.44	11.06 ic	---	---	---	---	---	---	---	---	---	11.06
2.48	1,227	102.48	11.19 ic	---	---	---	---	---	---	---	---	---	11.19
2.52	1,250	102.52	11.32 ic	---	---	---	---	---	---	---	---	---	11.32
2.56	1,273	102.56	11.45 ic	---	---	---	---	---	---	---	---	---	11.45
2.60	1,296	102.60	11.57 ic	---	---	---	---	---	---	---	---	---	11.57
2.64	1,318	102.64	11.70 ic	---	---	---	---	---	---	---	---	---	11.70
2.68	1,341	102.68	11.82 ic	---	---	---	---	---	---	---	---	---	11.82
2.72	1,364	102.72	11.94 ic	---	---	---	---	---	---	---	---	---	11.94
2.76	1,387	102.76	12.06 ic	---	---	---	---	---	---	---	---	---	12.06
2.80	1,410	102.80	12.18 ic	---	---	---	---	---	---	---	---	---	12.18
2.84	1,430	102.84	12.30 ic	---	---	---	---	---	---	---	---	---	12.30
2.88	1,451	102.88	12.42 ic	---	---	---	---	---	---	---	---	---	12.42
2.92	1,472	102.92	12.53 ic	---	---	---	---	---	---	---	---	---	12.53
2.96	1,493	102.96	12.65 ic	---	---	---	---	---	---	---	---	---	12.65
3.00	1,513	103.00	12.76 ic	---	---	---	---	---	---	---	---	---	12.76
3.04	1,534	103.04	12.87 ic	---	---	---	---	---	---	---	---	---	12.87
3.08	1,555	103.08	12.99 ic	---	---	---	---	---	---	---	---	---	12.99
3.12	1,576	103.12	13.10 ic	---	---	---	---	---	---	---	---	---	13.10
3.16	1,596	103.16	13.21 ic	---	---	---	---	---	---	---	---	---	13.21
3.20	1,617	103.20	13.32 ic	---	---	---	---	---	---	---	---	---	13.32
3.24	1,634	103.24	13.42 ic	---	---	---	---	---	---	---	---	---	13.42
3.28	1,651	103.28	13.53 ic	---	---	---	---	---	---	---	---	---	13.53
3.32	1,668	103.32	13.64 ic	---	---	---	---	---	---	---	---	---	13.64
3.36	1,685	103.36	13.74 ic	---	---	---	---	---	---	---	---	---	13.74
3.40	1,702	103.40	13.85 ic	---	---	---	---	---	---	---	---	---	13.85
3.44	1,719	103.44	13.95 ic	---	---	---	---	---	---	---	---	---	13.95
3.48	1,736	103.48	14.06 ic	---	---	---	---	---	---	---	---	---	14.06
3.52	1,753	103.52	14.16 ic	---	---	---	---	---	---	---	---	---	14.16
3.56	1,770	103.56	14.26 ic	---	---	---	---	---	---	---	---	---	14.26
3.60	1,787	103.60	14.36 ic	---	---	---	---	---	---	---	---	---	14.36
3.64	1,797	103.64	14.46 ic	---	---	---	---	---	---	---	---	---	14.46
3.68	1,807	103.68	14.56 ic	---	---	---	---	---	---	---	---	---	14.56
3.72	1,817	103.72	14.66 ic	---	---	---	---	---	---	---	---	---	14.66
3.76	1,827	103.76	14.76 ic	---	---	---	---	---	---	---	---	---	14.76
3.80	1,836	103.80	14.86 ic	---	---	---	---	---	---	---	---	---	14.86
3.84	1,846	103.84	14.96 ic	---	---	---	---	---	---	---	---	---	14.96
3.88	1,856	103.88	15.05 ic	---	---	---	---	---	---	---	---	---	15.05
3.92	1,866	103.92	15.15 ic	---	---	---	---	---	---	---	---	---	15.15
3.96	1,876	103.96	15.24 ic	---	---	---	---	---	---	---	---	---	15.24
4.00	1,885	104.00	15.34 ic	---	---	---	---	---	---	---	---	---	15.34

...End

Emergency Spillway

Trapezoidal Weir

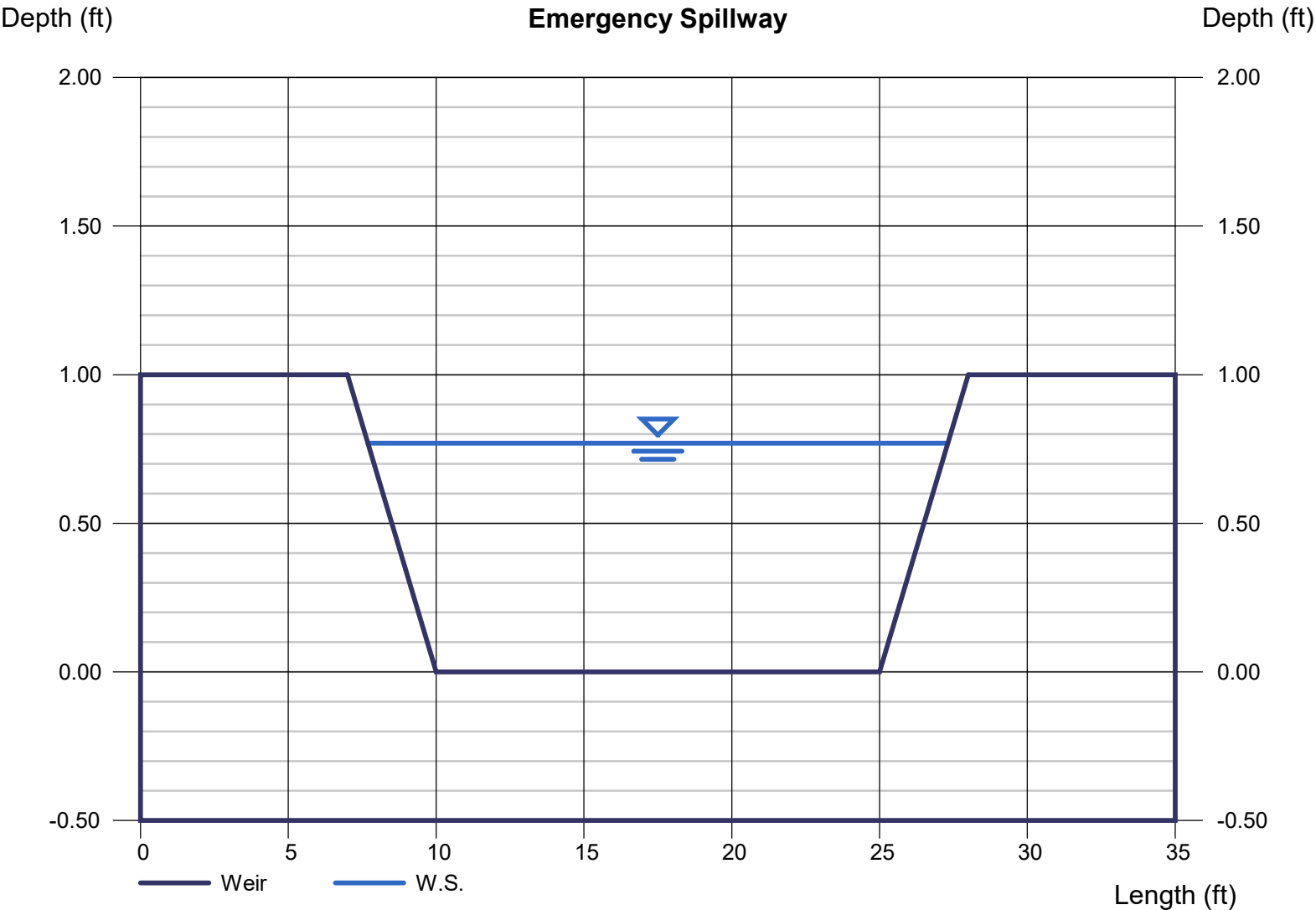
Crest = Sharp
Bottom Length (ft) = 15.00
Total Depth (ft) = 1.00
Side Slope (z:1) = 3.00

Highlighted

Depth (ft) = 0.77
Q (cfs) = 35.00
Area (sqft) = 13.33
Velocity (ft/s) = 2.63
Top Width (ft) = 19.62

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 35.00



Weir Report

Emergency Spillway: Node 128

Trapezoidal Weir

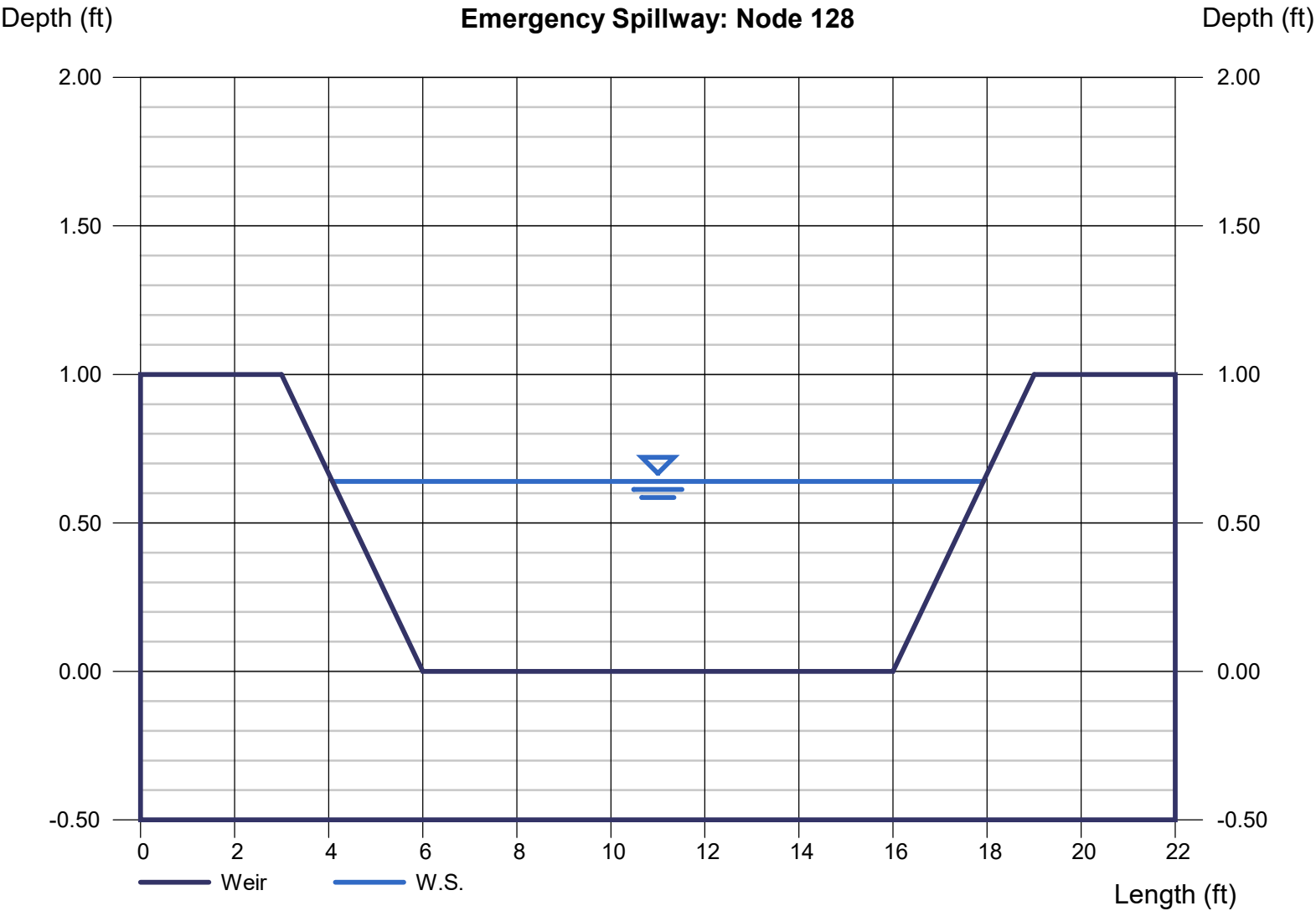
Crest = Sharp
Bottom Length (ft) = 10.00
Total Depth (ft) = 1.00
Side Slope (z:1) = 3.00

Highlighted

Depth (ft) = 0.64
Q (cfs) = 18.30
Area (sqft) = 7.63
Velocity (ft/s) = 2.40
Top Width (ft) = 13.84

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 18.30



Starlight
MBI 185614

Storage Drawdown - Node 106

Stage, Storage, and Discharge derived from Hydroflow Hydrographs routing analysis

Q100 Drawdown (max 96 hours)						
Stage (ft)	Storage (ft3)	Discharge (cfs)	Incremental Vol. (ft3)	Avg. Discharge (cfs)	Incremental Time (sec)	Incremental Time (hr)
5.00	11,783	30.25	-	-	-	-
4.50	11,171	28.30	612	29.2750	21	0.01
4.00	10,106	26.20	1,065	27.2500	39	0.01
3.50	8,811	23.91	1,295	25.0550	52	0.01
3.00	7,384	20.83	1,427	22.3700	64	0.02
2.50	5,893	15.66	1,491	18.2450	82	0.02
2.00	4,402	7.52	1,491	11.5900	129	0.04
1.50	2,975	6.13	1,427	6.8250	209	0.06
1.00	1,679	3.77	1,296	4.9500	262	0.07
0.50	614	1.40	1,065	2.5850	412	0.11
0.00	0	0.00	614	0.7000	877	0.24
Total Time (hours) =						0.59

Notes

Dual 410' LF (820 total) of 60" storage pipe with 24" discharge pipe

Starlight
MBI 185614

Storage Drawdown - Node 128

Stage, Storage, and Discharge derived from Hydroflow Hydrographs routing analysis

Q100 Drawdown (max 96 hours)						
Stage (ft)	Storage (ft3)	Discharge (cfs)	Incremental Vol. (ft3)	Avg. Discharge (cfs)	Incremental Time (sec)	Incremental Time (hr)
4.00	57,350	15.34	-	-	-	-
3.50	42,607	14.11	14,743	14.7250	1,001	0.28
3.00	27,863	12.76	14,744	13.4350	1,097	0.30
2.50	21,961	11.20	5,902	11.9800	493	0.14
2.00	16,059	9.15	5,902	10.1750	580	0.16
1.50	11,403	6.47	4,656	7.8100	596	0.17
1.00	6,746	4.26	4,657	5.3650	868	0.24
0.50	3,373	1.24	3,373	2.7500	1,227	0.34
0.00	0	0.00	3,373	0.6200	5,440	1.51
Total Time (hours) =						3.14

Notes

Detention Basin with 18" discharge pipe and overflow weir

Starlight
MBI 185614

Storage Drawdown - Node 129

Stage, Storage, and Discharge derived from Hydroflow Hydrographs routing analysis

Q100 Drawdown (max 96 hours)						
Stage (ft)	Storage (ft3)	Discharge (cfs)	Incremental Vol. (ft3)	Avg. Discharge (cfs)	Incremental Time (sec)	Incremental Time (hr)
4.00	1,257	15.34	-	-	-	-
3.60	1,192	14.36	65	14.8500	4	0.00
3.20	1,078	13.32	114	13.8400	8	0.00
2.80	940	12.18	138	12.7500	11	0.00
2.40	788	10.92	152	11.5500	13	0.00
2.00	629	8.59	159	9.7550	16	0.00
1.60	470	5.33	159	6.9600	23	0.01
1.20	317	3.60	153	4.4650	34	0.01
0.80	179	2.25	138	2.9250	47	0.01
0.40	66	0.81	113	1.5300	74	0.02
0.00	0	0.00	66	0.4050	163	0.05
Total Time (hours) =						0.11

Notes

100' LF of 48" storage pipe with 18" discharge pipe

Starlight
MBI 185614

Storage Drawdown - Node 156

Stage, Storage, and Discharge derived from Hydroflow Hydrographs routing analysis

Q100 Drawdown (max 96 hours)						
Stage (ft)	Storage (ft3)	Discharge (cfs)	Incremental Vol. (ft3)	Avg. Discharge (cfs)	Incremental Time (sec)	Incremental Time (hr)
4.00	3,771	15.34	-	-	-	-
3.60	3,575	14.36	196	14.8500	13	0.00
3.20	3,234	13.32	341	13.8400	25	0.01
2.80	2,820	12.18	414	12.7500	32	0.01
2.40	2,363	10.92	457	11.5500	40	0.01
2.00	1,886	8.59	477	9.7550	49	0.01
1.60	1,409	5.33	477	6.9600	69	0.02
1.20	952	3.60	457	4.4650	102	0.03
0.80	537	2.25	415	2.9250	142	0.04
0.40	197	0.81	340	1.5300	222	0.06
0.00	0	0.00	197	0.4050	486	0.14
Total Time (hours) =						0.32

Notes

300' LF of 48" storage pipe with 18" discharge pipe

Starlight
MBI 185614

Storage Drawdown - Node 165

Stage, Storage, and Discharge derived from Hydroflow Hydrographs routing analysis

Q100 Drawdown (max 96 hours)						
Stage (ft)	Storage (ft3)	Discharge (cfs)	Incremental Vol. (ft3)	Avg. Discharge (cfs)	Incremental Time (sec)	Incremental Time (hr)
3.00	76,671	12.76	-	-	-	-
2.50	58,280	11.20	18,391	11.9800	1,535	0.43
2.00	39,890	9.15	18,390	10.1750	1,807	0.50
1.50	28,664	6.47	11,226	7.8100	1,437	0.40
1.00	17,438	4.26	11,226	5.3650	2,092	0.58
0.50	8,719	1.24	8,719	2.7500	3,171	0.88
0.00	0	0.00	8,719	0.6200	14,063	3.91
Total Time (hours) =						6.70

Notes

Detention Basin with 18" discharge pipe and overflow weir

Inlet Report

Node 129

Drop Curb Inlet

Location	= Sag
Curb Length (ft)	= 16.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

Slope, Sw (ft/ft)	= 0.100
Slope, Sx (ft/ft)	= 0.100
Local Depr (in)	= -0-
Gutter Width (ft)	= -0-
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

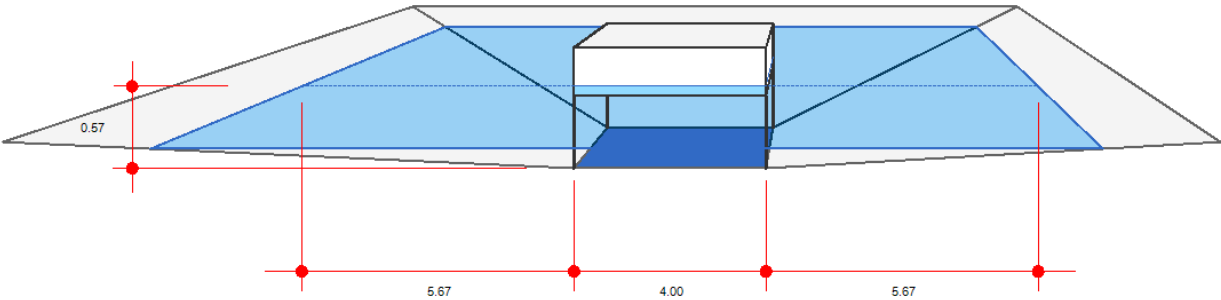
Calculations

Compute by:	Known Q
Q (cfs)	= 20.50

Highlighted

Q Total (cfs)	= 20.50
Q Capt (cfs)	= 20.50
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 6.80
Efficiency (%)	= 100
Gutter Spread (ft)	= 5.67
Gutter Vel (ft/s)	= -0-
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-

All dimensions in feet



Inlet Report

Node 156

Drop Curb Inlet

Location	= Sag
Curb Length (ft)	= 16.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

Slope, Sw (ft/ft)	= 0.100
Slope, Sx (ft/ft)	= 0.100
Local Depr (in)	= -0-
Gutter Width (ft)	= -0-
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

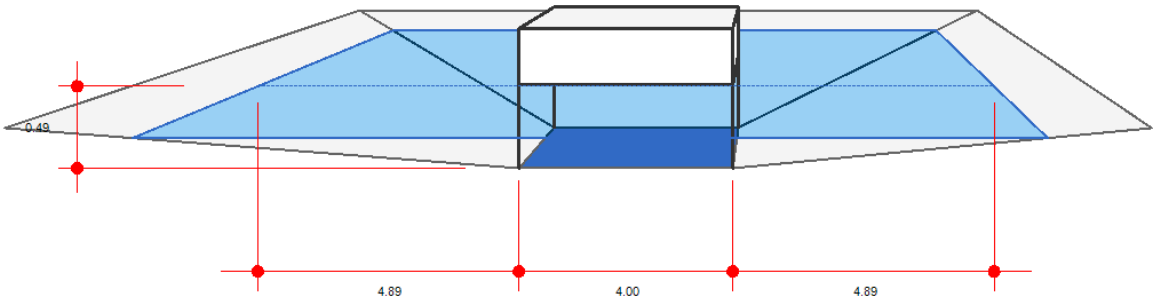
Calculations

Compute by:	Known Q
Q (cfs)	= 16.40

Highlighted

Q Total (cfs)	= 16.40
Q Capt (cfs)	= 16.40
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 5.86
Efficiency (%)	= 100
Gutter Spread (ft)	= 4.89
Gutter Vel (ft/s)	= -0-
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-

All dimensions in feet



Inlet Report

Node 106

Two (2) inlets are proposed

50% of Q100

Drop Curb Inlet

Location	= Sag
Curb Length (ft)	= 16.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

Slope, Sw (ft/ft)	= 0.100
Slope, Sx (ft/ft)	= 0.100
Local Depr (in)	= -0-
Gutter Width (ft)	= -0-
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations

Compute by:	Known Q
Q (cfs)	= 19.50

Highlighted

Q Total (cfs)	= 19.50
Q Capt (cfs)	= 19.50
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 6.58
Efficiency (%)	= 100
Gutter Spread (ft)	= 5.48
Gutter Vel (ft/s)	= -0-
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-

All dimensions in feet

